

# **AD8460**

# 110 V High Voltage, 1 A High Current, Arbitrary Waveform Generator with Integrated 14-Bit High Speed DAC

# **FEATURES**

- Wide high voltage supply range: ±12 V to ±55 V
- $\blacktriangleright$  High Output Capability
	- $\triangleright$  Output voltage range: Up to  $\pm 40$  V
	- $\blacktriangleright$  High output current drive: 1 A continuous
	- $\blacktriangleright$  High slew rate: ≥1800 V/µs into 1000 pF load
	- **Large signal bandwidth: 1 MHz**
- Extensive Programming and Diagnostics
	- ▶ 14-bit resolution arbitrary waveform generation (AWG) mode
	- ▶ 16 level analog pattern generation (APG) mode
	- $\triangleright$  Digitally programmable current, voltage and thermal fault monitoring and protection
	- $\blacktriangleright$  Programmable supply current with shutdown mode
- **Design-in Friendly** 
	- Unlimited capacitive load drive with external compensation and slew control
	- Package: 80-pin, 12mm x 12mm TQFP
		- EPAD-up package for mountable heatsink
	- Operating temperature range: −40 °C to +85 °C

# **APPLICATIONS**

- Automatic test equipment (ATE)
- Display panel formation and testing
- Piezo drivers
- Programmable power supplies



*Figure 1. Simplified Functional Block Diagram*

# **GENERAL DESCRIPTION**

The AD8460 is a "bits in, power out" high voltage, high-power, highspeed driver optimized for large output current (up to  $\pm 1$  A) and high slew rate (up to ±1800 V/μs) at high voltage (up to ±40 V) into capacitive loads. Combining a 14-bit high-speed DAC, a high voltage, high output current (HV-HI) analog driver, and fault monitoring and protection circuits, the AD8460 is ideally suited for high power applications such as arbitrary waveform generation (AWG), programmable power supplies, and high voltage automated test equipment (ATE).

A proprietary high-voltage BCDMOS process, novel high voltage architecture, and thermally enhanced package from Analog Devices Inc. enable this high-performance driver. A digital engine implements userconfigurable features: modes for digital input, programmable supply current, and fault monitoring and programmable protection settings for output current, output voltage, and junction temperature. Analog features extend functionality: external compensation enables unlimited capacitive load drive, programmable shutdown delay, and full-scale adjustment. The AD8460 operates on high voltage dual supplies up to ±55 V and a single low voltage supply of 5 V.



*Figure 2. Large Signal Pulse Response vs. Edge Speed with External Slew Control*

 $\approx$ 



# **AD8460**

110 V High Voltage, 1 A High Current, Arbitrary Waveform Generator with Integrated 14-Bit High Speed DAC



*Figure 3. Functional Block Diagram*

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# **REVISION HISTORY**

**10/2023 - Rev. 0**



# **SPECIFICATIONS**

#### **Table 1. Electrical Characteristics**

(HVCC = +50 V, HVEE = -50 V, SET\_IQ = 0x00, VCC\_5V = +5 V, VREF\_5V = +5 V, REFIO\_1P2V = +1.2 V, R<sub>TERM</sub> = 50 Ω, R<sub>SET</sub> to FS\_ADJ = 2 k $\Omega$ , COMP\_L, COMP\_H = 0 pF, C<sub>LOAD</sub> = 1 nF, T<sub>C</sub> = 30°C, unless otherwise noted.)



 $(HVCC = +50 V, HVEE = -50 V, SET_lQ = 0x00, VCC_5V = +5 V, VREF_5V = +5 V, REFIO_1P2V = +1.2 V, R<sub>TERM</sub> = 50 Ω, R<sub>SET</sub>$ to FS\_ADJ = 2 kΩ, COMP\_L, COMP\_H = 0 pF, C<sub>LOAD</sub> = 1 nF, T<sub>c</sub> = 30°C, unless otherwise noted.)









 $(HVCC = +50 V, HVEE = -50 V, SET_lQ = 0x00, VCC_5V = +5 V, VREF_5V = +5 V, REFIO_1P2V = +1.2 V, R<sub>TERM</sub> = 50 Ω, R<sub>SET</sub>$ to FS\_ADJ = 2 kQ, COMP\_L, COMP\_H = 0 pF,  $C<sub>LOAD</sub>$  = 1 nF, T<sub>C</sub> = 30°C, unless otherwise noted.)



 $HVCC = +50 V, HVEE = -12 V$ 

to -55 V 106  $\begin{vmatrix} 106 \\ 106 \end{vmatrix}$  dB

 $(HVCC = +50 V, HVEE = -50 V, SET$  = 0x00, VCC\_5V = +5 V, VREF\_5V = +5 V, REFIO\_1P2V = +1.2 V, R<sub>TERM</sub> = 50 Ω, R<sub>SET</sub>



<sup>2</sup> These specifications are referred to the output of the AD8460.

 $3$  FSR = Full scale range

Power Supply Rejection

Ratio

<sup>4</sup> This output voltage swing is set by the device's default configuration.

