## Data Sheet

## FEATURES

Very high dc precision<br>$30 \mu \mathrm{~V}$ maximum offset voltage<br>$0.3 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ maximum offset voltage drift<br>$0.35 \mu \mathrm{~V}$ p-p maximum voltage noise ( 0.1 Hz to 10 Hz )<br>5 million V/V minimum open-loop gain<br>130 dB minimum CMRR<br>120 dB minimum PSRR<br>Matching characteristics<br>$30 \mu \mathrm{~V}$ maximum offset voltage match<br>$0.3 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ maximum offset voltage drift match<br>130 dB minimum CMRR match<br>Available in 8-lead narrow body, PDIP, and hermetic CERDIP and CERDIP/883B packages

## GENERAL DESCRIPTION

The AD708 is a high precision, dual monolithic operational amplifier. Each amplifier individually offers excellent dc precision with maximum offset voltage and offset voltage drift of any dual bipolar op amp.

The matching specifications are among the best available in any dual op amp. In addition, the AD708 provides $5 \mathrm{~V} / \mu \mathrm{V}$ minimum open-loop gain and guaranteed maximum input voltage noise of 350 nV p-p ( 0.1 Hz to 10 Hz ). All dc specifications show excellent stability over temperature, with offset voltage drift typically $0.1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ and input bias current drift of $25 \mathrm{pA} /{ }^{\circ} \mathrm{C}$ maximum.

The AD708 is available in four performance grades. The AD708J is rated over the commercial temperature range of $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ and is available in a narrow body, PDIP. The AD708A and AD708B are rated over the industrial temperature range of $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ and are available in a CERDIP.

The AD708S is rated over the military temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ and is available in a CERDIP military version processed to MIL-STD-883B.

## PRODUCT HIGHLIGHTS

1. The combination of outstanding matching and individual specifications make the AD708 ideal for constructing high gain, precision instrumentation amplifiers.
2. The low offset voltage drift and low noise of the AD708 allow the designer to amplify very small signals without sacrificing overall system performance.
3. The AD708 $10 \mathrm{~V} / \mu \mathrm{V}$ typical open-loop gain and 140 dB common-mode rejection make it ideal for precision applications.

## TABLE OF CONTENTS

Features ..... 1
Pin Configuration ..... 1
General Description .....  1
Product Highlights ..... 1
Revision History ..... 2
Specifications ..... 3
Absolute Maximum Ratings .....  5
ESD Caution .....  5
Typical Performance Characteristics .....  6
Matching Characteristics. ..... 9
REVISION HISTORY
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Programmable Gain Amplifier Section ..... 11
Changes to Ordering Guide ..... 13
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Removed TO-99 Package Universal
Deleted AD707 References ..... Universal
Theory of Operation ..... 10
Crosstalk Performance ..... 10
Operation with a Gain of -100 . ..... 11
High Precision Programmable Gain Amplifier ..... 11
Bridge Signal Conditioner ..... 12
Precision Absolute Value Circuit ..... 12
Selection of Passive Components ..... 12
Outline Dimensions ..... 13
Ordering Guide ..... 13
Deleted LT1002 Reference. .....  1
Deleted Figure 1 .....  1
Deleted Metalization Photograph .....  5
Moved Figure 25, Figure 26, and Figure 27
to Theory of Operation section ..... 10
Updated Outline Dimensions ..... 13
Changes to Ordering Guide ..... 13

## SPECIFICATIONS

At $25^{\circ} \mathrm{C}$ and $\pm 15 \mathrm{~V} \mathrm{dc}$, unless otherwise noted.
Table 1.

