## FEATURES

Unity-gain bandwidth: 5.5 MHz
Low voltage offset: 1.0 mV
Slew rate: $7.5 \mathrm{~V} / \mu \mathrm{s}$
Single-supply operation: 5 V to 18 V
High output current: 70 mA
Low supply current: $\mathbf{8 0 0} \mu \mathrm{A} /$ amplifier
Stable with large capacitive loads
Rail-to-rail inputs and outputs

## APPLICATIONS

LCD gamma and $\mathrm{V}_{\text {com }}$ drivers

## Modems

Portable instrumentation
Direct access arrangement

## GENERAL DESCRIPTION

The AD8614 (single) and AD8644 (quad) are single-supply, 5.5 MHz bandwidth, rail-to-rail amplifiers optimized for LCD monitor applications.

They are processed using the Analog Devices, Inc. high voltage, extra fast complementary bipolar (HV XFCB) process. This proprietary process includes trench-isolated transistors that lower internal parasitic capacitance, which improves gain bandwidth, phase margin, and capacitive load drive. The low supply current of $800 \mu \mathrm{~A}$ (typical) per amplifier is critical for portable or densely packed designs. In addition, the rail-to-rail output swing provides greater dynamic range and control than standard video amplifiers provide.

These products operate from supplies of 5 V to as high as 18 V . The unique combination of an output drive of 70 mA , high slew rates, and high capacitive drive capability makes the AD8614/AD8644 an ideal choice for LCD applications.
The AD8614 and AD8644 are specified over the temperature range of $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. They are available in 5-lead SOT-23, 14-lead TSSOP, and 14-lead SOIC surface-mount packages in tape and reel.

## PIN CONFIGURATIONS



Figure 1. 5-Lead SOT-23 (RJ-5)


Figure 2. 14-Lead TSSOP
( $R U-14$ )


Figure 3. 14-Lead Narrow Body SOIC (R-14)

Rev. $B$

## AD8614/AD8644

## TABLE OF CONTENTS

Features1
Applications ..... 1
General Description .....  1
Pin Configurations ..... 1
Revision History ..... 2
Specifications ..... 3
Electrical Characteristics ..... 3
Absolute Maximum Ratings ..... 4
Thermal Resistance .....  4
ESD Caution .....  4
Typical Performance Characteristics ..... 5
Theory of Operation ..... 9
REVISION HISTORY
9/07—Rev. A to Rev B
Change to Current Noise Density in Table 1 ..... 3
12/06-Rev. 0 to Rev. A
Updated Format

$\qquad$
Universal
Deleted SPICE Model Availability Section ..... 12
Updated Outline Dimensions ..... 13
Changes to Ordering Guide ..... 14
10/99—Revision 0: Initial Version
Output Short-Circuit Protection .....  9
Input Overvoltage Protection ..... 10
Output Phase Reversal ..... 10
Power Dissipation ..... 10
Unused Amplifiers ..... 10
Capacitive Load Drive ..... 11
Direct Access Arrangement ..... 11
A One-Chip Headphone/Microphone Preamplifier Solution ..... 11
Outline Dimensions ..... 13
Ordering Guide ..... 14

## SPECIFICATIONS

## ELECTRICAL CHARACTERISTICS

$5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{S}} \leq 18 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=\mathrm{V}_{\mathrm{S}} / 2, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted. ${ }^{1}$
Table 1.

