## S-19902A/19902B/19903A/19903B Series

## AUTOMOTIVE, $125^{\circ} \mathrm{C}$ OPERATION, 36 V INPUT, 600 mA SYNCHRONOUS STEP-DOWN SWITCHING REGULATOR

The S-19902/19903 Series is a step-down switching regulator developed using high withstand voltage CMOS process technologies.
This IC has high maximum operation voltage of 36 V and maintains high-accuracy FB pin voltage at $\pm 1.5 \%$. As suitable packages for high-density mounting, such as small-sized HSNT-6(2025), are adopted, this IC contributes to miniaturization of electronic equipment.
PWM control (S-19902 Series) or PWM / PFM switching control (S-19903 Series) can be selected as an option.
Since the S-19903 Series, which features PWM / PFM switching control, operates with PWM control under heavy load and automatically switches to PFM control under light load, it achieves high-efficiency operation in accordance with the device's status. Furthermore, our distinctive PWM / PFM switching control technology suppresses the ripple voltage to be generated in Vout while PFM control is in operation.
Since the S-19902/19903 Series has the built-in synchronous circuit, it achieves high efficiency easier compared with conventional step-down switching regulators. In addition, it has the built-in overcurrent protection circuit which protects the IC and coils from excessive load current as well as a thermal shutdown circuit which prevents damage from heat generation.
ABLIC Inc. offers FIT rate calculated based on actual customer usage conditions in order to support customer functional safety design.
For more information regarding our FIT rate calculation, contact our sales representatives.
Caution This product can be used in vehicle equipment and in-vehicle equipment. Before using the product for these purposes, it is imperative to contact our sales representatives.

## Features

- Input voltage:
- Output voltage (externally set):
- Output current:
- FB pin voltage accuracy:
- Efficiency:
- Oscillation frequency:
- Overcurrent protection function:
- Thermal shutdown function:
- Short-circuit protection function:
- 100\% duty cycle operation:
- Soft-start function:
- Under voltage lockout function (UVLO):
- Input and output capacitors:
- Operation temperature range:
- Lead-free (Sn 100\%), halogen-free
- Withstand 45 V load dump
- AEC-Q100 qualified*1


## Applications

- Camera module
- For automotive use (engine, transmission, suspension, ABS, related-devices for EV / HEV / PHEV, etc.)
- Constant-voltage power supply for electrical application for vehicle interior
- Constant-voltage power supply for industrial equipment
- Constant-voltage power supply for home electric appliance


## $\square$ Packages

- HTMSOP-8
( $4.0 \mathrm{~mm} \times 2.9 \mathrm{~mm} \times \mathrm{t} 0.8 \mathrm{~mm} \max$.)
- HSNT-8(2030)
( $3.0 \mathrm{~mm} \times 2.0 \mathrm{~mm} \times \mathrm{t} 0.5 \mathrm{~mm}$ max.)
- HSNT-6(2025)
(2.46 mm $\times 1.96 \mathrm{~mm} \times \mathrm{t} 0.5 \mathrm{~mm}$ max.)
*1. Contact our sales representatives for details.


## - Typical Application Circuit



## ■ Efficiency



## ■ Block Diagrams

1. S-19902 Series (PWM control)

*1. Parasitic diode
Figure 1
2. S-19903 Series (PWM / PFM switching control)

*1. Parasitic diode
Figure 2

## ■ AEC-Q100 Qualified

This IC supports AEC-Q100 for operation temperature grade 1.
Contact our sales representatives for details of AEC-Q100 reliability specification.

## ■ Product Name Structure

1. Product name
*1. Refer to the tape drawing.
*2. Refer to "2. Function list of product types".
2. Function list of product types

Table 1

| Product Type | Oscillation Frequency | Short-circuit Protection Function |
| :---: | :---: | :--- |
| A | 2.2 MHz | Hiccup control |
| B | 2.2 MHz | Latch control |

## 3. Packages

Table 2 Package Drawing Codes

| Package Name | Dimension | Tape | Reel | Land | Stencil Opening |
| :--- | :---: | :---: | :---: | :---: | :---: |
| HTMSOP-8 | FP008-A-P-SD | FP008-A-C-SD | FP008-A-R-SD | FP008-A-L-SD | - |
| HSNT-8(2030) | PP008-A-P-SD | PP008-A-C-SD | PP008-A-R-SD | PP008-A-L-SD | - |
| HSNT-6(2025) | PJ006-B-P-SD | PJ006-B-C-SD | PJ006-B-R-SD | PJ006-B-LM-SD | PJ006-B-LM-SD |

## ■ Pin Configurations

1. HTMSOP-8

Table 3


| Pin No. | Symbol |  |
| :---: | :--- | :--- |
| 1 | VIN | Power supply pin |
| 2 | FB | Feedback pin |
| 3 | EN | Enable pin (active "H") |
| 4 | NC $^{*} 2$ | No connection |
| 5 | NC $^{*} 2$ | No connection |
| 6 | VREG $^{* 3}$ | Internal power supply pin |
| 7 | VSS | GND pin |
| 8 | SW | External inductor connection pin |

External inductor connection pin

Figure 3
*1. Connect the heat sink of backside at shadowed area to the board, and set electric potential GND. However, do not use it as the function of electrode.
*2. The NC pin is electrically open.
The NC pin can be connected to the VIN pin or the VSS pin.
*3. The VREG pin cannot supply load current outside.
2. HSNT-8(2030)

| Top view | Table 4 |  |  |
| :---: | :---: | :---: | :---: |
|  | Pin No. | Symbol | Description |
|  | 1 | VIN | Power supply pin |
|  | 2 | FB | Feedback pin |
|  | 3 | EN | Enable pin (active "H") |
| Bottom view | 4 | NC*2 | No connection |
|  | 5 | NC*2 | No connection |
|  | 6 | VREG** | Internal power supply pin |
|  | 7 | VSS | GND pin |
|  | 8 | SW | External inductor connection pin |

Figure 4
*1. Connect the heat sink of backside at shadowed area to the board, and set electric potential GND.
However, do not use it as the function of electrode.
*2. The NC pin is electrically open.
The NC pin can be connected to the VIN pin or the VSS pin.
*3. The VREG pin cannot supply load current outside.
3. HSNT-6(2025)

Table 5


| Pin No. | Symbol | Description |
| :---: | :--- | :--- |
| 1 | VIN | Power supply pin |
| 2 | FB | Feedback pin |
| 3 | EN | Enable pin (active "H") |
| 4 | VREG ${ }^{* 2}$ | Internal power supply pin |
| 5 | VSS | GND pin |
| 6 | SW | External inductor connection pin |

Figure 5
*1. Connect the heat sink of backside at shadowed area to the board, and set electric potential GND. However, do not use it as the function of electrode.
*2. The VREG pin cannot supply load current outside.

## ■ Absolute Maximum Ratings

Table 6
(Unless otherwise specified: $\mathrm{Ta}=+25^{\circ} \mathrm{C}$, $\mathrm{V}_{\mathrm{ss}}=0 \mathrm{~V}$ )

| Item | Symbol | Absolute Maximum Ratings | Unit |
| :---: | :---: | :---: | :---: |
| VIN pin voltage | VIN | $\mathrm{V}_{\text {ss }}-0.3$ to $\mathrm{V}_{\text {ss }}+45$ | V |
| EN pin voltage | $V_{\text {EN }}$ | $V_{\text {SS }}-0.3$ to $\mathrm{V}_{\text {SS }}+45$ | V |
| FB pin voltage | $\mathrm{V}_{\text {FB }}$ | $\mathrm{V}_{\text {SS }}-0.3$ to $\mathrm{V}_{\text {REG }}+0.3 \leq \mathrm{V}_{\text {SS }}+6.0$ | V |
| VREG pin voltage | VREG | $\mathrm{V}_{\text {ss }}-0.3$ to $\mathrm{V}_{\text {IN }}+0.3 \leq \mathrm{V}_{\text {Ss }}+6.0$ | V |
| SW pin voltage | Vsw | $\mathrm{V}_{\text {ss }}-2$ to $\mathrm{V}_{\text {IN }}+2 \leq \mathrm{V}_{\text {ss }}+45$ ( $<20 \mathrm{~ns} \mathrm{)}$ | V |
|  |  | $\mathrm{V}_{\text {SS }}-0.3$ to $\mathrm{V}_{\text {IN }}+0.3 \leq \mathrm{V}_{\text {Ss }}+45$ |  |
| Junction temperature | $\mathrm{T}_{\mathrm{j}}$ | -40 to +150 | ${ }^{\circ} \mathrm{C}$ |
| Operation ambient temperature | Topr | -40 to +125 | ${ }^{\circ} \mathrm{C}$ |
| Storage temperature | $\mathrm{T}_{\text {stg }}$ | -40 to +150 | ${ }^{\circ} \mathrm{C}$ |

Caution The absolute maximum ratings are rated values exceeding which the product could suffer physical damage. These values must therefore not be exceeded under any conditions.

