

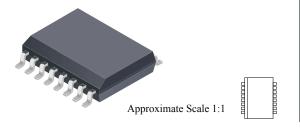
120 kHz Bandwidth, High Voltage Isolation Current Sensor with Integrated Overcurrent Detection

Features and Benefits

- Industry-leading noise performance with greatly improved bandwidth through proprietary amplifier and filter design techniques
- Small footprint package suitable for space-constrained applications
- 1 m Ω primary conductor resistance for low power loss
- High isolation voltage, suitable for line-powered
- applications
- User-adjustable Overcurrent Fault level
 Overcurrent Fault signal typically responds
- Overcurrent Fault signal typically responds to an overcurrent condition in $< 2 \ \mu s$
- Integrated shield virtually eliminates capacitive coupling from current conductor to die due to high dV/dt voltage transients
- Filter pin capacitor improves resolution in low bandwidth applications
- 3 to 5.5 V, single supply operation
- Factory trimmed sensitivity and quiescent output voltage
- Chopper stabilization results in extremely stable quiescent output voltage
- Ratiometric output from supply voltage



Package: 16-pin SOIC Hall Effect IC Package (suffix LA)



Description

The AllegroTM ACS710 current sensor provides economical and precise means for current sensing applications in industrial, commercial, and communications systems. The device is offered in a small footprint surface mount package that allows easy implementation in customer applications.

The ACS710 consists of a precision linear Hall sensor integrated circuit with a copper conduction path located near the surface of the silicon die. Applied current flows through the copper conduction path, and the analog output voltage from the Hall sensor linearly tracks the magnetic field generated by the applied current. The accuracy of the ACS710 is maximized with this patented packaging configuration because the Hall element is situated in extremely close proximity to the current to be measured.

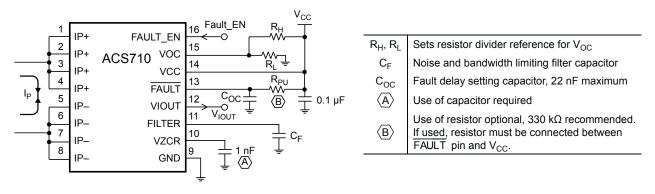
High level immunity to current conductor dV/dt and stray electric fields, offered by Allegro proprietary integrated shield technology, results in low ripple on the output and low offset drift in high-side, high voltage applications.

The voltage on the Overcurrent Input (VOC pin) allows customers to define an overcurrent fault threshold for the device. When the current flowing through the copper conduction path (between the IP+ and IP- pins) exceeds this threshold, the open drain Overcurrent Fault pin will transition to a logic low state. Factory programming of the linear Hall sensor inside of the ACS710 results in exceptional accuracy in both analog and digital output signals.

The internal resistance of the copper path used for current sensing is typically $1 \text{ m}\Omega$, for low power loss. Also, the current conduction path is electrically isolated from the low voltage

Continued on the next page...

Typical Application Circuit



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Description (continued)

sensor inputs and outputs. This allows the ACS710 family of sensors to be used in applications requiring electrical isolation, without the use of opto-isolators or other costly isolation techniques.

The ACS710 is provided in a small, surface mount SOIC16 package. The leadframe is plated with 100% matte tin, which is compatible with standard lead (Pb) free printed circuit board assembly processes. Internally, the device is Pb-free, except for flip-chip high-temperature Pb-based solder balls, currently exempt from RoHS. The device is fully calibrated prior to shipment from the factory.

Applications include:

- Motor control and protection
- Load management and overcurrent detection
- · Power conversion and battery monitoring / UPS systems

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Selection Guide					
Part Number	I _P (A)	Sens (typ) at V _{CC} = 5 V (mV/A)	Latched Fault	T _A (°C)	Packing ¹
ACS710KLATR-6BB-T ^{2,3}	±6	151			
ACS710KLATR-10BB-T ²	±10	85	Yes40 to 125		Tana and Real 1000 piezos per real
ACS710KLATR-12CB-T ²	±12.5	56	Yes -40 to 125	Tape and Reel, 1000 pieces per reel	
ACS710KLATR-25CB-T ²	±25	28			
ACS710KLATR-6BB-NL-T ^{2,3}	±6	151			
ACS710KLATR-10BB-NL-T ²	±10	85	No	-40 to 125	Tape and Reel, 1000 pieces per reel
ACS710KLATR-12CB-NL-T ²	±12.5	56	110 -40 10 125		
ACS710KLATR-25CB-NL-T ²	±25	28			

¹ Contact Allegro for packing options.

²Variant not intended for automotive applications.

³The formerly offered V_{CC} = 3.3 V version of the $I_P = \pm 6$ A variant (formerly the ACS710KLATR-6BB-T) is now offered as the ACS716KLATR-6BB-T. For additional information, please refer to the ACS716 datasheet.



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Absolute Maximum Ratings

Characteristic	Symbol	Notes	Rating	Unit
Supply Voltage	V _{CC}		8	V
Filter Pin	V _{FILTER}		8	V
Analog Output Pin	V _{IOUT}		32	V
Overcurrent Input Pin	V _{OC}		8	V
Overcurrent FAULT Pin	V FAULT		8	V
Fault Enable (FAULT_EN) Pin	V _{FAULTEN}		8	V
Voltage Reference Output Pin	V _{ZCR}		8	V
DC Reverse Voltage: VCC, FILTER, VIOUT, VOC, FAULT, FAULT_EN, and VZCR Pins	V _{Rdcx}		-0.5	V
Excess to Supply Voltage: FILTER, VIOUT, VOC, FAULT, FAULT_EN, and VZCR Pins	V _{EX}	Voltage by which pin voltage can exceed the VCC pin voltage	0.3	V
Output Current Source	I _{IOUT(Source)}		3	mA
Output Current Sink	I _{IOUT(Sink)}		1	mA
Operating Ambient Temperature	T _A	Range K	-40 to 125	°C
Junction Temperature	T _J (max)		165	°C
Storage Temperature	T _{stg}		-65 to 170	°C

Isolation Characteristics

Characteristic	Symbol	Notes	Rating	Unit
Dielectric Strength Test Voltage*	V _{ISO}	Agency type-tested for 60 seconds per UL standard 1577	3000	VAC
Working Voltage for Basic Isolation	V _{WFSI}	For basic (single) isolation per UL standard 1577; for higher continuous voltage ratings, please contact Allegro	277	VAC

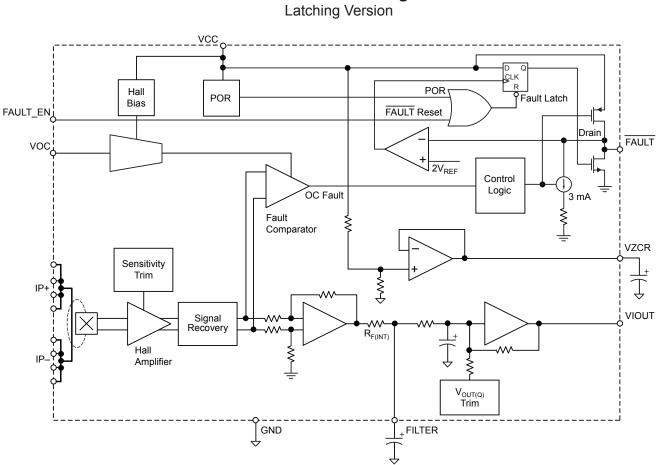
* Allegro does not conduct 60-second testing. It is done only during the UL certification process.