| Parameter | Conditions | AD708J/AD708A |  |  | AD708B |  |  | AD708S |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min ${ }^{1}$ | Typ | Max ${ }^{1}$ | Min ${ }^{1}$ | Typ | Max ${ }^{1}$ | Min ${ }^{1}$ | Typ | Max ${ }^{1}$ |  |
| INPUT OFFSET VOLTAGE ${ }^{2}$ |  |  | 30 | 100 |  | 5 | 50 |  | 5 | 30 | $\mu \mathrm{V}$ |
|  | $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  | 50 | 150 |  | 15 | 65 |  | 15 | 50 | $\mu \mathrm{V}$ |
| Drift |  |  | 0.3 | 1.0 |  | 0.1 | 0.4 |  | 0.1 | 0.3 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Long Term Stability |  |  | 0.3 |  |  | 0.3 |  |  | 0.3 |  | $\mu \mathrm{V} /$ month |
| INPUT BIAS CURRENT |  |  | 1.0 | 2.5 |  | 0.5 | 1.0 |  | 0.5 | 1 |  |
|  | $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  | 2.0 | 4.0 |  | 1.0 | 2.0 |  | 1.0 | 4 | nA |
| Average Drift |  |  | 15 | 40 |  | 10 | 25 |  | 10 | 30 | $\mathrm{pA} /{ }^{\circ} \mathrm{C}$ |
| OFFSET CURRENT | $\mathrm{V}_{\text {CM }}=0 \mathrm{~V}$ |  | 0.5 | 2.0 |  | 0.1 | 1.0 |  | 0.1 | 1 | nA |
|  | $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {MAX }}$ |  | 2.0 | 4.0 |  | 0.2 | 1.5 |  | 0.2 | 1.5 | nA |
| Average Drift |  |  | 2 | 60 |  | 1 | 25 |  | 1 | 25 | $\mathrm{pA} /{ }^{\circ} \mathrm{C}$ |
| MATCHING CHARACTERISTICS ${ }^{3}$ Offset Voltage |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | 80 |  |  | 50 |  |  | 30 | $\mu \mathrm{V}$ |
|  | $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ |  |  | 150 |  |  | 75 |  |  | 50 | $\mu \mathrm{V}$ |
| Offset Voltage Drift Input Bias Current |  |  |  | 1.0 |  |  | 0.4 |  |  | 0.3 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
|  |  |  |  | 4.0 |  |  | 1.0 |  |  | 1.0 | nA |
|  | $\mathrm{T}_{\text {Min }}$ to $\mathrm{T}_{\text {MAX }}$ |  |  | 5.0 |  |  | 2.0 |  |  | 2.0 | nA |
| Common-Mode Rejection |  | 120 | 140 |  | 130 | 140 |  | 130 | 140 |  | dB |
|  | $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ | 110 |  |  | 130 |  |  | 130 |  |  | dB |
| Power Supply Rejection |  | 110 |  |  | 120 |  |  | 120 |  |  | dB |
|  | $\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ | 110 |  |  | 120 |  |  | 120 |  |  | dB |
| Channel Separation |  | 135 |  |  | 140 |  |  | 140 |  |  | dB |
| INPUT VOLTAGE NOISE | 0.1 Hz to 10 Hz |  | 0.23 | 0.6 |  | 0.23 | 0.6 |  | 0.23 | 0.35 | $\mu \mathrm{V}$ p-p |
|  | $\mathrm{f}=10 \mathrm{~Hz}$ |  | 10.3 | 18 |  | 10.3 | 12 |  | 10.3 | 12 | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
|  | $\mathrm{f}=100 \mathrm{~Hz}$ |  | 10.0 | 13.0 |  | 10.0 | 11.0 |  | 10.0 | 11 | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
|  | $\mathrm{f}=1 \mathrm{kHz}$ |  | 9.6 | 11.0 |  | 9.6 | 11.0 |  | 9.6 | 11 | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| INPUT CURRENT NOISE | 0.1 Hz to 10 Hz |  | 14 | 35 |  | 14 | 35 |  | 14 | 35 | pA p-p |
|  | $\mathrm{f}=10 \mathrm{~Hz}$ |  | 0.32 | 0.9 |  | 0.32 | 0.8 |  | 0.32 | 0.8 | $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ |
|  | $\mathrm{f}=100 \mathrm{~Hz}$ |  | 0.14 | 0.27 |  | 0.14 | 0.23 |  | 0.14 | 0.23 | $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ |
|  | $\mathrm{f}=1 \mathrm{kHz}$ |  |  |  |  | 0.12 |  |  | 0.12 |  | $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ |
| COMMON-MODE REJECTION RATIO | $\mathrm{V}_{\text {CM }}= \pm 13 \mathrm{~V}$ | 120 | 140 |  | 130 | 140 |  | 130 | 140 |  | dB |
|  | $\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {Max }}$ | 120 | 140 |  | 130 | 140 |  | 130 | 140 |  | dB |
| OPEN-LOOP GAIN | $\begin{aligned} & \mathrm{V}_{\mathrm{O}}= \pm 10 \mathrm{~V} \\ & \mathrm{R}_{\text {LOAD }} \geq 2 \mathrm{k} \Omega \\ & \mathrm{~T}_{\text {MIN }} \text { to } \mathrm{T}_{\text {MAX }} \end{aligned}$ | $\begin{array}{r} 3 \\ 3 \\ \hline \end{array}$ | $\begin{aligned} & 10 \\ & 10 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \mathbf{5} \\ & 5 \end{aligned}$ | $\begin{aligned} & 10 \\ & 10 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & 4 \\ & 4 \end{aligned}$ | $\begin{aligned} & 10 \\ & 7 \end{aligned}$ |  | $\begin{aligned} & \mathrm{V} / \mu \mathrm{V} \\ & \mathrm{~V} / \mu \mathrm{V} \\ & \hline \end{aligned}$ |
| POWER SUPPLY REJECTION RATIO | $\mathrm{V}_{\mathrm{s}}= \pm 3 \mathrm{~V}$ to $\pm 18 \mathrm{~V}$ | $110$ | 130 |  | $120$ |  |  | 120 | 130 |  | dB |
|  | $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ | $110$ |  |  | $120$ | 130 |  |  |  |  |  |
| FREQUENCY RESPONSE <br> Closed-Loop Bandwidth Slew Rate |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 0.5 | 0.9 |  | 0.5 | 0.9 |  | 0.5 | 0.9 |  | MHz |
|  |  | 0.15 | 0.3 |  | 0.15 | 0.3 |  | 0.15 | 0.3 |  |  |
| INPUT RESISTANCE <br> Differential <br> Common Mode |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 60 |  |  | 200 |  |  | 200 |  | $\mathrm{M} \Omega$ |
|  |  |  |  |  |  |  |  |  |  |  |  |


