## FEATURES

Wide input range beyond supplies Rugged input overvoltage protection
Low supply current: $\mathbf{2 0 0} \mu \mathrm{A}$ maximum per channel
Low power dissipation: 0.54 mW at $\mathrm{V}_{\mathrm{s}}=\mathbf{2 . 7} \mathrm{V}$
Bandwidth: 550 kHz
CMRR: 86 dB minimum, dc to 10 kHz
System offset voltage: $\pm 2 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ maximum (B Grade)
Low gain drift: 1 ppm/ ${ }^{\circ} \mathrm{C}$ maximum (B Grade)
Enhanced slew rate: $1.1 \mathrm{~V} / \mu \mathrm{s}$
Wide power supply range
Single supply: 2.0 V to $\mathbf{3 6} \mathrm{V}$
Dual supplies: $\pm \mathbf{2}$ V to $\pm \mathbf{1 8} \mathrm{V}$

## APPLICATIONS

Voltage measurement and monitoring
Current measurement and monitoring
Differential output instrumentation amplifier
Portable, battery-powered equipment
Test and measurement

## GENERAL DESCRIPTION

The AD8276/AD8277 are general-purpose, unity-gain difference amplifiers intended for precision signal conditioning in power critical applications that require both high performance and low power. They provide exceptional 86 dB common-mode rejection ratio (CMRR) and high bandwidth while amplifying signals well beyond the supply rails. The on-chip resistors are laser trimmed for gain drift of $1 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ and high CMRR. The AD8276/AD8277 also have extremely low gain drift vs. temperature.

The common-mode range of the amplifiers extends to almost double the supply voltage, making these amplifiers ideal for single-supply applications that require a high common-mode voltage range. The internal resistors and electrostatic discharge (ESD) circuitry at the inputs also provide overvoltage protection to the op amps.
The AD8276/AD8277 are unity-gain stable. Although they are optimized for use as difference amplifiers, they can also be connected in high precision, single-ended configurations with $\mathrm{G}=-1,+1$, or +2 . The AD8276/AD8277 provide an integrated precision solution that has smaller size, lower cost, and improved performance than a discrete alternative.

The AD8276/AD8277 operate on single supplies ( 2.0 V to 36 V ) or dual supplies ( $\pm 2 \mathrm{~V}$ to $\pm 18 \mathrm{~V}$ ). The maximum quiescent supply current is $200 \mu \mathrm{~A}$ per channel, which is ideal for batteryoperated and portable systems.

## FUNCTIONAL BLOCK DIAGRAMS



Figure 2. AD8277
The AD8276 is available in the space-saving 8-lead mini small outline package (MSOP) and the standard small outline (SOIC) package, as well as in die form, and the AD8277 is offered in a 14-lead SOIC package. Both are specified for performance over the industrial temperature range of $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ and are fully RoHS compliant.

Table 1. Difference Amplifiers by Category

| Low <br> Distortion | High <br> Voltage | Current Sensing ${ }^{\mathbf{1}}$ | Low Power |
| :--- | :--- | :--- | :--- |
| AD8270 | AD628 | AD8202 (U) | AD8276 |
| AD8271 | AD629 | AD8203 (U) | AD8277 |
| AD8273 |  | AD8205 (B) | AD8278 |
| AD8274 |  | AD8206 (B) |  |
| AMP03 |  | AD8216 (B) |  |

${ }^{1}$ U means unidirectional, B means bidirectional.

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AD8276/AD8271

## SPECIFICATIONS

Supply voltage $\left(\mathrm{V}_{\mathrm{s}}\right)= \pm 5 \mathrm{~V}$ to $\pm 15 \mathrm{~V}$, reference voltage $\left(\mathrm{V}_{\mathrm{REF}}\right)=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, load resistance $\left(\mathrm{R}_{\mathrm{L}}\right)=10 \mathrm{k} \Omega$ connected to ground, $\mathrm{G}=1$ difference amplifier configuration, unless otherwise noted.

Table 2.


[^0]$\mathrm{V}_{\mathrm{S}}=+2.7 \mathrm{~V}$ to $\pm 5 \mathrm{~V}, \mathrm{~V}_{\text {REF }}=$ midsupply, $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ connected to midsupply, $\mathrm{G}=1$ difference amplifier configuration, unless otherwise noted.

