90V Boost DC/DC Converter with APD Current Monitor

General Description

The RT8541/A is a constant frequency current mode PWM step-up DC/DC converter designed to bias avalanche photodiodes (APD) at high voltage in optical receivers. It includes a voltage doubler charge pump to significantly reduce the noise level at output up to 90V. The RT8541A switching frequency can be adjusted by a resistor while RT8541 is internally set at 650kHz. The RT8541/A has a built-in APD current mirror that delivers 1/5 of the APD current with high accuracy for monitoring the APD current from $0.2\mu A$ to 2.5mA. This current can be used as a reference to provide a digital programmed output voltage via the CTRL pin. To protect the optical receiver system, the RT8541/A provides a built-in adjustable APD current limit function by sensing a 200mV voltage threshold between VOUT2 and MONIN pins. Only one resistor is needed to program the desired current limit. A charge pump voltage doubler is designed to achieve significantly lower noise level at the APD comparing to a simple boost converter type bias circuit.

The RT8541/A also features a built-in 9ms soft-start function to eliminate the inrush current during start-up interval. The RT8541/A provides a low cost optical receiver solution and can fit in very small PCB area.

The RT8541/A is available in the WQFN-16L 3x3 package.

Features

- Integrated Schottky Diodes for Boost Converter and Charge Pump Voltage Doubler
- 50V, 400mA Internal Switch
- High Side Low Noise and Accurate APD Current Monitor
- 650kHz Fixed Switching Frequency for RT8541 and Adjustable Switching Frequency for RT8541A
- Wide VIN Range : 2.7V to 16V
- Adjustable APD Current Limit with External Resistor
- Low Shutdown Current <1µA
- Built-In Soft-Start
- CTRL Pin Allows Output Adjustment with no Polarity Inversion
- Thin 16-Lead WQFN Package
- RoHS Compliant and Halogen Free

Applications

- APD Bias
- PIN Diode Bias
- Optical Receivers and Modules
- Fiber Optic Network Equipment

Simplified Application Circuit





Ordering Information

RT8541/A

- QW : WQFN-16L 3x3 (W-Type)
- —Lead Plating System
- G : Green (Halogen Free and Pb Free)
- ——Adjustable Switching Frequency
 - —Fixed Switching Frequency

Note :

Richtek products are :

- RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- Suitable for use in SnPb or Pb-free soldering processes.

Marking Information

RT8541GQW

8C=YM DNN 8C= : Product Code YMDNN : Date Code

RT8541AGQW



1G= : Product Code YMDNN : Date Code

Pin Configurations





WQFN-16L 3x3 RT8541A

Functional Pin Description

Pin No.	Pin Name	Pin Function		
1	VC	Compensation Node for Control Loop.		
2	APD	Output for APD. Connect this Pin to the APD Cathode.		
3	MONIN	Current Monitor Input Power Pin. An optional resistor between the VOUT2 and MONIN pins can be used for current limit setting.		
4	VOUT2	Voltage Doubler Output Pin. A 50V rated capacitor is needed between this pin and VOUT1 pin. A resistor divider for output voltage feedback is connected between this pin and GND pin.		
5	VOUT1	Output Pin of Boost Converter. A capacitor is needed between this pin and GND pin. The trace length from this pin to the capacitor should be minimized.		
6	PUMP	Charge Pump Pin for Voltage Doubler. Put a 50V capacitor between the SW and PUMP pins to form a complete voltage doubler with the internal Schottky diodes.		
7, 8	SW	Switch Node of Boost Converter. Minimize the trace area on this pin to reduce EMI.		
9, 10, 17 (Exposed Pad)	GND	Ground. The exposed pad must be soldered to a large PCB and connected to GND for maximum power dissipation.		
11	VIN	Supply Voltage Input. Connect a $1\mu F$ capacitor from this pin to GND.		
12	SHDN	Shutdown Control Input. Tie to 2V or higher with a resistor $200k\Omega$ to enable device.		
13	CTRL	External Reference Control Input. This allows the FB voltage to follow the external reference between 0V and 1.2V. Tie this pin higher than 1.5V to use the internal reference of 1.235V.		
14	FB	Feedback Input. Connect the pin to the output resistor divider for output voltage setting.		
15	NC (RT8541)	No Internal Connection. The switching frequency is set at 650kHz internally.		
10	FSET (RT8541A)	Oscillator Frequency Setting. Connect a resistor between this pin and GND for frequency setting.		
16MONOutput for Current Monitor. It sources a current equal to 20% of the current and converts to a reference voltage through an external resistor.				



