

## ACPL-P346/ACPL-W346

### 2.5-Amp Output Current Power, GaN and SiC MOSFET Gate Drive Optocoupler with Rail-to-Rail Output

#### Description

The Broadcom<sup>®</sup> ACPL-P346/W346 contains an AlGaAs LED, which is optically coupled to an integrated circuit with a power output stage. This optocoupler is ideally suited for driving power, GaN (Gallium Nitride) and SiC (Silicon Carbide) MOSFETs used in inverter or AC-DC/DC-DC converter applications. The high operating voltage range of the output stage provides the drive voltages required by gate controlled devices. The voltage and high peak output current supplied by this optocoupler make it ideally suited for direct driving MOSFETs at high frequency for high efficiency conversion. The ACPL-P346 and ACPL-W346 have the highest insulation voltage of  $V_{IORM} = 891 V_{peak}$  and  $V_{IORM} = 1140V_{peak}$  respectively in the IEC/EN/DIN EN 60747-5-5.

#### Features

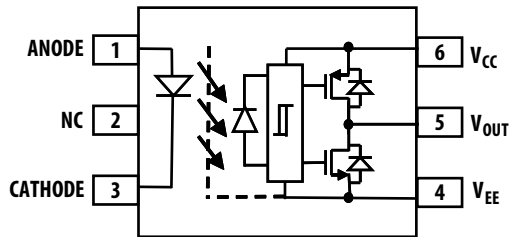
- 2.5A maximum peak output current
- 2.0A minimum peak output current
- Rail-to-rail output voltage
- 120 ns maximum propagation delay
- 50 ns maximum propagation delay difference
- LED current input with hysteresis
- 100 kV/ $\mu$ s minimum Common Mode Rejection (CMR) at  $V_{CM} = 1500V$
- $I_{CC} = 4.0$  mA maximum supply current
- Under Voltage Lock-Out protection (UVLO) with hysteresis
- Wide operating  $V_{CC}$  Range: 10V to 20V
- Industrial temperature range:  $-40^{\circ}C$  to  $+105^{\circ}C$
- Safety Approval
  - UL Recognized 3750V/5000  $V_{RMS}$  for 1 min.
  - CSA
  - IEC/EN/DIN EN 60747-5-5  $V_{IORM} = 891V/1140 V_{peak}$

#### Applications

- Power, GaN, and SiC MOSFET gate drive
- AC and brushless DC motor drives
- Switching power supplies

**CAUTION!** It is advised that normal static precautions be taken in handling and assembly of this component to prevent damage and/or degradation which may be induced by ESD. The components featured in this data sheet are not to be used in military or aerospace applications or environments.

## Functional Diagram



**NOTE:** A 1- $\mu$ F bypass capacity must be connected between pins  $V_{CC}$  and  $V_{EE}$ .

## Truth Table

LED	$V_{CC} - V_{EE}$ POSITIVE GOING (TURN-ON)	$V_{CC} - V_{EE}$ NEGATIVE GOING (TURN-OFF)	$V_O$
OFF	0V to 20V	0V to 20V	LOW
ON	0V to 8.1V	0V to 7.1V	LOW
ON	8.1V to 9.1V	7.1V to 8.1V	TRANSITION
ON	9.1V to 20V	8.1V to 20V	HIGH

## Ordering information

ACPL-P346 is UL Recognized with 3750  $V_{RMS}$  for 1 minute per UL1577.

ACPL-W346 is UL Recognized with 5000  $V_{RMS}$  for 1 minute per UL1577.

Part Number	Option	Package	Surface Mount	Tape and Reel	IEC/EN/DIN EN 60747-5-5	Quantity
	RoHS Compliant					
ACPL-P346	-000E	Stretched SO-6	X			100 per tube
ACPL-W346	-500E		X	X		1000 per reel
	-060E		X		X	100 per tube
	-560E		X	X	X	1000 per reel

To order, choose a part number from the part number column and combine with the desired option from the option column to form an order entry.

Example 1:

ACPL-P346-560E to order product of Stretched SO-6 Surface Mount package in Tape and Reel packaging with IEC/EN/DIN EN 60747-5-5 Safety Approval in RoHS compliant.

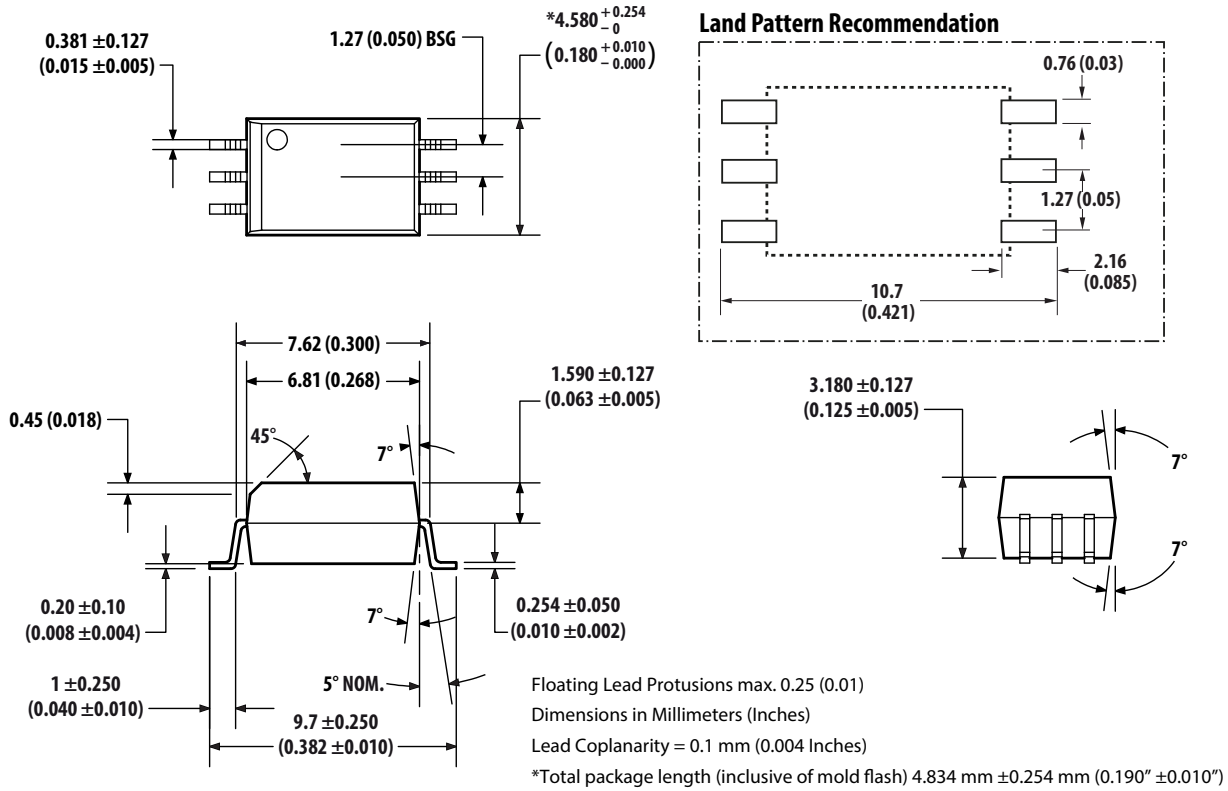
Example 2:

ACPL-W346-000E to order product of Stretched SO-6 Surface Mount package in Tube packaging and RoHS compliant.

