

ACT4060A

Wide Input 2 A Step Down Converter

FEATURES

- 2 A Output Current
- Up to 96% Efficiency
- 4.5 V to 24 V Input Range
- 10 μA Shutdown Supply Current
- 400 kHz Switching Frequency
- Adjustable Output Voltage
- Cycle-by-Cycle Current Limit Protection
- Thermal Shutdown Protection
- Frequency Foldback at Short Circuit
- Stability with Wide Range of Capacitors, Including Low ESR Ceramic Capacitors
- SOP-8 Package

APPLICATIONS

- TFT LCD Monitors
- Portable DVDs
- Car-Powered or Battery-Powered Equipment
- Set-Top Boxes
- Telecom Power Supplies
- DSL and Cable Modems and Routers
- Termination Supplies

GENERAL DESCRIPTION

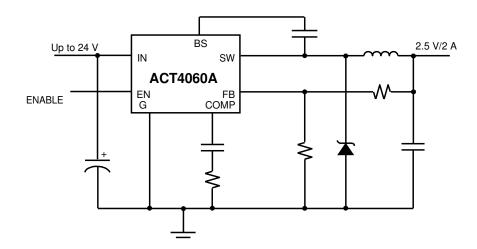
The ACT4060A is a current-mode step-down DC/DC converter that provides up to 2 A of output current at 400kHz switching frequency. The device utilizes Active-Semi's proprietary high voltage process for operation with input voltages up to 24 V.

The ACT4060A provides fast transient response and eases loop stabilization while providing excellent line and load regulation. This device features a very low ON-resistance power MOSFET which provides peak operating efficiency up to 96%. In shutdown mode, the ACT4060A consumes only 10 μ A of supply current.

This device also integrates protection features including cycle-by-cycle current limit, thermal shutdown and frequency fold-back at short circuit.

The ACT4060A is available in a SOP-8 package and requires very few external devices for operation.

TYPICAL APPLICATION CIRCUIT

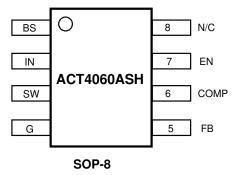




ORDERING INFORMATION

| PART NUMBER | TEMPERATURE RANGE | PACKAGE | PINS | PACKING |
|--------------|-------------------|---------|------|-------------|
| ACT4060ASH | -40 °C to 85 °C | SOP-8 | 8 | TUBE |
| ACT4060ASH-T | -40 °C to 85 °C | SOP-8 | 8 | TAPE & REEL |

PIN CONFIGURATION



PIN DESCRIPTIONS

| PIN | NAME | DESCRIPTION | |
|---|--|---|--|
| 1 | Bootstrap. This pin acts as the positive rail for the high-side switch's gate drive 10nF capacitor between BS and SW. | | |
| 2 | Input Supply. Bypass this pin to G with a low ESR capacitor. See <i>Input Capacitor</i> in the <i>Application Information</i> section. | | |
| 3 | SW | Switch Output. Connect this pin to the switching end of the inductor. | |
| 4 G Gro | | Ground. | |
| | | Feedback Input. The voltage at this pin is regulated to 1.293V. Connect to the resistor divider between output and ground to set output voltage. | |
| 6 COMP Compensation Pin. See Stability Compensation in the Application. | | Compensation Pin. See Stability Compensation in the Application Information section. | |
| | | Enable Input. When higher than 1.3V, this pin turns the IC on. When lower than 0.7V, this pin turns the IC off. Output voltage is discharged when the IC is off. When left unconnected, EN is pulled up to 4.5V with a 2μA pull-up current. | |
| 8 N/C Not Connected. | | Not Connected. | |



ABSOLUTE MAXIMUM RATINGS[®]

| PARAMETER | VALUE | UNIT |
|---|--------------------------------|------|
| IN Supply Voltage | -0.3 to 28 | V |
| SW Voltage | -1 to V _{IN} + 1 | V |
| BS Voltage | V_{SW} - 0.3 to V_{SW} + 8 | V |
| EN, FB, COMP Voltage | -0.3 to 6 | V |
| Continuous SW Current | Internally Limited | А |
| Junction to Ambient Thermal Resistance (θ _{JA}) | 105 | °C/W |
| Maximum Power Dissipation | 0.76 | W |
| Operating Junction Temperature | -40 to 150 | °C |
| Storage Temperature | -55 to 150 | °C |
| Lead Temperature (Soldering, 10 sec) | 300 | °C |

①: Do not exceed these limits to prevent damage to the device. Exposure to absolute maximum rating conditions for long periods may affect device reliability.