Function Block Diagram



Operation

The RT8541/A Boost converter uses a constant frequency current mode control scheme to provide excellent line and load regulation. Operation can be best understood by referring to the Functional Diagram. At the start of each oscillator cycle, the SR latch is set, which turns on the power switch, Q1. A voltage proportional to the switch current is added to a stabilizing slope compensation and the resulting sum is fed into the positive terminal of the PWM comparator, A2. When this voltage exceeds the level at the negative input of A2, the SR latch is reset and the power switch is turned off. The level at the negative input of A2 is set by the error amplifier A1, and is simply an amplified version of the difference between the feedback voltage and the reference voltage of 1.235V, or externally provided CTRL voltage. In this manner, the error amplifier sets the correct peak current level to keep the output in regulation. If the error amplifier's output increases, more current is delivered to the output; if it decreases, less current is delivered.

The RT8541/A has an integrated high side APD current monitor with a 5:1 ratio. The MONIN pin can accept a supply voltage up to 90V, which is suitable for APD photodiode applications. The MON pin has an open-circuit protection feature and is internally clamped to 15V.

If an APD is tied to the APD pin, the current will be mirrored to the MON pin and converted to a voltage signal by the resistor between MON and GND pins. This voltage signal can be used to drive an external control block to adjust the APD voltage by adjusting the feedback threshold of Error Amplifier A1 through the CTRL input.

The RT8541/A features a built-in 9ms soft-start function and provides current limit function with a 0.2V threshold between VOUT2 and MONIN pins to protect the APD system. The APD current limit can be adjusted by an external resistor between the VOUT2 and MONIN pins.

Absolute Maximum Ratings (Note 1)

• VIN, SHDN, FSET, CTRL, MON	16V
• VOUT1, SW	50V
VOUT2, PUMP, MONIN, APD	90V
• FB, VC, FSET	5V
• Power Dissipation, $P_D @ T_A = 25^{\circ}C$	
WQFN-16L 3x3	3.33W
Package Thermal Resistance (Note 2)	
WQFN-16L 3x3, θ _{JA}	30°C/W
WQFN-16L 3x3, θ_{JC}	7.5°C/W
Junction Temperature	150°C
Lead Temperature (Soldering, 10 sec.)	260°C
Storage Temperature Range	$-65^{\circ}C$ to $150^{\circ}C$
ESD Susceptibility (Note 3)	
HBM (Human Body Model)	2kV
MM (Machine Model)	200V

Recommended Operating Conditions (Note 4)

• ;	Supply Input Voltage, VIN	3V to 12V
• 、	Junction Temperature Range	$-40^\circ C$ to $125^\circ C$
• /	Ambient Temperature Range	$-40^{\circ}C$ to $85^{\circ}C$

Electrical Characteristics

(V _{IN} = 5V, T _A =	= 25°C,	unless	otherwise	specified)
---	---------	--------	-----------	------------

Parameter	Symbol	Test Conditions	Min	Тур	Max	Unit
Operating Voltage			2.7		16	V
Feedback Voltage	V _{FB}	CTRL = 1.5V	1.215	1.235	1.255	V
Feedback Line Regulation		$V_{IN} = 3V$ to 10V		0.025	0.07	%N
FB Pin Bias Current				30	100	nA
Supply Current	I _{VIN}	$FB = 1.3V, V_{\overline{SHDN}} = 2V$		3.3	4	mA
Shutdown Current		$V_{\overline{SHDN}} = 0V$, Not Switching		0.1	0.5	μΑ
Switching Frequency	f _{SW}	RSET = NC (RT8541)		650		
		RSET = 30k (RT8541A)		650		KΠZ
Maximum Duty Cycle	D _{MAX}	f _{SW} = 650kHz	95			%
Switch Current Limit	I _{LIM}		320	400	480	mA
Switch VCESAT		I _{SW} = 150mA		130	220	mV
Switch Leakage Current		SW = 5V			2	μA
Schottky Forward Voltage		ISCHOTTKY = 150mA		720		mV
Schottky Reverse Leakage		VOUT1 - SW = 50V			5	μA

