

Normally – OFF Silicon Carbide Junction Transistor

V_{DS}	=	600 V
$R_{DS(ON)}$	=	170 mΩ
$I_D (T_C = 25^\circ C)$	=	20 A
$h_{FE} (T_C = 25^\circ C)$	=	110

Features

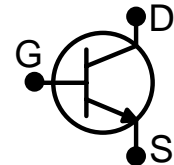
- 210°C maximum operating temperature
- Electrically Isolated Base Plate
- Gate Oxide Free SiC Switch
- Exceptional Safe Operating Area
- Excellent Gain Linearity
- Compatible with 5 V TTL Gate Drive
- Temperature Independent Switching Performance
- Low Output Capacitance
- Positive Temperature Coefficient of $R_{DS,ON}$
- Suitable for Connecting an Anti-parallel Diode

Advantages

- Compatible with Si MOSFET/IGBT Gate Drive ICs
- > 20 μs Short-Circuit Withstand Capability
- Lowest-in-class Conduction Losses
- High Circuit Efficiency
- Minimal Input Signal Distortion
- High Amplifier Bandwidth

Package

- RoHS Compliant



TO – 257 (Isolated Base-plate Hermetic Package)

Applications

- Down Hole Oil Drilling
- Geothermal Instrumentation
- Solenoid Actuators
- General Purpose High-Temperature Switching
- Amplifiers
- Solar Inverters
- Switched-Mode Power Supply (SMPS)
- Power Factor Correction (PFC)

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Section I: Absolute Maximum Ratings

Parameter	Symbol	Conditions	Values	Unit
Drain – Source Voltage	V_{DS}	$V_{GS} = 0 V$	600	V
Continuous Drain Current	I_D	$T_J = 210^\circ C, T_C = 25^\circ C$	20	A
Continuous Gate Current	I_{GM}		1.25	A
Turn-Off Safe Operating Area	RBSOA	$T_{VJ} = 210^\circ C, I_G = 1.25 A,$ Clamped Inductive Load	$I_{D,max} = 20$ @ $V_{DS} \leq V_{DSmax}$	A
Short Circuit Safe Operating Area	SCSOA	$T_{VJ} = 210^\circ C, I_G = 1.25 A, V_{DS} = 400 V,$ Non Repetitive	>20	μs
Reverse Gate – Source Voltage	V_{GS}		30	V
Reverse Drain – Source Voltage	V_{DS}		40	V
Power Dissipation	P_{tot}	$T_J = 210^\circ C, T_C = 25^\circ C$	80	W
Operating and Storage Temperature	T_J, T_{sig}		-55 to 210	°C

Section II: Static Electrical Characteristics

Parameter	Symbol	Conditions	Values			Unit
			min.	typ.	max.	
A: On State						
Drain – Source On Resistance	$R_{DS(ON)}$	$I_D = 7\text{ A}, T_J = 25\text{ °C}$		170		mΩ
		$I_D = 7\text{ A}, T_J = 175\text{ °C}$		320		
		$I_D = 7\text{ A}, T_J = 210\text{ °C}$		440		
Gate – Source Saturation Voltage	$V_{GS,SAT}$	$I_D = 10\text{ A}, I_D/I_G = 40, T_J = 25\text{ °C}$		3.50		V
		$I_D = 10\text{ A}, I_D/I_G = 30, T_J = 175\text{ °C}$		3.27		
DC Current Gain	h_{FE}	$V_{DS} = 5\text{ V}, I_D = 10\text{ A}, T_J = 25\text{ °C}$	80	110		
		$V_{DS} = 5\text{ V}, I_D = 10\text{ A}, T_J = 210\text{ °C}$	50	80		
B: Off State						
Drain Leakage Current	I_{DSS}	$V_R = 600\text{ V}, V_{GS} = 0\text{ V}, T_J = 25\text{ °C}$		10	100	μA
		$V_R = 600\text{ V}, V_{GS} = 0\text{ V}, T_J = 175\text{ °C}$		40	400	
		$V_R = 600\text{ V}, V_{GS} = 0\text{ V}, T_J = 210\text{ °C}$		100	600	
C: Thermal						
Thermal resistance, junction - case	R_{thJC}			2.5		°C/W