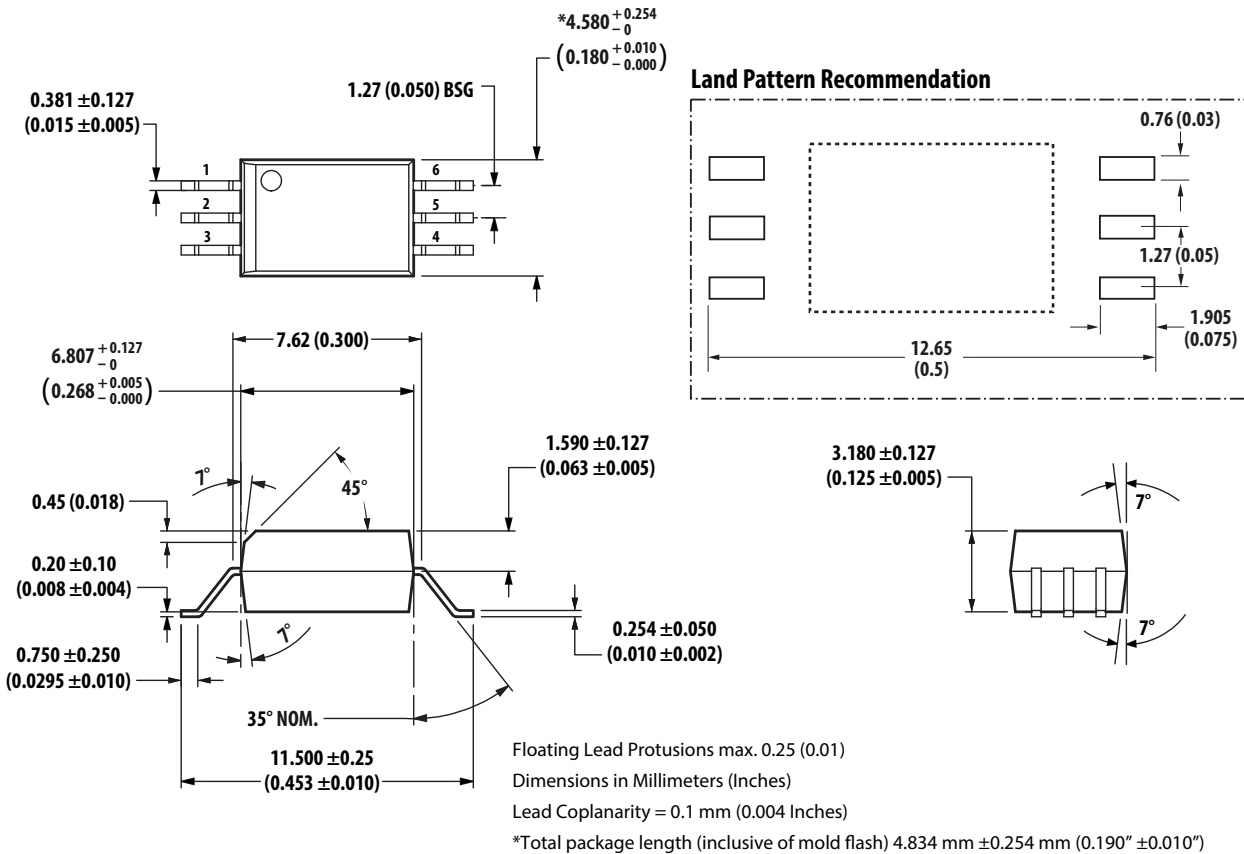
Option data sheets are available. Contact your Broadcom sales representative or authorized distributor for information.

# Package Outline Drawing

## ACPL-P346 Stretched SO-6 Package (7-mm Clearance)



## ACPL-W346 Stretched SO-6 Package (8-mm Clearance)



## Recommended Pb-Free IR Profile

Recommended reflow condition as per JEDEC Standard, J-STD-020 (latest revision). Non-Halide Flux should be used.

## Regulatory Information

The ACPL-P346/W346 is approved by the following organizations.

<b>UL</b>	Recognized under UL 1577, component recognition program up to $V_{ISO} = 3750 V_{RMS}$ (ACPL-P346) and $V_{ISO} = 5000 V_{RMS}$ (ACPL-W346).
<b>CSA</b>	CSA Component Acceptance Notice #5, File CA 88324
<b>IEC/EN/DIN EN 60747-5-5 (Option 060 Only)</b>	Maximum Working Insulation Voltage $V_{IORM} = 891 V_{peak}$ (ACPL-P346) and $V_{IORM} = 1140 V_{peak}$ (ACPL-W346)

**IEC/EN/DIN EN 60747-5-5 Insulation Characteristics (Option 060)<sup>a</sup>**

Description	Symbol	ACPL-P346 Option 060	ACPL-W346 Option 060	Units
Installation classification per DIN VDE 0110/39, Table 1 for rated mains voltage $\leq 150 V_{RMS}$ for rated mains voltage $\leq 300 V_{RMS}$ for rated mains voltage $\leq 450 V_{RMS}$ for rated mains voltage $\leq 600 V_{RMS}$ for rated mains voltage $\leq 1000 V_{RMS}$		I-IV I-IV I-III I-III	I-IV I-IV I-IV I-IV I-III	
Climatic Classification		40/105/21	40/105/21	
Pollution Degree (DIN VDE 0110/39)		2	2	
Maximum Working Insulation Voltage	$V_{IORM}$	891	1,140	$V_{peak}$
Input to Output Test Voltage, Method b <sup>a</sup> $V_{IORM} \times 1.875 = V_{PR}$ , 100% Production Test with $t_m = 1$ second, Partial discharge $< 5$ pC	$V_{PR}$	1,671	2,137	$V_{peak}$
Input to Output Test Voltage, Method a <sup>a</sup> $V_{IORM} \times 1.6 = V_{PR}$ , Type and Sample Test, $t_m = 10$ seconds, Partial discharge $< 5$ pC	$V_{PR}$	1,426	1,824	$V_{peak}$
Highest Allowable Overvoltage <sup>a</sup> (Transient Overvoltage $t_{ni} = 60$ seconds)	$V_{IOTM}$	6,000	8,000	$V_{peak}$
Safety-limiting values – maximum values allowed in the event of a failure				
Case Temperature	$T_S$	175	175	$^{\circ}C$
Input Current	$I_{S, INPUT}$	230	230	mA
Output Power	$P_{S, OUTPUT}$	600	600	mW
Insulation Resistance at $T_S, V_{IO} = 500V$	$R_S$	$>10^9$	$>10^9$	$\Omega$

a. Refer to IEC/EN/DIN EN 60747-5-5 Optoisolator Safety Standard section of the *Broadcom Regulatory Guide to Isolation Circuits*, AV02-2041EN, for a detailed description of Method a and Method b partial discharge test profiles.

**NOTE:** These optocouplers are suitable for “safe electrical isolation” only within the safety limit data. Maintenance of the safety data shall be ensured by means of protective circuits. Surface mount classification is Class A in accordance with CECC 00802.

## Insulation and Safety-Related Specifications

Parameter	Symbol	ACPL-P346	ACPL-W346	Unit	Conditions
Minimum External Air Gap (Clearance)	L(101)	7.0	8.0	mm	Measured from input terminals to output terminals, shortest distance through air.
Minimum External Tracking (Creepage)	L(102)	8.0	8.0	mm	Measured from input terminals to output terminals, shortest distance path along body.
Minimum Internal Plastic Gap (Internal Clearance)		0.08	0.08	mm	Through insulation distance conductor to conductor, usually the straight line distance thickness between the emitter and detector.
Tracking Resistance (Comparative Tracking Index)	CTI	>175	>175	V	DIN EN 60112 (2010-05)
Isolation Group		IIIa	IIIa		Material Group (DIN VDE 0110, 1/89, Table 1)

**NOTE:** All Broadcom data sheets report the creepage and clearance inherent to the optocoupler component itself. These dimensions are needed as a starting point for the equipment designer when determining the circuit insulation requirements. However, once mounted on a printed circuit board, minimum creepage and clearance requirements must be met as specified for individual equipment standards. For creepage, the shortest distance path along the surface of a printed circuit board between the solder fillets of the input and output leads must be considered (the recommended land pattern does not necessarily meet the minimum creepage of the device). There are recommended techniques, such as grooves and ribs, that may be used on a printed circuit board to achieve desired creepage and clearances. Creepage and clearance distances will also change depending on factors, such as pollution degree and insulation level.