Thermal Characteristics

Characteristic	Symbol	Test Conditions	Value	Unit
Package Thermal Resistance	R _{θJA}	When mounted on Allegro demo board with 1332 mm ² (654 mm ² on com- ponent side and 678 mm ² on opposite side) of 2 oz. copper connected to the primary leadframe and with thermal vias connecting the copper layers. Performance is based on current flowing through the primary leadframe and includes the power consumed by the PCB.	17	°C/W



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Functional Block Diagram

Terminal List Table, Latching Version

Pin-out Diagram

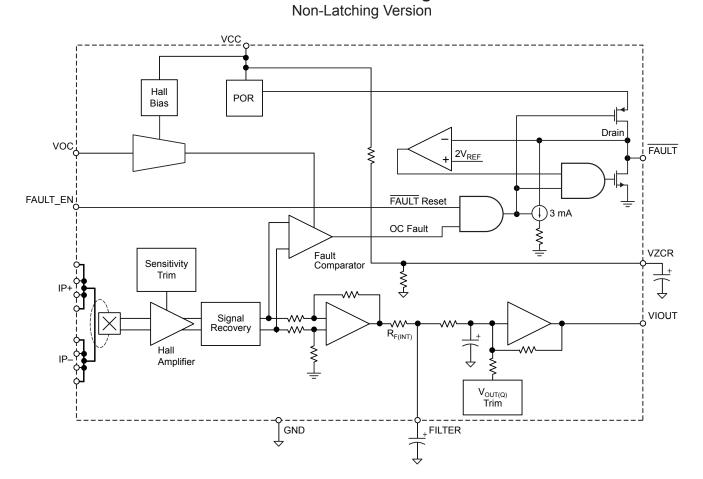
IP+ 1	16 FAULT_EN
IP+ 2	15 VOC
IP+ 3	14 VCC
IP+ 4	13 FAULT
IP- 5	12 VIOUT
IP- 6	11 FILTER

Number	Name	Description
1 through 4	IP+	Sensed current copper conduction path pins. Terminals for current being sensed; fused internally, loop to IP– pins; unidirectional or bidirectional current flow.
5 through 8	IP-	Sensed current copper conduction path pins. Terminals for current being sensed; fused internally, loop to IP+ pins; unidirectional or bidirectional current flow.
9	GND	Device ground connection.
10	VZCR	Voltage Reference Output pin. Zero current (0 A) reference; output voltage on this pin scales with V_{CC} . (Not a highly accurate reference.)
11	FILTER	Filter pin. Terminal for an external capacitor connected from this pin to GND to set the device bandwidth.
12	VIOUT	Analog Output pin. Output voltage on this pin is proportional to current flowing through the loop between the IP+ pins and IP– pins.
13	FAULT	Overcurrent Fault pin. When current flowing between IP+ pins and IP– pins exceeds the overcurrent fault threshold, this pin transitions to a logic low state.
14	VCC	Supply voltage.
15	VOC	Overcurrent Input pin. Analog input voltage on this pin sets the overcurrent fault threshold.
16	FAULT_EN	Enables overcurrent faulting when high. Resets FAULT when low.



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Terminal List Table, Non-Latching Version

Pin-out Diagram 16 FAULT_EN IP+ 1 15 VOC IP+ 2 14 VCC IP+ 3 13 FAULT IP+ 4 IP- 5 12 VIOUT IP-6 11 FILTER 10 VZCR IP- 7 IP- 8 9 GND

Number	Name	Description
1 through 4	IP+	Sensed current copper conduction path pins. Terminals for current being sensed; fused internally, loop to IP– pins; unidirectional or bidirectional current flow.
5 through 8	IP-	Sensed current copper conduction path pins. Terminals for current being sensed; fused internally, loop to IP+ pins; unidirectional or bidirectional current flow.
9	GND	Device ground connection.
10	VZCR	Voltage Reference Output pin. Zero current (0 A) reference; output voltage on this pin scales with V_{CC} . (Not a highly accurate reference.)
11	FILTER	Filter pin. Terminal for an external capacitor connected from this pin to GND to set the device bandwidth.
12	VIOUT	Analog Output pin. Output voltage on this pin is proportional to current flowing through the loop between the IP+ pins and IP– pins.
13	FAULT	Overcurrent Fault pin. When current flowing between IP+ pins and IP– pins exceeds the overcurrent fault threshold, this pin transitions to a logic low state.
14	VCC	Supply voltage.
15	VOC	Overcurrent Input pin. Analog input voltage on this pin sets the overcurrent fault threshold.
16	FAULT_EN	Enables overcurrent faulting when high.



120 kHz Bandwidth, High Voltage Isolation Current Sensor with Integrated Overcurrent Detection

COMMON OPERATING CHARACTERISTICS Valid at $T_A = -40^{\circ}$ C to 125°C, $V_{CC} = 5$ V, unless otherwise specified