Table 3.

|  |  | Grade B |  |  | Grade A |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Parameter | Test Conditions/Comments | Min | Typ | Max | Min | Typ | Max | Unit |
| INPUT CHARACTERISTICS |  |  |  |  |  |  |  |  |
| System Offset ${ }^{1}$ |  |  | 100 | 200 |  | 100 | 500 | $\mu \mathrm{V}$ |
| vs. Temperature | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |  |  | 200 |  |  | 500 | $\mu \mathrm{V}$ |
| Average Temperature Coefficient | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |  | 0.5 | 2 |  |  | 5 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| vs. Power Supply | $\mathrm{V}_{\mathrm{s}}= \pm 5 \mathrm{~V}$ to $\pm 18 \mathrm{~V}$ |  |  | 5 |  |  | 10 | $\mu \mathrm{V} / \mathrm{V}$ |
| Common-Mode Rejection Ratio (RTI) | $\begin{aligned} & \mathrm{V}_{\mathrm{s}}=2.7 \mathrm{~V}, \mathrm{~V}_{\mathrm{cm}}=0 \mathrm{~V} \text { to } 2.4 \mathrm{~V}, \\ & \mathrm{R}_{\mathrm{s}}=0 \Omega \end{aligned}$ | $86$ |  |  | $80$ |  |  | dB |
|  | $\begin{aligned} & \mathrm{V}_{\mathrm{s}}= \pm 5 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=-10 \mathrm{~V} \text { to }+7 \mathrm{~V}, \\ & \mathrm{R}_{\mathrm{S}}=0 \Omega \end{aligned}$ | $86$ |  |  | $80$ |  |  | dB |
| Input Voltage Range ${ }^{2}$ |  | $-2\left(V_{s}+0.1\right)$ |  | $+2\left(V_{s}-1.5\right)$ | $-2\left(V_{s}+0.1\right)$ |  | $+2\left(V_{s}-1.5\right)$ | V |
| Impedance ${ }^{3}$ |  |  |  |  |  |  |  |  |
| Differential |  |  | 80 |  |  | 80 |  | $\mathrm{k} \Omega$ |
| Common Mode |  |  | 40 |  |  | 40 |  | $\mathrm{k} \Omega$ |
| DYNAMIC PERFORMANCE |  |  |  |  |  |  |  |  |
| Bandwidth |  |  | 450 |  |  | 450 |  | kHz |
| Slew Rate |  |  | 1.0 |  |  | 1.0 |  | V/ $\mu \mathrm{s}$ |
| Settling Time to 0.01\% | 8 V step on output, $C_{L}=100 \mathrm{pF}, \mathrm{~V}_{\mathrm{S}}=10 \mathrm{~V}$ |  | 5 |  |  | 5 |  | $\mu \mathrm{s}$ |
| Channel Separation | $\mathrm{f}=1 \mathrm{kHz}$ |  | 130 |  |  | 130 |  | dB |
| GAIN |  |  |  |  |  |  |  |  |
| Gain Error | T $=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |  | 0.005 | $0.02$ |  |  | $0.05$ | $\%$ |
| Gain Drift | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |  |  |  |  |  |  | ppm/ ${ }^{\circ}$ |
| OUTPUT CHARACTERISTICS Output Swing ${ }^{4}$ | $\begin{aligned} & \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega, \\ & \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C} \text { to }+85^{\circ} \mathrm{C} \end{aligned}$ | $-\mathrm{V}_{s}+0.1$ |  | $+\mathrm{V}_{\text {S }}-0.15$ | $-V_{s}+0.1$ |  | $+\mathrm{V}_{s}-0.15$ |  |
| Short-Circuit Current Limit |  |  | $\pm 10$ |  |  | $\pm 10$ |  | mA |
| Capacitive Load Drive |  |  | 200 |  |  | 200 |  | pF |
| NOISE ${ }^{5}$ |  |  |  |  |  |  |  |  |
| Output Voltage Noise | $\mathrm{f}=0.1 \mathrm{~Hz}$ to 10 Hz |  | 2 |  |  | 2 |  | $\mu \mathrm{V}$ p-p |
|  | $\mathrm{f}=1 \mathrm{kHz}$ |  | 65 |  |  | 65 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| POWER SUPPLY |  |  |  |  |  |  |  |  |
| Supply Current ${ }^{67}$ | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |  |  | 200 |  |  | 200 | $\mu \mathrm{A}$ |
| Operating Voltage Range |  | 2.0 |  |  | 2.0 |  | 36 |  |
| TEMPERATURE RANGE |  |  |  |  |  |  |  |  |
| Operating Range |  | -40 |  | +125 | -40 |  | +125 | ${ }^{\circ} \mathrm{C}$ |