Section III: Dynamic Electrical Characteristics

Parameter	Symbol	Conditions	Values			Unit	
			min.	typ.	max.		
A: Capacitance and Gate Charge							
Input Capacitance	C_{ISS}	$V_{GS} = 0\text{ V}, V_D = 500\text{ V}, f = 1\text{ MHz}$		685		pF	
Reverse Transfer/Output Capacitance	C_{rss}/C_{OSS}	$V_D = 500\text{ V}, f = 1\text{ MHz}$		24		pF	
Output Capacitance Stored Energy	E_{OSS}	$V_{GS} = 0\text{ V}, V_D = 500\text{ V}, f = 1\text{ MHz}$		3.1		μJ	
Effective Output Capacitance, time related	$C_{oss,tr}$	$I_D = \text{constant}, V_{GS} = 0\text{ V}, V_{DS} = 0...400\text{ V}$		50		pF	
Effective Output Capacitance, energy related	$C_{oss,er}$	$V_{GS} = 0\text{ V}, V_{DS} = 0...400\text{ V}$		37		pF	
Gate-Source Charge	Q_{GS}	$V_{GS} = -5...3\text{ V}$		11		nC	
Gate-Drain Charge	Q_{GD}	$V_{GS} = 0\text{ V}, V_{DS} = 0...400\text{ V}$		20		nC	
Gate Charge - Total	Q_G			31		nC	
B: Switching							
Turn On Delay Time	$t_{d(on)}$	$T_J = 175\text{ °C}, V_{DS} = 400\text{ V}, I_D = 7\text{ A}, \text{Inductive Load}$ Refer to Section V for additional driving information.		10		ns	
Rise Time	t_r			30		ns	
Turn Off Delay Time	$t_{d(off)}$			75		ns	
Fall Time	t_f			40		ns	
Turn-On Energy Per Pulse	E_{on}			35		μJ	
Turn-Off Energy Per Pulse	E_{off}			65		μJ	
Total Switching Energy	E_{ts}			100		μJ	
Turn On Delay Time	$t_{d(on)}$		$T_J = 210\text{ °C}, V_{DS} = 400\text{ V}, I_D = 7\text{ A}, \text{Inductive Load}$ Refer to Section V for additional driving information.		10		ns
Rise Time	t_r				30		ns
Turn Off Delay Time	$t_{d(off)}$				75		ns
Fall Time	t_f			60		ns	
Turn-On Energy Per Pulse	E_{on}			45		μJ	
Turn-Off Energy Per Pulse	E_{off}			80		μJ	
Total Switching Energy	E_{ts}			125		μJ	