ELECTRICAL CHARACTERISTICS

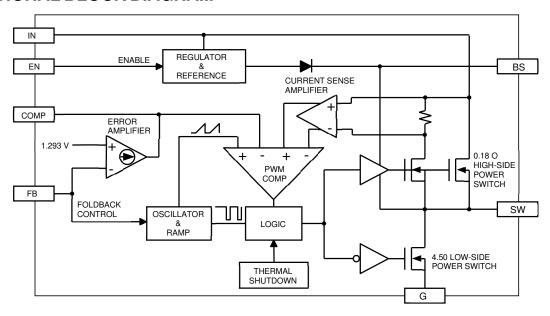
 $(V_{IN} = 12V, T_A = 25^{\circ}C, unless otherwise specified.)$

| PARAMETER | SYMBOL | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
|---|-------------------|---|-------|-------|-------|---------------|
| Input Voltage | V _{IN} | $V_{OUT} = 3.3V$, $I_{LOAD} = 0A$ to 1A | 4.5 | | 24 | ٧ |
| Feedback Voltage | V_{FB} | $4.5V \le V_{IN} \le 24V, V_{COMP} = 1.5V$ | 1.267 | 1.293 | 1.319 | ٧ |
| High-Side Switch On Resistance | R _{ONH} | | | 0.18 | | Ω |
| Low-Side Switch On Resistance | R _{ONL} | | | 4.5 | | Ω |
| SW Leakage | | $V_{EN} = 0$ | | 0 | 10 | μΑ |
| Current Limit | I _{LIM} | | 2.4 | 2.85 | | Α |
| COMP to Current Limit Transconductance | G _{COMP} | $V_{IN} = 12V, V_{OUT} = 5V$ | | 1.8 | | A/V |
| Error Amplifier Transconductance | G_{EA} | $\Delta I_{COMP} = \pm 10 \mu A$ | | 650 | | μ A /V |
| Error Amplifier DC Gain | A_{VEA} | | | 4000 | | V/V |
| Switching Frequency | f _{SW} | | 350 | 400 | 450 | kHz |
| Short Circuit Switching Frequency | | $V_{FB} = 0$ | | 60 | | kHz |
| Maximum Duty Cycle | D_{MAX} | V _{FB} = 1.1V | | 95 | | % |
| Minimum Duty Cycle | | V _{FB} = 1.4V | | | 0 | % |
| Enable Threshold Voltage | | Hysteresis = 0.1V | 0.7 | 1 | 1.3 | ٧ |
| Enable Pull-Up Current | | Pin pulled up to 4.5V typically when left unconnected | | 2 | | μΑ |
| Supply Current in Shutdown | | $V_{EN} = 0$ | | 10 | 20 | μΑ |
| IC Supply Current in Operation | | $V_{EN} = 3V$, $V_{FB} = 1.4V$ | | 0.55 | | mA |
| Thermal Shutdown Temperature | | Hysteresis = 10°C | | 160 | | °C |





FUNCTIONAL BLOCK DIAGRAM



FUNCTIONAL DESCRIPTION

As seen in *Functional Block Diagram*, the ACT4060A is a current mode pulse width modulation (PWM) converter. The converter operates as follows:

A switching cycle starts when the rising edge of the Oscillator clock output causes the High-Side Power Switch to turn on and the Low-Side Power Switch to turn off. With the SW side of the inductor now connected to IN, the inductor current ramps up to store energy in the magnetic field. The inductor current level is measured by the Current Sense Amplifier and added to the Oscillator ramp signal. If the resulting summation is higher than the COMP voltage, the output of the PWM Comparator goes high. When this happens or when Oscillator clock output goes low, the High-Side Power Switch turns off and the Low-Side Power Switch turns on. At this point, the SW side of the inductor swings to a diode voltage below ground, causing the inductor current to decrease and magnetic energy to be transferred to output. This state continues until the cycle starts again.