${ }^{1}$ Includes input bias and offset current errors, RTO
${ }^{2}$ The input voltage range may also be limited by absolute maximum input voltage or by the output swing. See the Input Voltage Range section in the Theory of Operation section for details.
${ }^{3}$ Internal resistors are trimmed to be ratio matched and have $\pm 20 \%$ absolute accuracy.
${ }^{4}$ Output voltage swing varies with supply voltage and temperature. See Figure 19 through Figure 22 for details.
${ }^{5}$ Includes amplifier voltage and current noise, as well as noise from internal resistors.
${ }^{6}$ Supply current varies with supply voltage and temperature. See Figure 24 and Figure 25 for details.
${ }^{7}$ Power dissipation ( $\mathrm{P}_{\text {DISS }}$ ) at quiescent condition is computed by multiplying the supply voltage and quiescent supply current ( $\mathrm{I}_{\mathrm{Q}}$ ). $\mathrm{P}_{\mathrm{DISS}}=\mathrm{V}_{S} \times \mathrm{I}_{\mathrm{Q}}, \mathrm{P}_{\mathrm{DISS}}=2.7 \mathrm{~V} \times 200 \mu \mathrm{~A}$, $P_{\text {DIIs }}=0.54 \mathrm{~mW}$.

## ABSOLUTE MAXIMUM RATINGS

Table 4.

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage | $\pm 18 \mathrm{~V}$ |
| Maximum Voltage at Any Input Pin | $-\mathrm{V}_{\mathrm{S}}+40 \mathrm{~V}$ |
| Minimum Voltage at Any Input Pin | $+\mathrm{V}_{\mathrm{S}}-40 \mathrm{~V}$ |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Specified Temperature Range | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Package Glass Transition Temperature $\left(\mathrm{T}_{\mathrm{G}}\right)$ | $150^{\circ} \mathrm{C}$ |

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

## THERMAL RESISTANCE

Thermal performance is directly linked to printed circuit board (PCB) design and operating environment. Close attention to PCB thermal design is required.
$\theta_{\mathrm{JA}}$ is junction-to-ambient thermal resistance and $\theta_{\mathrm{JC}}$ is junction-to-case thermal resistance.

Table 5.

| Package Type | $\boldsymbol{\theta}_{\mathbf{A A}}{ }^{\mathbf{1}}$ | $\boldsymbol{\theta}_{\mathbf{\prime}}$ | Unit |
| :--- | :--- | :--- | :--- |
| RM-8 | 135 | 67.8 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| R-8 | 121 | 57.6 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| R-14 | 105 | 35.8 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

${ }^{1}$ The $\theta_{\mathrm{JA}}$ values in Table 5 assume a 4-layer JEDEC standard board with zero airflow.

## MAXIMUM POWER DISSIPATION

The maximum safe power dissipation for the AD8276/AD8277 is limited by the associated rise in junction temperature $\left(\mathrm{T}_{\mathrm{J}}\right)$ on the die. At approximately $150^{\circ} \mathrm{C}$, which is the glass transition temperature, the properties of the plastic change. Even temporarily exceeding this temperature limit may change the stresses that the package exerts on the die, permanently shifting the parametric performance of the amplifiers. Exceeding a temperature of $150^{\circ} \mathrm{C}$ for an extended period may result in a loss of functionality.


Figure 3. Maximum Power Dissipation vs. Ambient Temperature

## SHORT-CIRCUIT CURRENT

The AD8276/AD8277 have built in, short-circuit protection that limits the output current (see Figure 26 for more information). While the short-circuit condition itself does not damage the device, the heat generated by the condition can cause the device to exceed its maximum junction temperature, with corresponding negative effects on reliability. Figure 3 and Figure 26, combined with knowledge of the supply voltages and ambient temperature of the device, can be used to determine whether a short circuit can cause the device to exceed its maximum junction temperature.

## ESD CAUTION



ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

## AD8276/AD8271

## PIN CONFIGURATIONS AND FUNCTION DESCRIPTIONS



Figure 4. AD8276 8-Lead MSOP Pin Configuration


Figure 5. AD8276 8-Lead SOIC Pin Configuration

Table 6. AD8276 Pin Function Descriptions

| Pin No. | Mnemonic | Description |
| :--- | :--- | :--- |
| 1 | REF | Reference Voltage Input. |
| 2 | - IN | Inverting Input. |
| 3 | +IN | Noninverting Input. |
| 4 | - VS | Negative Supply. |
| 5 | SENSE | Sense Terminal. |
| 6 | OUT | Output. |
| 7 | + VS | Positive Supply. |
| 8 | NC | No Connect. This pin is not internally connected. |



Figure 6. AD8276 7-Pad CHIP Pad Configuration
Table 7. AD8276 Pad Function Descriptions ${ }^{1}$

| Pad No. | Mnemonic | X Coordinate | Y Coordinate | Description |
| :--- | :--- | :--- | :--- | :--- |
| 1 | REF | -512 | +412 | Reference Voltage Input |
| 2 | - IN | -512 | +167 | Inverting Input |
| 3 | + IN | -512 | -188 | Noninverting Input |
| 4 | - VS | -106 | -400 | Negative Supply |
| 5 | SENSE | +511 | -376 | Sense Terminal |
| 6 | OUT | +530 | 0 | Output |
| 7 | + VS | +329 | +453 | Positive Supply |