| Parameter | Conditions | AD708J/AD708A |  |  | AD708B |  |  | AD708S |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min ${ }^{1}$ | Typ | Max ${ }^{1}$ | Min ${ }^{1}$ | Typ | Max ${ }^{1}$ | Min ${ }^{1}$ | Typ | Max ${ }^{1}$ |  |
| OUTPUT VOLTAGE | RLOAD $\geq 10 \mathrm{k} \Omega$ | 13.5 | 14 |  | 13.5 | 14.0 |  | 13.5 | 14 |  | $\pm \mathrm{V}$ |
|  | $\mathrm{R}_{\text {LOAD }} \geq 2 \mathrm{k} \Omega$ | 12.5 | 13.0 |  | 12.5 | 13.0 |  | 12.5 | 13 |  | $\pm \mathrm{V}$ |
|  | $\mathrm{R}_{\text {LOAD }} \geq 1 \mathrm{k} \Omega$ | 12.0 | 12.5 |  | 12.0 | 12.5 |  | 12.0 | 12.5 |  | $\pm \mathrm{V}$ |
|  | $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ | 12.0 | 13.0 |  | 12.0 | 13.0 |  | 12.0 | 13 |  | $\pm \mathrm{V}$ |
| OPEN-LOOP OUTPUT RESISTANCE |  |  | 60 |  |  | 60 |  |  | 60 |  | $\Omega$ |
| POWER SUPPLY |  |  |  |  |  |  |  |  |  |  |  |
| Quiescent Current |  |  | 4.5 | 5.5 |  | 4.5 | 5.5 |  | 4.5 | 5.5 | mA |
| Power Consumption | $\mathrm{V}_{\mathrm{s}}= \pm 15 \mathrm{~V}$ |  | 135 | 165 |  | 135 | 165 |  | 135 | 165 | mW |
|  | $\mathrm{V}_{\mathrm{s}}= \pm 3 \mathrm{~V}$ |  | 12 | 18 |  | 12 | 18 |  | 12 | 18 | mW |
| Operating Range |  | $\pm 3$ |  | $\pm 18$ | $\pm 3$ |  | $\pm 18$ | $\pm 3$ |  | $\pm 18$ | V |