PSRRHVEE

- <sup>5</sup> See *Thermal Management* section for more details.
- <sup>6</sup> The AD8460 has been lifetime tested with a 1 nF load, driven with an 80 Vp-p square wave at 1 kHz.
- <sup>7</sup> See the VREF\_5V section for details on the effects of supply variations on this pin.
- 8 The absolute maximum junction temperature is 150°C.
- <sup>9</sup> Guaranteed by design and characterization, not production tested.
- <sup>10</sup> T<sub>J</sub> = 30 °C to 105 °C

#### **Table 2. TIMING CHARACTERISTICS**

 $(HVCC = +50 V, HVEE = -50 V, SET_lQ = 0x00, VCC_5V = +5 V, VREF_5V = +5 V, REFIO_1P2V = +1.2 V, R<sub>TERM</sub> = 50 Ω, R<sub>SET</sub>$ to FS\_ADJ = 2 k $\Omega$ , COMP\_L, COMP\_H = 0 pF, C<sub>LOAD</sub> = 1 nF, T<sub>J</sub> = 30 °C to 105 °C, unless otherwise noted.)



<sup>1</sup> Guaranteed by design and characterization, not production tested.

<sup>2</sup> For details on the maximum achievable output frequency, see *Figure 26* and *Thermal Management* section.

# **Timing Diagrams**







#### *Figure 5. SPI Timing Diagram (Write Operation)*





# **ABSOLUTE MAXIMUM RATINGS**

 $T_A$  = 25 °C, unless otherwise specified.

#### **Table 3. Absolute Maximum Ratings**



<sup>1</sup> Subject to  $T_J \le 150$  °C

- 2 Extended operation of Tj at or near the absolute maximum junction temperature rating accelerates device aging. Ensure proper thermal management.
- <sup>3</sup> RoHS-compliant assemblies (20 sec to 40 sec)

Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only. Functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

### **Thermal Resistance**

Thermal performance is directly linked to PCB design and operating environment. Close attention to PCB thermal design is required. To keep the junction temperature  $(T<sub>J</sub>)$  below the absolute maximum rating, it is typically required to incorporate thermal management techniques. See the *Thermal Management* section for more details.

θ<sub>JA</sub> is the natural convection, junction-to-ambient thermal resistance.  $θ<sub>JC</sub>$  is the junction-to-case thermal resistance.

#### **Table 4. Thermal Resistance**



*<sup>1</sup>* Thermal impedance simulated values based on JEDEC JESD-51. For θJA with heatsink and airflow. See the *Thermal Management* section.

*2* Includes derating across the die.

*<sup>3</sup>* Equal power dissipation across the die.

## **Electrostatic Discharge (ESD)**

The following ESD information is provided for handling of ESD-sensitive devices in an ESD protected area only. Human body model (HBM) per ANSI/ESDA/JEDEC JS-001. Field induced charged device model (FICDM) per ANSI/ESDA/JEDEC JS-002.

#### **Table 5. AD8460 80-Lead TQFP**



### **ESD Caution**



# **PIN CONFIGURATION AND FUNCTION DESCRIPTIONS**



*Figure 7. Top View with Pin 1 in Upper Left and Pin Numbers Ascending Anticlockwise* **Table 6. Pin Function Descriptions**







### **INTERPRETING TYPICAL PERFORMANCE CURVES**

The AD8460's performance parameters are fundamentally dependent on junction temperature  $(T<sub>0</sub>)$ , which may be significantly higher than ambient temperature  $(T_A)$ . For this reason, all AD8460 typical performance curves (TPCs) relating to temperature are represented as a function of  $T_J$  (axis at bottom of plot), which can be measured through the TMP pin. See the TMP section for information on direct die temperature measurement.

To present a complete picture,  $T_A$  is shown as an alternative scale at the top of the plot. Refer to  $T_A$  scale for estimation of junction temperature when the TMP pin is not monitored. The relation between TJ and TA is valid for the default thermal management configuration and the specified test conditions indicated for each plot. See the *Thermal Management* section for the relationship among TJ, TA, and power dissipation.

Finally, note that each curve on a temperature−based TPC has both a solid and a dashed section. The solid portion represents typical performance that is exhibited when using the recommended passive heat sinking configuration. The dashed portion represents typical performance that is achievable when using active thermal management, such as with forced air or liquid cooling. See the *Thermal Management* section for more information.

# **TYPICAL PERFORMANCE CHARACTERISTICS**

HVCC = + 50 V, HVEE = - 50 V, SET\_IQ = 0x00, VCC\_5V = + 5 V, VREF\_5V = + 5 V, REFIO\_1P2V = + 1.2 V, RTERM = 50  $\Omega$ , Rsετ to FS\_ADJ = 2 kΩ, COMP\_L, COMP\_H = 0 pF, CLOAD = 1 nF, Tc = 30°C, unless otherwise noted.