## Absolute Maximum Ratings

Parameter	Symbol	Min.	Max.	Unit	Notes
Storage Temperature	$T_S$	-55	+125	°C	
Operating Temperature	$T_A$	-40	+105	°C	
Output IC Junction Temperature	$T_J$	—	125	°C	
Average Input Current	$I_{F(AVG)}$	—	25	mA	a
Peak Transient Input Current (<1 second pulse width, 300 pps)	$I_{F(TRAN)}$	—	1	A	
Reverse Input Voltage	$V_R$	—	5	V	
“High” Peak Output Current	$I_{OH(PEAK)}$	—	2.5	A	b
“Low” Peak Output Current	$I_{OL(PEAK)}$	—	2.5	A	b
Total Output Supply Voltage	$(V_{CC} - V_{EE})$	0	25	V	
Output Voltage	$V_{O(PEAK)}$	-0.5	$V_{CC}$	V	
Output IC Power Dissipation	$P_O$	—	500	mW	c
Total Power Dissipation	$P_T$	—	550	mW	d

- Derate linearly above 85°C free-air temperature at a rate of 0.3 mA/°C.
- Maximum pulse width = 10  $\mu$ s. This value is intended to allow for component tolerances for designs with  $I_O$  peak minimum = 2.0A. See applications section for additional details on limiting  $I_{OH}$  peak.
- Derate linearly above 85°C free-air temperature at a rate of 12.5 mW/°C.
- Derate linearly above 85°C free-air temperature at a rate of 13.75 mW/°C. The maximum LED junction temperature should not exceed 125°C.

## Recommended Operating Conditions

Parameter	Symbol	Min.	Max.	Units	Notes
Operating Temperature	$T_A$	-40	+105	°C	
Output Supply Voltage	$(V_{CC} - V_{EE})$	10	20	V	
Input Current (ON)	$I_{F(ON)}$	7	11	mA	
Input Voltage (OFF)	$V_{F(OFF)}$	-3.6	+0.8	V	

## Electrical Specifications (DC)

All typical values are at  $T_A = 25^\circ\text{C}$ ,  $V_{CC} - V_{EE} = 10\text{V}$ ,  $V_{EE} = \text{Ground}$ . All minimum and maximum specifications are at recommended operating conditions ( $T_A = -40^\circ\text{C}$  to  $+105^\circ\text{C}$ ,  $I_{F(ON)} = 7\text{ mA}$  to  $+11\text{ mA}$ ,  $V_{F(OFF)} = -3.6\text{V}$  to  $+0.8\text{V}$ ,  $V_{EE} = \text{Ground}$ ,  $V_{CC} = 10\text{V}$  to  $20\text{V}$ ), unless otherwise noted.

Parameter	Symbol	Min.	Typ.	Max.	Units	Test Conditions	Figure	Notes
High Level Peak Output Current	$I_{OH}$	-2.0	-3.4	—	A	$V_{CC} - V_O = 10\text{V}$	3, 4	a
Low Level Peak Output Current	$I_{OL}$	2.0	4.4	—	A	$V_O - V_{EE} = 10\text{V}$	6, 7	a
High Output Transistor RDS(ON)	$R_{DS,OH}$	0.3	1.7	3.5	$\Omega$	$I_{OH} = -2.0\text{A}$	8	b
Low Output Transistor RDS(ON)	$R_{DS,OL}$	0.3	0.7	2.0	$\Omega$	$I_{OL} = 2.0\text{A}$	9	b
High Level Output Voltage	$V_{OH}$	$V_{CC} - 0.3$	$V_{CC} - 0.2$	—	V	$I_O = -100\text{ mA}$ , $I_F = 9\text{ mA}$	2, 4	c, d
High Level Output Voltage	$V_{OH}$	—	$V_{CC}$	—	V	$I_O = 0\text{ mA}$ , $I_F = 9\text{ mA}$	1	
Low Level Output Voltage	$V_{OL}$	—	0.1	0.25	V	$I_O = 100\text{ mA}$	5, 7	
High Level Supply Current	$I_{CCH}$	—	2.6	4.0	mA	$I_F = 9\text{ mA}$	10, 11	
Low Level Supply Current	$I_{CCL}$	—	2.6	4.0	mA	$V_F = 0\text{V}$		
Threshold Input Current Low to High	$I_{FLH}$	0.5	1.5	4.0	mA	$V_O > 5\text{V}$	12, 13	
Threshold Input Voltage High to Low	$V_{FHL}$	0.8	—	—	V			
Input Forward Voltage	$V_F$	1.2	1.55	1.95	V	$I_F = 9\text{ mA}$	19	
Temperature Coefficient of Input Forward Voltage	$\Delta V_F / \Delta T_A$	—	-1.7	—	mV/°C			
Input Reverse Breakdown Voltage	$BV_R$	5	—	—	V	$I_R = 100\text{ A}$		
Input Capacitance	$C_{IN}$	—	70	—	pF	$f = 1\text{ MHz}$ , $V_F = 0\text{V}$		
UVLO Threshold	$V_{UVLO+}$	8.1	8.6	9.1	V	$V_O > 5\text{V}$ , $I_F = 9\text{ mA}$		
	$V_{UVLO-}$	7.1	7.6	8.1	V			
UVLO Hysteresis	$UVLO_{HYS}$	0.5	1.0	—	V			

- Maximum pulse width = 10  $\mu\text{s}$ .
- Output is sourced at  $-2.0\text{A}/+2.0\text{A}$  with a maximum pulse width = 10  $\mu\text{s}$ .
- In this test,  $V_{OH}$  is measured with a DC load current. When driving capacitive loads,  $V_{OH}$  will approach  $V_{CC}$  as  $I_{OH}$  approaches zero amps.
- Maximum pulse width = 1 ms.

## Switching Specifications (AC)

All typical values are at  $T_A = 25^\circ\text{C}$ ,  $V_{CC} - V_{EE} = 10\text{V}$ ,  $V_{EE} = \text{Ground}$ . All minimum and maximum specifications are at recommended operating conditions ( $T_A = -40^\circ\text{C}$  to  $+105^\circ\text{C}$ ,  $I_{F(\text{ON})} = 7\text{ mA}$  to  $11\text{ mA}$ ,  $V_{F(\text{OFF})} = -3.6\text{V}$  to  $+0.8\text{V}$ ,  $V_{EE} = \text{Ground}$ ), unless otherwise noted.

Parameter	Symbol	Min.	Typ.	Max.	Units	Test Conditions	Figure	Notes
Propagation Delay Time to High Output Level	$t_{\text{PLH}}$	30	55	120	ns	$R_g = 10\Omega$ , $C_g = 10\text{ nF}$ , $f = 200\text{ kHz}$ , Duty Cycle = 50%, $V_{CC} = 10\text{V}$	14, 15, 16, 17	
Propagation Delay Time to Low Output Level	$t_{\text{PHL}}$	30	55	120	ns			
Pulse Width Distortion	PWD		0	50	ns			a
Propagation Delay Difference Between Any Two Parts	PDD ( $t_{\text{PHL}} - t_{\text{PLH}}$ )	-50	—	+50	ns			24, 25
Propagation Delay Skew	$t_{\text{PSK}}$	—	—	40	ns			c
Rise Time	$t_{\text{R}}$	—	8	30	ns	$C_g = 1\text{ nF}$ , $f = 200\text{ kHz}$ , Duty Cycle = 50%, $V_{CC} = 10\text{V}$	18, 20	
Fall Time	$t_{\text{F}}$	—	8	30	ns			
Output High Level Common Mode Transient Immunity	$ CM_H $	100	—	—	kV/ $\mu\text{s}$	$T_A = 25^\circ\text{C}$ , $I_F = 9\text{ mA}$ , $V_{CC} = 20\text{V}$ , $V_{CM} = 1500\text{V}$ with split resistors	21	d, e
Output Low Level Common Mode Transient Immunity	$ CM_L $	100	—	—	kV/ $\mu\text{s}$			$T_A = 25^\circ\text{C}$ , $V_F = 0\text{V}$ , $V_{CC} = 20\text{V}$ , $V_{CM} = 1500\text{V}$ with split resistors