RT8541/A



Parameter	Symbol	Test Conditions	Min	Тур	Мах	Unit
SHDN Voltage High	VIH		2			V
SHDN Voltage Low	V _{IL}				0.4	V
SHDN Pin Bias Current				1	2	μA
Internal Soft-Start Time				9		ms
VC Threshold Voltage				0.7		V
ADD Current Menitor Coin	C	$I_{APD} = 250 nA, \ 10V \le MONIN \le 90V$	0.18	0.2	0.215	
APD Current Monitor Gain	GAPD	$I_{APD} = 2.5 mA, 20V \le MONIN \le 90V$	0.18	0.2	0.215	V/V
Monitor Output Voltage Clamp				15	16	V
APD Monitor Voltage Drop		MONIN – APD at I _{APD} = 1mA, MONIN = 90V			5	V
MONIN Pin Current Limit Threshold Voltage		APD = 0V, MONIN = 40V		200		mV
CTRL to FB Offset		CTRL = 0.5V	-5	2	12	mV
OTP Threshold Temperature				150		°C

Note 1. Stresses beyond those listed "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions may affect device reliability.

Note 2. θ_{JA} is measured at $T_A = 25^{\circ}C$ on a high effective thermal conductivity four-layer test board per JEDEC 51-7. θ_{JC} is measured at the exposed pad of the package.

Note 3. Devices are ESD sensitive. Handling precaution is recommended.

Note 4. The device is not guaranteed to function outside its operating conditions.

Typical Application Circuit





Figure 1. 3.3V to 63V/2mA APD Bias Power Supply Application Circuit



Typical Operating Characteristics













Current Monitor Output vs. MONIN Voltage



Switch Saturation Voltage vs. Switch Current



RICHTEK is a registered trademark of Richtek Technology Corporation. Copyright ©2013 Richtek Technology Corporation. All rights reserved.

www.richtek.com



Copyright ©2013 Richtek Technology Corporation. All rights reserved. RICHTEK is a registered trademark of Richtek Technology Corporation.

Application Information

Boost Regulator

The RT8541/A is a current mode Boost converter integrated with a 50V/400mA power switch over a wide VIN range from 2.8V to 16V. It performs fast transient responses to support the avalanche photodiodes (APDs) in optical receivers. The high operation frequency allows the use of small components to minimize the thickness of the optical transceiver.

The output voltage can be adjusted by an external resistive voltage divider connected to the FB pin. The error amplifier varies the VC voltage by sensing the FB pin to regulate the output voltage. For better stability, the slope compensation signal summed with the current sense signal will be compared with the VC voltage to determine the current trip point and duty cycle.

Output Voltage Setting

The RT8541/A regulated output voltage is showed as the following equation :

 $V_{OUT} = V_{FB} \times \left(1 + \frac{R1}{R2}\right)$, where $V_{FB} = 1.235V$ (typ.)

The recommended value for R2 should be at least $10k\Omega$. Place the resistive voltage divider as close as possible to the chip to reduce noise sensitivity.

Loop Compensation

The voltage feedback loop can be compensated with an external compensation network consisting of R4. Choose R4 to set high frequency integrator gain for fast transient response and C4 to set the integrator zero to maintain loop stability. For example, $V_{IN} = 3.3V$, $V_{OUT2} = 63V$, $C_{OUT} = 0.22\mu$ F, L = 6.8μ H, the recommended value for the compensation network is R4 = $1k\Omega$ and C4 = 3.3nF.

Inductor Selection

The inductance depends on the maximum input current. As a general rule, the inductor ripple current range is 20% to 40% of the maximum input current. If 40% is selected as an example, the inductor current can be calculated according to the following equation :

$$I_{IN(MAX)} = \frac{V_{OUT} \times I_{APD}}{\eta \times V_{IN}}$$

where η is the efficiency of the converter, $I_{IN(MAX)}$ is the maximum input current. The input peak current can then be obtained by adding the maximum input current with half of the inductor ripple current.

I_{PEAK} =1.2 x I_{IN(MAX)}

Note that the saturated current of the inductor must be greater than I_{PEAK} . The inductance can eventually be determined according to the following equation :

$$L = \frac{\eta \times (V_{IN})^{2} \times (V_{OUT2} - V_{IN})}{0.4 \times (V_{OUT2})^{2} \times I_{APD} \times f_{SET}}$$

where f_{SET} is the switching frequency. For better system performance, a shielded inductor is preferred to avoid EMI problems.

Switching Frequency

The RT8541A FSET frequency adjust pin allows the user to program the switching frequency from 100kHz to 1.3MHz for optimized efficiency, performance, and external component size. For an appropriate R_{SET} resistor value see Table 1. An external resistor from the FSET pin to GND is required. Do not leave this pin open. For RT8541 the switching frequency is fixed and set at 650kHz typically.