*Edge, CLOAD = 1 nF*



*Figure 9. Falling Edge - Large Signal Pulse Response vs. CCOMP, Falling Edge, CLOAD = 1 nF*

**–60 –50 –40 –30 –20 –10 0 10 20 30 40 50 60**

**VOUT (V)**



*Figure 10. Large Signal Pulse Response vs. CLOAD, Rising Edge Figure 11. Large Signal Pulse Response vs. CLOAD, Falling* 





*Figure 12. Large Signal Pulse Response vs. Edge Speed, CLOAD = 1 nF, CCOMP = None*



*Rising Edge*



121

130



**TIME (100ns/DIV)**

*Figure 13. Small Signal Pulse Response vs. Temperature, Rising Edge, V*<sup>OUT</sup> = 100 mV p-p



*Figure 15. Small Signal Pulse Response vs. Temperature, Falling Edge, V*<sub>*OUT</sub>* = 100 mV p-p</sub> 132



*Figure 16. Large Signal Pulse Response vs. Temperature, Falling Edge*



*Figure 18. Pulse Response vs. Temperature, Rising Edge, VOUT = 80 V p-p* **TIME (100ns/DIV)**



*VOUT = 10 V p-p*



*Figure 17. Pulse Response vs. Temperature, Falling Edge, VOUT = 80 V p-p*



*Figure 19. Pulse Response vs. Temperature, Falling Edge, VOUT = 10 V p-p* **TIME (100ns/DIV)** 136



*VOUT = 1 V p-p*







*Figure 24. Large Signal Pulse Response Overshoot vs. CLOAD and CCOMP, Positive Overshoot*



*Figure 26. Large Signal Bandwidth, CLOAD = 1 nF, CCOMP = None*



*Figure 23. Large Signal Pulse Response Overshoot vs. CLOAD and CCOMP, Negative Overshoot*



*Figure 25. Large Signal Bandwidth, CLOAD = 22 nF, CCOMP = 10 pF*



*Figure 27. Small Signal Frequency Response vs. CLOAD, T<sup>J</sup> = 85 °C*



*Figure 28. Large Signal Bandwidth, CLOAD = 47 nF, CCOMP = 20* 



*Figure 30. Small Signal Frequency Response vs. CLOAD, T<sup>J</sup> =* 



*Temperature, CLOAD = 1 nF, CCOMP = None*



*Figure 29. Small Signal Frequency Response vs. CLOAD, T<sup>J</sup> = 150 °C*



*Figure 31. Small Signal Frequency Response vs. Temperature, CLOAD = 22 nF, CCOMP = 10 pF*



*Temperature, CLOAD = 1 nF, CCOMP = None*

# **Data Sheet AD8460**





*Figure 38. Slew Rate vs. Output Amplitude Figure 39. Settling Time to 0.1% and 1%, V<sub>out</sub> = 10 Vp-p, V<sub>s</sub> = ±55 V, CLOAD = 1 nF, CCOMP = None*







*Figure 46. Output Impedance vs. Frequency, Enabled Figure 47. Output Impedance vs. Frequency, Disabled*







*Figure 50. Supply Current and Amplitude vs. Frequency, Square Wave, No Heatsink, CLOAD = 1 nF, CCOMP = None*







*Figure 51. Supply Current and Amplitude vs. Frequency Square Wave, with Heatsink, CLOAD = 1 nF, CCOMP = None*



*Figure 52. Supply Current and Amplitude vs. Frequency Square Wave, with Heatsink and Airflow, CLOAD = 1 nF, CCOMP = None*



*Figure 54. High Voltage Quiescent Supply Current vs. Temperature, V<sub>s</sub>* = ±50 V





*Figure 53. Junction Temperature vs. Internal Power Dissipation*



*Figure 55. VCC\_5V Quiescent Supply Current vs. Temperature, VCC\_5V = 5 V*



*Figure 56. Shutdown Response vs. Time Figure 57. Shutdown Response vs. SDNIO Capacitance*

# **TERMINOLOGY**

#### **Alarm**

Alarm refers to the detection of any ofthe five fault conditions monitored by the protection system: overcurrent (sourcing or sinking), overvoltage (positive or negative), or overtemperature. The alarm flag is customizable to either self-clear upon fault clear, or latch the alarm state as evidence of fault occurrence. When any alarm is latched, it must be cleared.

#### **Analog Pattern Generation (APG) Mode**

The APG mode is analogous to the operation of a digital pattern generator. In the AD8460, an analog pattern of up to 16 sequential elements may be created, with each element containing an analog voltage rather than a digital voltage (logic state). Each analog voltage value is represented by 14-bit data. Voltage data is loaded serially through serial peripheral interface (SPI) into pattern memory prior to updating driver output. The APG mode is recommended for simple, repetitive waveforms consisting of sequential voltage levels.

#### **Arbitrary Waveform Generation (AWG) Mode**

The AWG mode is analogous to the operation of an arbitrary waveform generator. Digital data is presented in parallel fashion to the DAC and the driver output is updated synchronously with the data transfer, allowing waveforms to be created in real time. The AWG mode is recommended for complex or non-repetitive waveforms.