- Pulse Width Distortion (PWD) is defined as  $|t_{\text{PHL}} - t_{\text{PLH}}|$  for any given device.
- The difference between  $t_{\text{PHL}}$  and  $t_{\text{PLH}}$  between any two ACPL-P346 parts under the same test condition.
- $t_{\text{PSK}}$  is equal to the worst case difference in  $t_{\text{PHL}}$  and/or  $t_{\text{PLH}}$  that will be seen between units at any given temperature and specified test conditions.
- Pin 2 must be connected to LED common. Split resistor network in the ratio 1.5:1 with  $232\Omega$  at the anode and  $154\Omega$  at the cathode.
- Common mode transient immunity in the high state is the maximum tolerable  $dV_{CM}/dt$  of the common mode pulse,  $V_{CM}$ , to assure that the output will remain in the high state (meaning  $V_O > 10.0\text{V}$ ).
- Common mode transient immunity in a low state is the maximum tolerable  $dV_{CM}/dt$  of the common mode pulse,  $V_{CM}$ , to assure that the output will remain in a low state (meaning  $V_O < 1.0\text{V}$ ).



## Package Characteristics

All typical values are at  $T_A = 25^\circ\text{C}$ . All minimum/maximum specifications are at recommended operating conditions, unless otherwise noted.

Parameter	Symbol	Device	Min.	Typ.	Max.	Units	Test Conditions	Fig.	Note
Input-Output Momentary Withstand Voltage <sup>a</sup>	$V_{ISO}$	ACPL-P346	3750	—	—	$V_{RMS}$	RH < 50%, t = 1 min., $T_A = 25^\circ\text{C}$		b, c
		ACPL-W346	5000	—	—	$V_{RMS}$	RH < 50%, t = 1 min., $T_A = 25^\circ\text{C}$		c, d
Input-Output Resistance	$R_{I-O}$		—	$>50^{12}$	—	$\Omega$	$V_{I-O} = 500 V_{DC}$		c
Input-Output Capacitance	$C_{I-O}$		—	0.6	—	pF	f = 1 MHz		
LED-to-Ambient Thermal Resistance	$R_{11}$		—	135	—	$^\circ\text{C/W}$			e
LED-to-Detector Thermal Resistance	$R_{12}$		—	27	—				
Detector-to-LED Thermal Resistance	$R_{21}$		—	39	—				
Detector-to-Ambient Thermal Resistance	$R_{22}$		—	47	—				

- The Input-Output Momentary Withstand Voltage is a dielectric voltage rating that should not be interpreted as an input-output continuous voltage rating. For the continuous voltage rating, refer to your equipment level safety specification or Broadcom Application Note 1074, *Optocoupler Input-Output Endurance Voltage*.
- In accordance with UL1577, each optocoupler is proof tested by applying an insulation test voltage  $\geq 4500 V_{RMS}$  for 1 second (leakage detection current limit,  $I_{I-O} \leq 5 \mu\text{A}$ ).
- Device considered a two-terminal device: pins 1, 2, and 3 shorted together and pins 4, 5, and 6 shorted together.
- In accordance with UL1577, each optocoupler is proof tested by applying an insulation test voltage  $\geq 6000 V_{RMS}$  for 1 second (leakage detection current limit,  $I_{I-O} \leq 5 \mu\text{A}$ ).
- The device was mounted on a high conductivity test board as per JEDEC 51-7.