## ■ Thermal Resistance Value

Table 7

| Item | Symbol | Condition |  | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Junction-to-ambient thermal resistance*1 | $\theta \mathrm{JA}$ | HTMSOP-8 | Board A | - | 159 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  |  | Board B | - | 113 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  |  | Board C | - | 39 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  |  | Board D | - | 40 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  |  | Board E | - | 30 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  | HSNT-8(2030) | Board A | - | 181 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  |  | Board B | - | 135 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  |  | Board C | - | 40 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  |  | Board D | - | 42 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  |  | Board E | - | 32 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  | HSNT-6(2025) | Board A | - | 180 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  |  | Board B | - | 128 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  |  | Board C | - | 43 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  |  | Board D | - | 44 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  |  | Board E | - | 36 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

*1. Test environment: compliance with JEDEC STANDARD JESD51-2A

Remark Refer to "■ Power Dissipation" and "Test Board" for details.

## ■ Electrical Characteristics

Table 8
$\left(\mathrm{V}_{\text {IN }}=12 \mathrm{~V}, \mathrm{~T}_{\mathrm{j}}=-40^{\circ} \mathrm{C}\right.$ to $+125^{\circ} \mathrm{C}$ unless otherwise specified $)$

| Item | Symbol | Condition | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Operating input voltage | VIN | - | 4.0 | - | 36.0 | V |
| Current consumption during shutdown | Isss | Ven $=0 \mathrm{~V}$ | - | 0 | 5 | $\mu \mathrm{A}$ |
| Current consumption during switching off | Iss | $\mathrm{V}_{\mathrm{FB}}=1.0 \mathrm{~V}$ | - | 175 | 260 | $\mu \mathrm{A}$ |
|  |  |  | - | 68 | 120 | $\mu \mathrm{A}$ |
| UVLO detection voltage | Vuvio- | VREG pin voltage | 3.1 | 3.35 | 3.6 | V |
| UVLO release voltage | Vuvlo+ | VREG pin voltage | 3.2 | 3.45 | 3.7 | V |
| FB pin voltage | $\mathrm{V}_{\text {FB }}$ | - | 0.788 | 0.8 | 0.812 | V |
| Oscillation frequency | fosc | - | 1.98 | 2.2 | 2.42 | MHz |
| Minimum ON time | ton_min | - | - | 60 | - | ns |
| Maximum duty ratio | MaxDuty | - | 100 | - | - | \% |
| Soft-start wait time | tssw | Time until Vout starts rising, $C_{\text {REG }}=1 \mu \mathrm{~F}$ | 0.30 | 0.58 | 0.90 | ms |
| Soft-start time | tss | Time until $\mathrm{V}_{\text {FB }}$ reaches $90 \%$ after it starts rising | 3.0 | 5.8 | 8.5 | ms |
| High side power MOS FET on-resistance | Rhfet | Isw $=50 \mathrm{~mA}$ | - | 0.85 | 1.75 | $\Omega$ |
| Low side power MOS FET on-resistance | Rlfet | Isw $=-50 \mathrm{~mA}$ | - | 0.35 | 0.65 | $\Omega$ |
| High side power MOS FET leakage current | Ihsw | V IN $=36.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{EN}}=0 \mathrm{~V}, \mathrm{~V}$ sw $=0 \mathrm{~V}$ | - | 0.01 | 2 | $\mu \mathrm{A}$ |
| Low side power MOS FET leakage current | ILsw | $\mathrm{V}_{\text {IN }}=36.0 \mathrm{~V}, \mathrm{~V}_{\text {EN }}=0 \mathrm{~V}, \mathrm{~V}$ Sw $=36.0 \mathrm{~V}$ | - | 0.01 | 4 | $\mu \mathrm{A}$ |
| Limit current | ILIM | - | 1.0 | 1.2 | 1.4 | A |
| Thermal shutdown detection temperature | Tsd | Junction temperature | - | 170 | - | ${ }^{\circ} \mathrm{C}$ |
| Thermal shutdown release temperature | TsR | Junction temperature | - | 150 | - | ${ }^{\circ} \mathrm{C}$ |
| High level input voltage | V ${ }_{\text {SH }}$ | EN pin | 2.0 | - | - | V |
| Low level input voltage | VsL | EN pin | - | - | 0.8 | V |
| High level input current | Ish | EN pin, $\mathrm{V}_{\text {EN }}=2.0 \mathrm{~V}$ | - | - | 1 | $\mu \mathrm{A}$ |
| Low level input current | ISL | EN pin, $\mathrm{V}_{\text {EN }}=0 \mathrm{~V}$ | -0.5 | - | 0.5 | $\mu \mathrm{A}$ |
| FB pin current | IfB | FB pin, $\mathrm{V}_{\text {FB }}=1.0 \mathrm{~V}$ | -0.06 | - | 0.06 | $\mu \mathrm{A}$ |

## Operation

## 1. Overview of operation

The S-19902/19903 Series adopts the current mode control. By comparing the current feedback signal which has slope compensation added to the current flows through high side power MOS FET with the output signal of error amplifier, the Duty ratio of the SW pin is determined. Using the negative feedback loop configured, the error amplifier output signal is maintained at the value that $\mathrm{V}_{\text {REF }}$ and FB pin voltage $\left(\mathrm{V}_{\mathrm{FB}}\right)$ will be equalized.

## 2. PWM control (S-19902 Series)

The S-19902 Series operates with the pulse width modulation method (PWM) regardless of the extent of load current and allows the switching frequency to stabilize.

## 3. PWM / PFM switching control (S-19903 Series)

The S-19903 Series automatically switches between PWM and pulse frequency modulation method (PFM) according to the load current. PFM control is selected when under light load, and the pulse will skip according to the load current. This reduces self-current consumption and improves efficiency when under light load.
In PFM control, the peak current, flows through an inductor, is set to 125 mA typ. in the IC. In addition, our distinctive PWM / PFM switching control technology suppresses the ripple voltage to be generated in Vout while PFM control is in operation.

## 4. Minimum ON time

ON time (ton) of the SW pin during current continuous mode can be calculated by the following expression.

$$
\mathrm{ton}=\frac{\mathrm{V}_{\text {OUT }}}{\mathrm{V}_{\text {IN }}} \times \frac{1}{\mathrm{fosc}^{\prime}}
$$

ton will be small when $\mathrm{V}_{\text {IN }}$ is high and $\mathrm{V}_{\text {out }}$ is low. Set the use conditions to realize ton > minimum ON time (ton_min). Although the maximum value of ton_min varies according to inductance, load current, and the conditions of VIN and Vout, the value is 80 ns. When ton < ton_min, the ripple voltage ( $\Delta V_{\text {OUT }}$ ) in Vout may increase by skipping a pulse during current continuous mode. In addition, when the S-19902/19903 Series changes to an overload status, the limit current (lııм) to protect the IC from overcurrent may increase. Sufficient evaluations under actual conditions are required.

## 5. $100 \%$ duty cycle operation

The high side power MOS FET allows for $100 \%$ duty cycle operation. Even when the input voltage is lowered up to the output voltage value set using the external output voltage setting resistor, the high side power MOS FET is kept on and current can be supplied to the load. The output voltage at this time is the input voltage from which the voltage drop due to the direct resistance of the inductor and the on-resistance of the high side power MOS FET are subtracted.