#### **Arm**

To arm the protection system is to put the driver into a mode where it detects an alarm condition and shuts down the device.

#### **Disarm**

To disarm the driver is to put it into a state where it ignores an alarm condition and does not shut down the device. Use extreme caution when the driver is disarmed as it is unprotected from faults and possible damage.

#### **Fault**

A fault is any of the five overload conditions detectable by the protection system. Any fault triggers an alarm, though an alarm must exist for some minimum (user-adjustable) duration to force a shutdown.

#### **Protection System**

The protection system comprises limit-setting DACs, comparators, and logic gates that detect faults according to user-specified limits. See *Figure 64* for a block diagram showing basic functionality.

#### **Reserved**

Reserved refers to internal registers not for user access.

#### **Safe Operating Area (SOA)**

The safe operating area is a two-dimensional envelope bounded by parameters the user must manage to prevent damage from overheating.

#### **Shutdown and Sleep**

Both shutdown and sleep refer to a state of inactivity characterized by floating (high impedance) output and greatly reduced power consumption. Shutdown may be initiated by the user, by pulsing SDN\_IO high, or may be initiated by the protection system in response to an alarm of sufficient duration. If there is any parasitic or added capacitance to SDN\_IO, wait until the SDN\_IO voltage goes below its threshold voltage before trying to exit shutdown. To exit shutdown, use any of the following three ways:

**Pulse SDN\_RESET high, then leave low.** 

- Pulse the HV\_RESET bit high through two SPI commands (drive high, then drive low).
- Pulse SDN\_IO low, then float.

Sleep refers to a non-latching state of inactivity like shutdown, but which is initiated (HV\_SLEEP = 0) and terminated (HV\_SLEEP = 1) through SPI commands. Sleep supersedes all commands that use the SDN\_IO shutdown mechanism, both fault-initiated and user-initiated. See *Figure 64* for a logic diagram of the protection system and shutdown mechanism.

#### **Slew Boost**

Slew boost refers to a design feature of the AD8460 that increases supply current during fast input signal transitions, permitting faster output slew without the continuous power-dissipation penalty of conventional high-speed amplifiers.

#### **Span**

Span refers to the difference between the highest and lowest output values. The AD8460 has a nominal span of 80 V (+40 V - (−40 V)).

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# **THEORY OF OPERATION**



*Figure 58. AD8460 Standard Configuration*

### **Overview**

The AD8460 is a "bits in, power out" high voltage, high-power, high-speed driver optimized for large output current (up to  $\pm 1$  A) and high slew rate (up to  $\pm 1800$  V/ $\mu$ s) at high voltage (up to  $\pm 40$  V) into capacitive loads. Combining a 14-bit high-speed DAC, a high voltage, high output current (HV-HI) analog driver, and fault monitoring and protection circuits, the AD8460 is ideally suited for high power applications such as arbitrary waveform generation (AWG), programmable power supplies, and high voltage automated test equipment (ATE).

The input to the system is provided as a 14 bit digital DAC code. The part can either operate in the analog pattern generation (APG) or arbitrary waveform generation (AWG) mode. In the APG mode, SPI communication is used to write up to 16 levels into digitalregisters, and clocking SYNC updates the output, serially proceeding to each next level in the table. In the AWG mode, the DAC uses 14 parallel digital inputs DB0 to DB13, and clocking SYNC updates the output. See *INPUT AND MODE OF OPERATION* .

With configurable DAC parameters R<sub>SET</sub>, V<sub>REFIO\_1P2V</sub>, and R<sub>TERM</sub> = 50  $\Omega$ , the driver output transfer function is equal to:

$$
V_{OUT}=\left(80\ V\times\left(\frac{DAC\ CODE}{2^{14}}\right)-40\ V\right)\times\left(\frac{2\ k\Omega}{R_{SET}}\right)\times\left(\frac{V_{REFIO_{1P2V}}}{1.2\ V}\right)
$$

Under conventional V<sub>REFIO\_1P2V</sub> = 1.2 V, R<sub>SET</sub> = 2 kΩ, and R<sub>TERM</sub> = 50 Ω, the driver output transfer function simplifies to:

$$
V_{OUT} = \left(80 V \times \left(\frac{DAC\ CODE}{2^{14}}\right) - 40 V\right)
$$

The maximum output swing is established by the internal DAC configuration. See *FULL-SCALE ADJUSTMENT*.

The AD8460 requires dual high voltage (up to ±55 V) power supplies at HVCC and HVEE, and a single low voltage (5 V) power supply at VCC\_5V. The part generates 3.3 V internally from a LDO output at AVDD\_3P3V, and DVDD\_3P3V is an internal digital supply bypass point that should be connected to AVDD\_3P3V. See *POWER SUPPLIES AND DECOUPLING*.