${ }^{1}$ All min and max specifications are guaranteed. Specifications in boldface are tested on all production units at final electrical test. Results from those tests are used to calculate outgoing quality levels.
${ }^{2}$ Input offset voltage specifications are guaranteed after five minutes of operation at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
${ }^{3}$ Matching is defined as the difference between parameters of the two amplifiers.

## ABSOLUTE MAXIMUM RATINGS

Table 2.

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage | $\pm 22 \mathrm{~V}$ |
| Internal Power Dissipation $^{1}$ |  |
| Input Voltage $^{2}$ | $\pm \mathrm{V}_{\mathrm{s}}$ |
| Output Short-Circuit Duration | Indefinite |
| Differential Input Voltage | $+\mathrm{V}_{\mathrm{s}}$ and $-\mathrm{V}_{\mathrm{s}}$ |
| Storage Temperature Range (Q) | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Storage Temperature Range (N) | $-65^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering 60 sec ) | $300^{\circ} \mathrm{C}$ |

${ }^{1}$ Thermal Characteristics
8-lead PDIP: $\theta_{\mathrm{Jc}}=33^{\circ} \mathrm{C} / \mathrm{W}, \theta_{\mathrm{JA}}=100^{\circ} \mathrm{C} / \mathrm{W}$
8-lead CERDIP: $\theta_{\mathrm{Jc}}=30^{\circ} \mathrm{C} / \mathrm{W}, \theta_{\mathrm{JA}}=110^{\circ} \mathrm{C} / \mathrm{W}$
${ }^{2}$ For supply voltages less than $\pm 22 \mathrm{~V}$, the absolute maximum input voltage is equal to the supply voltage.

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

## ESD CAUTION

## TYPICAL PERFORMANCE CHARACTERISTICS

$\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}$ and $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 2. Input Common-Mode Range vs. Supply Voltage


Figure 3. Output Voltage Swing vs. Supply Voltage


Figure 4. Output Voltage Swing vs. Load Resistance


Figure 5. Supply Current vs. Supply Voltage


Figure 6. Typical Distribution of Offset Voltage Drift


Figure 7. Output Impedance vs. Frequency


Figure 8. Input Bias Current vs. Differential Input Voltage


Figure 9. Input Noise Spectral Density


Figure 10. 0.1 Hz to 10 Hz Voltage Noise


Figure 11. Open-Loop Gain vs. Temperature


Figure 12. Open-Loop Gain vs. Supply Voltage


Figure 13. Open-Loop Gain and Phase vs. Frequency


Figure 14. Common-Mode Rejection vs. Frequency


Figure 15. Large Signal Frequency Response


Figure 16. Power Supply Rejection vs. Frequency


Figure 17. Small Signal Transient Response; $A_{v}=+1, R_{L}=2 \mathrm{k} \Omega, C_{L}=50 \mathrm{pF}$


Figure 18. Small Signal Transient Response; $A_{v}=+1, R_{L}=2 \mathrm{k} \Omega, C_{L}=1000 \mathrm{pF}$