| Parameter | Symbol | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT CHARACTERISTICS <br> Offset Voltage <br> Input Bias Current <br> Input Offset Current <br> Input Voltage Range Common-Mode Rejection Ratio Voltage Gain | Vos <br> $I_{B}$ <br> los <br> CMRR <br> Avo | $\begin{aligned} & -20^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\ & -20^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\ & -20^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\ & \mathrm{~V}_{\mathrm{CM}}=0 \mathrm{~V} \text { to } \mathrm{V}_{\mathrm{S}} \\ & \text { V out }=0.5 \mathrm{~V} \text { to } \mathrm{V}_{\mathrm{S}}-0.5 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \end{aligned}$ | $\begin{aligned} & 0 \\ & 60 \\ & 10 \\ & \hline \end{aligned}$ | 1.0 <br> 80 <br> 5 <br> 75 <br> 150 | $\begin{aligned} & 2.5 \\ & 3 \\ & 400 \\ & 500 \\ & 100 \\ & 200 \\ & V_{s} \end{aligned}$ | mV <br> mV <br> nA <br> nA <br> nA <br> nA <br> V <br> dB <br> V/mV |
| OUTPUT CHARACTERISTICS <br> Output Voltage High <br> Output Voltage Low <br> Output Short-Circuit Current | Voн <br> Vol <br> Isc | $\begin{aligned} & \mathrm{I}_{\text {LOAD }}=10 \mathrm{~mA} \\ & \mathrm{I}_{\mathrm{LOAD}}=10 \mathrm{~mA} \\ & -20^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & V_{s}-0.15 \\ & 35 \\ & 30 \end{aligned}$ | $\begin{aligned} & 65 \\ & 70 \end{aligned}$ | 150 | V <br> mV <br> mA <br> mA |
| POWER SUPPLY <br> Power Supply Rejection Ratio Supply Current/Amplifier | $\begin{aligned} & \text { PSRR } \\ & \mathrm{I}_{\mathrm{SY}} \end{aligned}$ | $\begin{aligned} & V_{S}= \pm 2.25 \mathrm{~V} \text { to } \pm 9.25 \mathrm{~V} \\ & -20^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \end{aligned}$ | 80 |  | $\begin{aligned} & 1.1 \\ & 1.5 \\ & \hline \end{aligned}$ | dB <br> mA <br> mA |
| DYNAMIC PERFORMANCE <br> Slew Rate <br> Gain Bandwidth Product <br> Phase Margin <br> Settling Time | SR <br> GBP <br> Фо <br> ts | $C_{L}=200 \mathrm{pF}$ $0.01 \%, 10 \mathrm{~V} \text { step }$ |  | $\begin{aligned} & 7.5 \\ & 5.5 \\ & 65 \\ & 3 \end{aligned}$ |  | V/ $\mu \mathrm{s}$ <br> MHz <br> Degrees $\mu \mathrm{s}$ |
| NOISE PERFORMANCE Voltage Noise Density Current Noise Density | $e_{n}$ <br> $e_{n}$ <br> $\mathrm{i}_{\mathrm{n}}$ | $\begin{aligned} & \mathrm{f}=1 \mathrm{kHz} \\ & \mathrm{f}=10 \mathrm{kHz} \\ & \mathrm{f}=10 \mathrm{kHz} \end{aligned}$ |  | $\begin{aligned} & 12 \\ & 11 \\ & 1 \end{aligned}$ |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ |

${ }^{1}$ All typical values are for $V_{S}=18 \mathrm{~V}$.

## AD8614/AD8644

## ABSOLUTE MAXIMUM RATINGS

Table 2.

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage | 20 V |
| Input Voltage | GND to Vs |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operating Temperature Range | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Junction Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature Range (Soldering, 60 sec ) | $300^{\circ} \mathrm{C}$ |

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## THERMAL RESISTANCE

$\theta_{\text {IA }}$ is specified for the worst-case conditions, that is, a device soldered in a circuit board for surface-mount packages.

Table 3. Thermal Resistance

| Package Type | $\boldsymbol{\theta}_{\mathrm{JA}}$ | $\boldsymbol{\theta}_{\mathrm{Jc}}$ | Unit |
| :--- | :--- | :--- | :--- |
| 5-Lead SOT-23 (RJ) | 230 | 140 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 14-Lead TSSOP (RU) | 180 | 35 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 14-Lead SOIC (R) | 120 | 56 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

## ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## TYPICAL PERFORMANCE CHARACTERISTICS



Figure 4. Small Signal Overshoot vs. Load Capacitance


Figure 5. Output Swing vs. Settling Time


Figure 6. Open-Loop Gain and Phase Shift vs. Frequency


Figure 7. Large Signal Transient Response, $V_{S}=5 \mathrm{~V}$


Figure 8. Large Signal Transient Response, $V_{s}=18 \mathrm{~V}$


Figure 9. Small Signal Transient Response


Figure 10. Output Voltage to Supply Rail vs. Load Current


Figure 11. Supply Current vs. Supply Voltage


Figure 12. Input Bias Current vs. Common-Mode Voltage, $V_{s}= \pm 2.5 \mathrm{~V}$