## 6. Under voltage lockout function (UVLO)

The S-19902/19903 Series has a built-in UVLO circuit to prevent the IC from malfunctioning due to a transient status at power-on or a momentary drop in the supply voltage. When UVLO status is detected, the high side power MOS FET and low side power MOS FET will turn off, and the SW pin will change to "High-Z". For this reason, switching operation will stop. The soft-start function is reset if UVLO status is detected once and is restarted by releasing the UVLO status.
Note that the other internal circuits operate normally, and the status is different from the disabled status.
Also, there is a hysteresis width for avoiding malfunctions due to generation of noise etc. in the input voltage.

## 7. EN pin

This pin starts and stops switching operation. When the EN pin is set to "L", the operation of all internal circuits, including the high side power MOS FET, is stopped, reducing current consumption. When not using the EN pin, connect it to the VIN pin. Since the EN pin is neither pulled down nor pulled up internally, do not use it in the floating status. The structure of the EN pin is shown in Figure 6, and the clamp circuit is internally connected. Refer to "3. 1 High level input current (Ish) vs. EN pin voltage (VEN)" in "■ Characteristics (Typical Data)" for the input current of EN pin.

Table 9

| EN Pin | Internal Circuit | Vout |
| :--- | :--- | :--- |
| "H" | Enable (normal operation) | Constant value ${ }^{* 1}$ |
| "L" | Disable (standby) | Pulled down to $\mathrm{Vss}^{* 2}$ |

*1. The constant value is output due to the regulating based on the output voltage setting resistors ( $R_{F B 1}$ and $R_{F B 2}$ ).
*2. Vout is pulled down to $V_{s s}$ due to the output voltage setting resistors ( $\mathrm{R}_{\mathrm{FB} 1}$ and $\mathrm{R}_{\text {FB2 }}$ ) and a load.


Figure 6

## 8. Thermal shutdown function

The S-19902/19903 Series has a built-in thermal shutdown circuit to limit overheating. When the junction temperature increases to $170^{\circ} \mathrm{C}$ typ., the thermal shutdown circuit becomes the detection status, and the switching operation is stopped. When the junction temperature decreases to $150^{\circ} \mathrm{C}$ typ., the thermal shutdown circuit becomes the release status, and the switching operation is restarted.
If the thermal shutdown circuit becomes the detection status due to self-heating, the switching operation is stopped and output voltage (Vout) decreases. For this reason, the self-heating is limited and the temperature of the IC decreases. The thermal shutdown circuit becomes release status when the temperature of the IC decreases, and the switching operation is restarted, thus the self-heating is generated again. Repeating this procedure makes the waveform of Vout into a pulse-like form. Note that the product may suffer physical damage such as deterioration if the above phenomenon occurs continuously. Switching operation stopping and starting can be stopped by either setting the EN pin to "L", lowering the output current (lout) to reduce internal power consumption, or decreasing the ambient temperature.

Table 10

| Thermal Shutdown Circuit | Vout |
| :--- | :--- |
| Release: $150^{\circ} \mathrm{C}$ typ. ${ }^{* 1}$ | Constant value ${ }^{2}{ }^{2}$ |
| Detection: $170^{\circ} \mathrm{C}$ typ. ${ }^{* 1}$ | Pulled down to $\mathrm{Vss}^{* 3}$ |

*1. Junction temperature
*2. The constant value is output due to the regulating based on the output voltage setting resistors ( $\mathrm{R}_{\mathrm{FB} 1}$ and $\mathrm{R}_{\mathrm{FB} 2}$ ).
*3. Vout is pulled down to $V_{s S}$ due to the output voltage setting resistors ( $R_{F B 1}$ and $R_{F B 2}$ ) and a load.

## 9. Overcurrent protection function

The overcurrent protection circuit monitors the current that flows through the high side power MOS FET and limits current to prevent thermal destruction of the IC due to an overload, magnetic saturation in the inductor, etc.
When a current exceeding the limit current (lıIm) flows through the high side power MOS FET, the high side power MOS FET is turned off. When the next switching cycle starts, the high side power MOS FET is turned on. If the current value continues to remain at lıIM or higher, the high side power MOS FET is turned off again, repeating this series of operation.
Meanwhile, when the current, which flows through the high side power MOS FET, falls to lum or lower, the S-19902/19903 Series will return to the normal operation.
When the slope of inductor current is large, Ilim may appear to increase due to the delay time of overcurrent protection circuit. This phenomenon tends to occur when low-inductance inductor is used or when the voltage different between VIN and Vout is large.

## 10. Frequency foldback function

The frequency foldback function has FB pin voltage ( $\mathrm{V}_{\mathrm{FB}}$ ) and oscillation frequency ( fosc ) to have a proportional relation when $V_{F B}$ is 0.7 V typ. or lower. Refer to "11. Short-circuit protection function" for details. The frequency foldback function in the S-19902 Series is set to invalid at start-up.

## 11. Short-circuit protection function

## 11. 1 Hiccup control

The S-19902/19903 Series A type has a built-in short-circuit protection function for Hiccup control.
Hiccup control is a method for periodically carrying out automatic recovery when the IC detects overcurrent and stops the switching operation.

## 11. 1. 1 When overload status is released

<1> Overcurrent detection
$<2>$ After detection of the FB pin voltage $\left(\mathrm{V}_{\mathrm{FB}}\right)<0.7 \mathrm{~V}$ typ., frequency foldback function becomes valid.
$<3>$ Detection of $\mathrm{V}_{\mathrm{FB}}<0.5 \mathrm{~V}$ typ.
<4> 0.3 ms elapse
$<5>$ Switching operation stop (for 21 ms typ.)
<6> Overload status release
<7> The IC restarts, soft-start function starts.
In this case, it is unnecessary to input an external reset signal for restart.
<8> $\mathrm{V}_{\mathrm{FB}}$ reaches 0.72 V typ. after 5.8 ms typ. elapses.

*1. Inductor current
Figure 7

### 11.1.2 When overload status continues

<1> Overcurrent detection
<2> After detection of $\mathrm{V}_{\mathrm{FB}}<0.7 \mathrm{~V}$ typ., frequency foldback function becomes valid.
$<3>$ Detection of $\mathrm{V}_{\mathrm{FB}}<0.5 \mathrm{~V}$ typ.
<4> 0.3 ms elapse
<5> Switching operation stop (for 21 ms typ.)
<6> The IC restarts, soft-start function starts.
$<7>$ The status returns to <3> when overload status continues after 8.6 ms typ. elapses.

*1. Inductor current
Figure 8
ABLIC Inc.

### 11.2 Latch control

The S-19902/19903 Series B type has a built-in short-circuit protection function for Latch control.
Latch control is a method for maintaining the Latch status when the IC detects overcurrent and stops the switching operation.
<1> Overcurrent detection
<2> After detection of $\mathrm{V}_{\mathrm{FB}}<0.7 \mathrm{~V}$ typ., frequency foldback function becomes valid.
<3> Detection of $\mathrm{V}_{\mathrm{FB}}<0.5 \mathrm{~V}$ typ.
<4> 0.3 ms elapse
<5> Switching operation stop

*1. Inductor current
Figure 9

In addition, Latch status is reset under the following conditions.

## - At UVLO detection

- When the EN pin changes from "H" to "L".


## 12. Pre-bias compatible soft-start function

The S-19902/19903 Series has a built-in pre-bias compatible soft-start circuit.
If the pre-bias compatible soft-start circuit starts when electrical charge remains in the output voltage (Vout) as a result of power supply restart, etc., or when Vout is biased beforehand (pre-bias status), switching operation is stopped until the soft-start voltage exceeds the FB pin voltage ( $\mathrm{V}_{\mathrm{FB}}$ ), and then Vout is maintained. If the soft-start voltage exceeds $\mathrm{V}_{\mathrm{FB}}$, switching operation will restart and $\mathrm{V}_{\text {OUT }}$ will rise to the output voltage setting value (VOUT(s)). This allows Vout(s) to be reached without lowering the pre-biased Vout.
In soft-start circuits which are not pre-bias compatible, a large current flows as a result of the discharge of the residual electric charge through the low side power MOS FET when switching operation starts, which could cause damage, however in a pre-bias compatible soft-start circuit, the IC is protected from the large current when switching operation starts, and it makes power supply design for the application circuit simpler.