# Typical Performance Plots

Figure 1: High Output Rail Voltage vs. Temperature

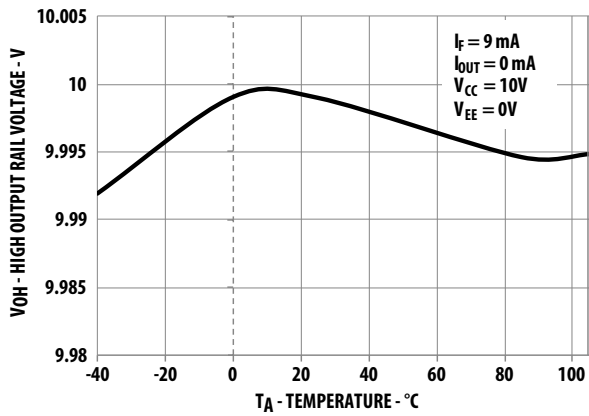


Figure 2:  $V_{OH}$  vs. Temperature

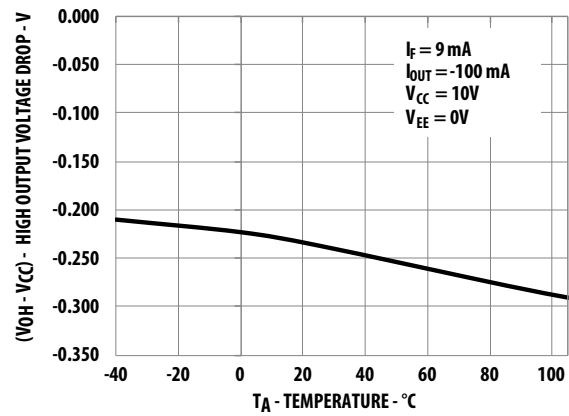


Figure 3:  $I_{OH}$  vs. Temperature

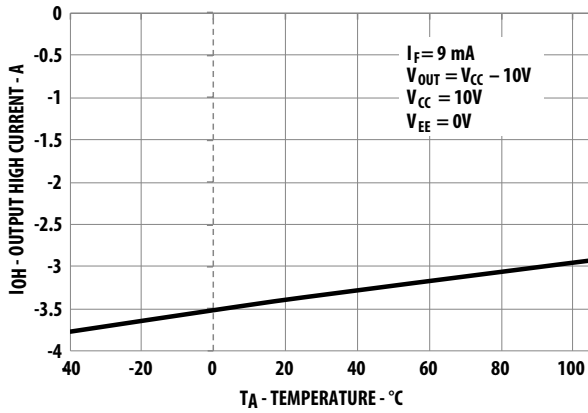


Figure 4:  $I_{OH}$  vs.  $V_{OH}$

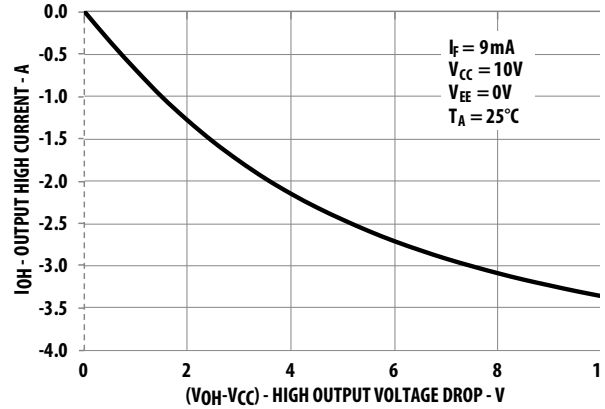


Figure 5:  $V_{OL}$  vs. Temperature

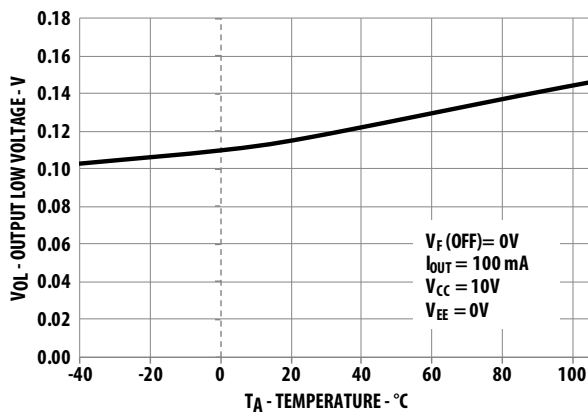


Figure 6:  $I_{OL}$  vs. Temperature

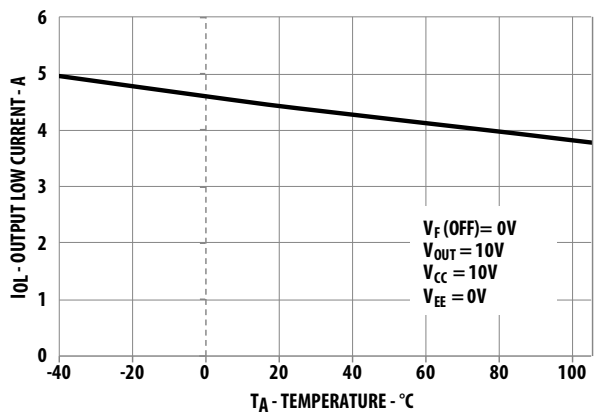


Figure 7:  $I_{OL}$  vs.  $V_{OL}$

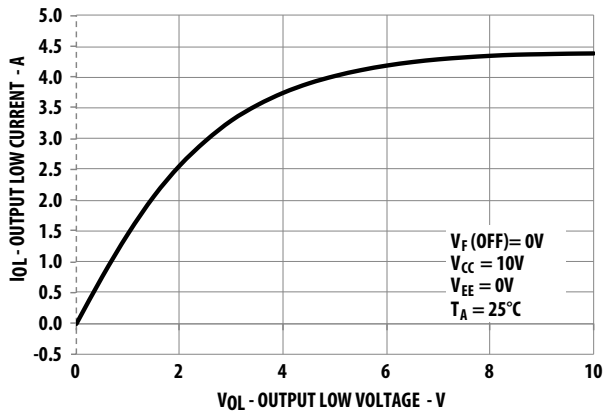


Figure 8:  $R_{DS,OH}$  vs. Temperature

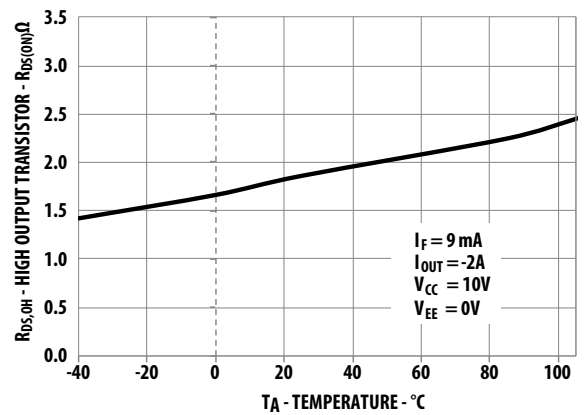


Figure 9:  $R_{DS,OL}$  vs. Temperature

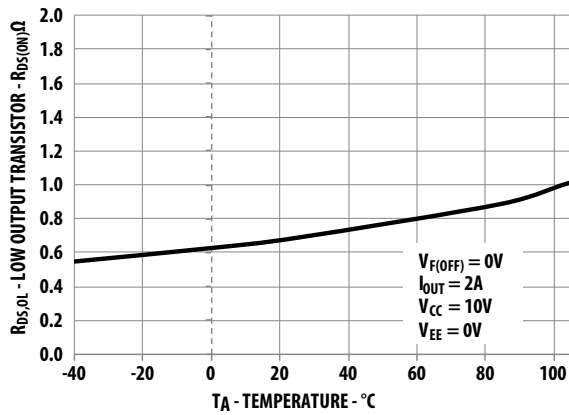


Figure 10:  $I_{CC}$  vs. Temperature

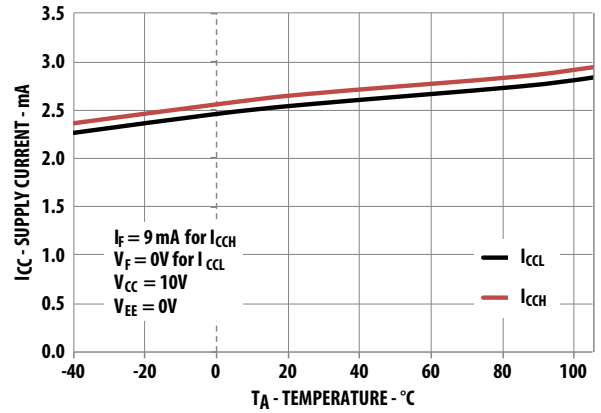


Figure 11:  $I_{CC}$  vs.  $V_{CC}$

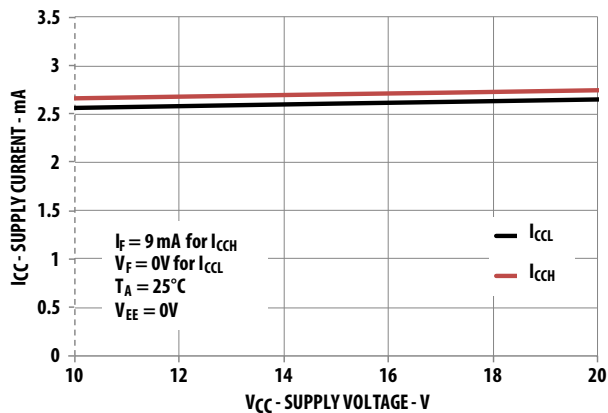


Figure 12:  $I_{FLH}$  Hysteresis

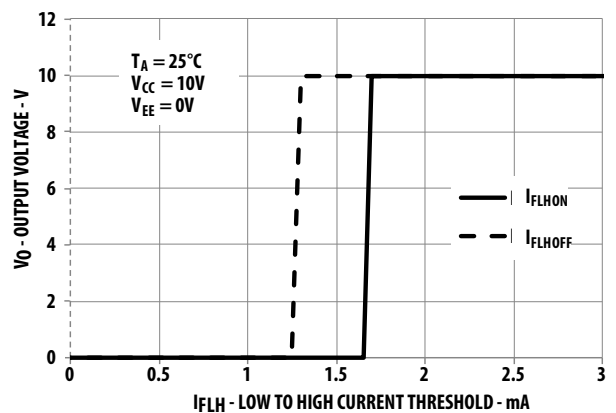


Figure 13:  $I_{FLH}$  vs. Temperature

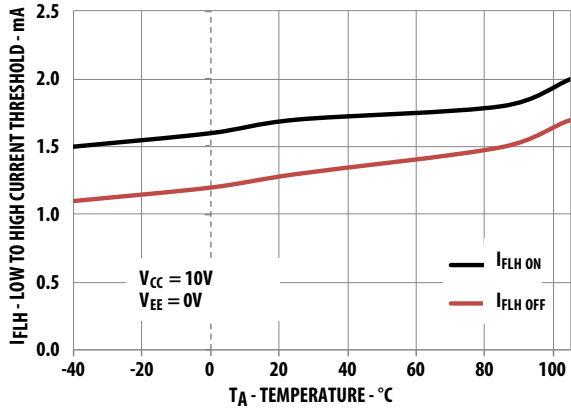