[^1]

Figure 7. AD8277 14-Lead SOIC Pin Configuration
Table 8. AD8277 Pin Function Descriptions

| Pin No. | Mnemonic | Description |
| :--- | :--- | :--- |
| 1 | NC | No Connect. This pin is not internally connected. |
| 2 | -INA | Channel A Inverting Input. |
| 3 | +INA | Channel A Noninverting Input. |
| 4 | - VS | Negative Supply. |
| 5 | +INB | Channel B Noninverting Input. |
| 6 | -INB | Channel B Inverting Input. |
| 7 | NC | No Connect. This pin is not internally connected. |
| 8 | REFB | Channel B Reference Voltage Input. |
| 9 | OUTB | Channel B Output. |
| 10 | SENSEB | Channel B Sense Terminal. |
| 11 | +VS | Positive Supply. |
| 12 | SENSEA | Channel A Sense Terminal. |
| 13 | OUTA | Channel A Output. |
| 14 | REFA | Channel A Reference Voltage Input. |

## TYPICAL PERFORMANCE CHARACTERISTICS

$\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ connected to ground, $\mathrm{G}=1$ difference amplifier configuration, unless otherwise noted. SD is standard deviation.


Figure 8. Distribution of Typical System Offset Voltage


Figure 9. Distribution of Typical Common-Mode Rejection Ratio


Figure 10. CMRR vs. Temperature, Normalized at $25^{\circ} \mathrm{C}$


Figure 11. System Offset vs. Temperature, Normalized at $25^{\circ} \mathrm{C}$


Figure 12. Gain Error vs. Temperature, Normalized at $25^{\circ} \mathrm{C}$


Figure 13. Gain vs. Frequency, $V_{s}= \pm 15 \mathrm{~V},+2.7 \mathrm{~V}$


Figure 14. CMRR vs. Frequency


Figure 15. PSRR vs. Frequency


Figure 16. Input Common-Mode Voltage vs. Output Voltage, $\pm 15 \mathrm{~V}$ and $\pm 5 \mathrm{~V}$ Supplies


Figure 17. Input Common-Mode Voltage vs. Output Voltage, 5 V and 2.7 V Supplies, V $V_{\text {REF }}=$ Midsupply


Figure 18. Input Common-Mode Voltage vs. Output Voltage,
5 V and 2.7 V Supplies, $V_{\text {REF }}=0 \mathrm{~V}$


Figure 19. Output Voltage Swing (V) Referred to Supply Voltages vs. Supply Voltage Per Channel and Temperature, $R_{L}=10 \mathrm{k} \Omega$


Figure 20. Output Voltage Swing (V) Referred to Supply Voltages vs. Supply Voltage Per Channel and Temperature, $R_{L}=2 \mathrm{k} \Omega$


Figure 21. Output Voltage Swing (V) Referred to Supply Voltages vs. Load Resistance and Temperature, $V_{S}= \pm 15 \mathrm{~V}$


Figure 22. Output Voltage Swing (V) Referred to Supply Voltages vs. Output Current and Temperature, $V_{S}= \pm 15 \mathrm{~V}$


Figure 23. Supply Current Per Channel vs. Dual Supply Voltage, $V_{I N}=0 V$


Figure 24. Supply Current Per Channel vs. Single-Supply Voltage, $V_{I N}=O V$, $V_{\text {REF }}=0 \mathrm{~V}$


Figure 25. Supply Current Per Channel vs. Temperature


Figure 26. Short-Circuit Current Per Channel vs. Temperature


Figure 27. Slew Rate vs. Temperature, $V_{I N}=20 \mathrm{Vp}-\mathrm{p}, 1 \mathrm{kHz}$


Figure 28. Gain Nonlinearity, $V_{S}= \pm 15 \mathrm{~V}, R_{L} \geq 2 \mathrm{k} \Omega$


Figure 29. Large Signal Pulse Response and Settling Time, 10 V Step, $V_{S}= \pm 15 \mathrm{~V}$


Figure 30. Large Signal Pulse Response and Settling Time, 2 V Step, $V_{s}=2.7 \mathrm{~V}$


Figure 31. Large Signal Step Response


Figure 32. Maximum Output Voltage vs. Frequency, $V_{s}= \pm 15 \mathrm{~V}, \pm 5 \mathrm{~V}$


Figure 33. Maximum Output Voltage vs. Frequency, $V_{s}=5 \mathrm{~V}, 2.7 \mathrm{~V}$

Figure 34. Small Signal Step Response for Various Capacitive Loads



Figure 35. Small Signal Overshoot vs. Capacitive Load, $R_{L} \geq 2 \mathrm{k} \Omega$


Figure 36. Voltage Noise Density vs. Frequency


Figure 37. 0.1 Hz to 10 Hz Voltage Noise


Figure 38. Channel Separation vs. Frequency

## THEORY OF OPERATION

## CIRCUIT INFORMATION

Each channel of the AD8276/AD8277 consists of a low power, low noise op amp and four laser trimmed on-chip resistors. These resistors can be externally connected to make a variety of amplifier configurations, including difference, noninverting, and inverting configurations. Taking advantage of the integrated resistors of the AD8276/AD8277 provides the designer with several benefits over a discrete design, including smaller size, lower cost, and improved ac and dc performance. See Figure 1.