Characteristic	Symbol	Test Conditions	Min.	Тур.	Max.	Units
ELECTRICAL CHARACTERISTICS		-				
Supply Voltage ¹	V _{CC}		3	_	5.5	V
Nominal Supply Voltage	V _{CCN}		-	5	-	V
Supply Current	I _{CC}	VIOUT open, FAULT pin high	-	11	14.5	mA
Output Capacitance Load	C _{LOAD}	VIOUT pin to GND	-	_	10	nF
Output Resistive Load	R _{LOAD}	VIOUT pin to GND	10	_	-	kΩ
Magnetic Coupling from Device Conductor to Hall Element	MC _{HALL}	Current flowing from IP+ to IP- pins	-	9.5	-	G/A
Internal Filter Resistance ²	R _{F(INT)}		-	1.7	-	kΩ
Primary Conductor Resistance	R _{PRIMARY}	T _A = 25°C	-	1	-	mΩ
ANALOG OUTPUT SIGNAL CHARACTERIS						
Full Range Linearity ³	E _{LIN}	$I_{P} = \pm I_{P0A}$	-0.75	±0.25	0.75	%
Symmetry ⁴	E _{SYM}	$I_{P} = \pm I_{P0A}$	99.1	100	100.9	%
Bidirectional Quiescent Output	V _{OUT(QBI)}	$I_{\rm P} = 0 \text{ A}, T_{\rm A} = 25^{\circ} \text{C}$	-	V _{CC} ×0.5	-	V
TIMING PERFORMANCE CHARACTERISTI					1	
VIOUT Signal Rise Time	tr	$ T_A = 25^{\circ}C$, Swing I _p from 0 A to I _{P0A} , no capacitor on FILTER pin, 100 pF from VIOUT to GND	_	3	-	μs
VIOUT Signal Propagation Time	t _{PROP}	T _A = 25°C, no capacitor on FILTER pin, 100 pF from VIOUT to GND	-	1	-	μs
VIOUT Signal Response Time	t _{RESPONSE}	$T_A = 25^{\circ}$ C, Swing I _P from 0 A to I _{P0A} , no capacitor on FILTER pin, 100 pF from VIOUT to GND	-	4	_	μs
VIOUT Large Signal Bandwidth	f _{3dB}	-3 dB, Apply I _P such that V _{IOUT} = 1 V _{pk-pk} , no capacitor on FILTER pin, 100 pF from VIOUT to GND	-	120	-	kHz
Power-On Time	t _{PO}	Output reaches 90% of steady-state level, no capacitor on FILTER pin, $T_A = 25^{\circ}C$	-	35	_	μs
OVERCURRENT CHARACTERISTICS						
Setting Voltage for Overcurrent Switchpoint ⁵	V _{OC}		V _{CC} ×0.25	-	V _{CC} ×0.4	V
Signal Noise at Overcurrent Comparator Input	I _{NCOMP}		-	±1	-	A
Overcurrent Fault Switchpoint Error ^{6,7}	E _{OC}	Switchpoint in V_{OC} safe operating area; assumes $I_{NCOMP} = 0 A$	-	±5	-	%
Overcurrent FAULT Pin Output Voltage	VFAULT	1 mA sink current at FAULT pin	-	_	0.4	V
Fault Enable (FAULT_EN Pin) Input Low Voltage Threshold	V _{IL}		-	_	0.1×V _{CC}	V
Fault Enable (FAULT_EN Pin) Input High Voltage Threshold	V _{IH}		$0.8 \times V_{CC}$	_	_	V
Fault Enable (FAULT_EN Pin) Input Resistance	R _{FEI}		-	1	_	MΩ

Continued on the next page...



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COMMON OPERATING CHARACTERISTICS (continued) Valid at T_A = -40°C to 125°C, V_{CC} = 5 V, unless otherwise specified

Characteristic	Symbol	Test Conditions	Min.	Тур.	Max.	Units
OVERCURRENT CHARACTERISTICS (con	ntinued)					
Fault Enable (FAULT_EN Pin) Delay ⁸	t _{FED}	$\label{eq:second} \begin{array}{ c c c c c } \hline Set FAULT_EN to low, V_{OC} = 0.25 \times V_{CC}, \\ C_{OC} = 0 \ F; then run a DC I_P exceeding the corresponding overcurrent threshold; then reset FAULT_EN from low to high and measure the delay from the rising edge of FAULT_EN to the falling edge of FAULT \\ \hline \end{array}$	_	15	_	μs
Fault Enable (FAULT_EN Pin) Delay (Non-Latching versions) ⁹	t _{FED(NL)}	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	_	150	_	ns
Overcurrent Fault Response Time	toc	FAULT_EN set to high for a minimum of 20 µs before the overcurrent event; switchpoint set at $V_{OC} = 0.25 \times V_{CC}$; delay from I _P exceeding overcurrent fault threshold to $V_{\overline{FAULT}} < 0.4$ V, without external C _{OC} capacitor	_	1.9	_	μs
Undercurrent Fault Response Time (Non-Latching versions)	t _{uc}	FAULT_EN set to high for a minimum of 20 µs before the undercurrent event; switchpoint set at $V_{OC} = 0.25 \times V_{CC}$; delay from I _P falling below the overcurrent fault threshold to $V_{FAULT} > 0.8 \times V_{CC}$, without external C _{OC} capacitor, R _{PU} = 330 kΩ	_	3	-	μs
Overcurrent Fault Reset Delay	t _{OCR}	Time from $V_{FAULTEN} < V_{IL}$ to $V_{\overline{FAULT}} > 0.8 \times V_{CC}$, $R_{PU} = 330 \text{ k}\Omega$	-	500	-	ns
Overcurrent Fault Reset Hold Time	t _{OCH}	Time from $V_{FAULTEN} < V_{IL}$ to rising edge of $V_{\overline{FAULT}}$	-	250	-	ns
Overcurrent Input Pin Resistance	R _{OC}	$T_A = 25^{\circ}C$, VOC pin to GND	2	-	-	MΩ
VOLTAGE REFERENCE CHARACTERISTI	CS					
Voltage Reference Output	V _{ZCR}	T _A = 25 °C (Not a highly accurate reference)	0.48 x V _{CC}	$0.5 \times V_{CC}$	0.51 x V _{CC}	V
Voltage Reference Output Load Current	I _{ZCR}	Source current	3	-	-	mA
5		Sink current	50	-	-	μA
Voltage Reference Output Drift	ΔV_{ZCR}		-	±10	-	mV

¹Devices are programmed for maximum accuracy at V_{CC} = 5 V. The device contains ratiometry circuits that accurately alter the 0 A Output Voltage and Sensitivity level of the device in proportion to the applied V_{CC} level. However, as a result of minor nonlinearities in the ratiometry circuit, additional output error will result when V_{CC} varies from the V_{CC} level at which the device was programmed. Customers that plan to operate the device at a V_{CC} level other than the V_{CC} level at which the device was programmed should contact their local Allegro sales representative regarding expected device accuracy levels under these bias conditions.

²R_{F(INT)} forms an RC circuit via the FILTER pin.

³This parameter can drift by as much as 0.8% over the lifetime of this product.

⁴This parameter can drift by as much as 1% over the lifetime of this product.

⁵See page 8 on how to set overcurrent fault switchpoint.

⁶Switchpoint can be lower at the expense of switchpoint accuracy.

⁷This error specification does not include the effect of noise. See the I_{NCOMP} specification in order to factor in the additional influence of noise on the fault switchpoint.

⁸Fault Enable Delay is designed to avoid false tripping of an Overcurrent (OC) fault at power-up. A 15 μs (typical) delay will always be needed, every time FAULT_EN is raised from low to high, before the device is ready for responding to any overcurrent event.

⁹During power-up, this delay is 15 µs in order to avoid false tripping of an Overcurrent (OC) fault.