In the S-19902/19903 Series, Vout reaches Vout(s) gradually due to the soft-start circuit. In the following cases, rush current and Vout overshoot are reduced.

- When the EN pin changes from "L" to " H ".
- When UVLO operation is released. ${ }^{* 1}$
- When thermal shutdown is released. ${ }^{* 1}$
- At short-circuit recovery* ${ }^{*}$
*1. In this case, the soft-start wait time is eliminated.
The soft-start circuit starts operating after " H " is input to the EN pin and the soft-start wait time (tssw) $=0.58 \mathrm{~ms}$ typ. elapses. The soft-start time (tss) is set to 5.8 ms typ.


Figure 10

## 13. Internal power supply ( $\mathrm{V}_{\mathrm{REG}}$ )

Some of the circuits in the IC operate using the VREG pin voltage (VREG) as the power supply. To stabilize this internal power supply, a ceramic capacitor with $1 \mu \mathrm{~F}$ needs to be connected between the VREG pin and the VSS pin. To achieve low impedance, this capacitor should be placed as close to the IC as possible. Additionally, note that any external parts other than CREG or any load must not connect to the VREG pin.

■ Typical Circuit


Figure 11
Caution The above connection diagram will not guarantee successful operation. Perform thorough evaluation using an actual application to set the constants.

## ■ External Parts Selection

The recommended values for each external part are shown in Table 11, and the recommended parts are shown in Table 12 to Table 16. When selecting an input capacitor ( $\mathrm{C}_{\mathrm{IN}}$ ), output capacitor (Cout), and internal power supply stabilized capacitor ( $\mathrm{C}_{\text {REG }}$ ), take into consideration the temperature range and DC bias characteristics of the capacitor to be used.

Table 11

| $V_{\text {OUT }}$ | $\mathrm{C}_{\text {IN }}$ | Cout | $\mathrm{C}_{\text {FB }}$ | C $_{\text {REG }}$ | L | $\mathrm{R}_{\text {FB } 1}$ | $\mathrm{R}_{\text {FB2 }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2.5 V | $4.7 \mu \mathrm{~F}$ | $10 \mu \mathrm{~F}$ | 33 pF | $1 \mu \mathrm{~F}$ | $3.3,4.7 \mu \mathrm{H}$ | $31.9 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ |
| 3.3 V | $4.7 \mu \mathrm{~F}$ | $10 \mu \mathrm{~F}$ | 33 pF | $1 \mu \mathrm{~F}$ | $3.3,4.7 \mu \mathrm{H}$ | $46.9 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ |
| 5.0 V | $4.7 \mu \mathrm{~F}$ | $10 \mu \mathrm{~F}$ | 33 pF | $1 \mu \mathrm{~F}$ | $4.7,6.8 \mu \mathrm{H}$ | $84 \mathrm{k} \Omega$ | $16 \mathrm{k} \Omega$ |
| 12.0 V | $4.7 \mu \mathrm{~F}$ | $10 \mu \mathrm{~F}$ | 33 pF | $1 \mu \mathrm{~F}$ | $6.8,10 \mu \mathrm{H}$ | $210 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ |

Table 12 Recommended Capacitors ( $\mathrm{C}_{\mathrm{IN}}$ ) List

| Manufacturer | Part Number | Capacitance | Withstanding <br> Voltage | Dimensions $(\mathrm{L} \times \mathrm{W} \times \mathrm{H})$ |
| :--- | :--- | :---: | :---: | :---: |
| TDK Corporation | CGA4J1X7R1H475K125AC | $4.7 \mu \mathrm{~F}$ | 50 V | $2.0 \mathrm{~mm} \times 1.25 \mathrm{~mm} \times 1.25 \mathrm{~mm}$ |
| TDK Corporation | CGA5L3X7R1H475K160AB | $4.7 \mu \mathrm{~F}$ | 50 V | $3.2 \mathrm{~mm} \times 1.6 \mathrm{~mm} \times 1.6 \mathrm{~mm}$ |
| Murata Manufacturing <br> Co., Ltd. | GCM31CC71H475KA03 | $4.7 \mu \mathrm{~F}$ | 50 V | $3.2 \mathrm{~mm} \times 1.6 \mathrm{~mm} \times 1.6 \mathrm{~mm}$ |

Table 13 Recommended Capacitors (Cout) List

| Manufacturer | Part Number | Capacitance | Withstanding <br> Voltage | Dimensions $(\mathrm{L} \times \mathrm{W} \times \mathrm{H})$ |
| :--- | :--- | :---: | :---: | :---: |
| TDK Corporation | CGA4J3X7S1A106K125AB | $10 \mu \mathrm{~F}$ | 10 V | $2.0 \mathrm{~mm} \times 1.25 \mathrm{~mm} \times 1.25 \mathrm{~mm}$ |
| TDK Corporation | CGA5L1X7R1C106K160AC | $10 \mu \mathrm{~F}$ | 16 V | $3.2 \mathrm{~mm} \times 1.6 \mathrm{~mm} \times 1.6 \mathrm{~mm}$ |
| TDK Corporation | CGA4J1X7S1E106K125AC | $10 \mu \mathrm{~F}$ | 25 V | $2.0 \mathrm{~mm} \times 1.25 \mathrm{~mm} \times 1.25 \mathrm{~mm}$ |
| Murata Manufacturing <br> Co., Ltd. | GCM188D70J106ME36 | $10 \mu \mathrm{~F}$ | 6.3 V | $1.6 \mathrm{~mm} \times 0.8 \mathrm{~mm} \times 0.8 \mathrm{~mm}$ |

Table 14 Recommended Capacitor ( $\mathrm{C}_{\mathrm{FB}}$ ) List

| Manufacturer | Part Number | Capacitance | Withstanding <br> Voltage | Dimensions ( $\mathrm{L} \times \mathrm{W} \times \mathrm{H}$ ) |
| :---: | :---: | :---: | :---: | :---: |
| TDK Corporation | CGA1A2C0G1H330J030BA | 33 pF | 50 V | $0.6 \mathrm{~mm} \times 0.3 \mathrm{~mm} \times 0.3 \mathrm{~mm}$ |

Table 15 Recommended Capacitors ( $\mathrm{C}_{\mathrm{REG}}$ ) List

| Manufacturer | Part Number | Capacitance | Withstanding <br> Voltage | Dimensions $(\mathrm{L} \times \mathrm{W} \times \mathrm{H})$ |
| :--- | :--- | :---: | :---: | :---: |
| TDK Corporation | CGA3E1X7R1C105K080AC | $1 \mu \mathrm{~F}$ | 16 V | $1.6 \mathrm{~mm} \times 0.8 \mathrm{~mm} \times 0.8 \mathrm{~mm}$ |
| Murata Manufacturing <br> Co., Ltd. | GCM155C71A105KE38 | $1 \mu \mathrm{~F}$ | 10 V | $1.0 \mathrm{~mm} \times 0.5 \mathrm{~mm} \times 0.5 \mathrm{~mm}$ |