Figure 13. Input Bias Current vs. Common-Mode Voltage, $V_{s}= \pm 9 \mathrm{~V}$


Figure 14. Input Offset Voltage Distribution


Figure 15. Supply Current vs. Temperature


Figure 16. Maximum Output Swing vs. Frequency, $V_{S}=5 \mathrm{~V}$


Figure 17. Maximum Output Swing vs. Frequency, $V_{S}=18 \mathrm{~V}$


Figure 18. Closed-Loop Output Impedance vs. Frequency


Figure 19. Closed-Loop Gain vs. Frequency


Figure 20. Common-Mode Rejection vs. Frequency


Figure 21. Power Supply Rejection vs. Frequency

## AD8614/AD8644



Figure 22. Slew Rate vs. Supply Voltage


Figure 23. Voltage Noise Density vs. Frequency, $V_{s}=5 \mathrm{~V}$


Figure 24. Voltage Noise Density vs. Frequency, $V_{s}=18 \mathrm{~V}$

## THEORY OF OPERATION

The AD8614/AD8644 are processed using Analog Devices high voltage, extra fast complementary bipolar (HV XFCB) process. This process includes trench-isolated transistors that lower parasitic capacitance.
Figure 26 shows a simplified schematic of the AD8614/AD8644. The input stage is rail-to-rail, consisting of two complementary differential pairs, one NPN pair and one PNP pair. The input stage is protected against avalanche breakdown by two back-toback diodes. Each input has a $1.5 \mathrm{k} \Omega$ resistor that limits input current during overvoltage events and furnishes phase reversal protection if the inputs are exceeded. The two differential pairs are connected to a double-folded cascode. This is the stage in the amplifier with the most gain. The double-folded cascode differentially feeds the output stage circuitry. Two complementary common emitter transistors are used as the output stage. This allows the output to swing to within 125 mV from each rail with a 10 mA load. The gain of the output stage, and thus the open-loop gain of the op amp, depends on the load resistance.
The AD8614/AD8644 have no built-in short-circuit protection. The short-circuit limit is a function of high current roll-off of the output stage transistors and the voltage drop over the resistor shown on the schematic at the output stage. The voltage over this resistor is clamped to one diode during short-circuit voltage events.

## OUTPUT SHORT-CIRCUIT PROTECTION

To achieve a wide bandwidth and high slew rate, the output of the AD8614/AD8644 is not short-circuit protected. Shorting the output directly to ground or to a supply rail can destroy the device. The typical maximum safe output current is 70 mA .

In applications where some output current protection is needed, but not at the expense of reduced output voltage headroom, a low value resistor in series with the output can be used. This is shown in Figure 25. The resistor is connected within the feedback loop of the amplifier so that if Vout is shorted to ground and $\mathrm{V}_{\text {IN }}$ swings up to 18 V , the output current does not exceed 70 mA .

For 18 V single-supply applications, resistors less than $261 \Omega$ are not recommended.


Figure 25. Output Short-Circuit Protection


## AD8614/AD8644

## INPUT OVERVOLTAGE PROTECTION

As with any semiconductor device, whenever the condition exists for the input to exceed either supply voltage, attention needs to be paid to the input overvoltage characteristic. As an overvoltage occurs, the amplifier can be damaged, depending on the voltage level and the magnitude of the fault current. When the input voltage exceeds either supply by more than 0.6 V , internal pin junctions energize, allowing current to flow from the input to the supplies. Observing Figure 26, the AD8614/AD8644 have $1.5 \mathrm{k} \Omega$ resistors in series with each input, which helps to limit the current. This input current is not inherently damaging to the device as long as it is limited to 5 mA or less. If the voltage is large enough to cause more than 5 mA of current to flow, an external series resistor should be added. The size of this resistor is calculated by dividing the maximum overvoltage by 5 mA and subtracting the internal $1.5 \mathrm{k} \Omega$ resistor. For example, if the input voltage could reach 100 V , the external resistor should be $(100 \mathrm{~V} \div 5 \mathrm{~mA})-1.5 \mathrm{k} \Omega=18.5 \mathrm{k} \Omega$. This resistance should be placed in series with either or both inputs if they are subjected to the overvoltages.