Section IV: Figures

A: Static Characteristics

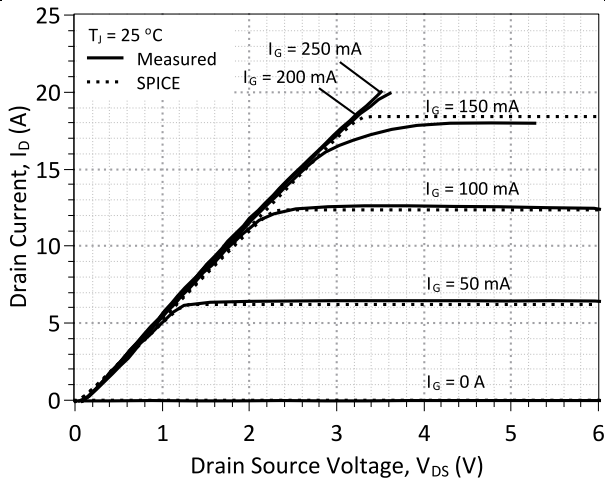


Figure 1: Typical Output Characteristics at 25 °C

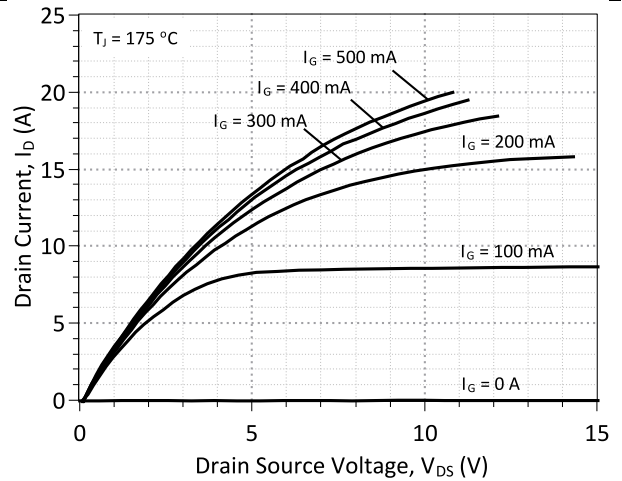


Figure 2: Typical Output Characteristics at 175 °C

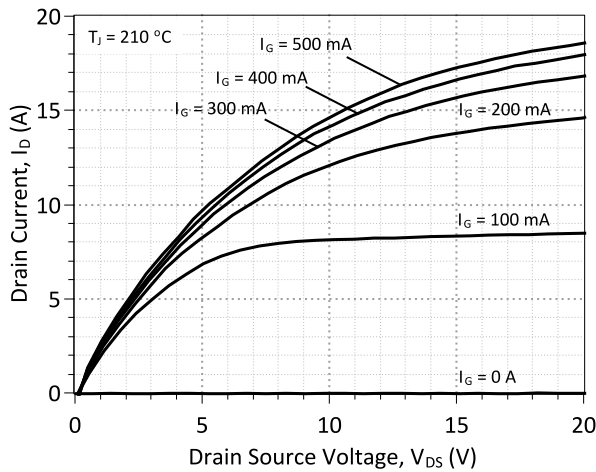


Figure 3: Typical Output Characteristics at 210 °C

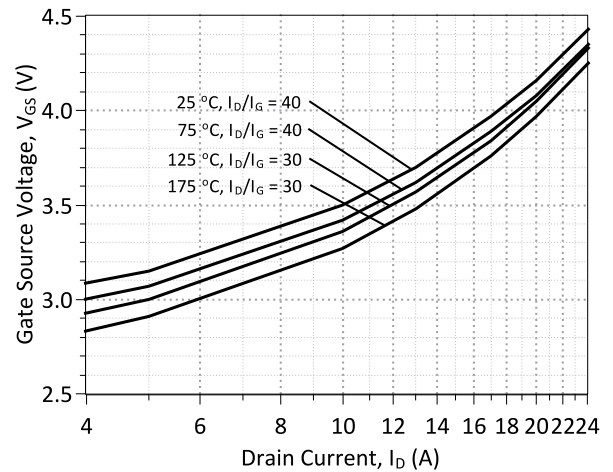


Figure 4: Typical Gate – Source Saturation Voltage

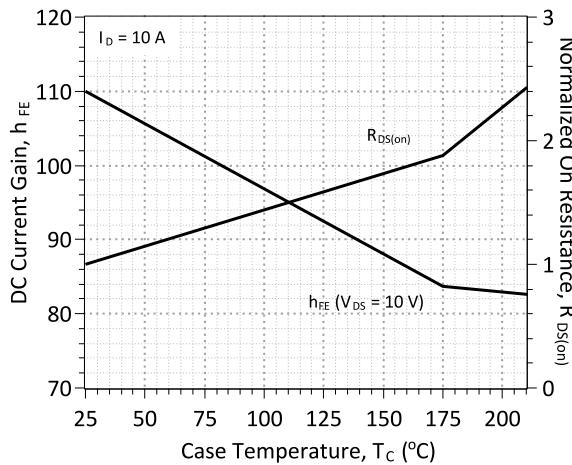


Figure 5: DC Current Gain and Normalized On-Resistance vs. Temperature

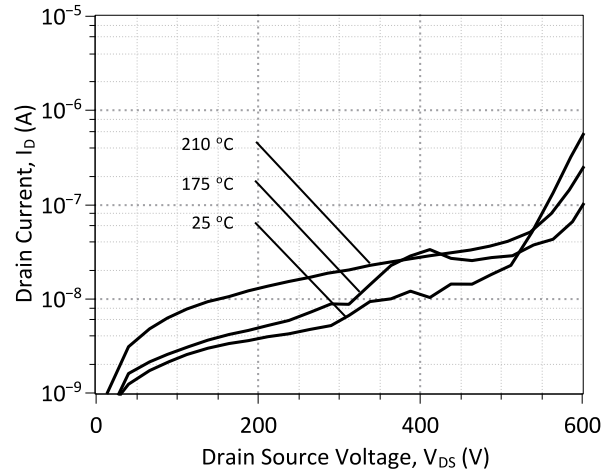


Figure 6: Typical Blocking Characteristics

B: Dynamic Characteristics

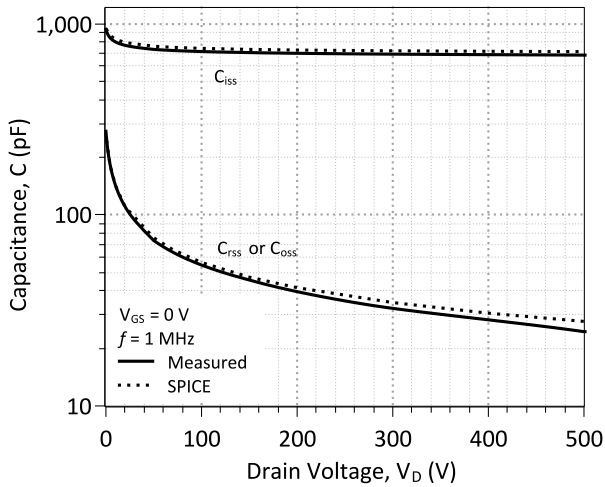


Figure 7: Capacitance Characteristics

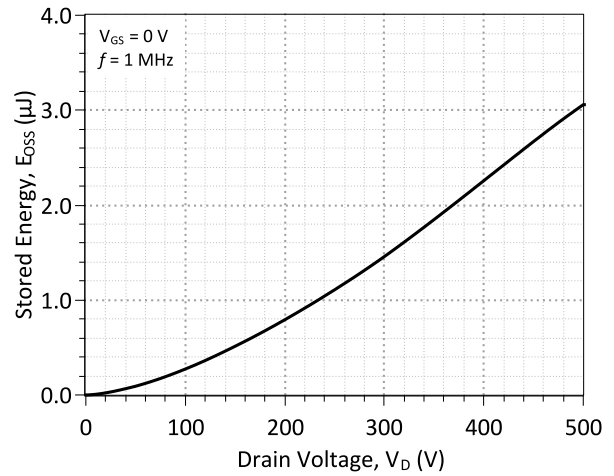


Figure 8: Output Capacitance Stored Energy

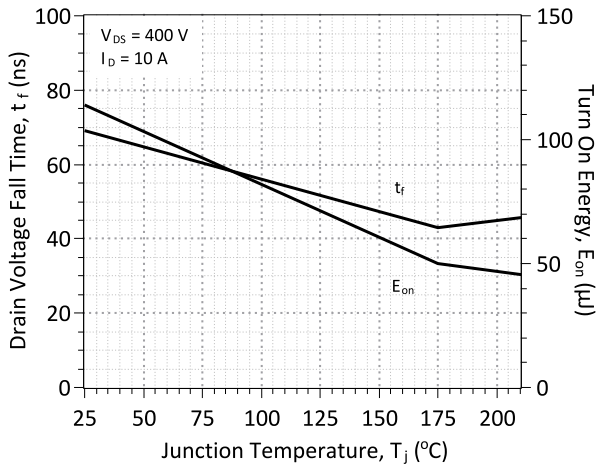


Figure 9: Typical Turn On Energy Losses and Switching Times vs. Temperature

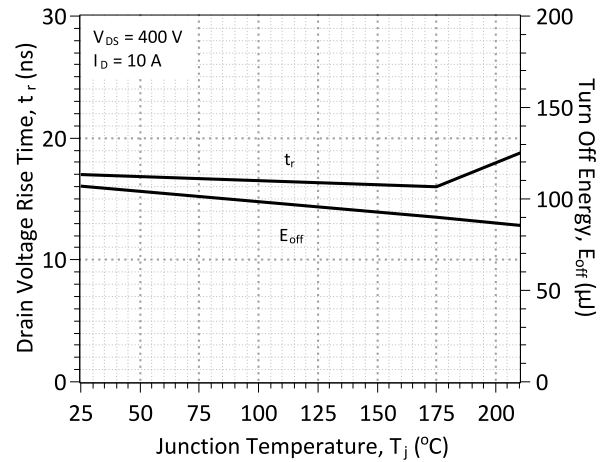


Figure 10: Typical Turn Off Energy Losses and Switching Times vs. Temperature

Section V: Driving the 2N7637-GA

The 2N7637-GA is a current controlled SiC transistor which requires a positive gate current for turn-on and to remain in on-state. It may be driven by different drive topologies depending on the intended application.