Table 16 Recommended Inductors (L) List

| Manufacturer | Part Number | Inductance | Withstanding <br> Voltage | Dimensions $(\mathrm{L} \times \mathrm{W} \times \mathrm{H})$ |
| :--- | :--- | :---: | :---: | :---: |
| TDK Corporation | TFM252012ALVA3R3MTAA | $3.3 \mu \mathrm{H}$ | 40 V | $2.5 \mathrm{~mm} \times 2.0 \mathrm{~mm} \times 1.2 \mathrm{~mm}$ |
| TDK Corporation | CLF5030NIT-3R3N-D | $3.3 \mu \mathrm{H}$ | - | $5.0 \mathrm{~mm} \times 5.3 \mathrm{~mm} \times 2.7 \mathrm{~mm}$ |
| TDK Corporation | TFM252012ALVA4R7MTAA | $4.7 \mu \mathrm{H}$ | 40 V | $2.5 \mathrm{~mm} \times 2.0 \mathrm{~mm} \times 1.2 \mathrm{~mm}$ |
| TDK Corporation | CLF5030NIT-4R7N-D | $4.7 \mu \mathrm{H}$ | - | $5.0 \mathrm{~mm} \times 5.3 \mathrm{~mm} \times 2.7 \mathrm{~mm}$ |
| TDK Corporation | CLF5030NIT-6R8N-D | $6.8 \mu \mathrm{H}$ | - | $5.0 \mathrm{~mm} \times 5.3 \mathrm{~mm} \times 2.7 \mathrm{~mm}$ |
| TDK Corporation | CLF5030NIT-100M-D | $10 \mu \mathrm{H}$ | - | $5.0 \mathrm{~mm} \times 5.3 \mathrm{~mm} \times 2.7 \mathrm{~mm}$ |
| Murata Manufacturing <br> Co., Ltd. | LQH44PH4R7MPR | $4.7 \mu \mathrm{H}$ | - | $4.0 \mathrm{~mm} \times 4.0 \mathrm{~mm} \times 1.65 \mathrm{~mm}$ |

## 1. Input capacitor ( $\mathrm{C}_{\mathrm{IN}}$ )

$\mathrm{C}_{\mathrm{IN}}$, which has an effect to suppress the ripple voltage and switching noise to be generated in the power supply line, is used for the stable operation of IC. A ceramic capacitor with $4.7 \mu \mathrm{~F}$ or higher is recommended.

## 2. Output capacitor (Cout)

Cout is used to smooth output voltage. The ripple voltage ( $\Delta \mathrm{V}_{\text {OUT }}$ ) to be generated in Vout is inversely proportional to Cout. When selecting a capacitor whose ESR is sufficiently small, $\Delta$ Vout during current continuous mode is calculated by the following expression.

$$
\Delta \text { V out }=\frac{\Delta l_{\mathrm{L}}}{8 \times \text { fosc } \times \text { Cout }}
$$

In addition, since Cout contributes to the stability of feedback loop, a ceramic capacitor with $10 \mu \mathrm{~F}$ or higher is recommended. When selecting a capacitor whose capacitance is extremely large, the overcurrent protection function may start the operation and cause a start-up failure. Therefore, select a capacitor with $200 \mu \mathrm{~F}$ or lower.

## 3. Inductor (L)

To suppress the intrinsic subharmonic oscillation in current mode control, the optimal $L$ value needs to be selected. Considering the slope compensation in the IC, select an inductor from the range of $3.3 \mu \mathrm{H}$ to $10 \mu \mathrm{H}$ depending on Vout.

When selecting L , note the allowable current. If a current exceeding the allowable current flows through the inductor, magnetic saturation may occur, and there may be risks which substantially lower efficiency and damage the IC as a result of large current.
The ripple current ( $\Delta \mathrm{I} \mathrm{L}$ ) and peak current (ІРк) flow through the inductor during current continuous mode are calculated by the following expressions respectively. Make sure IPK will not exceed the allowable current of inductor.

$$
\begin{aligned}
& \Delta \mathrm{I}_{\mathrm{L}}=\frac{\mathrm{V}_{\text {OUT }} \times\left(\mathrm{V}_{\text {IN }}-\mathrm{V}_{\text {OUT }}\right)}{f_{\text {Osc }} \times \mathrm{L} \times \mathrm{V}_{\text {IN }}} \\
& \text { IPK }=\text { Iout }+\frac{\Delta \mathrm{I}_{\mathrm{L}}}{2}
\end{aligned}
$$

In order to maintain the allowable current of inductor even in cases Vout shorts to Vss or other fault conditions occur, an inductor with 1.4 A or higher, the maximum value of lııм, needs to be selected.

## 4. Internal power supply stabilized capacitor (Creg)

Creg is used to stabilize the operation of IC's internal power supply ( $\mathrm{V}_{\text {REG }}=4.5 \mathrm{~V}$ typ.) A ceramic capacitor with $1 \mu \mathrm{~F}$ is recommended.

## 5. Output voltage setting resistors ( $\mathrm{R}_{\mathrm{FB} 1}, \mathrm{R}_{\mathrm{FB} 2}$ ), capacitor for phase compensation ( $\mathrm{C}_{F B}$ )

Vout can be set to any value using $\mathrm{R}_{\mathrm{FB} 1}$ and $\mathrm{R}_{\mathrm{Fb} 2}$. Vout can be calculated by the following expression substituting $V_{F B}=0.8 \mathrm{~V}$ typ. Note that if the $R_{F B 1}$ and $R_{F B 2}$ values are increased, the $F B$ pin will more likely to be affected by noise. A resistor with approximately $15 \mathrm{k} \Omega$ is recommended for $\mathrm{R}_{\mathrm{FB} 2}$.

$$
V_{\text {OUT }}=\frac{\left(R_{F B 1}+R_{F B 2}\right)}{R_{F B 2}} \times 0.8
$$

$C_{F B}$ connected in parallel with $R_{F B 1}$ is a capacitor for phase compensation. Using $R_{F B 1}$ and $C_{F B}$ to set the zero point (the phase feedback) allows the feedback loop to gain larger phase margin.
When selecting $\mathrm{C}_{\text {FB }}$, refer to the following expressions. In addition, perform thorough evaluations with the actual applications to set the constants.

First, calculate the zero point frequency ( $\mathrm{f}_{\mathrm{z}}$ ) by the following expression.

$$
\mathrm{f}_{\mathrm{Z}}=3.94 \times \frac{1}{\text { CoUT }} \times \frac{\mathrm{V}_{\mathrm{FB}}}{\mathrm{~V}_{\text {OUT }}}
$$

Next, substitute $R_{F B 1}$ and $f z$ gained by the above expression into the below expression to calculate $C_{F B}$ value.

$$
C_{F B}=\frac{1}{2 \times \pi \times R_{F B 1} \times f_{Z}}
$$

Caution Generally a switching regulator may cause oscillation depending on the selection of external parts. Perform thorough evaluations including the temperature characteristics with actual applications to confirm no oscillation occurs.

## Board Layout Guidelines

Note the following cautions when determining the board layout for the S-19902/19903 Series.

- Place $\mathrm{C}_{\mathrm{IN}}$ as close to the VIN pin and the VSS pin as possible. Prioritize the layout of $\mathrm{C}_{\mathrm{IN}}$.
- Place Creg as close to the VREG pin and the VSS pin as possible.
- Mount $C_{\text {in }}$ and $C_{\text {reg }}$ on the same surface layer as the IC. If they are connected through thermal vias, the impedance of the thermal vias may influence the operation, resulting in unstable condition.
- Make the wiring of the FB pin as short as possible. The parasitic capacitance of FB pin may affect the phase margin of feedback loop.
- Do not place the FB pin close to noise sources such as the wiring of SW pin to avoid unstable operations.
- Make the GND pattern as wide as possible.
- Place thermal vias in the GND pattern to ensure sufficient heat dissipation.
- Large current flows through the SW pin. Make the wiring area of the pattern to be connected to the SW pin small to minimize parasitic capacitance and emission noise.
- Make a short loop wiring of the SW pin $\rightarrow \mathrm{L} \rightarrow$ Cout $\rightarrow$ VSS pin. This is effective to reduce emission noise.
- Do not wire the SW pin pattern under the IC.


Figure 12 Reference Board Pattern

Caution The above pattern diagram does not guarantee successful operation. Perform thorough evaluation using the actual application to determine the pattern.

## ■ Related Source

Refer to the following application note for recommended noise suppression parts and board layouts that help reduce conductive noise and emission noise for the S-19902/19903 Series.
This application note also summarizes CISPR25 compliant measurement results.