Figure 14: Propagation Delay vs.  $I_F$

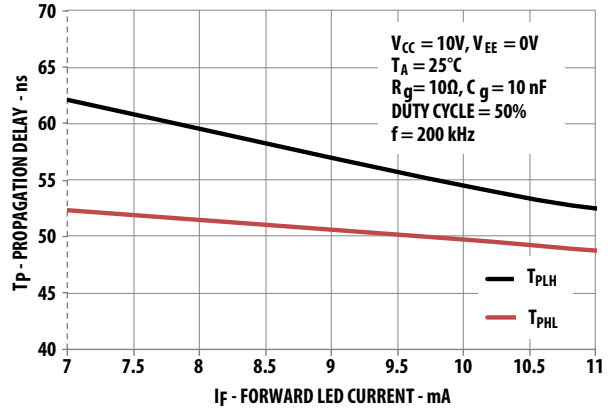


Figure 15: Propagation Delay vs. Temperature

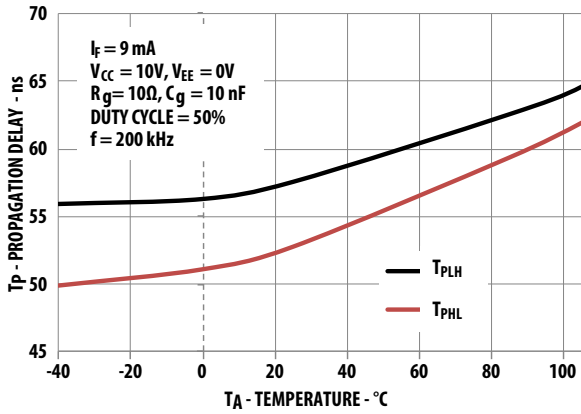


Figure 16: Propagation Delay vs.  $R_g$

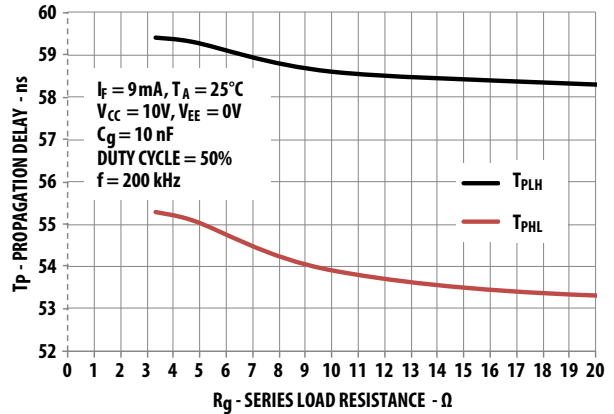


Figure 17: Propagation Delay vs.  $C_g$

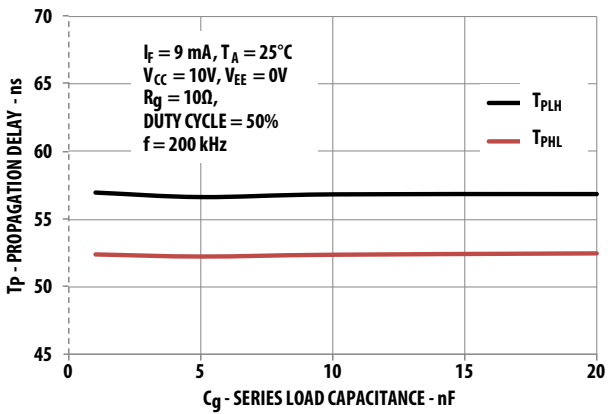


Figure 18: Rise and Fall Times vs.  $C_g$

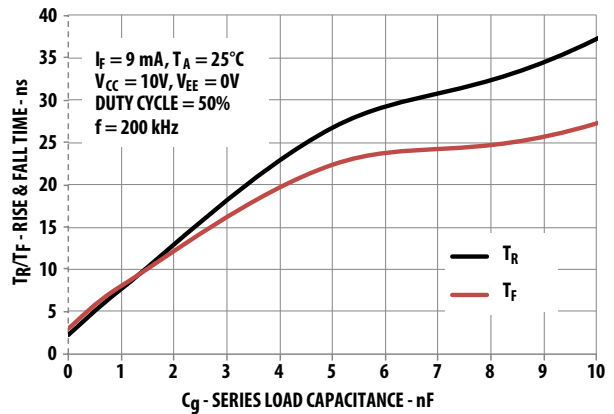


Figure 19: Input Current vs. Forward Voltage

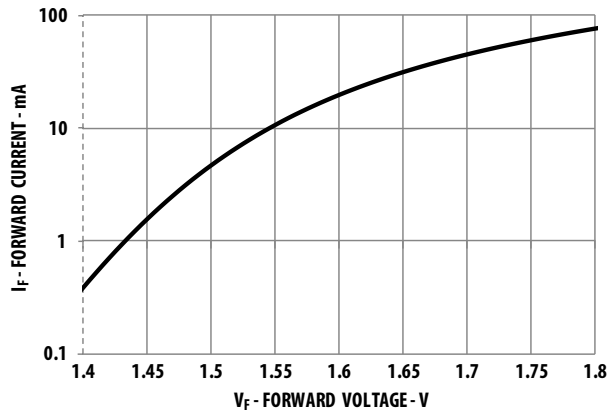


Figure 20:  $t_r$  and  $t_f$  Test Circuit and Waveforms

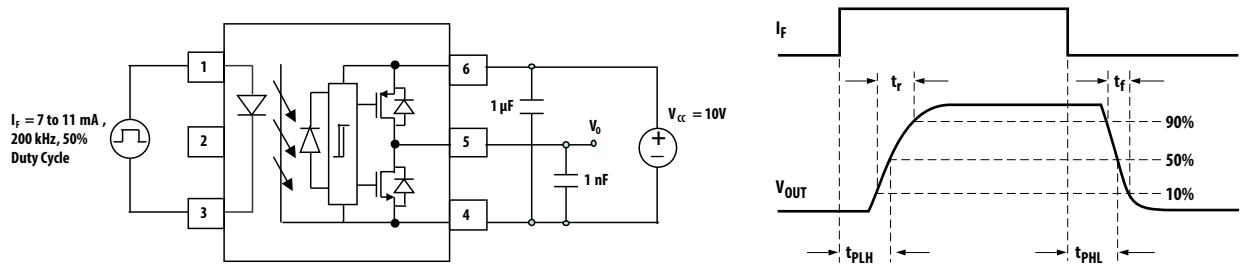
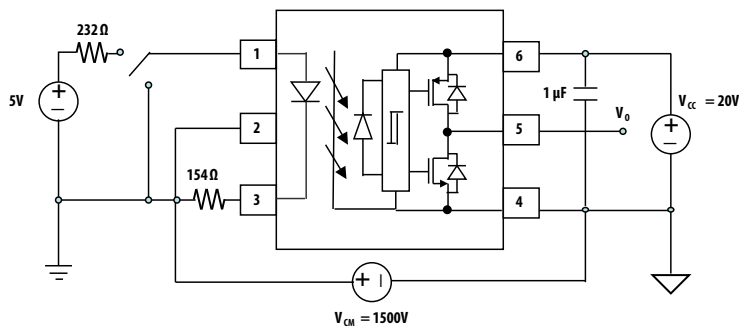


Figure 21: CMR Test Circuit with Split Resistors Network



## Application Information

### Product Overview Description

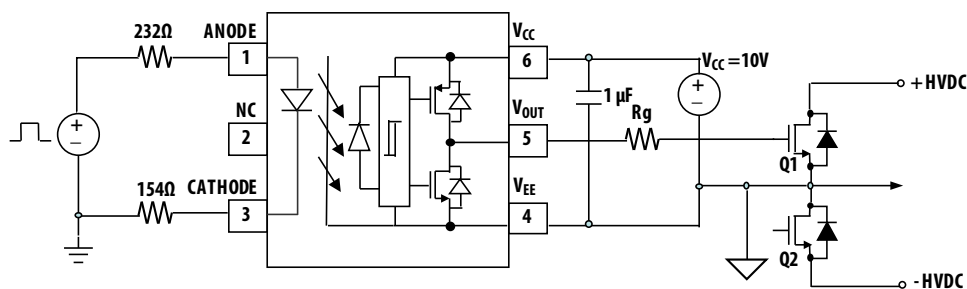
The ACPL-P346/W346 is an optically isolated power output stage capable of driving power, GaN or SiC MOSFET. Based on BCDMOS technology, this gate drive optocoupler delivers higher peak output current, better rail-to-rail output voltage performance and two times faster speed than the previous generation products.