## DC Performance

Much of the dc performance of op amp circuits depends on the accuracy of the surrounding resistors. Using superposition to analyze a typical difference amplifier circuit, as is shown in Figure 39, the output voltage is found to be

$$
V_{\text {OUT }}=V_{I N+}\left(\frac{R 2}{R 1+R 2}\right)\left(1+\frac{R 4}{R 3}\right)-V_{I N-}\left(\frac{R 4}{R 3}\right)
$$

This equation demonstrates that the gain accuracy and CMRR of the AD8276/AD8277 is determined primarily by the matching of resistor ratios. Even a $0.1 \%$ mismatch in one resistor degrades the CMRR to 66 dB for a $\mathrm{G}=1$ difference amplifier.
The difference amplifier output voltage equation can be reduced to

$$
V_{O U T}=\frac{R 4}{R 3}\left(V_{I N+}-V_{I N-}\right)
$$

as long as the following ratio of the resistors is tightly matched:

$$
\frac{R 2}{R 1}=\frac{R 4}{R 3}
$$

The resistors on the AD8276/AD8277 are laser trimmed to match accurately. As a result, the AD8276/AD8277 provide superior performance over a discrete solution, enabling higher CMRR, higher gain accuracy, and lower gain drift, even over a wide temperature range.

## AC Performance

Component sizes and trace lengths are much smaller in an IC than on a PCB, therefore, the corresponding parasitic elements are also smaller, which results in improved ac performance of the AD8276/AD8277. For example, the positive and negative input terminals of the AD8276/AD8277 op amps are intentionally not pinned out, meaning that there is no direct connection to the inputs of the amplifier. The op amps are connected internally through the resistors, and there is no direct access to the pins. By not connecting these nodes to the traces on the PCB, the capacitance remains low, resulting in improved loop stability and excellent CMRR over frequency of 86 dB .

## DRIVING THE AD8276/AD8277

Care must be taken to drive the AD8276/AD8277 with a low impedance source, for example, another amplifier. Source resistance of even a few kilohms ( $k \Omega$ ) can unbalance the resistor ratios and, therefore, significantly degrade the gain accuracy and CMRR of the AD8276/AD8277. Because all configurations present several kilohms of input resistance, the AD8276/AD8277 do not require a high current drive from the source and therefore are easy to drive.

## INPUT VOLTAGE RANGE

The AD8276/AD8277 are able to measure input voltages beyond the supply rails. The internal resistors divide down the voltage before it reaches the internal op amp and provide protection to the op amp inputs. Figure 39 shows an example of how the voltage division works in a difference amplifier configuration. For the AD8276/AD8277 to measure correctly, the input voltages at the input nodes of the internal op amp must stay below 1.5 V of the positive supply rail and can exceed the negative supply rail by 0.1 V . Refer to the Power Supplies section for more details.


Figure 39. Voltage Division in the Difference Amplifier Configuration
The AD8276/AD8277 have integrated ESD diodes at the inputs that provide overvoltage protection. This feature simplifies system design by eliminating the need for additional external protection circuitry, and enables a more robust system.
The voltages at any of the inputs of the devices can safely range from $+V_{s}-40 \mathrm{~V}$ up to $-\mathrm{V}_{\mathrm{s}}+40 \mathrm{~V}$. For example, on $\pm 10 \mathrm{~V}$ supplies, input voltages can go as high as $\pm 30 \mathrm{~V}$. Care must be taken to not exceed the $+\mathrm{V}_{\mathrm{s}}-40 \mathrm{~V}$ to $-\mathrm{V}_{\mathrm{s}}+40 \mathrm{~V}$ input limits to avoid risking damage to the devices.