## MATCHING CHARACTERISTICS



Figure 19. Typical Distribution of Offset Voltage Match


Figure 20. Typical Distribution of Offset Voltage Drift Match


Figure 21. Typical Distribution of Input Bias Current Match


Figure 22. Typical Distribution of Input Offset Current Match


Figure 23. PSRR Match vs. Temperature


Figure 24. Common-Mode Rejection Ratio (CMRR) Match vs. Temperature

## THEORY OF OPERATION

## CROSSTALK PERFORMANCE

The AD708 exhibits very low crosstalk as shown in Figure 25, Figure 26, and Figure 27. Figure 25 shows the offset voltage induced on Side B of the AD708 when Side A output is moving slowly ( 0.2 Hz ) from -10 V to +10 V under no load. This is the least stressful situation to the part because the overall power in the chip does not change. Only the location of the power in the output device changes. Figure 26 shows the input offset voltage change to Side $B$ when Side $A$ is driving a $2 \mathrm{k} \Omega$ load. Here the power changes in the chip with the maximum power change occurring at 7.5 V . Figure 27 shows crosstalk under the most severe conditions. Side A is connected as a follower with 0 V input, and is forced to sink and source $\pm 5 \mathrm{~mA}$ of output current.

$$
\text { Power }=(30 \mathrm{~V})(5 \mathrm{~mA})=150 \mathrm{~mW}
$$

Even this large change in power causes only an $8 \mu \mathrm{~V}$ (linear) change in the input offset voltage of Side B.


Figure 25. Crosstalk with No Load


Figure 26. Crosstalk with $2 \mathrm{k} \Omega$ Load


Figure 27. Crosstalk Under Forced Source and Sink Conditions

## OPERATION WITH A GAIN OF -100

To show the outstanding dc precision of the AD708 in a real application, Table 3 shows an error budget calculation for a gain of -100 . This configuration is shown in Figure 28.

Table 3.

| Error Sources | Maximum Error Contribution, $A_{v}=100$ <br> (S Grade), (Full Scale: $\mathrm{V}_{\text {OUT }}=\mathbf{1 0} \mathrm{V}, \mathrm{V}_{\text {IN }}=\mathbf{1 0 0} \mathbf{~ m V}$ ) |  |
| :---: | :---: | :---: |
| Vos | $30 \mu \mathrm{~V} / 100 \mathrm{mV}$ | $=300 \mathrm{ppm}$ |
| los | (100 k $\Omega$ )(1 nA)/10 V | $=10 \mathrm{ppm}$ |
| Gain (2 k $\Omega$ Load) | $10 \mathrm{~V} /(5 \times 106) / 100 \mathrm{mV}$ | $=20 \mathrm{ppm}$ |
| Noise | $0.35 \mathrm{mV} / 100 \mathrm{mV}$ | $=4 \mathrm{ppm}$ |
| Vos Drift | $\left(0.3 \mathrm{mV} /{ }^{\circ} \mathrm{C}\right) / 100 \mathrm{mV}$ | $=3 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| Total Unadjusted |  |  |
|  | At $25^{\circ} \mathrm{C}$ | $=334 \mathrm{ppm}>11$ bits |
|  | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | $=634 \mathrm{ppm}>10$ bits |
| With Offset |  |  |
| Calibrated Out | At $25^{\circ} \mathrm{C}$ | $=34 \mathrm{ppm}>14$ bits |
|  | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | $=334 \mathrm{ppm}>11$ bits |



Figure 28. Gain of -100 Configuration
This error budget assumes no error in the resistor ratio and no error from power supply variation (the 120 dB minimum PSRR of the AD708S makes this a good assumption). The external resistors can cause gain error from mismatch and drift over temperature.

## HIGH PRECISION PROGRAMMABLE GAIN AMPLIFIER

The 3-op-amp programmable gain amplifier shown in Figure 29 utilizes the matching characteristics of the AD708 to achieve high dc precision.