120 kHz Bandwidth, High Voltage Isolation Current Sensor with Integrated Overcurrent Detection

PERFORMANCE CHARACTERISTICS, T_A Range K, valid at $T_A = -40^{\circ}$ C to 125°C, $V_{CC} = 5$ V, unless otherwise specified

Characteristic	Symbol	Test Conditions	Min.	Тур.	Max.	Units
X6BB CHARACTERISTIC	S					
Optimized Accuracy Range ¹	I _{POA}		-7.5	_	7.5	A
Linear Sensing Range	I _R		-14	_	14	A
Noise ²	V _{NOISE(rms)}	$T_A = 25^{\circ}C$, Sens = 100 mV/A, $C_f = 0$, $C_{LOAD} = 4.7$ nF, R_{LOAD} open	_	4.05	_	mV
		I _P = 6.5 A, T _A = 25°C	_	151	_	mV/A
Sensitivity ³	Sens	$I_{P} = 6.5 \text{ A}, T_{A} = 25^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$	_	151	_	mV/A
		$I_{P} = 6.5 \text{ A}, T_{A} = -40^{\circ}\text{C} \text{ to } 25^{\circ}\text{C}$	_	152	_	mV/A
Electrical Offset Voltage		$I_{P} = 0 \text{ A}, T_{A} = 25^{\circ}\text{C}$	_	±10	_	mV
Variation Relative to $V_{OUT(QBI)}^4$	V _{OE}	$I_{P} = 0 \text{ A}, T_{A} = 25^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$	_	±11	_	mV
		$I_{P} = 0 \text{ A}, T_{A} = -40^{\circ} \text{C} \text{ to } 25^{\circ} \text{C}$	_	±40	_	mV
Tatal Quitaut Error5		Over full scale of I_{POA} , I_P applied for 5 ms, T_A = 25°C to 125°C	_	±1.6	-	%
Total Output Error ⁵	E _{TOT}	Over full scale of I_{POA} , I_P applied for 5 ms, $T_A = -40^{\circ}$ C to 25°C	_	±5.6	_	%
X10BB CHARACTERISTI	CS					
Optimized Accuracy Range ¹	I _{POA}		-10	_	10	A
Linear Sensing Range	I _R		-24	_	24	A
Noise ²	V _{NOISE(rms)}	$T_A = 25^{\circ}C$, Sens = 85 mV/A, $C_f = 0$, $C_{LOAD} = 4.7$ nF, R_{LOAD} open	_	2.3	_	mV
	Sens	I _P = 10 A, T _A = 25°C	_	85	_	mV/A
Sensitivity ³		$I_{P} = 10 \text{ A}, T_{A} = 25^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$	_	85	_	mV/A
		$I_{P} = 10 \text{ A}, T_{A} = -40^{\circ} \text{C} \text{ to } 25^{\circ} \text{C}$	_	85	_	mV/A
Electrical Offset Voltage		$I_{P} = 0 A, T_{A} = 25^{\circ}C$	_	±5	_	mV
Variation Relative to	V _{OE}	$I_{P} = 0 \text{ A}, T_{A} = 25^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$	_	±12	_	mV
V _{OUT(QBI)} ⁴		$I_{P} = 0 \text{ A}, T_{A} = -40^{\circ} \text{C} \text{ to } 25^{\circ} \text{C}$	_	±22	_	mV
Total Quitaut Error5		Over full scale of I_{POA} , I_P applied for 5 ms, T_A = 25°C to 125°C	_	±1.8	_	%
Total Output Error ⁵	E _{TOT}	Over full scale of I_{POA} , I_P applied for 5 ms, $T_A = -40^{\circ}$ C to 25°C	_	±5	_	%
X12CB CHARACTERISTI	CS					
Optimized Accuracy Range ¹	I _{POA}		-12.5	_	12.5	A
Linear Sensing Range	I _R		-37.5	_	37.5	А
Noise ²	V _{NOISE(rms)}	$T_A = 25^{\circ}C$, Sens = 56 mV/A, $C_f = 0$, $C_{LOAD} = 4.7$ nF, R_{LOAD} open	_	1.50	_	mV
		I _P = 12.5 A, T _A = 25°C	_	56	_	mV/A
Sensitivity ³	Sens	I _P = 12.5 A, T _A = 25°C to 125°C	_	56	_	mV/A
		$I_{P} = 12.5 \text{ A}, T_{A} = -40^{\circ}\text{C} \text{ to } 25^{\circ}\text{C}$	_	57	_	mV/A
Electrical Offset Voltage		$I_{\rm P} = 0 \text{ A}, T_{\rm A} = 25^{\circ} \text{C}$	_	±4	_	mV
Variation Relative to	V _{OE}	$I_{P} = 0 \text{ A}, T_{A} = 25^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$	_	±14	_	mV
V _{OUT(QBI)} ⁴		$I_{P} = 0 \text{ A}, T_{A} = -40^{\circ} \text{C} \text{ to } 25^{\circ} \text{C}$	_	±23	_	mV
Total Quitaut Error5		Over full scale of I_{POA} , I_P applied for 5 ms, T_A = 25°C to 125°C	_	±2.2	_	%
Total Output Error ⁵	E _{TOT}	Over full scale of I_{POA} , I_P applied for 5 ms, $T_A = -40^{\circ}$ C to 25°C	_	±3.9	_	%

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120 kHz Bandwidth, High Voltage Isolation Current Sensor with Integrated Overcurrent Detection

PERFORMANCE CHARACTERISTICS (continued), T_A Range K, valid at T_A = -40°C to 125°C, V_{CC} = 5 V, unless otherwise specified

X25CB CHARACTERISTIC	s					
Optimized Accuracy Range ¹	I _{POA}		-25	_	25	A
Linear Sensing Range	I _R		-75	_	75	А
Noise ²	V _{NOISE(rms)}	$T_A = 25^{\circ}C$, Sens = 28 mV/A, $C_f = 0$, $C_{LOAD} = 4.7$ nF, R_{LOAD} open	-	1	_	mV
		I _P = 25 A, T _A = 25°C	-	28	-	mV/A
Sensitivity ³	Sens	$I_{P} = 25 \text{ A}, T_{A} = 25^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$	-	27.9	-	mV/A
		$I_{P} = 25 \text{ A}, T_{A} = -40^{\circ}\text{C} \text{ to } 25^{\circ}\text{C}$	-	28.5	-	mV/A
Electrical Offset Voltage		$I_{P} = 0 A, T_{A} = 25^{\circ}C$	_	±3	_	mV
Variation Relative to	V _{OE}	$I_{P} = 0 \text{ A}, T_{A} = 25^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$	_	±12	_	mV
V _{OUT(QBI)} ⁴		$I_{P} = 0 \text{ A}, T_{A} = -40^{\circ}\text{C} \text{ to } 25^{\circ}\text{C}$	-	±18	-	mV
Tatal Output Error5		Over full scale of I_{POA} , I_P applied for 5 ms, T_A = 25°C to 125°C	-	±2.9	_	%
Total Output Error⁵	E _{TOT}	Over full scale of I_{POA} , I_P applied for 5 ms, $T_A = -40^{\circ}$ C to 25°C	-	±5.2	_	%

¹Although the device is accurate over the entire linear range, the device is programmed for maximum accuracy over the range defined by I_{POA}. The reason for this is that in many applications, such as motor control, the start-up current of the motor is approximately three times higher than the running current.

 $^{2}V_{pk-pk}$ noise (6 sigma noise) is equal to 6 × $V_{NOISE(rms)}$. Lower noise levels than this can be achieved by using C_f for applications requiring narrower bandwidth. See Characteristic Performance page for graphs of noise versus C_f and bandwidth versus C_f.

³This parameter can drift by as much as 2.4% over the lifetime of this product.