The high peak output current and short propagation delay are needed for fast MOSFET switching to reduce dead time and improve system overall efficiency. Rail-to-rail output voltage ensures that the MOSFET's gate voltage is driven to the optimum intended level with no power loss across the MOSFET. This helps the designer lower the system power which is suitable for bootstrap power supply operation.

It has very high CMR (common mode rejection) rating which allows the microcontroller and the MOSFET to operate at very large common mode noise found in industrial motor drives and other power switching applications. The input is driven by direct LED current and has a hysteresis that prevents output oscillation if insufficient LED driving current is applied. This will eliminate the need of additional Schmitt trigger circuit at the input LED.

The stretched SO6 package, which is up to 50% smaller than a conventional DIP package, facilitates a smaller and more compact design. These stretched packages are compliant to many industrial safety standards, such as IEC/EN/DIN EN 60747-5-5, UL 1577 and CSA.

**Figure 22: Recommended Application Circuit with Split Resistors LED**



## Recommended Application Circuit

The recommended application circuit shown in [Figure 22](#) illustrates a typical gate drive implementation using the ACPL-P346.

The supply bypass capacitors (1  $\mu\text{F}$ ) provide the large transient currents necessary during a switching transition. Because of the transient nature of the charging currents, a low current (4.0 mA) power supply will be enough to power the device. The split resistors (in the ratio of 1.5:1) across the LED will provide a high CMR response by providing a balanced resistance network across the LED.

The gate resistor  $R_G$  serves to limit gate charge current and controls the MOSFET switching times.

In PC board design, care should be taken to avoid routing the MOSFET drain or source traces close to the ACPL-P346 input as this can result in unwanted coupling of transient signals into ACPL-P346 and degrade performance.

## Selecting the Gate Resistor (R<sub>g</sub>)

**Step 1:** Calculate R<sub>g</sub> minimum from the I<sub>OL</sub> peak specification. The MOSFET and R<sub>g</sub> in Figure 22 can be analyzed as a simple RC circuit with a voltage supplied by ACPL-P346/W346.

$$\begin{aligned} R_g &\geq ((V_{CC} - V_{EE}) / I_{OLPEAK}) - R_{DS(ON)(MIN)} \\ &= ((10 - 0V) / 25A) - 0.3\Omega \\ &= 3.7\Omega \end{aligned}$$

The external gate resistor, R<sub>g</sub> and internal minimum turn-on resistance, R<sub>DS(ON)</sub> will ensure the output current will not exceed the device absolute maximum rating of 2.5A.

**Step 2:** Check the ACPL-P346/W346 power dissipation and increase R<sub>g</sub> if necessary. The ACPL-P346/W346 total power dissipation (P<sub>T</sub>) is equal to the sum of the emitter power (P<sub>E</sub>) and the output power (P<sub>O</sub>).

$$\begin{aligned} P_T &= P_E + P_O \\ P_E &= I_F \times V_F \times \text{Duty Cycle} \\ P_O &= P_{O(BIAS)} + P_{O(SWITCHING)} \\ &= I_{CC} \times (V_{CC} - V_{EE}) + P_{HS} + P_{LS} \\ P_{HS} &= (V_{CC} \times Q_G \times f) \times R_{DS,OH(MAX)} / (R_{DS,OH(MAX)} + R_g) / 2 \\ P_{LS} &= (V_{CC} \times Q_G \times f) \times R_{DS,OL(MAX)} / (R_{DS,OL(MAX)} + R_g) / 2 \end{aligned}$$

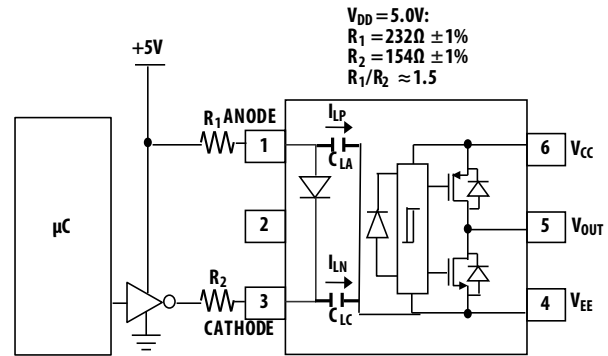
Using I<sub>F</sub> (worst case) = 11 mA, R<sub>g</sub> = 3.7Ω, Max Duty Cycle = 80%, Q<sub>G</sub> = 100 nC (650V 20A MOSFET), f = 200 kHz, and T<sub>A</sub> max. = 85°C:

$$\begin{aligned} P_E &= 11 \text{ mA} \times 1.95V \times 0.8 = 17 \text{ mW} \\ P_{HS} &= (10V \times 100 \text{ nC} \times 200 \text{ kHz}) \times 3.5 / (3.5 + 3.7) / 2 \\ &= 48.6 \text{ mW} \\ P_{LS} &= (10V \times 100 \text{ nC} \times 200 \text{ kHz}) \times 2.0 / (2.0 + 3.7) / 2 \\ &= 35.1 \text{ mW} \\ P_O &= 4 \text{ mA} \times 10V + 48.6 \text{ mW} + 35.1 \text{ mW} \\ &= 123.7 \text{ mW} < 500 \text{ mW } (P_{O(MAX)} \text{ at } 85^\circ\text{C}) \end{aligned}$$

The value of 4 mA for I<sub>CC</sub> in the previous equation is the maximum I<sub>CC</sub> over the entire operating temperature range.

Since P<sub>O</sub> is less than P<sub>O(MAX)</sub>, R<sub>g</sub> = 3.7Ω is alright for the power dissipation.

Figure 23: Recommended High-CMR Drive Circuit



## LED Drive Circuit Considerations for High CMR Performance

Figure 23 shows the recommended drive circuit for the ACPL-P346/W346 that gives optimum common-mode rejection. The two current setting resistors balance the common mode impedances at the LED's anode and cathode. Common-mode transients can be capacitive coupled from the LED anode, through C<sub>LA</sub> (or cathode through C<sub>LC</sub>) to the output-side ground causing current to be shunted away from the LED (which is not wanted when the LED should be on) or conversely cause current to be injected into the LED (which is not wanted when the LED should be off).

Table 1 shows the directions of I<sub>LP</sub> and I<sub>LN</sub> depend on the polarity of the common-mode transient. For transients occurring when the LED is on, common-mode rejection (CM<sub>H</sub>, since the output is at "high" state) depends on LED current (I<sub>F</sub>). For conditions where I<sub>F</sub> is close to the switching threshold (I<sub>FLH</sub>), CM<sub>H</sub> also depends on the extent to which I<sub>LP</sub> and I<sub>LN</sub> balance each other. In other words, any condition where a common-mode transient causes a momentary decrease in I<sub>F</sub> (meaning when dV<sub>CM</sub>/dt > 0 and |I<sub>LP</sub>| > |I<sub>LN</sub>|, referring to Table 1) will cause a common-mode failure for transients which are fast enough.

Likewise for a common-mode transient that occurs when the LED is off (that is, CM<sub>L</sub>, since the output is at "low" state), if an imbalance between I<sub>LP</sub> and I<sub>LN</sub> results in a transient I<sub>F</sub> equal to or greater than the switching threshold of the optocoupler, the transient "signal" may cause the output to spike above 1V, which constitutes a CM<sub>L</sub> failure. The balanced I<sub>LED</sub>-setting resistors help equalize the common mode voltage change at the anode and cathode. The shunt drive input circuit will also help to achieve high CML performance by shunting the LED in the off state.