## OUTPUT PHASE REVERSAL

The AD8614/AD8644 are immune to phase reversal as long as the input voltage is limited to within the supply rails. Although the device's output does not change phase, large currents due to input overvoltage can result, damaging the device. In applications where the possibility of an input voltage exceeding the supply voltage exists, overvoltage protection should be used, as described in the previous section.

## POWER DISSIPATION

The maximum power that can be safely dissipated by the AD8614/AD8644 is limited by the associated rise in junction temperature. The maximum safe junction temperature is $150^{\circ} \mathrm{C}$, and should not be exceeded or device performance could suffer. If this maximum is momentarily exceeded, proper circuit operation is restored as soon as the die temperature is reduced. Leaving the device in an overheated condition for an extended period can result in permanent damage to the device.

To calculate the internal junction temperature of the AD8614/AD8644, the following formula can be used:

$$
T_{J}=P_{D I S S} \times \theta_{I A}+T_{A}
$$

where:
$T_{J}$ is the AD8614/AD8644 junction temperature.
$P_{\text {DISS }}$ is the AD8614/AD8644 power dissipation.
$\theta_{\text {IA }}$ is the AD8614/AD8644 junction-to-ambient package thermal resistance.
$T_{A}$ is the ambient temperature of the circuit.
The power dissipated by the device can be calculated as:

$$
P_{D I S S}=I_{L O A D} \times\left(V_{S}-V_{O U T}\right)
$$

where:
$I_{\text {LOAD }}$ is the AD8614/AD8644 output load current. $V_{S}$ is the AD8614/AD8644 supply voltage.
$V_{\text {out }}$ is the AD8614/AD8644 output voltage.
Figure 27 provides a convenient way to determine if the device is being overheated. The maximum safe power dissipation can be found graphically, based on the package type and the ambient temperature around the package. By using the previous equation, it is a simple matter to see if $\mathrm{P}_{\text {Diss }}$ exceeds the device's power derating curve. To ensure proper operation, it is important to observe the recommended derating curves shown in Figure 27.


Figure 27. Maximum Power Dissipation vs. Temperature (5-Lead and 14-Lead Package Types)

## UNUSED AMPLIFIERS

It is recommended that any unused amplifiers in the quad package be configured as a unity-gain follower with a $1 \mathrm{k} \Omega$ feedback resistor connected from the inverting input to the output, and the noninverting input tied to the ground plane.

## CAPACITIVE LOAD DRIVE

The AD8614/AD8644 exhibit excellent capacitive load driving capabilities. Although the device is stable with large capacitive loads, there is a decrease in amplifier bandwidth as the capacitive load increases.

When driving heavy capacitive loads directly from the AD8614/AD8644 output, a snubber network can be used to improve the transient response. This network consists of a series R-C connected from the amplifier's output to ground, placing it in parallel with the capacitive load. The configuration is shown in Figure 28. Although this network does not increase the bandwidth of the amplifier, it does significantly reduce the amount of overshoot.


Figure 28. Snubber Network Compensation for Capacitive Loads
The optimum values for the snubber network should be determined empirically based on the size of the capacitive load. Table 4 shows a few sample snubber network values for a given load capacitance.

Table 4. Snubber Networks for Large Capacitive Loads

| Load Capacitance $\left(\mathbf{C}_{\mathrm{L}}\right)$ | Snubber Network $\left(\mathbf{R}_{\mathrm{x}}, \mathbf{C}_{\mathrm{x}}\right)$ |
| :--- | :--- |
| 0.47 nF | $300 \Omega, 0.1 \mu \mathrm{~F}$ |
| 4.7 nF | $30 \Omega, 1 \mu \mathrm{~F}$ |
| 47 nF | $5 \Omega, 10 \mu \mathrm{~F}$ |

## DIRECT ACCESS ARRANGEMENT

Figure 29 shows a schematic for a 5 V single-supply transmit/ receive telephone line interface for $600 \Omega$ transmission systems. It allows full duplex transmission of signals on a transformercoupled $600 \Omega$ line. Amplifier A1 provides gain that can be adjusted to meet the modem's output drive requirements. Both A1 and A2 are configured to apply the largest possible differential signal to the transformer. The largest signal available on a single 5 V supply is approximately 4.0 V p-p into a $600 \Omega$ transmission system. Amplifier A3 is configured as a difference amplifier to extract the receive information from the transmission line for amplification by A4. A3 also prevents the transmit signal from interfering with the receive signal. The gain of A4 can be adjusted in the same manner as A1 to meet the modem input signal requirements. Standard resistor values permit the use of single in-line package (SIP) format resistor arrays. Couple this with the AD8644 14-lead SOIC or TSSOP package and this circuit can offer a compact solution.