 Table 1. Switching Frequency vs. RSET Value

 (1% Resistors)

RSET (kΩ)	Frequency (kHz)
15	1300
20	1000
25	840
30	720
32	650
40	556
50	456
60	360

Output Capacitor Selection

The output ripple voltage is an important index for estimating chip performance. This portion consists of two parts. One is the product of the inductor current with the ESR of the output capacitor, while the other part is formed by the charging and discharging process of the output capacitor. As shown in Figure 1, ΔV_{OUT2} can be evaluated based on the ideal energy equalization. According to the definition of Q, the Q value can be calculated as the following equation :

$$\begin{split} \mathsf{Q} &= \frac{1}{2} \times \left[\left(\mathsf{I}_{\mathsf{IN}} + \frac{1}{2} \Delta \mathsf{I}_{\mathsf{L}} - \mathsf{I}_{\mathsf{APD}} \right) + \left(\mathsf{I}_{\mathsf{IN}} - \frac{1}{2} \Delta \mathsf{I}_{\mathsf{L}} - \mathsf{I}_{\mathsf{APD}} \right) \right] \\ &\times \frac{\mathsf{V}_{\mathsf{IN}}}{\mathsf{V}_{\mathsf{OUT2}}} \times \frac{1}{\mathsf{f}_{\mathsf{SET}}} = \mathsf{C}_{\mathsf{OUT}} \times \Delta \mathsf{V}_{\mathsf{OUT2}} \end{split}$$

where f_{SET} is the switching frequency, and ΔI_L is the inductor ripple current. Bring C_{OUT} to the left side to estimate the value of ΔV_{OUT2} according to the following equation :

$$\Delta V_{OUT2} = \frac{D \times I_{APD}}{\eta \times C_{OUT} \times f_{SET}}$$

where D is the duty cycle and η is the Boost converter efficiency. Finally, taking ESR into account, the overall output ripple voltage can be determined by the following equation :

$$\Delta V_{OUT} = I_{IN} \times ESR \times \frac{D \times I_{OUT}}{\eta \times C_{OUT} \times f_{OSC}}$$

For applications with out voltage less than 45V, intermediate output pin VOUT1 can directly serve as the output pin. Typically use a 2μ F capacitor for output voltage less than 25V and 1μ F capacitor for output voltage between 25V and 45V. When output voltage goes beyond 45V, a charge pump must be formed with cascaded 0.47 μ F capacitors C1 and C2 at the output nodes. A typical 0.1 μ F capacitor is used as the flying capacitor CFLY to form the charge pump. Always use a capacitor with sufficient voltage rating. Either ceramic or solid tantalum capacitors may be used for the input decoupling capacitor, which should be placed as close as possible to the RT8541. A 1 μ F capacitor is sufficient for most applications.

Input Capacitor Selection

Low ESR ceramic capacitors are recommended for input capacitor applications. Low ESR will effectively reduce the input voltage ripple caused by switching operation. A 10μ F capacitor is sufficient for most applications. Nevertheless, this value can be decreased for lower output current requirement. Another consideration is the voltage rating of the input capacitor which must be greater than the maximum input voltage.

APD Current Monitor

The power supply switching noise associated with a switching power supply can interfere with the photodiode DC measurement. To suppress this noise, a 0.1μ F capacitor is recommended at APD pin. An additional output low-pass filter, a 10k resistor and a 10nF capacitor in parallel at MON pin might limit the measurement accuracy of low level signals. For applications requiring fast current monitor response time, a RC low-pass filter at MONIN pin is used to replace the 0.1μ F capacitor at APD pin to reduce the power supply noise and other wide band noise.

APD Short Current Protection

In some applications, a long cable or wire is used to connect the RT8541/A to APD. When APD is shorted to GND, APD pin voltage might ring below ground and damage the internal circuitry. To prevent damage from short-circuit event, a 100Ω resistor must be added between MONIN and VOUT2 pins. The APD short current is 200mV/R6. For a typical 2mA short current protection of APD, the R6 should be set at 100Ω .

Thermal Considerations

For continuous operation, do not exceed absolute maximum junction temperature. The maximum power dissipation depends on the thermal resistance of the IC package, PCB layout, rate of surrounding airflow, and difference between junction and ambient temperature. The maximum power dissipation can be calculated by the following formula :

$\mathsf{P}_{\mathsf{D}(\mathsf{MAX})} = (\mathsf{T}_{\mathsf{J}(\mathsf{MAX})} - \mathsf{T}_{\mathsf{A}}) / \theta_{\mathsf{J}\mathsf{A}}$

where $T_{J(MAX)}$ is the maximum junction temperature, T_A is the ambient temperature, and θ_{JA} is the junction to ambient thermal resistance.