Table 1: Estimated Power Consumption and switching frequencies for various Gate Drive topologies.

Drive Topology	Gate Drive Power Consumption	Switching Frequency
Simple TTL	High	Low
Constant Current	Medium	Medium
High Speed – Boost Capacitor	Medium	High
High Speed – Boost Inductor	Low	High
Proportional	Lowest	Medium
Pulsed Power	Medium	N/A

A: Simple TTL Drive

The 2N7637-GA may be driven by 5 V TTL logic using a simple current amplification stage. The current amplifier output current must meet or exceed the steady state gate current, $I_{G,steady}$, required to operate the 2N7637-GA. An external gate resistor R_G , shown in the Figure 11 topology, sets $I_{G,steady}$ to the required level which is dependent on the SJT drain current I_D and DC current gain h_{FE} , R_G may be calculated from the equation below. The value of $V_{EC,sat}$ can be taken from the PNP datasheet, a partial list of high-temperature PNP and NPN transistors options is given below. High-temperature MOSFETs may also be used in the topology.

$$R_{G,max} = \frac{(5.0 V - V_{EC,sat} (PNP) - V_{GS,sat} (SJT)) * h_{FE}(T, I_D)}{I_D * 1.5}$$

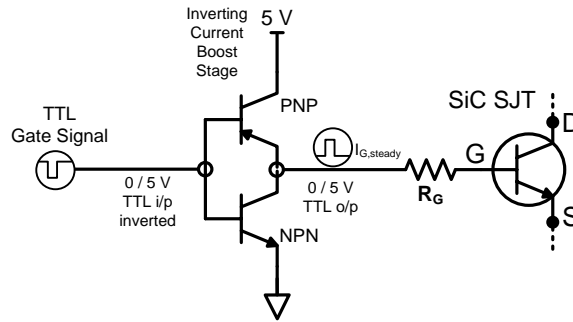