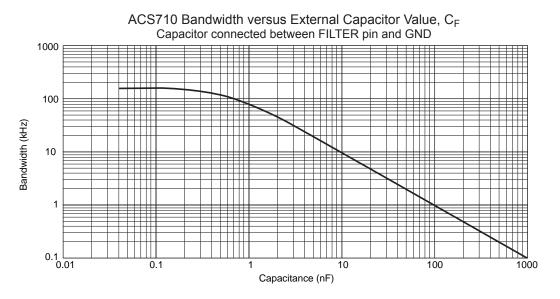
⁴This parameter can drift by as much as 13 mV over the lifetime of this product.

 $^5\mathrm{This}$ parameter can drift by as much as 2.5% over the lifetime of this product.

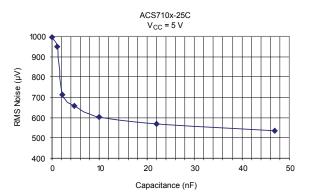


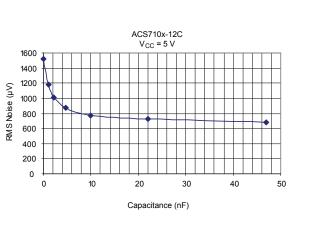
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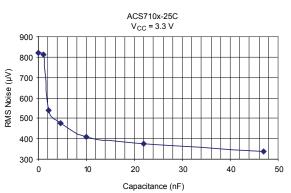
Characteristic Performance

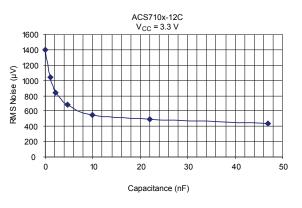


ACS710 Noise versus External Capacitor Value, C_F Capacitor connected between FILTER pin and GND











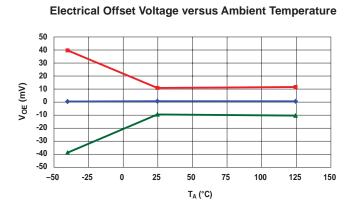
Allegro MicroSystems, LLC 115 Northeast Cutoff Worcester, Massachusetts 01615-0036 U.S.A. 1.508.853.5000; www.allegromicro.com

120 kHz Bandwidth, High Voltage Isolation Current Sensor with Integrated Overcurrent Detection

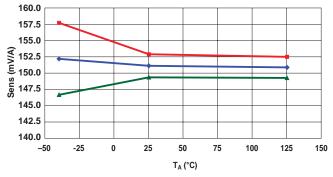
Characteristic Performance Data

Data taken using the ACS710-6BB

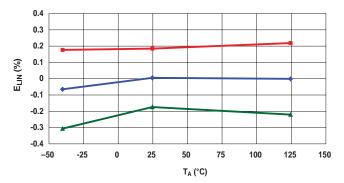
Accuracy Data



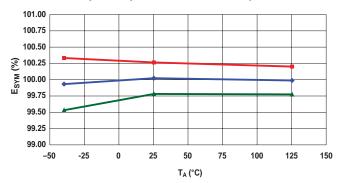
Sensitivity versus Ambient Temperature



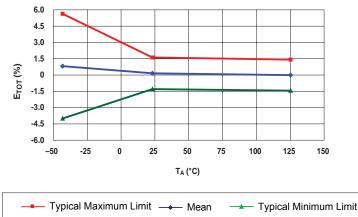
Nonlinearity versus Ambient Temperature



Symmetry versus Ambient Temperature







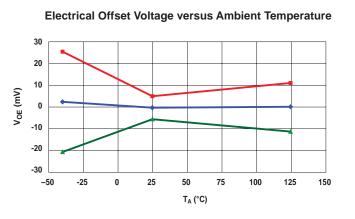


120 kHz Bandwidth, High Voltage Isolation Current Sensor with Integrated Overcurrent Detection

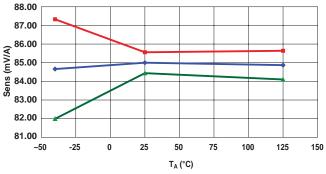
Characteristic Performance Data

Data taken using the ACS710-10BB

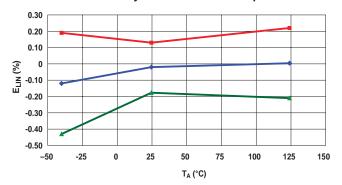
Accuracy Data



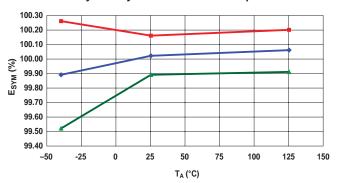
Sensitivity versus Ambient Temperature



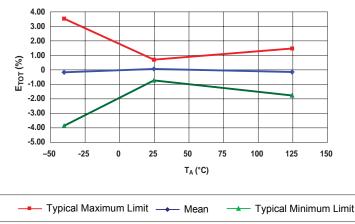
Nonlinearity versus Ambient Temperature



Symmetry versus Ambient Temperature









-0.05

-0.10

-0.20 -0.25

-0.30 -0.35

-0.40

-0.45 -50

-25

0

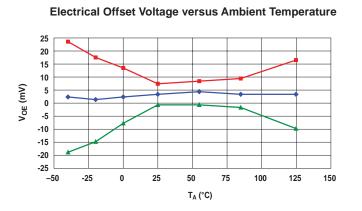
ELIN (%) -0.15

120 kHz Bandwidth, High Voltage Isolation **Current Sensor with Integrated Overcurrent Detection**

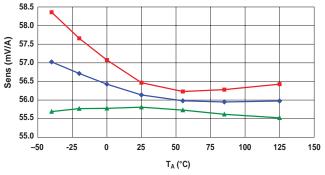
Characteristic Performance Data

Data taken using the ACS710-12CB

Accuracy Data



Sensitivity versus Ambient Temperature



0.10 0.05 0

25

Nonlinearity versus Ambient Temperature

50

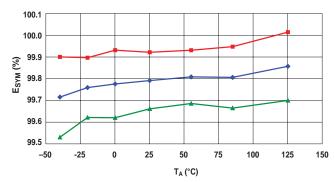
T_A (°C)

75

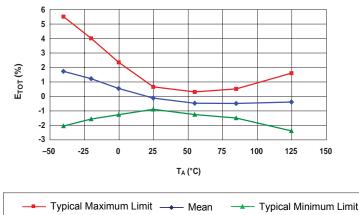
100

125











-0.15 -0.20

-0.25

-0.30

-0.35 -50

-25

0

25

50

T_A (°C)

75

100

125

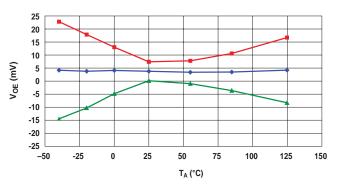
120 kHz Bandwidth, High Voltage Isolation **Current Sensor with Integrated Overcurrent Detection**