## POWER SUPPLIES

The AD8276/AD8277 operate over a wide range of supply voltages. They can operate on a single supply as low as 2 V and as high as 36 V , under appropriate setup conditions.
For optimal performance, the user must ensure that the internal op amp is biased correctly through proper setup conditions. The internal input terminals of the op amp must have sufficient voltage headroom to operate properly. Proper operation of the device requires at least 1.5 V between the positive supply rail and the op amp input terminals. This relationship is expressed in the following equation:

$$
\frac{R 1}{R 1+R 2} \times V_{R E F}<+V_{S}-1.5 \mathrm{~V}
$$

For example, when operating on $\mathrm{a}+\mathrm{V}_{\mathrm{s}}=2 \mathrm{~V}$ single supply and $\mathrm{V}_{\text {Ref }}=0 \mathrm{~V}$, it can be seen from Figure 40 that the input terminals of the op amp are biased at 0 V , allowing more than the required 1.5 V headroom. However, if $\mathrm{V}_{\text {Ref }}=1 \mathrm{~V}$ under the same conditions, the input terminals of the op amp are biased at 0.5 V , barely allowing the required 1.5 V headroom. This setup does not allow any practical voltage swing on the noninverting input. Therefore, the user must increase the supply voltage or decrease $\mathrm{V}_{\text {REF }}$ to restore proper operation.

The AD8276/AD8277 are typically specified at single and dual supplies, but they can be used with unbalanced supplies, as well, for example, $-\mathrm{V}_{s}=-5 \mathrm{~V},+\mathrm{V}_{s}=20 \mathrm{~V}$. The difference between the two supplies must be kept below 36 V . The positive supply rail must be at least 2 V above the negative supply and reference voltage.


Figure 40. Ensure Sufficient Voltage Headroom on the Internal Op Amp Inputs

Use a stable dc voltage to power the AD8276/AD8277. Noise on the supply pins can adversely affect performance. Place a bypass capacitor of $0.1 \mu \mathrm{~F}$ between each supply pin and ground, as close as possible to each supply pin. Use a tantalum capacitor of $10 \mu \mathrm{~F}$ between each supply and ground. The tantalum capacitor can be farther away from the supply pins and, typically, other precision integrated circuits can share the capacitor.

## APPLICATIONS INFORMATION

## CONFIGURATIONS

The AD8276/AD8277 can be configured in several ways (see Figure 42 to Figure 46). Note that Figure 43 shows the AD8276/AD8277 as difference amplifiers with a midsupply reference voltage at the noninverting input, allowing the AD8276/AD8277 to be used as a level shifter, which is appropriate in single-supply applications that are referenced to midsupply.
As with the other inputs, the reference must be driven with a low impedance source to maintain the internal resistor ratio. An example using the low power, low noise OP1177 as a reference is shown in Figure 41.


Figure 41. Driving the Reference Pin


Figure 42. Difference Amplifier, Gain $=1$


Figure 43. Difference Amplifier, Gain $=1$, Referenced to Midsupply


Figure 44. Inverting Amplifier, Gain $=-1$


Figure 45. Noninverting Amplifier, Gain $=1$


Figure 46. Noninverting Amplifier, Gain $=2$

## DIFFERENTIAL OUTPUT

Certain systems require a differential signal for improved performance, such as the inputs to differential analog-to-digital converters. Figure 47 shows how the AD8276/AD8277 can be used to convert a single-ended output from an AD8226 instrumentation amplifier into a differential signal. The internal matched resistors of the AD8276/AD8277 at the inverting input maximize gain accuracy while generating a differential signal. The resistors at the noninverting input can be used as a divider to set and track the common-mode voltage accurately to midsupply, especially when running on a single supply or in an environment where the supply fluctuates. The resistors at the noninverting input can also be shorted and set to any appropriate bias voltage. Note that the $V_{\text {bias }}=V_{\text {см }}$ node indicated in Figure 47 is internal to the AD8276/AD8277 because it is not pinned out, meaning that there is no direct connection to the inputs of the amplifier. Figure 47 represents a differential output amplifier configuration with the use of +OUT and -OUT.


Figure 47. Differential Output with Supply Tracking on Common-Mode Voltage Reference

The differential output voltage and common-mode voltage of the AD8226 is shown in the following equations:

$$
\begin{aligned}
& V_{\text {DIFF_OUT }}=V_{+ \text {OUT }}-V_{-O U T}=\text { Gain }_{A D 8226} \times\left(V_{+I N}-V_{-I N}\right) \\
& V_{C M}=\left(+V_{S}-\left(-V_{S}\right)\right) / 2=V_{\text {BIAS }}
\end{aligned}
$$

Refer to the AD8226 data sheet for additional information.