Figure 11: Simple TTL Gate Drive Topology

Table 2: Partial List of High-Temperature BJTs for TTL Gate Driving

BJT Part Number	Type	T _{j,max} (°C)
PHPT60603PY	PNP	175
PHPT60603NY	NPN	175
2N2222	NPN	200
2N6730	PNP	200
2N2905	PNP	200
2N5883	PNP	200
2N5885	NPN	200

B: High Speed Driving

For ultra high speed 2N7637-GA switching ($t_r, t_f < 20$ ns) while maintaining low gate drive losses the supplied gate current should include a positive current peak during turn-on, a negative voltage peak during turn-off, and continuous gate current I_G to remain on.

An SJT is rapidly switched from its blocking state to on-state, when the necessary gate charge for turn-on, Q_G , is supplied by a burst of high gate current until the gate-source capacitance, C_{GS} , and gate-drain capacitance, C_{GD} , are fully charged. Ideally, the burst should terminate when the drain voltage has fallen to its on-state value in order to avoid unnecessary drive losses. A negative voltage peak is recommended for the turn-off transition in order to ensure that the gate current is not being supplied under high dV/dt due to the Miller effect. While satisfactory turn off can be achieved with $V_{GS} = 0$ V, a negative V_{GS} value may be used in order to speed up the turn-off transition.