Characteristic Performance Data

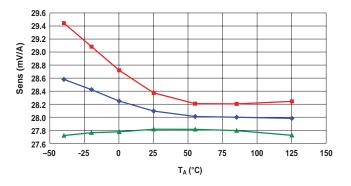
Data taken using the ACS710-25CB

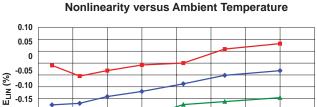
Accuracy Data

Electrical Offset Voltage versus Ambient Temperature

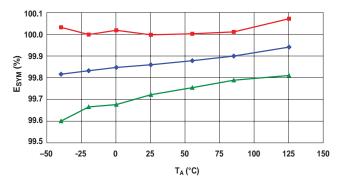


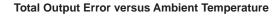
Sensitivity versus Ambient Temperature

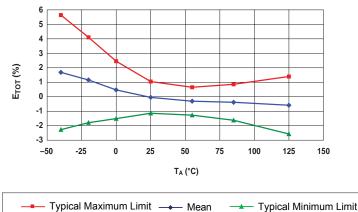




Symmetry versus Ambient Temperature









120 kHz Bandwidth, High Voltage Isolation Current Sensor with Integrated Overcurrent Detection

Setting Overcurrent Fault Switchpoint

Setting 12CB and 25CB Versions

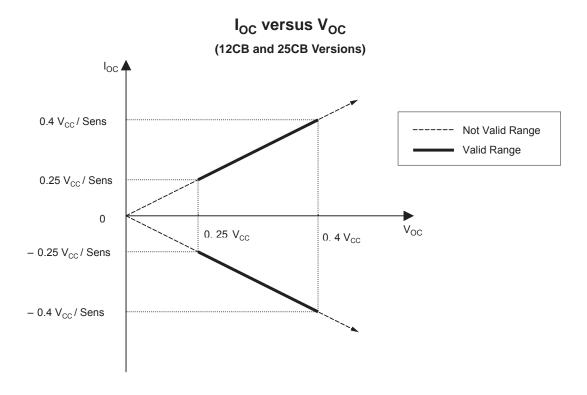
The V_{OC} needed for setting the overcurrent fault switchpoint can be calculated as follows:

$$V_{\rm OC} = {\rm Sens} \times |I_{\rm OC}|$$
,

where V_{OC} is in mV, Sens in mV/A, and I_{OC} (overcurrent fault switchpoint) in A.

| Ioc | is the overcurrent fault switchpoint for a bidirectional (AC) current, which means a bi-directional sensor will have two symmetrical overcurrent fault switchpoints, $+I_{OC}$ and $-I_{OC}$.

See the following graph for I_{OC} and V_{OC} ranges.



Example: For ACS710KLATR-25CB-T, if required overcurrent fault switchpoint is 50 A, and V_{CC} = 5 V, then the required V_{OC} can be calculated as follows:

 V_{OC} = Sens × I_{OC} = 28 × 50 = 1400 (mV)



Setting 6BB and 10BB Versions

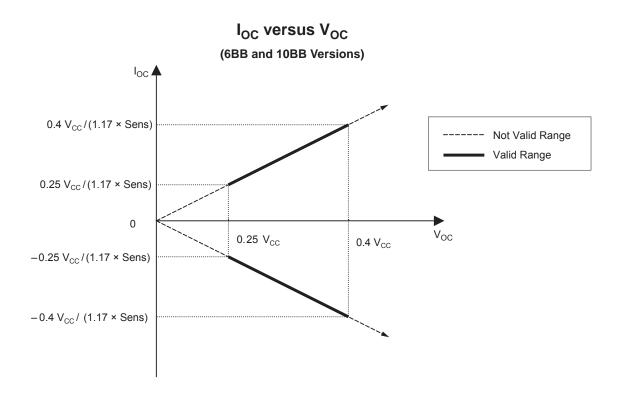
The V_{OC} needed for setting the overcurrent fault switchpoint can be calculated as follows:

 $V_{\rm OC} = 1.17 \times \text{Sens} \times |I_{\rm OC}|$,

where V_{OC} is in mV, Sens in mV/A, and I_{OC} (overcurrent fault switchpoint) in A.

| Ioc | is the overcurrent fault switchpoint for a bidirectional (AC) current, which means a bi-directional sensor will have two symmetrical overcurrent fault switchpoints, $+I_{OC}$ and $-I_{OC}$.

See the following graph for I_{OC} and V_{OC} ranges.



Example: For ACS710KLATR-6BB-T, if required overcurrent fault switchpoint is 10 A, and V_{CC} = 5 V, then the required V_{OC} can be calculated as follows:

 V_{OC} = 1.17 × Sens × I_{OC} = 1.17 × 151 × 10 = 1767 (mV)



Functional Description (Latching Versions)

Overcurrent Fault Operation

The primary concern with high-speed fault detection is that noise may cause false tripping. Various applications have or need to be able to ignore certain faults that are due to switching noise or other parasitic phenomena, which are application dependant. The problem with simply trying to filter out this noise in the main signal path is that in high-speed applications, with asymmetric noise, the act of filtering introduces an error into the measurement. To get around this issue, and allow the user to prevent the fault signal from being latched by noise, a circuit was designed to slew the FAULT pin voltage based on the value of the capacitor from that pin to ground. Once the voltage on the pin falls below 2 V, as established by an internal reference, the fault output is latched and pulled to ground quickly with an internal N-channel MOSFET.

Fault Walk-through

The following walk-through references various sections and attributes in the figure below. This figure shows different fault set/reset scenarios and how they relate to the voltages on the FAULT pin, FAULT_EN pin, and the internal Overcurrent (OC) Fault node, which is invisible to the customer.

- 1. Because the device is enabled (FAULT_EN is high for a minimum period of time, the Fault Enable Delay, t_{FED} , 15 µs typical) and there is an OC fault condition, the device FAULT pin starts discharging.
- 2. When the FAULT pin voltage reaches approximately 2 V, the fault is latched, and an internal NMOS device pulls the FAULT pin voltage to approximately 0 V. The rate at which the FAULT pin slews downward (see [4] in the figure) is dependent on the external capacitor, C_{OC} , on the FAULT pin.
- 3. When the FAULT_EN pin is brought low, the FAULT pin starts resetting if no OC fault condition exists, and if FAULT_EN is low for a time period greater than t_{OCH}. The

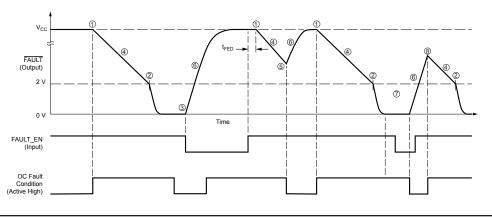
internal NMOS pull-down turns off and an internal PMOS pullup turns on (see [7] if the OC fault condition still exists).