A reference of 5 V is required at VREF\_5V to provide the reference voltage for analog low voltage and protection threshold DACs. Connect VREF\_5V to an external 5 V reference or to VCC\_5V (reduced accuracy). The AD8460 utilizes a reference of 1.2 V at REFIO\_1P2V to provide the reference voltage for the high-speed DAC. Connect REFIO\_1P2V to an external 1.2 V reference or float to use the internal 1.2 V reference, which can give rise to reduced accuracy. See *REFERENCE OPERATION*. An external resistor R<sub>SET</sub> connected to FS\_ADJ establishes the internal DAC's reference current  $I_{REF}$ . When  $R_{SET} = 2 kΩ$ , as in *Figure 58*, the DAC's full scale complementary output currents are set to the nominal value of 20 mA. See *FULL-SCALE ADJUSTMENT.*

The DACand the high-voltage, high-current(HV-HI) output driver canbe connected externally through pin IOUTP and INPonthe high side, and pinIOUTNandINNonthe low side. The termination resistors (R<sub>TERM</sub>) set the inputs to the HV-HI driver. The R<sub>TERM</sub> resistors are recommended to be high precision 50  $\Omega$ . The % tolerance on the  $R_{TERN}$  corresponds to possible error at the output. Typically, a tolerance of 0.1% is recommended in systems that balance precision and cost. 0.01% resistors are recommended for higher precision systems.

In addition to drive capability, the AD8460 provides a suite of features relating to fault monitoring and load protection. The part features a junction temperature monitor providing voltage at output indicating junction temperature up to 2.5 V at maximum junction temperature of 150 °C. The digital engine allows for programmable output current limit (source current and/or sink current), programmable output voltage limit (positive voltage and/or negative voltage), and programmable temperature limit (maximum junction temperature). See *SHUTDOWN PROTECTION SETTINGS*.

## **INITIAL POWER-UP**

#### **POWER SUPPLIES AND DECOUPLING**

The AD8460 requires dual high voltage supplies in the range of  $\pm 12$  V to  $\pm 50$  V at HVCC and HVEE, as well as a single 5 V low voltage supply at VCC\_5V. Bypass all supply pins to ground using high quality, low ESR 0.1 μF capacitors.

Place bypass capacitors as close to the supply pins as possible, with a short, direct connection to the PCB's analog ground plane. Additionally, place four 1.2 μF ceramic capacitors from each high voltage supply to ground to provide good low frequency bypassing, and to provide the needed current to support large, fast-slewing signals. Low-inductance planes are recommended for high voltage supply routing.

AVDD\_3P3V is the analog supply bypass point for the internal 3.3 V LDO. AVDD\_3P3V requires a 0.1 µF bypass capacitor from AVDD\_3P3V to GND. Connect AVDD\_3P3V to DVDD\_3P3V.

#### **VREF\_5V**

VREF\_5V sets the reference voltage for internal alarm threshold DACs and needs to be biased. A precise 5 V reference IC is recommended. Alternatively, VREF\_5V can be connected to VCC\_5V (reduced accuracy).

A reduced accuracy VREF\_5V reference shifts the internal LDO reference voltage and causes the SDN\_IO shutdown voltage, overvoltage, and overtemperature thresholds to vary from table specified values. For example, if a 5 V reference with 1% tolerance at VREF\_5V is utilized, these levels may vary 1% from typical values.

The order of VCC\_5V and VREF\_5V power-on affects the initial state of the HV-HI driver. See *POWER SUPPLY SEQUENCING*.

#### **POWER SUPPLY SEQUENCING**

DVDD\_3P3V must be tied to AVDD\_3P3V before power-up. The high voltage power supplies (HVCC and HVEE) and VCC\_5V may be brought up individually, in any order.

AD8460 can be powered up in shutdown or active mode. Powering the AD8460 in shutdown mode is recommended and this can be accomplished by powering on VCC\_5V before VREF\_5V. After initial power-up in shutdown mode, the SDN\_IO pin must be pulled low to ensure the AD8460 is turned on. Subsequently, floating the SDN\_IO pin enables the fault monitoring and protection feature while the AD8460 remains on. When powering down, bring VREF\_5V down first, then bring down VCC\_5V.

If VCC\_5V is powered on connected to VREF\_5V, the part powers on with the driver enabled and DAC disabled. Use extreme caution when powering up in active mode as the output voltage can power on at high voltage. This may result in high output current.

#### **REFERENCE OPERATION**

The AD8460 internal DAC contains an internal 1.2 V band gap reference. The internal reference cannot be disabled, but can be easily overridden by an external reference for greater output accuracy. *Figure 59* shows a representative circuit of the band gap reference. Pin REFIO\_1P2V serves as either an output or an input depending on whether the internal or an external reference is used. To use the internal reference, simply decouple the REFIO\_1P2V pin to GND with a 0.1 μF capacitor. The internal reference voltage is present at REFIO\_1P2V. If the voltage at REFIO\_1P2V is to be used anywhere else in the circuit, an external buffer amplifier with an input bias current of less than 100 nA should be used. *Figure 60* shows an example of buffered internal reference configuration.