Figure 48. AD8277 Differential Output Configuration
The two difference amplifiers of the AD8277 can be configured to provide a differential output, as shown in Figure 48. This differential output configuration is suitable for various applications, such as strain gage excitation and single-ended-todifferential conversion. The differential output voltage has a gain of 2 as shown in the following equation:

$$
V_{\text {DIFF_OUT }}=V_{+ \text {OUT }}-V_{- \text {OUT }}=2 \times\left(V_{+I N}-V_{-I N}\right)
$$

## CURRENT SOURCE

The AD8276 difference amplifier can be implemented as part of a voltage to current converter or a precision constant current source, as shown in Figure 50. Using an integrated precision solution such as the AD8276 provides several advantages over a discrete solution, including space-saving, improved gain accuracy, and temperature drift. The internal resistors are tightly matched to minimize error and temperature drift. If the external resistors, R1 and R2, are not well matched, they become a significant source of error in the system. Therefore, precision resistors are recommended to maintain performance. The ADR4525 provides a precision voltage reference that also reduces error in the signal chain.
The AD8276 has rail-to-rail output capability that allows higher current outputs.

## VOLTAGE AND CURRENT MONITORING

Voltage and current monitoring is critical in the following applications: power line metering, power line protection, motor control applications, and battery monitoring. The AD8276/ AD8277 can be used to monitor voltages and currents in a system, as shown in Figure 49. As the signals monitored by the AD8276/AD8277 rise above or drop below critical levels, a circuit event can be triggered to correct the situation or raise a warning.


Figure 49. Voltage and Current Monitoring in 3-Phase Power Line Protection Using the AD8276

Figure 49 shows an example of how the AD8276/AD8277 can be used to monitor voltage and current on a 3-phase power supply. $I_{1}$ through $I_{3}$ are the currents to be monitored, and $V_{1}$ through $V_{3}$ are the voltages to be monitored on each phase. I $I_{C}$ and $V_{C}$ are the common or zero lines. Couplers or transformers interface the power lines to the front-end circuitry and provide attenuation, isolation, and protection.
On the current monitoring side, current transformers (CTs) step down the power line current and isolate the front-end circuitry from the high voltage and high current lines. Across the inputs of each difference amplifier is a shunt resistor that converts the coupled current into a voltage. The value of the resistor is determined by the characteristics of the coupler or transformer and desired input voltage ranges to the AD8276/AD8277.


Figure 50. Constant Current Source
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On the voltage monitoring side, potential transformers (PTs) are used to provide coupling and galvanic isolation. The PTs present a load to the power line and step down the voltage to a measurable level. The AD8276/AD8277 help to build a robust system because it allows input voltages that are almost double its supply voltage, while providing additional input protection in the form of the integrated ESD diodes.

Not only does the AD8276/AD8277 monitor the voltage and currents on the power lines, the AD8276/AD8277 are able to reject very high common-mode voltages that may appear at the inputs. The AD8276/AD8277 also perform the differential to single-ended conversion on the input voltages. The $80 \mathrm{k} \Omega$ differential input impedance that the AD8276/AD8277 presents is high enough that it does not load the input signals.


Figure 51. AD8276 Monitoring Current Through a Shunt Resistor
Figure 51 shows how the AD8276 can be used to monitor the current through a small shunt resistor ( $\mathrm{R}_{\text {sH }}$ ), which is useful in power critical applications such as motor control (current sense) and battery monitoring.

## INSTRUMENTATION AMPLIFIER

The AD8276/AD8277 can be used as building blocks for a low power, low cost instrumentation amplifier. An instrumentation amplifier provides high impedance inputs and delivers high CMRR. Combining the AD8276/AD8277 with an Analog Devices, Inc., low power amplifier (see Table 9) creates a precise, power efficient voltage measurement solution suitable for power critical systems.


Figure 52. Low Power Precision Instrumentation Amplifier

Table 9. Low Power Op Amps

| Op Amp (A1, A2) | Features |
| :--- | :--- |
| AD8506 | Dual micropower op amp |
| AD8607 | Precision dual micropower op amp |
| AD8617 | Low cost CMOS micropower op amp |
| AD8667 | Dual precision CMOS micropower op amp |

It is preferable to use dual op amps for the high impedance inputs because their performance is matched and track each other over temperature compared to discrete amplifiers. The AD8276 difference amplifiers cancel out common-mode errors from the input op amps, if they track each other. The differential gain accuracy of the in-amp is proportional to how well the input feedback resistors ( $\mathrm{R}_{\mathrm{F}}$ ) match each other. The CMRR of the inamp increases as the differential gain is increased $\left(1+2 R_{F} / R_{G}\right)$, but a higher gain also reduces the common-mode voltage range. Note that dual supplies must be used for proper operation of this configuration.
Refer to A Designer's Guide to Instrumentation Amplifiers for more design ideas and considerations.

## RTD

Resistive temperature detectors (RTDs) are often measured remotely in industrial control systems. The wire lengths needed to connect the RTD to a controller add significant cost and resistance errors to the measurement. The AD8276/AD8277 difference amplifier is effective in measuring errors caused by wire resistance in remote 3-wire RTD systems, allowing the user to cancel out the errors introduced by the wires. The gain drift of the AD8276/AD8277 provides accurate measurements and stable performance over a wide temperature range.