Figure 29. A Single-Supply Direct Access Arrangement for Modems

## A ONE-CHIP HEADPHONE/MICROPHONE PREAMPLIFIER SOLUTION

Because of its high output current performance, the AD8644 makes an excellent amplifier for driving an audio output jack in a computer application. Figure 30 shows how the AD8644 can be interfaced with an ac codec to drive headphones or speakers.


NOTES

1. ADDITIONAL PINS OMITTED FOR CLARITY.

Figure 30. A PC-99-Compliant Headphone/Line Out Amplifier

## AD8614/AD8644

If gain is required from the output amplifier, four additional resistors should be added as shown in Figure 31.


Figure 31. A PC-99-Compliant Headphone/Speaker Amplifier with Gain
The gain of the AD8644 can be set as

$$
A_{V}=\frac{R 6}{R 5}
$$

Input coupling capacitors are not required for either circuit as the reference voltage is supplied from the AD1881A.
The resistors R4 and R5 help protect the AD8644 output in case the output jack or headphone wires are accidentally shorted to ground. The output coupling capacitors C1 and C2 block dc
current from the headphones and create a high-pass filter with a corner frequency of

$$
f_{-3 \mathrm{~dB}}=\frac{1}{2 \pi C 1\left(R 4+R_{L}\right)}
$$

where $R_{L}$ is the resistance of the headphones.
The remaining two amplifiers can be used as low voltage microphone preamplifiers. A single AD8614 can be used as a standalone microphone preamplifier. Figure 32 shows this implementation.


Figure 32. Microphone Preamplifier

## OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARDS MO-178-AA
Figure 33. 5-Lead Small Outline Transistor Package [SOT-23] (RJ-5)
Dimensions shown in millimeters


Figure 34. 14-Lead Thin Shrink Small Outline Package [TSSOP] (RU-14)
Dimensions shown in millimeters


CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR
REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

Figure 35. 14-Lead Standard Small Outline Package [SOIC_N]
Narrow Body
(R-14)
Dimensions shown in millimeters and (inches)

## AD8614/AD8644

| Model | Temperature Range | Package Description | Package Option | Branding |
| :---: | :---: | :---: | :---: | :---: |
| AD8614ART-R2 | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | A6A |
| AD8614ART-REEL | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | A6A |
| AD8614ART-REEL7 | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | A6A |
| AD8614ARTZ-REEL ${ }^{1}$ | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | A0Z |
| AD8614ARTZ-REEL71 | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | A0Z |
| AD8644AR | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8644AR-REEL | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8644AR-REEL7 | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8644ARZ ${ }^{1}$ | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8644ARZ-REEL ${ }^{1}$ | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8644ARZ-REEL7 ${ }^{1}$ | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8644ARU | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |  |
| AD8644ARU-REEL | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |  |
| AD8644ARUZ ${ }^{1}$ | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |  |
| AD8644ARUZ-REEL ${ }^{1}$ | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |  |

${ }^{1} \mathrm{Z}=$ RoHS Compliant Part.

NOTES

## AD8614/AD8644

## NOTES

## X-ON Electronics

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9316401MXA 5962-9452101M2A EV1HMC1160LP5 EV1HMC305SLP4 EV1HMC306AMS10 EV1HMC557ALC4 EV1HMC6146BLC5A
EV1HMC6832ALP5L EV1HMC7912LP5 EV1HMC7992LP3D EV1HMC951BLP4 EV-AD5443/46/53SDZ EV-ADF70301-433AZ EV-
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HMC835LP6G EVAL01-HMC985LP4KE EVAL01-HMC987LP5E EVAL01-HMC988LP3E EVAL01-HMC995LP5GE EVAL02-
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