*Figure 59. Representative Circuit of Internal Reference* 



*Figure 60. Buffered Internal Reference Configuration*

An external reference can be applied to REFIO\_1P2V, as shown in *Figure 61*. The external reference may provide either a fixed reference voltage to enhance accuracy and drift performance or a varying reference voltage for gain control. Note that the 0.1 μF compensation capacitor may not be required since the internal reference is overridden, and the relatively high input impedance of REFIO\_1P2V minimizes loading of the external reference.



*Figure 61. External Reference Configuration* 

### **INPUT AND MODE OF OPERATION**

The AD8460 can generate waveforms in either the analog pattern generation (APG) or arbitrary waveform generation (AWG) mode.

The APG mode is used when the desired waveform is a series of sequential DC voltage levels, and edge speed control is not a requirement. In the APG mode, a pattern of up to 16 discrete DC voltage levels is loaded serially into pattern memory through the SPI. After a pattern is loaded, SYNC is used to clock pattern data to the output. 14-bit data is latched into the DAC on the rising edge of SYNC, and the data pointer advances to the next register on the subsequent falling edge. After the final value in pattern memory is sent to the DAC, the data pointer returns to the first data register and the pattern loops as long as SYNC is clocked. In the APG mode, the parallel data port (pins DB13:DB0) must be floated, as these pins are driven internally by the digital engine.

In the AWG mode, 14-bit digital input data representing the desired waveform is loaded through the parallel interface (pins DB13:DB0) and clocked in on the rising edge of SYNC, corresponding to conventional parallel mode high-speed DAC usage to update the output. The AWG mode is used when complex waveforms, specific edge speeds, or digital predistortion are required. *Table 7* briefly compares the APG and AWG input modes.





## **ANALOG PATTERN GENERATION (APG)**

To enable the APG mode, set the APG\_MODE\_ENABLE bit to (1) in the CTRL\_REG\_02 register and then set WAVE\_GEN\_MODE bit to (1) in the CTRL\_REG\_00 register.

The pattern is generated in non-real time and data is loaded serially through SPI into pattern memory prior to updating the driver output. The SYNC signal loads the DAC input on its rising edge based on the values in the pattern memory in the HVDAC\_DATA\_REGMAP and updates the driver output on its falling edge. The pattern loops if SYNC is pulsed. The maximum SYNC rate for APG mode is 20 MHz.

In HVDAC\_DATA\_REGMAP, each 14 bit level is stored in a combination of two 8 bit registers, containing the low order byte and high order byte. For example, the first level in the pattern is stored in HVDAC\_DATA\_BYTE\_00 and HVDAC\_DATA\_BYTE\_01, If the first level is 14 bit binary sequence  $b_{13}b_{12}b_{11}b_{10}b_9b_8b_7b_6b_5b_4b_3b_2b_1b_0,$ HVDAC\_DATA\_BYTE\_00 contains the 8 low order bits (binary  $b_7b_6b_5b_4b_3b_2b_1b_0$ ), and HVDAC\_DATA\_BYTE\_01 contains the 8 high order bits (binary  $b_\emptyset b_\emptyset b_{13}b_{12}b_{11}b_{10}b_\emptyset b_8)$ , where the first two bits are reserved. The second level in the pattern is stored in HVDAC\_DATA\_BYTE\_02 and HVDAC\_DATA\_BYTE\_03, and so forth.

The default pattern memory value produces a 4-level, ±20 V up-down sequential staircase waveform at a frequency defined by the SYNC clock rate, as shown in *Figure 62*. These default values may be overwritten through SPI. The APG mode generates analog pattern of up to 16 sequential voltage levels. The pulse width for each voltage level is defined by the SYNC clock rate and can be calculated by:

$$
Pulse Width = \frac{\frac{1}{SYNC \text{ clock Rate}}}{\text{# of Sequential Voltage Levels}}
$$

Assume the SYNC clock rate is 1 MHz and the output is a 2-level sequential pulse, the pulse width is:



*Figure 62. APG Mode Reference Example*

## **ARBITRARY WAVEFORM GENERATION (AWG)**

The AD8460 powers on by default in the AWG mode.

Clear the APG\_MODE\_ENABLE bit to 0 in the CTRL\_REG\_02 register and clear the WAVE\_GEN\_MODE bit to 0 in the CTRL\_REG\_00 register to select the AWG mode. The waveform is generated in real-time and data is loaded into registers through the parallel data port. The SYNC signal loads the HVDAC on its rising edge and updates the driver output on its falling edge. The maximum SYNC rate for the AWG mode is 100 MHz.

In the AWG mode, operation is essentially that of a high-speed DAC. The user provides 14-bit parallel data to pins DB0 to DB13 and provides a SYNC clock. Data is usually provided through the user field-programmable gate array (FPGA).



*Figure 63. AWG Mode Reference Example*

### **PREDISTORTION AND ADJUSTABLE INPUT EDGE SPEED**

Capacitive loading, cable length, and edge speed may produce distortion in the AD8460's transient settling characteristic, such as overshoot and ringing. The AWG mode allows the users to modify the waveform data to minimize this distortion. The modifications include adding an inverse characteristic to improve the shape of the response or adjusting the input edge to a slower speed.