The High-Side Power Switch is driven by logic using BS as the positive rail. This pin is charged to $V_{SW} + 6\ V$ when the Low-Side Power Switch turns on.

The COMP voltage is the integration of the error between FB input and the internal 1.293 V

reference. If FB is lower than the reference voltage, COMP tends to go higher to increase current to the output. Current limit happens when COMP reaches its maximum clamp value of 2.55 V.

The Oscillator normally switches at 400kHz. However, if FB voltage is less than 0.7 V, then the switching frequency decreases until it reaches a typical value of 60 kHz at $V_{\text{FB}} = 0.5 \text{ V}$.

Shutdown Control

The ACT4060A has an enable input EN for turning the IC on or off. When EN is less than 0.7V, the IC is in $10\mu A$ low current shutdown mode and output is discharged through the Low-Side Power Switch. When EN is higher than 1.3V, the IC is in normal operation mode. EN is internally pulled up with a $2\mu A$ current source and can be left unconnected for always-on operation. Note that EN is a low voltage input with a maximum voltage of 6V, it should never be directly connected to IN.

Thermal Shutdown

The ACT4060A automatically turns off when its junction temperature exceeds 160 $^{\circ}\text{C}.$

APPLICATIONS INFORMATION

Output Voltage Setting

Figure 1:

Output Voltage Setting

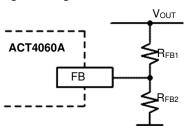


Figure 1 shows the connections for setting the output voltage. Select the proper ratio of the two feedback resistors R_{FB1} and R_{FB2} based on the output voltage. Typically, use $R_{FB2}\approx 10~k\Omega$ and determine R_{FB1} from the following equation:

$$R_{FB1} = R_{FB2} \left(\frac{V_{OUT}}{1.293V} - 1 \right) \tag{1}$$

Inductor Selection

The inductor maintains a continuous current to the output load. This inductor current has a ripple that is dependent on the inductance value: higher inductance reduces the peak-to-peak ripple current. The trade off for high inductance value is the increase in inductor core size and series resistance, and the reduction in current handling capability. In general, select an inductance value L based on ripple current requirement:

$$L = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{V_{IN} f_{SW} I_{OUTMAX} K_{RIPPLE}}$$
 (2)

where V_{IN} is the input voltage, V_{OUT} is the output voltage, fSW is the switching frequency, IOUTMAX is the maximum output current, and KRIPPLE is the ripple factor. Typically, choose KRIPPLE = 30% to correspond to the peak-to-peak ripple current being 30% of the maximum output current.

With this inductor value, the peak inductor current is $I_{OUT} \times (1 + KRIPPLE/2)$. Make sure that this peak inductor current is less that the 3 A current limit. Finally, select the inductor core size so that it does not saturate at 3 A. Typical inductor values for various output voltages are shown in Table 1.

Table 1:

Typical Inductor Values

| Vout | 1.5 V | 1.8 V | 2.5 V | 3.3 V | 5 V |
|------|--------|--------|-------|-------|-------|
| L | 6.8 µH | 6.8 µH | 10 µH | 15 µH | 22 µH |

Input Capacitor

The input capacitor needs to be carefully selected to

Data Sheet Rev. C, September 2019 | Subject to change without notice

maintain sufficiently low ripple at the supply input of the converter. A low ESR capacitor is highly recommended. Since large current flows in and out of this capacitor during switching, its ESR also affects efficiency.

The input capacitance needs to be higher than 10 μ F. The best choice is the ceramic type, however, low ESR tantalum or electrolytic types may also be used provided that the RMS ripple current rating is higher than 50% of the output current. The input capacitor should be placed close to the IN and G pins of the IC, with the shortest traces possible. In the case of tantalum or electrolytic types, they can be further away if a small parallel 0.1 μ F ceramic capacitor is placed right next to the IC.

Output Capacitor

The output capacitor also needs to have low ESR to keep low output voltage ripple. The output ripple voltage is:

$$V_{RIPPLE} = I_{LPK-PK} \times (R_{ESR} + \frac{1}{8 \times f_{SW} \times C_{OUT}})$$
 (3)

where Ioutmax is the maximum output current, Kripple is the ripple factor, Resr is the ESR of the output capacitor, fSW is the switching frequency, L is the inductor value, and Cout is the output capacitance. In the case of ceramic output capacitors, RESR is very small and does not contribute to the ripple Therefore, a lower capacitance value can be used for ceramic type. In the case of tantalum or electrolytic capacitors, the ripple is dominated by RESR multiplied by the ripple current. In that case, the output capacitor is chosen to have sufficiently low ESR.