Figure 29. Precision PGA
The gains of the circuit are controlled by the select lines, A0 and A1, of the ADG1209 multiplexer and are 1, 10, 100, and 1000 in this design.

The input stage attains very high dc precision due to the $30 \mu \mathrm{~V}$ maximum offset voltage match of the AD708 and the 1 nA maximum input bias current match. The accuracy is maintained over temperature because of the ultralow drift performance of the AD708.
The AD8276 unity-gain difference amplifier eliminates the need for trimming in the second stage of the instrumentation amplifier. The AD8276 has on-chip resistors that are laser trimmed for excellent gain accuracy and high CMRR.
To determine the CMRR, follow these steps:

1. Connect $\mathrm{V}_{\text {INB }}$ to $\mathrm{V}_{\text {INA }}$ and apply an input voltage equal to the maximum and minimum full-scale common mode expected.
2. Use the following equation to determine the CMRR:

$$
C M R R=20 \times \log \frac{\Delta V_{C M}}{\Delta V_{\text {OUT }}}
$$

where $V_{C M}$ is the common-mode voltage.
To minimize gain errors, follow these steps:

1. Select gain $=10$ with the control lines and apply a differential input voltage.
2. Adjust the $10 \mathrm{k} \Omega$ potentiometer to $\mathrm{V}_{\text {out }}=10 \mathrm{~V}_{\mathrm{IN}}$ (adjust $\mathrm{V}_{\text {IN }}$ magnitude as necessary).
3. Repeat Step 1 and Step 2 for gain $=100$ and gain $=1000$, adjusting the $1 \mathrm{k} \Omega$ and $100 \Omega$ potentiometers, respectively.

The design shown in Figure 29 allows $0.1 \%$ gain accuracy and 100 dB common-mode rejection when $\pm 1 \%$ resistors and $\pm 10 \%$ potentiometers are used.

## BRIDGE SIGNAL CONDITIONER

The AD708 can be used in the circuit shown in Figure 30 to produce an accurate and inexpensive dynamic bridge conditioner. The low offset voltage match and low offset voltage drift match of the AD708 combine to achieve circuit performance better than all but the best instrumentation amplifiers. The outstanding specifications of the AD708, such as open-loop gain, input offset currents, and low input bias currents, do not limit circuit accuracy.
As configured, the circuit only requires a gain resistor, $\mathrm{R}_{\mathrm{G}}$, of suitable accuracy and a stable, accurate voltage reference. The transfer function is

$$
V_{O}=V_{R E F}[\Delta \mathrm{R} /(\mathrm{R}+\Delta \mathrm{R})]\left[\mathrm{R}_{\mathrm{G}} / \mathrm{R}\right]
$$

The only significant errors due to the AD708S are

$$
\begin{aligned}
& V_{\text {os_out }}=\left(V_{\text {OS_MATCH }}\right)\left(2 \mathrm{R}_{\mathrm{G}} / \mathrm{R}\right)=30 \mathrm{mV} \\
& \operatorname{Vos\_ out}(T)=(V \text { os_DRIFT })\left(2 \mathrm{R}_{\mathrm{G}} / \mathrm{R}\right)=0.3 \mathrm{mV} /{ }^{\circ} \mathrm{C}
\end{aligned}
$$

To achieve high accuracy, Resistor $\mathrm{R}_{\mathrm{G}}$ should be $0.1 \%$ or better with a low drift coefficient.


Figure 30. Bridge Signal Conditioning Circuit


Figure 31. Precision Absolute Value Circuit

## PRECISION ABSOLUTE VALUE CIRCUIT

The AD708 is ideally suited to the precision absolute value circuit shown in Figure 31. The low offset voltage match of the AD708 enables this circuit to accurately resolve the input signal.