The predistortion feature creates an input waveshape with undershoot, which can be used to compensate the overshoot for a given load. While this can be done in both the AWG and APG modes, the AWG mode provides higher resolution and therefore better distortion cancellation in all but the simplest waveforms.

In the AWG mode, it is possible to provide input data to the DAC at a higher sample rate, using a faster SYNC clock than is available in the APG mode. This allows the user to shape the input edges to smaller steps. By increasing the steps width, the user can adjust the input edge speed to any user-specified value. A slower edge speed reduces overshoot on a given cap load.

The number of steps needed during an edge event is calculated by Eq. 1:

$$
n_{STEPS} = \frac{AMPLITUDE_{P-P} (V) \times f_{SYNC} (MHz)}{EDGE SPEED(\frac{V}{\mu s})}
$$
 (Eq. 1)

For a 100 MHz clock and a step of 80 V, 100 steps are needed. To produce a linear output, the number of bits per step is  $\bigl\lfloor2^{14}/n_{\rm STEPS}\bigr\rfloor$ , in this case 163. A state machine can be implemented in HDL to control an edge event, or the edge may be a part of a longer pattern of codes. Examples of edge speed can be found in *Figure 12* in the *Typical Performance Characteristics* section.

### **OUTPUT CURRENT DRIVE**

The AD8460's output stage is constructed with cascoded, double diffused, metal-oxide-semiconductor (DMOS) high voltage transistors and is optimized for high currents into capacitive loads. It is designed to generate edge speeds of up to 1800 V/μs and deliver ±1 A continuously with proper thermal management. The default heatsink for AD8460 is Wakefield-Vette P/N 518-95AB and active cooling is preferred for higher power dissipation applications. See *Thermal Management* for thermal related details.

The AD8460's protection system is highly configurable to suit a wide variety of applications. To provide maximum flexibility across applications, the AD8460 integrates independent monitoring of output current (sourcing and sinking), output voltage (positive and negative), and die temperature, providing protection for the driver and its load against five individual faults. See *FAULT MONITORING AND PROTECTION* for details.

The AD8460 is configured with protection features disabled by default. Use SPI to enable and program the protection features. For manual overtemperature shutdown, tie SDN\_IO pin to TMP. The shutdown response time can be adjustable through a capacitor on SDN\_IO pin. See *SHUTDOWN CONTROL (SDN\_IO)* for delayed shutdown and manual thermal shutdown.

### **FAULT MONITORING AND PROTECTION**

Fault monitoring and protection are implemented by setting thresholds and arming the protection system for each fault type individually. Thresholds are programmed through SPI for the desired protections to be implemented. Exceeding a programmed threshold triggers an alarm and shuts down the AD8460. *Figure 64* shows the control logic for the fault monitoring and protection.

Each of the five monitored faults has four digital registers associated with it:

- 1. A programmable threshold. The threshold can be programmed through register 0x08 (CTL\_REG\_08) through 0x0C (CTL\_REG\_12), bit [6:0]. See *SHUTDOWN PROTECTION SETTINGS* for ranges and resolutions settings.
- 2. ARM. The ARM can be programmed through register 0x08 (CTL REG 08) through 0x0C (CTL REG 12), bit [7]. Setting the corresponding ARM to (1) directs the protection system to shut down in response to an alarm. Setting the corresponding ARM to (0) disarms the protection system, inhibiting shutdown in case of an alarm. There is no protection from faults when ARM is (0).
- 3. ALARM indicator flags. ALARM indicator flags can be read and cleared through register 0x0E (CTRL\_ REG\_14). ALARM indicator flags are set to (1) by the protection system if a fault occurs while the protection system is armed. ALARM remains at (1) for as long the fault condition persists and returns to (0) when the fault condition clears. If the ALARM forces a shutdown of the driver, the driver remains in shutdown even if the fault condition clears and the ALARM flag resets. The ALARM bits indicate the status of the fault conditions. Once the ALARM clears, it may not be possible to determine what fault(s) occurred previously. See the ALARM\_LATCH function for transient faults detections. To clear an ALARM indicator flag, write a (1) to the respective ALARM register bit.
- 4. ALARM LATCH is set by the user to latch any ALARM flag, preserving evidence of any transient fault that may occur. ALARM\_LATCH can be programed through register 0x0D (CTRL\_REG\_13). When an ALARM\_LATCH is enabled and when an ALARM indicator flag is triggered, the ALARM indicator flag remains even if the associated fault condition clears. This is helpful in identifying transient faults. To clear an ALARM\_LATCH flag, write a (0) to the respective ALARM\_LATCH register bit.