**Table 1: Common Mode Pulse Polarity and LED Current Transients**

dVCM/dt	$I_{LP}$ Direction	$I_{LP}$ Direction	If $ I_{LP}  <  I_{LN} $ , $I_F$ Is Momentarily	If $ I_{LP}  >  I_{LN} $ , $I_F$ Is Momentarily
Positive (>0)	Away from LED anode through $C_{LA}$	Away from LED cathode through $C_{LC}$	Increase	Decrease
Negative(<0)	Toward LED anode through $C_{LA}$	Toward LED cathode through $C_{LC}$	Decrease	Increase

## Dead Time and Propagation Delay Specifications

The ACPL-P346/W346 includes a Propagation Delay Difference (PDD) specification intended to help designers minimize “dead time” in their power inverter designs. Dead time is the time period during which both the high and low side power transistors (Q1 and Q2 in Figure 22) are off. Any overlap in Q1 and Q2 conduction will result in large currents flowing through the power devices between the high and low voltage motor rails.

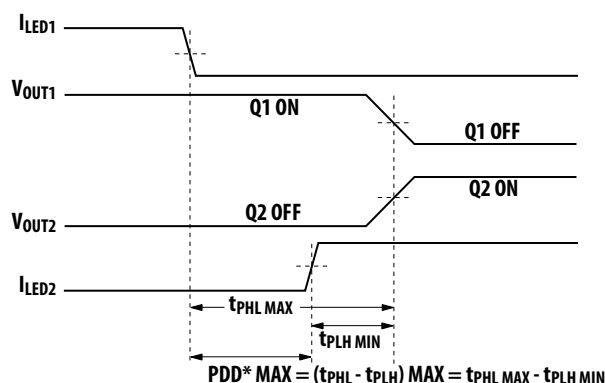
To minimize dead time in a given design, the turn on of LED2 should be delayed (relative to the turn off of LED1) so that under worst-case conditions, transistor Q1 has just turned off when transistor Q2 turns on, as shown in Figure 24. The amount of delay necessary to achieve this condition is equal to the maximum value of the propagation delay difference specification,  $PDD_{MAX}$ , which is specified to be 100 ns over the operating temperature range of  $-40^{\circ}\text{C}$  to  $105^{\circ}\text{C}$ .

Delaying the LED signal by the maximum propagation delay difference ensures that the minimum dead time is zero, but it does not tell a designer what the maximum dead time will be. The maximum dead time is equivalent to the difference between the maximum and minimum propagation delay difference specifications as shown in Figure 25. The maximum dead time for the ACPL-P346/W346 is 100 ns (= 50 ns – (–50 ns)) over an operating temperature range of  $-40^{\circ}\text{C}$  to  $105^{\circ}\text{C}$ .

Note that the propagation delays used to calculate PDD and dead time are taken at equal temperatures and test conditions because the optocouplers under consideration are typically mounted in close proximity to each other and are switching identical MOSFETs.

## LED Current Input with Hysteresis

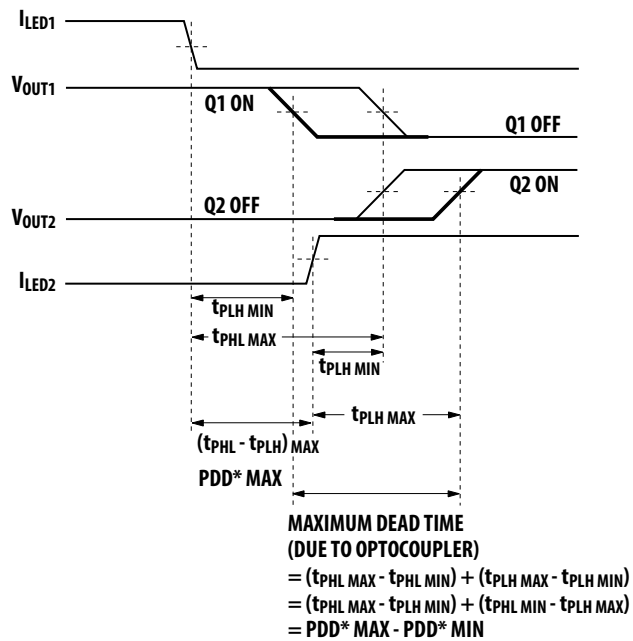
The detector has optical receiver input stage with built-in Schmitt trigger to provide logic compatible waveforms, eliminating the need for additional wave shaping. The hysteresis (Figure 12) provides differential mode noise immunity and minimizes the potential for output signal chatter.

**Figure 24: Minimum LED Skew for Zero Dead Time**

\*PDD = Propagation Delay Difference  
Note: For PDD calculations, the propagation delays are taken at the same temperature and test conditions.



Figure 25: Waveforms for Dead Time



\*PDD = Propagation Delay Difference

Note: For Dead Time and PDD calculations, all propagation delays are taken at the same temperature and test conditions.

## Thermal Model for ACPL-P346/W346 Stretched SO6 Package Optocoupler

### Definitions

$R_{11}$ : Junction to Ambient Thermal Resistance of LED due to heating of LED

$R_{12}$ : Junction to Ambient Thermal Resistance of LED due to heating of Detector (Output IC)

$R_{21}$ : Junction to Ambient Thermal Resistance of Detector (Output IC) due to heating of LED.

$R_{22}$ : Junction to Ambient Thermal Resistance of Detector (Output IC) due to heating of Detector (Output IC).

$P_1$ : Power dissipation of LED (W).

$P_2$ : Power dissipation of Detector / Output IC (W).

$T_1$ : Junction temperature of LED ( $^{\circ}\text{C}$ ).

$T_2$ : Junction temperature of Detector ( $^{\circ}\text{C}$ ).

$T_a$ : Ambient temperature.

Ambient Temperature: Junction to Ambient Thermal Resistances were measured approximately 1.25 cm above optocoupler at  $\sim 23^{\circ}\text{C}$  in still air.

Thermal Resistance	$^{\circ}\text{C}/\text{W}$
$R_{11}$	135
$R_{12}$	27
$R_{21}$	39
$R_{22}$	47

This thermal model assumes that an 6-pin single-channel plastic package optocoupler is soldered into a 7.62-cm  $\times$  7.62-cm printed circuit board (PCB) per JEDEC standards. The temperature at the LED and Detector junctions of the optocoupler can be calculated using the following equations.

#### Equation 1:

$$T_1 = (R_{11} \times P_1 + R_{12} \times P_2) + T_a$$

#### Equation 2:

$$T_2 = (R_{21} \times P_1 + R_{22} \times P_2) + T_a$$

Using the given thermal resistances and thermal model formula in this data sheet, we can calculate the junction temperature for both LED and the output detector. Both junction temperatures should be within the absolute maximum rating.

For example, given  $P_1 = 17 \text{ mW}$ ,  $P_2 = 124 \text{ mW}$ ,  $T_a = 85^{\circ}\text{C}$ :

LED junction temperature,

$$\begin{aligned} T_1 &= (R_{11} \times P_1 + R_{12} \times P_2) + T_a \\ &= (135 \times 0.017 + 27 \times 0.124) + 85 \\ &= 90.7^{\circ}\text{C} \end{aligned}$$

Output IC junction temperature,

$$\begin{aligned} T_2 &= (R_{21} \times P_1 + R_{22} \times P_2) + T_a \\ &= (39 \times 0.017 + 47 \times 0.124) + 85 \\ &= 91.5^{\circ}\text{C} \end{aligned}$$

$T_1$  and  $T_2$  should be limited to  $125^{\circ}\text{C}$  based on the board layout and part placement.

## Related Documents

AV02-0421EN	Application Note 5336	<i>Gate Drive Optocoupler Basic Design for IGBT/MOSFET</i>
AV02-3698EN	Application Note 1043	<i>Common-Mode Noise: Sources and Solutions</i>
AV02-0310EN	Reliability Data	<i>Plastics Optocouplers Product ESD and Moisture Sensitivity</i>

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