## S-19902/19903 Series NOISE COUNTERMEASURES AND CISPR25 MEASUREMENT RESULTS Application Note

## ■ Precautions

- Mount external capacitors and inductors as close as possible to the IC, and make single GND.
- Characteristic ripple voltage and spike noise occur in the IC containing switching regulators. Moreover rush current flows at the time of a power supply injection. Because these largely depend on the inductor, the capacitor and impedance of power supply to be used, fully check them using an actually mounted model.
- The $4.7 \mu \mathrm{~F}$ capacitor connected between the VIN pin and the VSS pin is a bypass capacitor. It stabilizes the power supply in the IC, and thus effectively works for stable switching regulator operation. Allocate the bypass capacitor as close to the IC as possible, prioritized over other parts.
- Although the IC contains a static electricity protection circuit, static electricity or voltage that exceeds the limit of the protection circuit should not be applied.
- The power dissipation of the IC greatly varies depending on the size and material of the board to be connected. Perform sufficient evaluation using an actual application before designing.
- ABLIC Inc. assumes no responsibility for the way in which this IC is used on products created using this IC or for the specifications of that product, nor does ABLIC Inc. assume any responsibility for any infringement of patents or copyrights by products that include this IC either in Japan or in other countries.


## ■ Characteristics (Typical Data)

1. Example of major power supply dependence characteristics ( $\mathrm{Ta}=+25^{\circ} \mathrm{C}$ )
2. 1 Current consumption during switching off (Iss) vs. Input voltage (Viv)

1.2 Current consumption during shutdown (Isss) vs. Input voltage (Vin)

1.1.2 S-19903 Series

3. 3 FB pin voltage ( $\mathrm{V}_{\mathrm{FB}}$ ) vs. Input voltage ( $\mathrm{V}_{\mathrm{IN}}$ )

4. 4 Oscillation frequency (fosc) vs. Input voltage (Vı)

5. 5 Soft-start wait time (tssw) vs. Input voltage (Vin)

6. 6 Soft-start time (tss) vs. Input voltage (Vin)

7. 7 High side power MOS FET on-resistance (RHFET) vs. Input voltage (VIN)

8. 9 High side power MOS FET leakage current (Insw) vs. Input voltage (Vin)

9. 11 Limit current (lisim) vs. Input voltage (ViN)

10. 12 High level input voltage $\left(\mathrm{V}_{\text {SH }}\right)$ vs. Input voltage ( $\mathrm{V}_{\mathrm{IN}}$ )

11. 8 Low side power MOS FET on-resistance (RLFET)
vs. Input voltage (Vin)

12. 10 Low side power MOS FET leakage current (ILsw) vs. Input voltage ( $\mathrm{V}_{\mathrm{IN}}$ )

13. 13 Low level input voltage ( $\mathrm{V}_{\mathrm{sL}}$ ) vs. Input voltage ( $\mathrm{V}_{\mathrm{IN}}$ )

14. Example of major temperature characteristics ( $\mathrm{Ta}=-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ )
15. 1 Current consumption during switching off (Iss) vs. Temperature (Ta)
16. 17. 1 S-19902 Series

1. 2 Current consumption during shutdown (Isss) vs. Temperature ( Ta )

2. 4 Oscillation frequency (fosc) vs. Temperature (Ta)

2.5 UVLO detection voltage (VuvLo-) vs. Temperature (Ta)

2.1.2 S-19903 Series

3. 3 FB pin voltage ( $\mathrm{V}_{\mathrm{FB}}$ ) vs. Temperature ( Ta )

4. 6 UVLO release voltage (VuvLo+) vs. Temperature ( Ta )


## 2. 7 Soft-start wait time (tssw) vs. Temperature (Ta)


2. 9 High side power MOS FET on-resistance ( $\mathrm{R}_{\mathrm{hFET}}$ ) vs. Temperature (Ta)

2. 11 High side power MOS FET leakage current (lHsw) vs. Temperature (Ta)

2. 13 Limit current (ILim) vs. Temperature ( Ta )
2. 8 Soft-start time (tss) vs. Temperature ( Ta )

2. 10 Low side power MOS FET on-resistance (RLFET) vs. Temperature (Ta)

2. 12 Low side power MOS FET leakage current (LLsw) vs. Temperature (Ta)

2. 14 High level input voltage ( $\mathrm{V}_{\mathrm{SH}}$ ) vs. Temperature ( Ta ) 2. 15 Low level input voltage ( $\mathrm{V}_{\mathrm{SL}}$ ) vs. Temperature ( Ta )


3. EN pin characteristics $\left(\mathrm{Ta}=+25^{\circ} \mathrm{C}\right)$
3. 1 High level input current (Ish) vs. EN pin voltage (VEN)


## 4. Transient response characteristics

The external parts shown in Table 17 are used in "4. Transient response characteristics".

Table 17

| Element Name | Constant | Manufacturer | Part Number |
| :--- | :---: | :--- | :--- |
| Inductor | $4.7 \mu \mathrm{H}$ | TDK Corporation | CLF5030NIT-4R7N-D |
| Input capacitor | $4.7 \mu \mathrm{~F}$ | TDK Corporation | CGA5L3X7R1H475K160AB |
| Output capacitor | $10 \mu \mathrm{~F}$ | TDK Corporation | CGA5L1X7R1C106K160AC |

4. 1 Power-on (VOUT $=5.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=\mathrm{V}_{\text {EN }}=0 \mathrm{~V} \rightarrow 12 \mathrm{~V}, \mathrm{Ta}=+25^{\circ} \mathrm{C}$ )

5. 2 Transient response characteristics of EN pin
(Vout $=5.0 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=12 \mathrm{~V}, \mathrm{~V}_{\text {EN }}=0 \mathrm{~V} \rightarrow 2 \mathrm{~V}, \mathrm{Ta}=+25^{\circ} \mathrm{C}$ )

6. 3 Power supply fluctuation ( $\mathrm{V}_{\text {OUt }}=5.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=12 \mathrm{~V} \rightarrow 16 \mathrm{~V} \rightarrow 12 \mathrm{~V}, \mathrm{Ta}=+25^{\circ} \mathrm{C}$ )

7. 4 Load fluctuation ( $\mathrm{V}_{\text {out }}=5.0 \mathrm{~V}, \mathrm{Ta}=+25^{\circ} \mathrm{C}$ )



## ■ Reference Data

The external parts shown in Table 18 are used in "■ Reference Data".

Table 18

| Condition | Inductor $(\mathrm{L})$ | Input Capacitor (Cin) | Output Capacitor (Cout) |
| :---: | :--- | :--- | :--- |
| $<1>$ | CLF5030NIT-4R7N-D $(4.7 \mu \mathrm{H})$ <br> TDK Corporation | CGA5L3X7R1H475K160AB (4.7 $\mu \mathrm{F})$ <br> TDK Corporation | CGA5L1X7R1C106K160AC $(10 \mu \mathrm{~F})$ <br> TDK Corporation |
| $<2>$ | CLF5030NIT-3R3N-D $(3.3 \mu \mathrm{H})$ <br> TDK Corporation | CGA5L3X7R1H475K160AB (4.7 $\mu \mathrm{F})$ <br> TDK Corporation | $\left.\begin{array}{l}\text { CGA5L1X7R1C106K160AC }(10 ~\end{array} \mathrm{FF}\right)$ |
| TDK Corporation |  |  |  |

1. Vout $=5.0 \mathrm{~V}$ (External parts: Condition<1>)
2. 1 Efficiency $(\eta)$ vs. Output current (lout)
3. 4. S -19902 Series

1.1.2 S-19903 Series

1.2 Output voltage (Vout) vs. Output current (lout)
1. 2. 1 S-19902 Series

1. 3 Ripple voltage ( $\Delta \mathrm{V}_{\text {out }}$ vs. Output current (lout)
2. 3. 1 S-19902 Series