B:1: High Speed, Low Loss Drive with Boost Capacitor

The 2N7637-GA may be driven using a High Speed, Low Loss Drive with Boost Capacitor topology in which multiple voltage levels, a gate resistor, and a gate capacitor are used to provide current peaks at turn-on and turn-off for fast switching and a continuous gate current while in on-state. As shown in Figure 12, in this topology two gate driver ICs are utilized. An external gate resistor R_G is driven by a low voltage driver to supply the continuous gate current throughout on-state, and a gate capacitor C_G is driven at a higher voltage level to supply a high current peak at turn-on and turn-off. A 3 kV isolated evaluation gate drive board (GA03IDDJT30-FR4) from GeneSiC Semiconductor utilizing this topology is commercially available for high and low-side driving, its datasheet provides additional details about this drive topology.

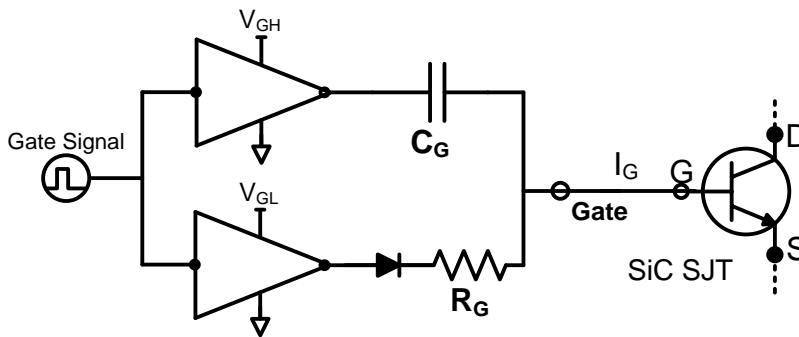


Figure 12: High Speed, Low Loss Drive with Boost Capacitor Topology

B:2: High Speed, Low Loss Drive with Boost Inductor

A High Speed, Low-Loss Driver with Boost Inductor is also capable of driving the 2N7637-GA at high-speed. It utilizes a gate drive inductor instead of a capacitor to provide the high-current gate current pulses $I_{G,on}$ and $I_{G,off}$. During operation, inductor L is charged to a specified $I_{G,on}$ current value then made to discharge I_L into the SJT gate pin using logic control of S_1, S_2, S_3 , and S_4 , as shown in Figure 13. After turn on, while the device remains on the necessary steady state gate current $I_{G,steady}$ is supplied from source V_{CC} through R_G . Please refer to the article "A current-source concept for fast and efficient driving of silicon carbide transistors" by Dr. Jacek Rąbkowski for additional information on this driving topology.³

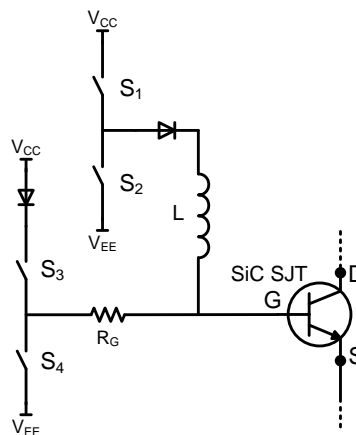


Figure 13: High Speed, Low-Loss Driver with Boost Inductor Topology

³ – Archives of Electrical Engineering. Volume 62, Issue 2, Pages 333–343, ISSN (Print) 0004-0746, DOI: 10.2478/ae-2013-0026, June 2013

C: Proportional Gate Current Driving

A proportional gate drive topology may be beneficial for applications in which the 2N7637-GA will operate over a wide range of drain current conditions to lower the gate drive power consumption. A proportional gate driver relies on instantaneous drain current I_D feedback to vary the steady state gate current $I_{G,steady}$ supplied to the 2N7637-GA.

C:1: Voltage Controlled Proportional Driver

A voltage controlled proportional driver relies on a gate drive integrated circuit to detect the 2N7637-GA drain-source voltage V_{DS} during on-state to sense I_D . The integrated circuit will then increase or decrease I_G in response to I_D . This allows I_G and gate drive power consumption to reduce while I_D is low or for I_G to increase when I_D increases. A high voltage diode connected between the drain and sense protects the integrated circuit from high-voltage when blocking. A simplified version of this topology is shown in Figure 14. Additional information will be available in the future at <http://www.genesicsemi.com/references/product-notes/>.