In addition, the tight offset voltage drift match maintains the resolution of the circuit over the full military temperature range. The high dc open-loop gain and exceptional gain linearity allows the circuit to perform well at both large and small signal levels.
In this circuit, the only significant dc errors are due to the offset voltage of the two amplifiers, the input offset current match of the amplifiers, and the mismatch of the resistors. Errors associated with the AD708S contribute less than $0.001 \%$ error over $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$.
Maximum error at $25^{\circ} \mathrm{C}$

$$
\frac{30 \mu \mathrm{~V}+(10 \mathrm{k} \Omega)(1 \mathrm{nA})}{10 \mathrm{~V}}=40 \mu \mathrm{~V} / 10 \mu \mathrm{~V}=4 \mathrm{ppm}
$$

Maximum error at $+125^{\circ} \mathrm{C}$ or $-55^{\circ} \mathrm{C}$

$$
\frac{50 \mu \mathrm{~V}+(2 \mathrm{nA})(10 \mathrm{k} \Omega)}{10 \mathrm{~V}}=7 \mathrm{ppm} @+125^{\circ} \mathrm{C}
$$

Figure 32 shows $V_{\text {out }}$ vs. $V_{\text {IN }}$ for this circuit with a $\pm 3 \mathrm{mV}$ input signal at 0.05 Hz . Note that the circuit exhibits very low offset at the zero crossing. This circuit can also produce $\mathrm{V}_{\text {out }}=-\left|\mathrm{V}_{\text {IN }}\right|$ by reversing the polarity of the two diodes.


Figure 32. Absolute Value Circuit Performance (Input Signal $=0.05 \mathrm{~Hz}$ )

## SELECTION OF PASSIVE COMPONENTS

Use high quality passive components to take full advantage of the high precision and low drift characteristics of the AD708. Discrete resistors and resistor networks with temperature coefficients of less than $10 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ are available from Vishay, Caddock, Precision Replacement Parts (PRP), and others.

## OUTLINE DIMENSIONS




Figure 34. 8-Lead Ceramic Dual In-Line Package [CERDIP] ( $Q-8$ )
Dimensions shown in inches and (millimeters)

ORDERING GUIDE

| Model $^{1}$ | Temperature Range | Package Description | Package Option |
| :--- | :--- | :--- | :--- |
| AD708JNZ | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ | 8-Lead Plastic Dual In-Line Package [PDIP] | $\mathrm{N}-8$ |
| AD708AQ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead Ceramic Dual In-Line Package [CERDIP] | Q-8 |
| AD708BQ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 -Lead Ceramic Dual In-Line Package [CERDIP] | Q-8 |
| AD708SQ/883B | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8 -Lead Ceramic Dual In-Line Package [CERDIP] | Q-8 |

${ }^{1} Z=$ RoHS Compliant Part.

NOTES
Data Sheet AD708

NOTES

## X-ON Electronics

Largest Supplier of Electrical and Electronic Components
Click to view similar products for Operational Amplifiers - Op Amps category:
Click to view products by Analog Devices manufacturer:
Other Similar products are found below :
NCV33072ADR2G LM258AYDT LM358SNG 430227FB UPC824G2-A LT1678IS8 042225DB 058184EB UPC822G2-A UPC259G2-A UPC258G2-A NCV33202DMR2G NTE925 AZV358MTR-G1 AP4310AUMTR-AG1 HA1630D02MMEL-E HA1630S01LPEL-E SCY33178DR2G NJU77806F3-TE1 NCV5652MUTWG NCV20034DR2G LM324EDR2G LM2902EDR2G NTE7155 NTE778S NTE871 NTE924 NTE937 MCP6V17T-E/MNY MCP6V19-E/ST MXD8011HF MCP6V16UT-E/OT MCP6V17T-E/MS MCP6V19T-E/ST SCY6358ADR2G ADA4523-1BCPZ LTC2065HUD\#PBF ADA4523-1BCPZ-RL7 2SD965T-R RS6332PXK BDM8551 BDM321 MD1324 COS8052SR COS8552SR COS8554SR COS2177SR COS2353SR COS724TR LM2902M/TR