For ceramic output capacitor, typically choose a capacitance of about 22 μF . For tantalum or electrolytic capacitors, choose a capacitor with less than 50 m Ω ESR

Rectifier Diode

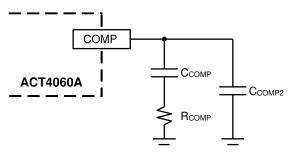
Use a Schottky diode as the rectifier to conduct current when the High-Side Power Switch is off. The Schottky diode must have current rating higher than the maximum output current and a reverse voltage rating higher than the maximum input voltage.



STABILITY COMPENSATION

Figure 2:

Stability Compensation



①: C_{COMP2} is needed only for high ESR output capacitor

The feedback loop of the IC is stabilized by the components at the COMP pin, as shown in Figure

2. The DC loop gain of the system is determined by the following equation:

$$A_{VDC} = \frac{1.3V}{I_{OUT}} A_{VEA} G_{COMP} \tag{4}$$

The dominant pole P1 is due to CCOMP:

$$f_{P1} = \frac{G_{EA}}{2\pi A_{VEA} C_{COMP}} \tag{5}$$

The second pole P2 is the output pole:

$$f_{P2} = \frac{I_{OUT}}{2\pi V_{OUT} C_{OUT}} \tag{6}$$

The first zero Z1 is due to RCOMP and CCOMP:

$$f_{Z1} = \frac{1}{2\pi R_{COMP} C_{COMP}} \tag{7}$$

And finally, the third pole is due to R_{COMP} and C_{COMP2} (if C_{COMP2} is used):

$$f_{P3} = \frac{1}{2\pi \, R_{COMP} \, C_{COMP2}} \tag{8}$$

The following steps should be used to compensate the IC:

STEP 1. Set the cross over frequency at 1/10 of the switching frequency via R_{COMP} :

$$R_{COMP} = \frac{2\pi V_{OUT} C_{OUT} f_{SW}}{10 G_{EA} G_{COMP} \times 1.3V}$$

$$= 1.7 \times 10^8 V_{OUT} C_{OUT} (\Omega)$$
(9)

but limit R_{COMP} to 15 k Ω maximum.

STEP 2. Set the zero f_{Z1} at 1/4 of the cross over frequency. If R_{COMP} is less than 15 $k\Omega$, the equation for

C_{COMP} is:

$$C_{COMP} = \frac{1.8 \times 10^{-5}}{R_{COMP}} \quad (F) \tag{10}$$

If R_{COMP} is limited to 15 k Ω , then the actual cross over frequency is 3.4 / ($V_{OUT}C_{OUT}$). Therefore:

$$C_{COMP} = 1.2 \times 10^{-5} V_{OUT} C_{OUT} (F)$$
 (11)

STEP 3. If the output capacitor's ESR is high enough to cause a zero at lower than 4 times the cross over frequency, an additional compensation capacitor C_{COMP2} is required. The condition for using C_{COMP2} is:

$$R_{ESRCOUT} \ge Min\left(\frac{1.1 \times 10^{-6}}{C_{OUT}}, 0.012 \times V_{OUT}\right) (\Omega)$$
 (12)

And the proper value for CCOMP2 is:

$$C_{COMP2} = \frac{C_{OUT} R_{ESRCOUT}}{R_{COMP}} \tag{13}$$

Though C_{COMP2} is unnecessary when the output capacitor has sufficiently low ESR, a small value C_{COMP2} such as 100 pF may improve stability against PCB layout parasitic effects.

Table 2 shows some calculated results based on the compensation method above.