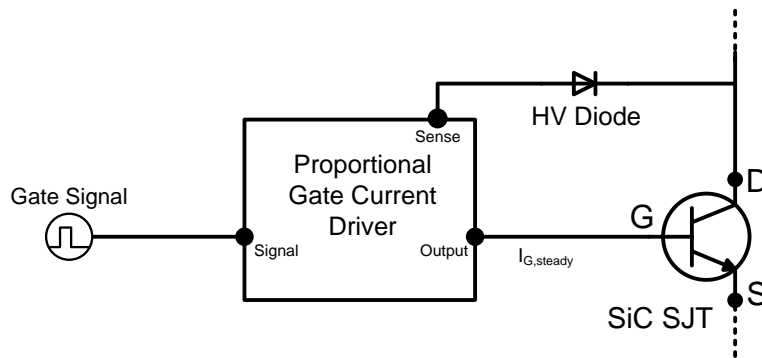


Figure 14: Simplified Voltage Controlled Proportional Driver

C:2: Current Controlled Proportional Driver

The current controlled proportional driver relies on a low-loss transformer in the drain or source path to provide feedback of the 2N7637-GA drain current during on-state to supply $I_{G,steady}$ into the gate. $I_{G,steady}$ will increase or decrease in response to I_D at a fixed forced current gain which is set by the turns ratio of the transformer, $h_{force} = I_D / I_G = N_2 / N_1$. 2N7637-GA is initially tuned-on using a gate current pulse supplied into an RC drive circuit to allow I_D current to begin flowing. This topology allows $I_{G,steady}$ and the gate drive power consumption to reduce while I_D is relatively low or for $I_{G,steady}$ to increase when I_D increases. A simplified version of this topology is shown in Figure 15. Additional information will be available in the future at <http://www.genesicsemi.com/references/product-notes/>.

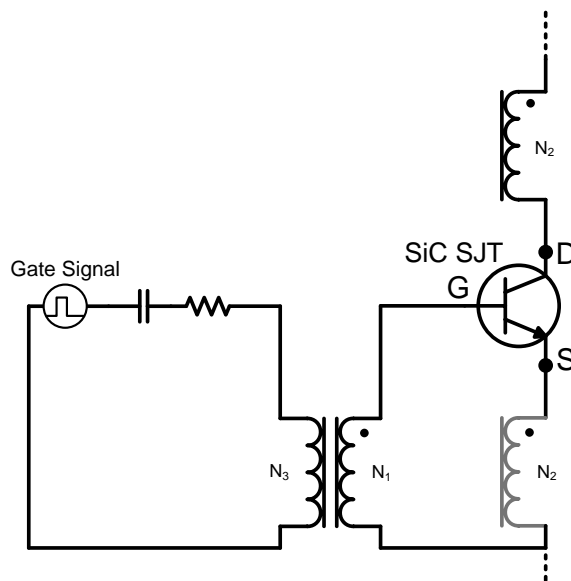
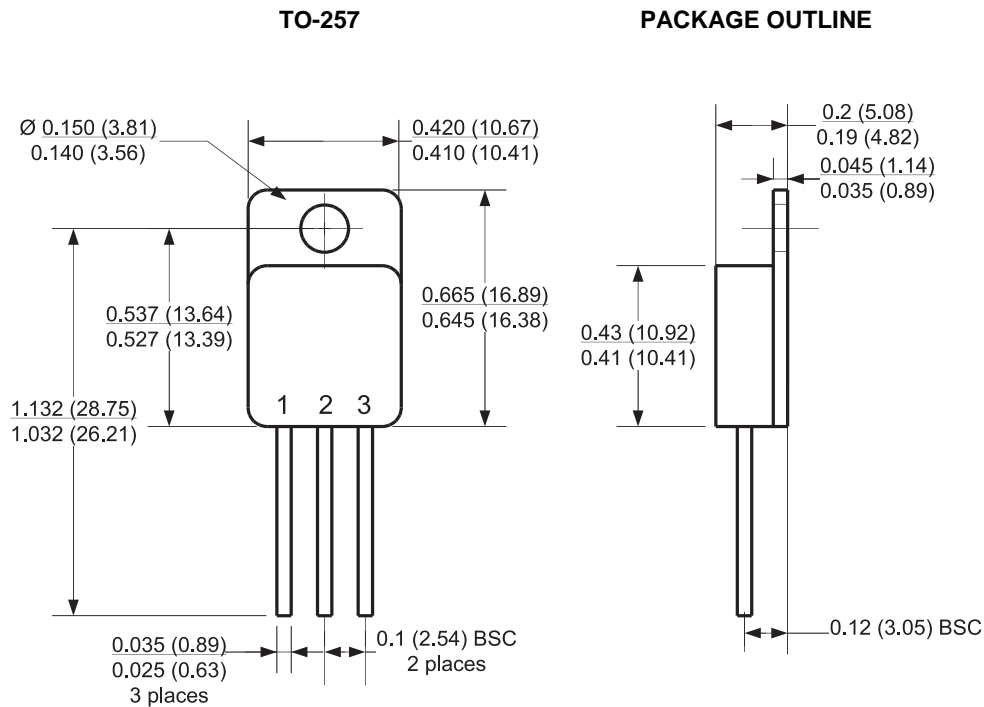