1.3.2 S-19903 Series

1. Vout $=3.3$ V (External parts: Condition<2>)
2. 1 Efficiency $(\eta)$ vs. Output current (lout)
2.1.1 S-19902 Series

3. 2 Output voltage (Vout) vs. Output current (lout)
4. 2. 1 S-19902 Series

1. 3 Ripple voltage ( $\Delta \mathrm{V}_{\text {out }}$ ) vs. Output current (lout)
2. 3. 1 S-19902 Series

1. Load dump characteristics $\left(\mathrm{Ta}=+25^{\circ} \mathrm{C}\right)$
2. $1 \mathrm{~V}_{\text {OUt }}=5.0 \mathrm{~V}$



3. 2. 2 S-19903 Series


## ■ Power Dissipation

## HTMSOP-8



| Board | Power Dissipation (PD) |
| :---: | :---: |
| A | 0.79 W |
| B | 1.11 W |
| C | 3.21 W |
| D | 3.13 W |
| E | 4.17 W |

HSNT-8(2030)


| Board | Power Dissipation (PD) |
| :---: | :---: |
| A | 0.69 W |
| B | 0.93 W |
| C | 3.13 W |
| D | 2.98 W |
| E | 3.91 W |

## HSNT-6(2025)



| Board | Power Dissipation (PD) |
| :---: | :---: |
| A | 0.69 W |
| B | 0.98 W |
| C | 2.91 W |
| D | 2.84 W |
| E | 3.47 W |

## HTMSOP-8 Test Board

(1) Board A

IC Mount Area


| Item |  | Specification |
| :---: | :---: | :---: |
| Size [mm] |  | $114.3 \times 76.2 \times \mathrm{t} 1.6$ |
| Material |  | FR-4 |
| Number of copper foil layer |  | 2 |
| Copper foil layer [mm] | 1 | Land pattern and wiring for testing: 0.070 |
|  | 2 | - |
|  | 3 | - |
|  | 4 | $74.2 \times 74.2 \times$ t0.070 |
| Thermal via |  | - |

(2) Board B


| Item | Specification |  |  |
| :--- | :--- | :--- | :---: |
| Size $[\mathrm{mm}]$ | $114.3 \times 76.2 \times \mathrm{t1} .6$ |  |  |
| Material | FR-4 |  |  |
| Number of copper foil layer | 4 |  |  |
| Copper foil layer [mm] | 1 | Land pattern and wiring for testing: t0.070 |  |
|  | 2 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |  |
|  | 3 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |  |
|  | 4 | $74.2 \times 74.2 \times \mathrm{t0.070}$ |  |
| Thermal via |  |  |  |

(3) Board C


| Item | Specification |  |
| :--- | ---: | :--- |
| Size $[\mathrm{mm}]$ | $114.3 \times 76.2 \times \mathrm{t} 1.6$ |  |
| Material | FR-4 |  |
| Number of copper foil layer | 4 |  |
| Copper foil layer [mm] | 1 | Land pattern and wiring for testing: t0.070 |
|  | 2 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |
|  | 3 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |
|  | 4 | $74.2 \times 74.2 \times \mathrm{t0.070}$ |
| Thermal via | Number: 4 <br> Diameter: 0.3 mm |  |

enlarged view
No. HTMSOP8-A-Board-SD-1.0

## HTMSOP-8 Test Board

## (5) Board E



| Item | Specification |  |
| :--- | :--- | :--- |
| Size $[\mathrm{mm}]$ | $114.3 \times 76.2 \times \mathrm{t} 1.6$ |  |
| Material | FR-4 |  |
| Number of copper foil layer | 4 |  |
| Copper foil layer $[\mathrm{mm}]$ | 1 | Pattern for heat radiation: $2000 \mathrm{~mm}^{2}$ t0.070 |
|  | 2 | $74.2 \times 74.2 \times \mathrm{t} 0.035$ |
|  | 3 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |
|  | 4 | $74.2 \times 74.2 \times \mathrm{t0.070}$ |
| Thermal via |  | Number: 4 <br> Diameter: 0.3 mm |


| Item | Specification |  |  |  |
| :--- | :--- | :--- | :---: | :---: |
| Size $[\mathrm{mm}]$ | $114.3 \times 76.2 \times \mathrm{t} 1.6$ |  |  |  |
| Material | FR-4 |  |  |  |
| Number of copper foil layer | 4 |  |  |  |
| Copper foil layer [mm] | 1 | Pattern for heat radiation: $2000 \mathrm{~mm}^{2}$ t0.070 |  |  |
|  | 2 | $74.2 \times 74.2 \times \mathrm{t} 0.035$ |  |  |
|  | 3 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |  |  |
|  | 4 | $74.2 \times 74.2 \times \mathrm{t} 0.070$ |  |  |
| Thermal via |  |  |  |  |


enlarged view

No. HTMSOP8-A-Board-SD-1.0

## (1) Board A



| Item | Specification |  |
| :--- | :---: | :--- |
| Size $[\mathrm{mm}]$ | $114.3 \times 76.2 \times \mathrm{t1.6}$ |  |
| Material | FR-4 |  |
| Number of copper foil layer | 2 |  |
| Copper foil layer [mm] | 1 | Land pattern and wiring for testing: t0.070 |
|  | 2 | - |
|  | 3 | - |
|  | 4 | $74.2 \times 74.2 \times \mathrm{t0.070}$ |
| Thermal via |  |  |

(2) Board B


| Item | Specification |  |
| :--- | :---: | :--- |
| Size $[\mathrm{mm}]$ | $114.3 \times 76.2 \times \mathrm{t1.6}$ |  |
| Material | FR-4 |  |
| Number of copper foil layer | 4 |  |
| Copper foil layer [mm] | 1 | Land pattern and wiring for testing: t0.070 |
|  | 2 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |
|  | 3 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |
|  | 4 | $74.2 \times 74.2 \times \mathrm{t} 0.070$ |
| Thermal via |  |  |

## (3) Board C



| Item | Specification |  |
| :--- | :--- | :--- |
| Size $[\mathrm{mm}]$ | $114.3 \times 76.2 \times \mathrm{t} 1.6$ |  |
| Material | FR-4 |  |
| Number of copper foil layer | 4 |  |
| Copper foil layer [mm] | 1 | Land pattern and wiring for testing: t0.070 |
|  | 2 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |
|  | 3 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |
|  | 4 | $74.2 \times 74.2 \times \mathrm{t0.070}$ |
| Thermal via | Number: 4 <br> Diameter: 0.3 mm |  |

No. HSNT8-A-Board-SD-2.0

ABLIC Inc.
(4) Board D


| Item |  | Specification |
| :---: | :---: | :---: |
| Size [mm] |  | $114.3 \times 76.2 \times$ t1.6 |
| Material |  | FR-4 |
| Number of copper foil layer |  | 4 |
| Copper foil layer [mm] | 1 | Pattern for heat radiation: $2000 \mathrm{~mm}^{2}$ t0.070 |
|  | 2 | $74.2 \times 74.2 \times$ t0.035 |
|  | 3 | $74.2 \times 74.2 \times$ t0.035 |
|  | 4 | $74.2 \times 74.2 \times$ t0.070 |
| Thermal via |  | - |


enlarged view

## (5) Board E



| Item | Specification |  |
| :--- | :---: | :--- |
| Size $[\mathrm{mm}]$ | $114.3 \times 76.2 \times \mathrm{t} 1.6$ |  |
| Material | FR-4 |  |
| Number of copper foil layer | 4 |  |
| Copper foil layer $[\mathrm{mm}]$ | 1 | Pattern for heat radiation: $2000 \mathrm{~mm}^{2}$ t0.070 |
|  | 2 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |
|  | 3 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |
|  | 4 | $74.2 \times 74.2 \times \mathrm{t0.070}$ |
| Thermal via |  |  |

enlarged view

No. HSNT8-A-Board-SD-2.0

## (1) Board A

IC Mount Area

| Item | Specification |  |
| :--- | :--- | :--- |
| Size $[\mathrm{mm}]$ | $114.3 \times 76.2 \times \mathrm{t1.6}$ |  |
| Material | FR-4 |  |
| Number of copper foil layer | 2 |  |
| Copper foil layer [mm] | 1 | Land pattern and wiring for testing: t0.070 |
|  | 2 | - |
|  | 3 | - |
|  | 4 | $74.2 \times 74.2 \times$ t0.070 |
| Thermal via |  |  |