Table 2:

Typical Compensation for Different Output Voltages and Output Capacitors

| V _{OUT} | C _{OUT} | R _{COMP} | C _{COMP} |
|------------------|--------------------|-------------------|-------------------|
| 2.5 V | 22 μF Ceramic | 8.2 kΩ | 2.2 nF |
| 3.3 V | 22 μF Ceramic | 12 kΩ | 1.5 nF |
| 5 V | 22 μF Ceramic | 15 kΩ | 1.5 nF |
| 2.5 V | 47 μF SP CAP | 15 kΩ | 1.5 nF |
| 3.3 V | 47 μF SP CAP | 15 kΩ | 1.8 nF |
| 5 V | 47 μF SP CAP | 15 kΩ | 2.7 nF |
| 2.5 V | 470 μF/6.3 V/30 mΩ | 15 kΩ | 15 nF |
| 3.3 V | 470 μF/6.3 V/30 mΩ | 15 kΩ | 22 nf |
| 5 V | 470 μF/6.3 V/30 mΩ | 15 kΩ | 22 nF |

Figure 4 shows an example ACT4060A application circuit generating a $3.3\ V/2\ A$ output.

ACT4060A PCB Layout Guidelines.

Place all the power components (Diode, Inductor, filter Capacitors) as close as possible. Use short and wide trace between them.



If double layer PCB is used, it is good if the bottom layer is almost fill as ground. Use ground planes for power ground and signal ground, connect signal ground and power ground at single point close to the IC GND.

Arrange the power components so that the switching current loop curl in the same direction.

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Separate noise sensitive traces, such as the voltage feedback path, compensation from noisy sources such as inductor, diode, input capacitor.

Place components, such as compensation, feedback network and boost-trap capacitors, as close to the IC as possible.

Ceramic cap C1 is closely placed across V_{IN} and GND of the IC, as close as possible.

Figure 3: ACT4060A PCB Layout Reference

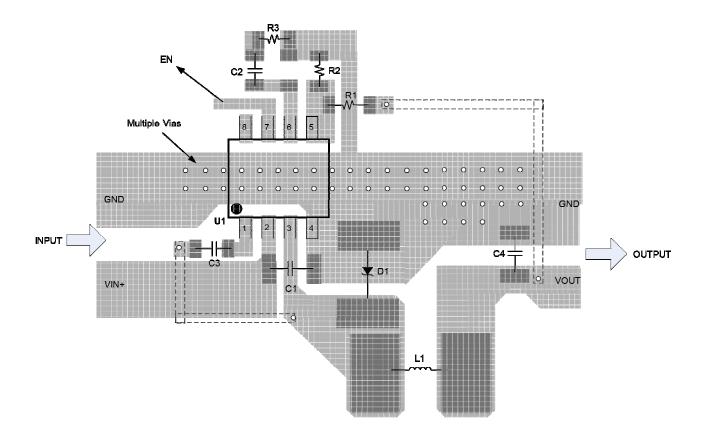
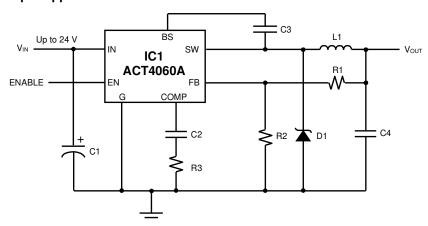




Figure 4: ACT4060A 3.3V/2A Output Application[®]



①: D1 is a 40V, 3A Schottky diode with low forward voltage, an IR 30BQ040 or SK34 equivalent. C4 can be either a ceramic capacitor (Panasonic ECJ-3YB1C226M) or SP-CAP (Specialty Polymer) Aluminum Electrolytic Capacitor such as Panasonic EEFCD0J470XR. The SP-Cap is based on aluminum electrolytic capacitor technology, but uses a solid polymer electrolyte and has very stable capacitance characteristics in both operating temperature and frequency compared to ceramic, polymer, and low ESR tantalum capacitors.