Figure 53. 3-Wire RTD Cable Resistance Error Measurement

## AD8276/AD8271

## DIE INFORMATION

DIE SPECIFICATIONS AND ASSEMBLY RECOMMENDATIONS
Table 10. Die Specifications

| Parameter | Value | Unit |
| :--- | :--- | :--- |
| Scribe Line Width | 90 | $\mu \mathrm{~m}$ |
| Die Size | $1390 \times 2085$ | $\mu \mathrm{~m}$ |
| Thickness | 305 | $\mu \mathrm{~m}$ |
| Backside | Negative supply | Not applicable |
| Passivation | 1 (silicon nitride) | $\mu \mathrm{m}$ |
| Polyimide | 18 | $\mu \mathrm{~m}$ |
| Bond Pads (Minimum) | $70 \times 70$ | $\mu \mathrm{~m}$ |
| Bond Pad Composition | 98.5 aluminum (Al)/1.0 silicon $(\mathrm{Si}) / 0.5$ copper (Cu) | $\%$ |

Table 11. Assembly Recommendations

| Assembly Component | Recommendation |
| :--- | :--- |
| Die Attach | Hitachi CEL 9240HF10AK |
| Bonding Method | Gold ball or aluminum wedge |
| Bonding Sequence | Unspecified |

## OUTLINE DIMENSIONS



Figure 54. 8-Lead Mini Small Outline Package [MSOP] (RM-8)
Dimensions shown in millimeters



Figure 56. 7-Pad Bare Die [CHIP] (C-7-8)
Dimensions shown in millimeters


ORDERING GUIDE

| Model ${ }^{1,2}$ | Temperature Range | Package Description | Package Option | Marking Code |
| :---: | :---: | :---: | :---: | :---: |
| AD8276ARMZ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | H1P |
| AD8276ARMZ-R7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead MSOP, 7" Tape and Reel | RM-8 | H1P |
| AD8276ARMZ-RL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead MSOP, 13" Tape and Reel | RM-8 | H1P |
| AD8276ARZ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8276ARZ-R7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead SOIC_N, 7" Tape and Reel | R-8 |  |
| AD8276ARZ-RL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead SOIC_N, 13" Tape and Reel | R-8 |  |
| AD8276BRMZ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | H1Q |
| AD8276BRMZ-R7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead MSOP, 7" Tape and Reel | RM-8 | H1Q |
| AD8276BRMZ-RL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead MSOP, 13" Tape and Reel | RM-8 | H1Q |
| AD8276BRZ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8276BRZ-R7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead SOIC_N, 7" Tape and Reel | R-8 |  |
| AD8276BRZ-RL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead SOIC_N, 13" Tape and Reel | R-8 |  |
| AD8276-CHIPS-WP | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 7-Pad Bare Die [CHIP], Waffle Pack | C-7-8 |  |
| AD8277ARZ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8277ARZ-R7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead SOIC_N, 7" Tape and Reel | R-14 |  |
| AD8277ARZ-RL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead SOIC_N, 13" Tape and Reel | R-14 |  |
| AD8277BRZ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8277BRZ-R7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead SOIC_N, 7" Tape and Reel | R-14 |  |
| AD8277BRZ-RL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 14-Lead SOIC_N, 13" Tape and Reel | R-14 |  |

[^2]
## X-ON Electronics

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[^0]:    ${ }^{1}$ Includes input bias and offset current errors, referred to output (RTO).
    ${ }^{2}$ The input voltage range can also be limited by the absolute maximum input voltage or by the output swing. See the Input Voltage Range section in the Theory of Operation section for details.
    ${ }^{3}$ Internal resistors are trimmed to be ratio matched and have $\pm 20 \%$ absolute accuracy.
    ${ }^{4}$ Output voltage swing varies with supply voltage and temperature. See Figure 19 through Figure 22 for details.
    ${ }^{5}$ Includes amplifier voltage and current noise, as well as noise from internal resistors.
    ${ }^{6}$ Supply current varies with supply voltage and temperature. See Figure 23 and Figure 25 for details.
    ${ }^{7}$ Unbalanced dual supplies can be used, such as $-V_{s}=-0.5 \mathrm{~V}$ and $+\mathrm{V}_{s}=+2 \mathrm{~V}$. The positive supply rail must be at least 2 V above the negative supply and reference voltage.

[^1]:    ${ }^{1}$ All dimensions are referenced from the center of the die to the center of each bond pad.

[^2]:    ${ }^{1} \mathrm{Z}=$ RoHS Compliant Part.
    ${ }^{2}$ The AD8276-CHIPS-WP is a RoHS Compliant Part.