For recommended operating condition specifications, the maximum junction temperature is 125° C. The junction to ambient thermal resistance, θ_{JA} , is layout dependent. For

Copyright ©2013 Richtek Technology Corporation. All rights reserved. RICHTEK is a registered trademark of Richtek Technology Corporation.

RT8541/A



WQFN-16L 3x3 package, the thermal resistance, θ_{JA} , is 30°C/W on a standard JEDEC 51-7 four-layer thermal test board. The maximum power dissipation at $T_A = 25^{\circ}C$ can be calculated by the following formula :

 $P_{D(MAX)}$ = (125°C - 25°C) / (30°C/W) = 3.33W for WQFN-16L 3x3 package

The maximum power dissipation depends on the operating ambient temperature for fixed $T_{J(MAX)}$ and thermal resistance, θ_{JA} . The derating curve in Figure 2 allows the designer to see the effect of rising ambient temperature on the maximum power dissipation.





Layout Considerations

PCB layout is very important for designing switching power converter circuits. The following layout guides should be strictly followed for best performance of the RT8541/A.

- Place L and C1 as close as possible to the SW and PUMP pin. The trace should be as short and wide as possible.
- The compensation circuit should be kept away from the power loops and should be shielded with a ground trace to prevent any noise coupling. Place the compensation components as close as possible to VC pin.
- The exposed pad of the chip should be connected to ground plane for thermal consideration.



Figure 3. PCB Layout Guide

Outline Dimension



Note : The configuration of the Pin #1 identifier is optional, but must be located within the zone indicated.

Symbol	Dimensions I	In Millimeters	Dimensions In Inches		
Зутрог	Min	Max	Min	Мах	
А	0.700	0.800	0.028	0.031	
A1	0.000	0.050	0.000	0.002	
A3	0.175	0.250	0.007	0.010	
b	0.180	0.300	0.007	0.012	
D	2.950	3.050	0.116	0.120	
D2	1.300	1.750	0.051	0.069	
E	2.950	3.050	0.116	0.120	
E2	1.300	1.750	0.051	0.069	
е	0.500		0.0)20	
L	0.350	0.450	0.014	0.018	

W-Type 16L QFN 3x3 Package

Richtek Technology Corporation

5F, No. 20, Taiyuen Street, Chupei City Hsinchu, Taiwan, R.O.C. Tel: (8863)5526789

Richtek products are sold by description only. Richtek reserves the right to change the circuitry and/or specifications without notice at any time. Customers should obtain the latest relevant information and data sheets before placing orders and should verify that such information is current and complete. Richtek cannot assume responsibility for use of any circuitry other than circuitry entirely embodied in a Richtek product. Information furnished by Richtek is believed to be accurate and reliable. However, no responsibility is assumed by Richtek or its subsidiaries for its use; nor for any infringements of patents or other rights of third parties which may result from its use. No license is granted by implication or otherwise under any patent or patent rights of Richtek or its subsidiaries.

X-ON Electronics

Largest Supplier of Electrical and Electronic Components

Click to view similar products for Richtek manufacturer:

Other Similar products are found below :

EVB_RT5047GSP_EVB_RT7275GQW_EVB_RT7297CHZSP_RT9080N-08GJ5_EVB_RT5047AGSP_EVB_RT7243GQW EVB_RT7272BGSP_RT8097AHGE_EVB_RT7247CHGSP_EVB_RT7276GQW_EVB_RT8293AHZSP_EVB_RT6200GE EVB_RT7235GQW_EVB_RT7237AHGSP_EVB_RT7251AZQW_RT5047AGSP_EVB_RT7272AGSP_EVB_RT7237CHGSP EVB_RT7247AHGSP_EVB_RT7252BZSP_EVB_RT7280GQW_EVB_RT8292AHZSP_EVB_RT8297BZQW_EVB_RT7231GQW EVB_RT7232GQW_EVB_RT7236GQW_EVB_RT7250BZSP_EVB_RT7251BZQW_EVB_RT7279GQW_EVB_RT8008GB_RT8207MZQW RT8296AHZSP_RT9011-JGPJ6_RT8258GE_RT5711AHGQW_RT9081AGQZA(2)_RT6154BGQW_RT7238BGQUF_RT5788AGJ8F RT8812AGQW_RT6278BHGQUF_RT7270HZSP_RD0004_RT5789AGQUF_RT9076-18GVN_RT9193-15GU5_RT3602AJGQW RT8296BHZSP_RT6214AHGJ6F_RT9276GQW(Z00)