(2) Board B


| Item | Specification |  |  |  |
| :--- | :--- | :--- | :---: | :---: |
| Size $[\mathrm{mm}]$ | $114.3 \times 76.2 \times \mathrm{t1} .6$ |  |  |  |
| Material | FR-4 |  |  |  |
| Number of copper foil layer | 4 |  |  |  |
| Copper foil layer [mm] | 1 | Land pattern and wiring for testing: t0.070 |  |  |
|  | 2 | $74.2 \times 74.2 \times \mathrm{t} 0.035$ |  |  |
|  | 3 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |  |  |
|  | 4 | $74.2 \times 74.2 \times \mathrm{t} 0.070$ |  |  |
| Thermal via |  |  |  |  |

## (3) Board C



| Item | Specification |  |
| :--- | ---: | :--- |
| Size $[\mathrm{mm}]$ | $114.3 \times 76.2 \times \mathrm{t1} .6$ |  |
| Material | FR-4 |  |
| Number of copper foil layer | 4 |  |
| Copper foil layer [mm] | 1 | Land pattern and wiring for testing: t0.070 |
|  | 2 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |
|  | 3 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |
|  | 4 | $74.2 \times 74.2 \times \mathrm{t0.070}$ |
| Thermal via | Number: 4 <br> Diameter: 0.3 mm |  |



| Item | Specification |  |  |
| :--- | :--- | :--- | :---: |
| Size $[\mathrm{mm}]$ | $114.3 \times 76.2 \times \mathrm{t} 1.6$ |  |  |
| Material | FR-4 |  |  |
| Number of copper foil layer | 4 |  |  |
| Copper foil layer $[\mathrm{mm}]$ | 1 | Pattern for heat radiation: $2000 \mathrm{~mm}^{2}$ t0.070 |  |
|  | 2 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |  |
|  | 3 | $74.2 \times 74.2 \times \mathrm{t0} 0.035$ |  |
|  | 4 | $74.2 \times 74.2 \times \mathrm{t0.070}$ |  |
| Thermal via |  |  |  |


enlarged view

## (5) Board E



| Item | Specification |  |
| :--- | :--- | :--- |
| Size $[\mathrm{mm}]$ | $114.3 \times 76.2 \times \mathrm{t} 1.6$ |  |
| Material | FR-4 |  |
| Number of copper foil layer | 4 |  |
| Copper foil layer $[\mathrm{mm}]$ | 1 | Pattern for heat radiation: $2000 \mathrm{~mm}^{2} \mathrm{t} 0.070$ |
|  | 2 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |
|  | 3 | $74.2 \times 74.2 \times \mathrm{t0.035}$ |
|  | 4 | $74.2 \times 74.2 \times \mathrm{t} 0.070$ |
| Thermal via |  | Number: 4 <br> Diameter: 0.3 mm |

No. HSNT6-B-Board-SD-1.0

ABLIC Inc.


No. FP008-A-P-SD-2.0

| TITLE | HTMSOP8-A-PKG Dimensions |
| :---: | :---: |
| No. | FP008-A-P-SD-2.0 |
| ANGLE | $\square$ |
| UNIT | mm |
|  |  |
|  |  |
| ABLIC Inc. |  |



No. FP008-A-C-SD-1.0

| TITLE | HTMSOP8-A-Carrier Tape |
| :---: | :---: |
| No. | FP008-A-C-SD-1.0 |
| ANGLE |  |
| UNIT | mm |
|  |  |
|  |  |
| ABLIC Inc. |  |


$\underline{\text { Enlarged drawing in the central part }}$


No. FP008-A-R-SD-1.0

| TITLE | HTMSOP8-A-Reel |  |
| :---: | :---: | :---: |
| No. | FP008-A-R-SD-1.0 |  |
| ANGLE |  | QTY. |
| UNIT | mm | 4,000 |
|  |  |  |
|  |  |  |
| ABLIC Inc. |  |  |



No. FP008-A-L-SD-2.0

| TITLE | HTMSOP8-A <br> -Land Recommendation |
| :---: | :---: |
| No. | FP008-A-L-SD-2.0 |
| ANGLE |  |
| UNIT | mm |
|  |  |
|  |  |
| ABLIC Inc. |  |





※ The heat sink of back side has different electric potential depending on the product.
Confirm specifications of each product.
Do not use it as the function of electrode.
No. PP008-A-P-SD-2.0

| TITLE | HSNT-8-A-PKG Dimensions |
| :---: | :---: |
| No. | PP008-A-P-SD-2.0 |
| ANGLE | ¢ |
| UNIT | mm |
|  |  |
|  |  |
| ABLIC Inc. |  |



Feed direction

No. PP008-A-C-SD-1.0

| TITLE | HSNT-8-A-Carrier Tape |
| :---: | :---: |
| No. | PP008-A-C-SD-1.0 |
| ANGLE |  |
| UNIT | mm |
|  |  |
|  |  |
| ABLIC Inc. |  |



Enlarged drawing in the central part


No. PP008-A-R-SD-1.0

| TITLE | HSNT-8-A-Reel |  |  |
| :---: | :---: | :---: | :---: |
| No. | PP008-A-R-SD-1.0 |  |  |
| ANGLE | QTY. |  |  |
| UNIT | mm |  |  |
|  |  |  |  |
|  |  |  |  |
| ABLIC Inc. |  |  |  |



No. PP008-A-L-SD-1.0

| TITLE | HSNT-8-A <br> -Land Recommendation |
| :---: | :---: |
| No. | PP008-A-L-SD-1.0 |
| ANGLE |  |
| UNIT | mm |
|  |  |
|  |  |
| ABLIC Inc. |  |


※ The heat sink of back side has different electric potential depending on the product.
Confirm specifications of each product.
Do not use it as the function of electrode.

No. PJ006-B-P-SD-1.0

| TITLE | HSNT-6-C-PKG Dimensions |
| :---: | :---: |
| No. | PJ006-B-P-SD-1.0 |
| ANGLE | $\rightarrow$ |
| UNIT | mm |
|  |  |
|  |  |
| ABLIC Inc. |  |



No. PJ006-B-C-SD-1.0

| TITLE | HSNT-6-C-Carrier Tape |
| :---: | :---: |
| No. | PJ006-B-C-SD-1.0 |
| ANGLE |  |
| UNIT | mm |
|  |  |
|  |  |
| ABLIC Inc. |  |



Enlarged drawing in the central part


No. PJ006-B-R-SD-1.0

| TITLE | HSNT-6-C-Reel |  |
| :---: | :---: | :---: |
|  | PJ006-B-R-SD-1.0 |  |
| ANGLE |  | QTY. |
| UNIT | mm |  |
|  |  |  |
|  |  |  |
| ABLIC Inc. |  |  |

## Land Recommendation



Caution It is recommended to solder the heat sink to a board in order to ensure the heat radiation．
注意 放熱性を確保する為に，PKGの裏面放熱板（ヒートシンク）を基板に半田付けする事を推奨いたします。

## Stencil Opening



No．PJ006－B－LM－SD－1．0

Caution（1）Mask aperture ratio of the lead mounting part is 100～120\％．
（2）Mask aperture ratio of the heat sink mounting part is $30 \%$ ．
（3）Mask thickness： 0.12 mm
（4）Reflow atmosphere：Nitrogen atmosphere is recommended． （Oxygen concentration：1000ppm or less）

注意（1）リード実装部のマスク開口率は100～120\％です。
②放熱板実装のマスク開口率は30\％です。
（3）マスク厚み： t 0.12 mm
（4）リフロー雰囲気•窒素雾囲気（酸素濃度1000ppm以下）推奨

| TITLE | HSNT－6－C <br> －Land \＆Stencil Opening |
| :---: | :---: |
| No． | PJ006－B－LM－SD－1．0 |
| ANGLE |  |
| UNIT | mm |
|  |  |
|  |  |
| ABLIC Inc． |  |

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