4. The slope, and thus the delay to latch the fault is controlled by the capacitor, C_{OC} , placed on the FAULT pin to ground. During this portion of the fault (when the FAULT pin is between V_{CC} and 2 V), there is a 3 mA constant current sink, which discharges C_{OC} . The length of the fault delay, t, is equal to:

$$t = \frac{C_{\rm oc} \times (V_{\rm CC} - 2\,\rm V)}{3\,\rm mA} \tag{1}$$

where V_{CC} is the device power supply voltage in volts, t is in seconds and C_{OC} is in Farads. This formula is valid for R_{PU} equal to or greater than 330 k Ω . For lower-value resistors, the current flowing through the R_{PU} resistor during a fault event, I_{PU} , will be larger. Therefore, the current discharging the capacitor would be 3 mA – I_{PU} and equation 1 may not be valid.

- 5. The FAULT pin did not reach the 2 V latch point before the OC fault condition cleared. Because of this, the fixed 3 mA current sink turns off, and the internal PMOS pull-up turns on to recharge C_{OC} through the FAULT pin.
- 6. This curve shows V_{CC} charging external capacitor C_{OC} through the internal PMOS pull-up. The slope is determined by C_{OC} .
- 7. When the FAULT_EN pin is brought low, if the fault condition still exists, the latched FAULT pin will be pulled low by the internal 3mA current source. When fault condition is removed then the Fault pin charges as shown in step 6.
- 8. At this point there is a fault condition, and the part is enabled before the \overline{FAULT} pin can charge to V_{CC} . This shortens the user-set delay, so the fault is latched earlier. The new delay time can be calculated by equation 1, after substituting the voltage seen on the \overline{FAULT} pin for V_{CC} .





Functional Description (Non-Latching Versions)

Overcurrent Fault Operation

The primary concern with high-speed fault detection is that noise may cause false tripping. Various applications have or need to be able to ignore certain faults that are due to switching noise or other parasitic phenomena, which are application dependant. The problem with simply trying to filter out this noise in the main signal path is that in high-speed applications, with asymmetric noise, the act of filtering introduces an error into the measurement. To get around this issue, and allow the user to prevent the fault signal from going low due to noise, a circuit was designed to slew the FAULT pin voltage based on the value of the capacitor from that pin to ground. Once the voltage on the pin falls below 2 V, as established by an internal reference, the fault output is pulled to ground quickly with an internal N-channel MOSFET.

Fault Walk-through

The following walk-through references various sections and attributes in the figure below. This figure shows different fault set/reset scenarios and how they relate to the voltages on the FAULT pin, FAULT_EN pin, and the internal Overcurrent (OC) Fault node, which is invisible to the customer.

- 1. Because the device is enabled (FAULT_EN is high for a minimum period of time, the Fault Enable Delay, t_{FED}, and there is an OC fault condition, the device FAULT pin starts discharging.
- 2. When the FAULT pin voltage reaches approximately 2 V, an internal NMOS device pulls the FAULT pin voltage to approximately 0 V. The rate at which the FAULT pin slews downward (see [4] in the figure) is dependent on the external capacitor, C_{OC} , on the FAULT pin.
- 3. When the FAULT_EN pin is brought low, the FAULT pin starts resetting if FAULT_EN is low for a time period greater

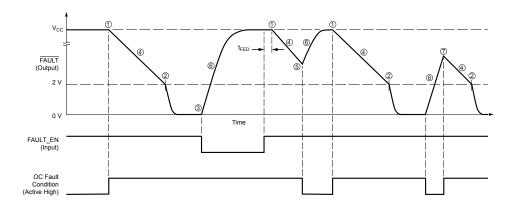
than t_{OCH} . The internal NMOS pull-down turns off and an internal PMOS pull-up turns on.

4. The slope, and thus the delay to pull the fault low is controlled by the capacitor, C_{OC} , placed on the FAULT pin to ground. During this portion of the fault (when the FAULT pin is between V_{CC} and 2 V), there is a 3 mA constant current sink, which discharges C_{OC}. The length of the fault delay, t, is equal to:

$$t = \frac{C_{\rm oc} \times (V_{\rm CC} - 2 \,\mathrm{V})}{3 \,\mathrm{mA}} \tag{2}$$

where V_{CC} is the device power supply voltage in volts, t is in seconds and C_{OC} is in Farads. This formula is valid for R_{PU} equal to or greater than 330 k Ω . For lower-value resistors, the current flowing through the R_{PU} resistor during a fault event, I_{PU} , will be larger. Therefore, the current discharging the capacitor would be 3 mA – I_{PU} and equation 1 may not be valid.

- 5. The FAULT pin did not reach the 2 V latch point before the OC fault condition cleared. Because of this, the fixed 3 mA current sink turns off, and the internal PMOS pull-up turns on to recharge C_{OC} through the FAULT pin.
- 6. This curve shows V_{CC} charging external capacitor C_{OC} through the internal PMOS pull-up. The slope is determined by C_{OC} .
- 7. At this point there is a fault condition, and the part is enabled before the \overline{FAULT} pin can charge to V_{CC} . This shortens the user-set delay, so the fault gets pulled low earlier. The new delay time can be calculated by equation 1, after substituting the voltage seen on the \overline{FAULT} pin for V_{CC} .



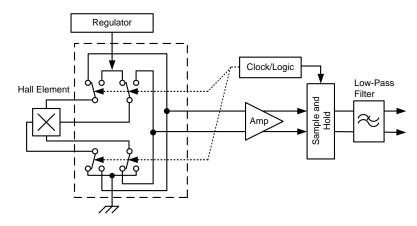


120 kHz Bandwidth, High Voltage Isolation Current Sensor with Integrated Overcurrent Detection

Chopper Stabilization Technique

Chopper Stabilization is an innovative circuit technique that is used to minimize the offset voltage of a Hall element and an associated on-chip amplifier. Allegro patented a Chopper Stabilization technique that nearly eliminates Hall IC output drift induced by temperature or package stress effects. This offset reduction technique is based on a signal modulation-demodulation process. Modulation is used to separate the undesired dc offset signal from the magnetically induced signal in the frequency domain. Then, using a low-pass filter, the modulated DC offset is suppressed while the magnetically induced signal passes through the filter. As a result of this chopper stabilization approach, the output voltage from the Hall IC is desensitized to the effects of temperature and mechanical stress. This technique produces devices that have an extremely stable Electrical Offset Voltage, are immune to thermal stress, and have precise recoverability after temperature cycling.

This technique is made possible through the use of a BiCMOS process that allows the use of low-offset and low-noise amplifiers in combination with high-density logic integration and sample and hold circuits.



Concept of Chopper Stabilization Technique



120 kHz Bandwidth, High Voltage Isolation Current Sensor with Integrated Overcurrent Detection

Definitions of Accuracy Characteristics

Sensitivity (Sens). The change in sensor output in response to a 1 A change through the primary conductor. The sensitivity is the product of the magnetic circuit sensitivity (G/A) and the linear IC amplifier gain (mV/G). The linear IC amplifier gain is programmed at the factory to optimize the sensitivity (mV/A) for the full-scale current of the device.

Noise (V_{NOISE}). The product of the linear IC amplifier gain (mV/G) and the noise floor for the Allegro Hall effect linear IC. The noise floor is derived from the thermal and shot noise observed in Hall elements. Dividing the noise (mV) by the sensitivity (mV/A) provides the smallest current that the device is able to resolve.