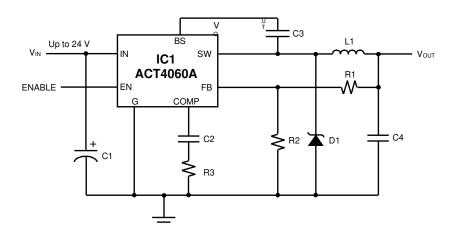
Table 3: ACT4060A Bill of Materials (Apply for 3.3V Output Application)

| ITEM | DESCRIPTION | MANUFACTURER | QTY | REFERENCE |
|------|--|----------------------------|-----|-----------|
| 1 | IC, ACT4060A | Active-Semi | 1 | U1 |
| | $15\mu H \pm 20\%$, $I_{SAT} = 2.7A$, $I_{DC} = 2.4A@ \Delta T = 40°C$ | Taiyo Yuden NR 8040T 150M | | |
| 2 | $15\mu H \pm 10\%$, $I_{SAT} = 2.88A$, $I_{DC} = 2.47A @ \Delta T = 40 °C$ | Wurth Electronik 744776115 | 4 | |
| 2 | $10\mu H \pm 20\%$, $I_{SAT} = 3.4A$, $I_{DC} = 2.5A@\Delta T = 40°C$ | Taiyo Yuden NR 6045T 100M | ı | L1 |
| | $10\mu H \pm 10\%$, $I_{SAT} = 2.95A$, $I_{DC} = 2.3A@ \Delta T = 40°C$ | Wurth Electronik 74477510 | | |
| 3 | Schottky Diode SK34/40V, 3A, SMB | Transys electronics | 1 | D1 |
| 3 | Schottky Diode B340C/40V, 3A, SMB | Diodes Inc | 1 | - D1 |
| 4 | Ceramic cap 10µF/35V, X7R, 1210 | Murata, TDK, Taiyo Yuden | 1 | C1 |
| 5 | Ceramic cap 2.2nF/6.3V, X7R, 0603 | Murata, TDK, Taiyo Yuden | 1 | C2 |
| 6 | Ceramic cap 10nF/50V, X7R, 0603 | Murata, TDK, Taiyo Yuden | 1 | C3 |
| 7 | Ceramic cap 22µF/10V, X7R, 1210 | Murata, TDK, Taiyo Yuden | 1 | C4 |
| / | SP cap 47μF/6.3V, 50mΩ | Kemet, Panasonic | | |
| 8 | Resistor, 15.5kΩ, 1/16W, 1%, 0603 | | | R1 |
| 9 | Resistor, 10kΩ, 1/16W, 1%, 0603 | FengHua, Neohm, Yageo | 1 | R2 |
| 10 | Resistor, 12kΩ, 1/16W, 5%, 0603 | | | R3 |





Figure 5: ACT4060A 5V/2A Output Application[®]



①: D1 is a 40V, 3A Schottky diode with low forward voltage, an IR 30BQ040 or SK34 equivalent. C4 can be either a ceramic capacitor (Panasonic ECJ-3YB1C226M) or SP-CAP (Specialty Polymer) Aluminum Electrolytic Capacitor such as Panasonic EEFCD0J470XR. The SP-Cap is based on aluminum electrolytic capacitor technology, but uses a solid polymer electrolyte and has very stable capacitance characteristics in both operating temperature and frequency compared to ceramic, polymer, and low ESR tantalum capacitors.

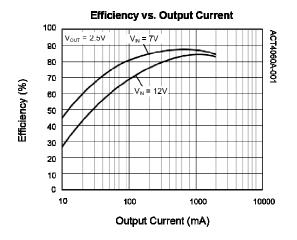
Table 4:
ACT4060A Bill of Materials (Apply for 5 V Output Application)

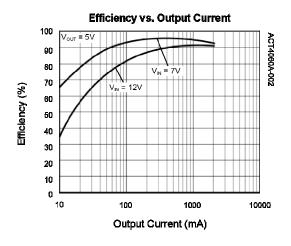
| ITEM | DESCRIPTION | MANUFACTURER | QTY | REFERENCE |
|------|--|----------------------------|-----|-----------|
| 1 | IC, ACT4060A | Active-Semi | 1 | U1 |
| 2 | $15\mu H \pm 20\%$, $I_{SAT} = 2.7A$, $I_{DC} = 2.4A@ \Delta T = 40°C$ | Taiyo Yuden NR 8040T 150M | , | 1.4 |
| | $15\mu H \pm 10\%$, $I_{SAT} = 2.88A$, $I_{DC} = 2.47A@ \Delta T = 40°C$ | Wurth Electronik 744776115 | ı | L1 |
| 3 | Schottky Diode SK34/40V, 3A, SMB | Transys electronics | 1 | D1 |
| 3 | Schottky Diode B340C/40V, 3A, SMB | Diodes Inc | ' | וטו |
| 4 | Ceramic cap 10μF/35V, X7R, 1210 | Murata, TDK, Taiyo Yuden | 1 | C1 |
| 5 | Ceramic cap 2.2nF/6.3V, X7R, 0603 | Murata, TDK, Taiyo Yuden | 1 | C2 |
| 6 | Ceramic cap 10nF/50V, X7R, 0603 | Murata, TDK, Taiyo Yuden | 1 | C3 |
| 7 | Ceramic cap 22μF/10V, X7R, 1210 | Murata, TDK, Taiyo Yuden | 1 | C4 |
| , | SP cap 47μF/6.3V, 50mΩ | Kemet, Panasonic | 1 | 04 |
| 8 | Resistor, 28.7kΩ, 1/16W, 1%, 0603 | | | R1 |
| 9 | Resistor, 10kΩ, 1/16W, 1%, 0603 | FengHua, Neohm, Yageo | 1 | R2 |
| 10 | Resistor, 15kΩ, 1/16W, 5%, 0603 | | | R3 |