Figure 15: Simplified Current Controlled Proportional Driver

Section VI: Package Dimensions:



- NOTE**
 1. CONTROLLED DIMENSION IS INCH. DIMENSION IN BRACKET IS MILLIMETER.
 2. DIMENSIONS DO NOT INCLUDE END FLASH, MOLD FLASH, MATERIAL PROTRUSIONS

Revision History			
Date	Revision	Comments	Supersedes
2014/12/12	6	Updated Electrical Characteristics	
2014/08/23	5	Updated Electrical Characteristics	
2014/03/20	4	Updated Gate Drive Section	
2014/02/11	3	Updated Electrical Characteristics	
2013/12/19	2	Updated Gate Drive Section	
2013/11/18	1	Updated Electrical Characteristics	
2012/08/24	0	Initial release	

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Section VII: SPICE Model Parameters

This is a secure document. Please copy this code from the SPICE model PDF file on our website (http://www.genesicsemi.com/images/hit_sic/sjt/2N7637-GA_SPICE.pdf) into LTSPICE (version 4) software for simulation of the 2N7637-GA.

```
*      MODEL OF GeneSiC Semiconductor Inc.
*
*      $Revision:   1.3           $
*      $Date:      12-DEC-2014   $
*
*      GeneSiC Semiconductor Inc.
*      43670 Trade Center Place Ste. 155
*      Dulles, VA 20166
*
*      COPYRIGHT (C) 2014 GeneSiC Semiconductor Inc.
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*      These models are provided "AS IS, WHERE IS, AND WITH NO WARRANTY
*      OF ANY KIND EITHER EXPRESSED OR IMPLIED, INCLUDING BUT NOT LIMITED
*      TO ANY IMPLIED WARRANTIES OF MERCHANTABILITY AND FITNESS FOR A
*      PARTICULAR PURPOSE."
*      Models accurate up to 2 times rated drain current.
*
.model 2N7637 NPN
+ IS      9.8338E-48
+ ISE     1.0733E-26
+ EG      3.23
+ BF      130
+ BR      0.55
+ IKF     200
+ NF      1
+ NE      2.
+ RB      7.2
+ IRB     0.002
+ RBM     0.2
+ RE      0.1039
+ RC      0.06188
+ CJC     2.73E-10
+ VJC     3.04
+ MJC     0.448
+ CJE     6.86E-10
+ VJE     2.89
+ MJE     0.466
+ XTI     3
+ XTB     -0.35
+ TRC1    1.90E-2
+ VCEO    600
+ ICRATING 20
+ MFG     GeneSiC_Semiconductor
*
*      End of 2N7637-GA SPICE Model
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