Linearity (\mathbf{E}_{LIN}). The degree to which the voltage output from the sensor varies in direct proportion to the primary current through its full-scale amplitude. Nonlinearity in the output can be attributed to the saturation of the flux concentrator approaching the full-scale current. The following equation is used to derive the linearity:

$$100 \left\{ 1 - \left[\frac{V_{\text{IOUT}} \text{_full-scale amperes} - V_{\text{IOUT}(Q)}}{2 (V_{\text{IOUT}} \frac{1}{2} \text{ full-scale amperes} - V_{\text{IOUT}(Q)})} \right] \right\}$$

where $V_{\text{IOUT}_{full-scale amperes}} =$ the output voltage (V) when the sensed current approximates full-scale $\pm I_{\text{P}}$.

Symmetry (E_{SYM}). The degree to which the absolute voltage output from the sensor varies in proportion to either a positive or negative full-scale primary current. The following formula is used to derive symmetry:

$$00 \left(\frac{V_{\text{IOUT}} + \text{full-scale amperes} - V_{\text{IOUT}(Q)}}{V_{\text{IOUT}(Q)} - V_{\text{IOUT}} - \text{full-scale amperes}} \right)$$

1

Quiescent output voltage (V_{IOUT(Q)}). The output of the sensor when the primary current is zero. For a unipolar supply voltage, it nominally remains at $0.5 \times V_{CC}$. For example, in the case of a bidirectional output device, $V_{CC} = 5$ V translates into $V_{IOUT(Q)} = 2.5$ V. Variation in $V_{IOUT(Q)}$ can be attributed to the resolution of the Allegro linear IC quiescent voltage trim and thermal drift.

Electrical offset voltage (V_{OE}). The deviation of the device output from its ideal quiescent voltage due to nonmagnetic causes. To convert this voltage to amperes, divide by the device sensitivity, Sens.

Accuracy (E_{TOT}). The accuracy represents the maximum deviation of the actual output from its ideal value. This is also known as the total ouput error. The accuracy is illustrated graphically in the output voltage versus current chart at right. Note that error is directly measured during final test at Allegro.

Accuracy is divided into four areas:

- **0** A at 25°C. Accuracy of sensing zero current flow at 25°C, without the effects of temperature.
- **0** A over Δ temperature. Accuracy of sensing zero current flow including temperature effects.
- Full-scale current at 25°C. Accuracy of sensing the full-scale current at 25°C, without the effects of temperature.
- Full-scale current over ∆ temperature. Accuracy of sensing fullscale current flow including temperature effects.

Ratiometry. The ratiometric feature means that its 0 A output, $V_{IOUT(Q)}$, (nominally equal to $V_{CC}/2$) and sensitivity, Sens, are proportional to its supply voltage, V_{CC} . The following formula is used to derive the ratiometric change in 0 A output voltage, $\Delta V_{IOUT(O)RAT}$ (%).

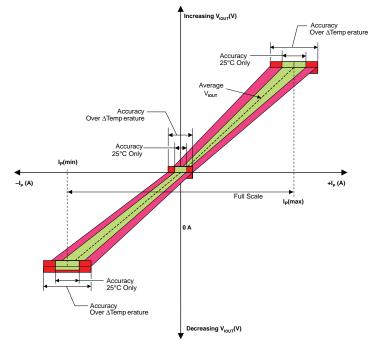
$$00 \left(\frac{V_{\text{IOUT}(Q)\text{VCC}} / V_{\text{IOUT}(Q)\text{SV}}}{V_{\text{CC}} / 5 \text{ V}} \right)$$

The ratiometric change in sensitivity, ΔSens_{RAT} (%), is defined as:

$$100 \left(\frac{Sens_{\rm VCC} / Sens_{\rm 5V}}{V_{\rm CC} / 5 \rm V} \right)$$

Output Voltage versus Sensed Current

Accuracy at 0 A and at Full-Scale Current





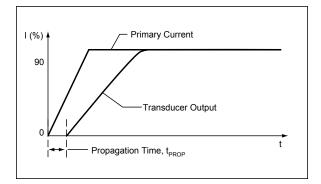
120 kHz Bandwidth, High Voltage Isolation Current Sensor with Integrated Overcurrent Detection

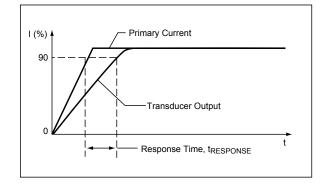
Definitions of Dynamic Response Characteristics

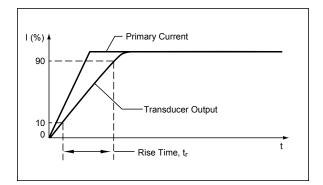
Propagation delay (t_{PROP}). The time required for the sensor output to reflect a change in the primary current signal. Propagation delay is attributed to inductive loading within the linear IC package, as well as in the inductive loop formed by the primary conductor geometry. Propagation delay can be considered as a fixed time offset and may be compensated.

Response time (t_{RESPONSE}). The time interval between a) when the primary current signal reaches 90% of its final value, and b) when the sensor reaches 90% of its output corresponding to the applied current.

Rise time (t_r). The time interval between a) when the sensor reaches 10% of its full scale value, and b) when it reaches 90% of its full scale value. The rise time to a step response is used to derive the bandwidth of the current sensor, in which $f(-3 \text{ dB}) = 0.35/t_r$. Both t_r and t_{RESPONSE} are detrimentally affected by eddy current losses observed in the conductive IC ground plane.



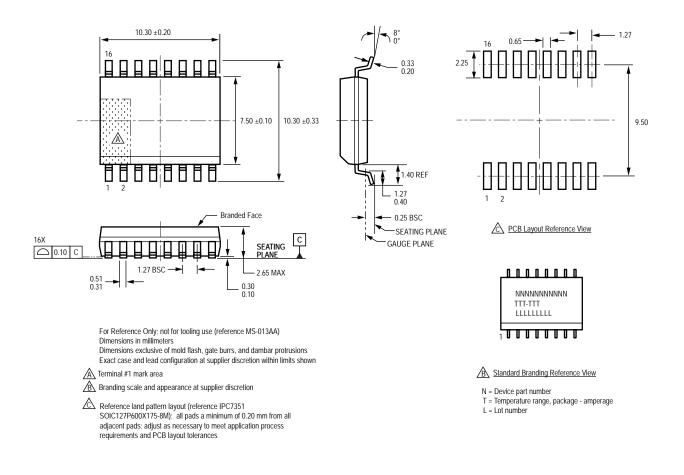






120 kHz Bandwidth, High Voltage Isolation Current Sensor with Integrated Overcurrent Detection

Package LA, 16-pin SOICW





120 kHz Bandwidth, High Voltage Isolation Current Sensor with Integrated Overcurrent Detection

Revision History

Revision	Revision Date	Description of Revision
Rev. 9	June 17, 2013	Add 10BB variant

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