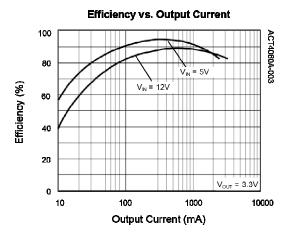


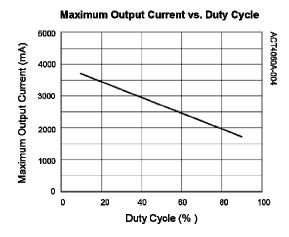
TYPICAL PERFORMANCE CHARACTERISTICS

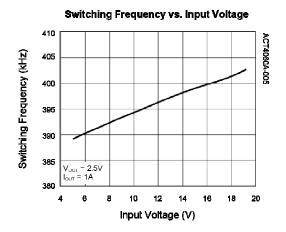
(Circuit of Figure 4, unless otherwise specified.)

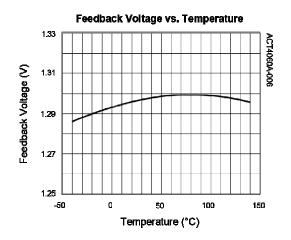






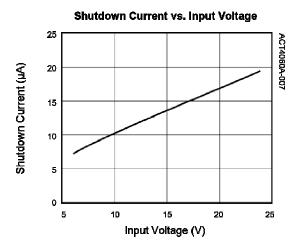






TYPICAL PERFORMANCE CHARACTERISTICS CONT'D

(Circuit of Figure 4, unless otherwise specified.)

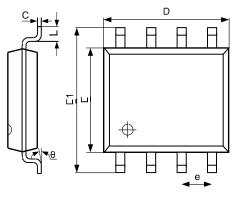


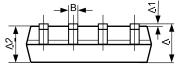




PACKAGE OUTLINE

SOP-8 PACKAGE OUTLINE AND DIMENSIONS





| SYMBOL | SYMBOL DIMENSION | | DIMENSIC INCHE | |
|--------|------------------|-------|-------------------|-------|
| | MIN | MAX | MIN | MAX |
| Α | 1.350 | 1.750 | 0.053 | 0.069 |
| A1 | 0.100 | 0.250 | 0.004 | 0.010 |
| A2 | 1.350 | 1.550 | 0.053 | 0.061 |
| В | 0.330 | 0.510 | 0.013 | 0.020 |
| С | 0.190 | 0.250 | 0.007 | 0.010 |
| D | 4.700 | 5.100 | 0.185 | 0.201 |
| E | 3.800 | 4.000 | 0.150 | 0.157 |
| E1 | 5.800 | 6.300 | 0.228 | 0.248 |
| е | 1.270 | TYP | 0.050 TYP | |
| L | 0.400 | 1.270 | 0.016 0.050 | |
| θ | 0° | 8° | 0° | 8° |



ACT4060A Wide Input 2 A Step Down Converter

Contact Information

For the latest specifications, additional product information, worldwide sales and distribution locations:

Web: <u>www.gorvo.com</u> Tel: 1-844-890-8163

Email: customer.support@gorvo.com

For technical questions and application information:

Email: appsupport@gorvo.com

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