*Figure 64. Fault Monitoring and Protection Control Logic*

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### **FAULT-INITIATED SHUTDOWN PROTECTION FEATURES**

The AD8460 is equipped with a power saving shutdown feature through SDN\_IO. The shutdown can be either userinitiated to reduce power dissipation or fault-initiated by AD8460's protection system to prevent part damage. See *SHUTDOWN CONTROL (SDN\_IO)* for user-initiated shutdown details. The AD8460 monitors five operating conditions internally and may be configured to shut down if any programmable alarm limit is exceeded:

- Sourcing overcurrent limit (to  $+1$  A)
- Sinking overcurrent limit (to −1 A)
- Positive overvoltage limit (to +55 V)
- Negative overvoltage limit (to −55 V)
- $\blacktriangleright$  Junction overtemperature limit (T<sub>J</sub> = 20°C to T<sub>J</sub> = 150°C)

See *Table 24* through *Table 28* or register addresses assigned to these limits.

Any of the five internal fault monitors latch the SDN\_IO pin high if an alarm condition is detected. The latch condition persists until the fault condition is cleared and the AD8460 is re-enabled.

To re-enable the driver after shutdown, pulse the HV\_RESET bit high through two SPI (drive high, then drive low). The AD8460 can also be re-enabled by pulsing SDN\_RESET high, then leaving it low or pulling SDN\_IO low and then floating the SDN\_IO pin. This re-enables the fault monitoring and protection. The digital resource used to pulse SDN\_IO low must be capable of driving ~180 µA to override SDN\_IO's high state. See *SHUTDOWN CONTROL (SDN\_IO)* for details.

### **SHUTDOWN PROTECTION SETTINGS**

The code range for the shutdown protection features exceeds the device's operational range; the range is selected to optimize linearity and accuracy at the limitations of the part, where shutdown control is most critical. It should be noted that the values from *Table 9* to *Table 11* are rounded values to trigger at values that are smaller than the desired trigger point and are not the exact values based on the conversion factor from the code to threshold value.

*Table 8* shows the shutdown ranges and resolutions.





#### **PROGRAMMING OVERCURRENT PROTECTION**

The threshold programming resolution (1 LSB) for overcurrent protection is nominally 15.625 mA.

To convert code to current threshold:

$$
Current Threshold (mA) = Code_{Decimal}(LSB) \times 15.625 \left(\frac{mA}{LSB}\right)
$$

To convert current to code:

$$
Code_{Decimal}(LSB) = \frac{15.625 \left(\frac{mA}{LSB}\right)}{Current Threshold (mA)}
$$
If the user converts the desired current into a code in decimal, round down the calculated value to the nearest integer. Plug the integer value back into the code-to-current-threshold equation to determine the actual temperature threshold value.

See *Table 9* for typical threshold codes tied to common operating currents.

See the *PROGRAMMING SHUTDOWN THRESHOLD SETTINGS* on how to properly program the shutdown threshold settings.





#### **PROGRAMMING OVERVOLTAGE PROTECTION**

The threshold programming resolution (1 LSB) for overvoltage protection is nominally 1.953 V.

To convert code to voltage threshold:

$$
Voltage Threshold (V) = Code_{Decimal}(LSB) \times 1.953 \left(\frac{V}{LSB}\right)
$$

To convert voltage to code:

$$
Code_{Decimal}(LSB) = \frac{1.953 \left(\frac{V}{LSB}\right)}{Voltage Threshold (V)}
$$

If the user converts the desired voltage into a code in decimal, round down the calculated value to the nearest integer. Plug the integer value back into the code-to-voltage-threshold equation to determine the actual temperature threshold value.

See *Table 10* for typical threshold codes tied to common operating voltages.

See the *PROGRAMMING SHUTDOWN THRESHOLD SETTINGS* section on how to properly program the shutdown threshold settings.

#### **Table 10.Typical Threshold Codes for Operating Voltages**





### **PROGRAMMING OVERTEMPERATURE PROTECTION**

The threshold programming resolution (1 LSB) for overtemperature protection is nominally 6.51°C.

To convert code to temperature:

Temperature Threshold (°C) = 
$$
Code_{Decimal}(LSB) * 6.51 \left(\frac{{}^{\circ}\text{C}}{LSB}\right)
$$
 - 266.64 (°C)

To convert temperature to code:

$$
Code_{Decimal}(LSB) = Temperature Threshold \text{ (°C)} + \frac{266.64 \text{ (LSB)}}{6.51 \left(\frac{^{\circ}\text{C}}{LSB}\right)}
$$

If the user converts the desired temperature into a code in decimal, round down the calculated value to the nearest integer. Plug the integer value back into the code-to-temperature equation to determine the actual temperature threshold value.

See *Table 11* for typical threshold codes tied to common operating temperatures.

See the *PROGRAMMING SHUTDOWN THRESHOLD SETTINGS* section on how to properly program the shutdown threshold settings.



### **Table 11.Typical Threshold Codes for Operating Temperatures**

### **PROGRAMMING SHUTDOWN THRESHOLD SETTINGS**

The register map in *Table 18* shows that the 8-bit registers, CTRL\_REG\_08 through CTRL\_REG\_12, are used to arm the five internal fault monitors and program the desired threshold value. For these internal fault monitoring registers, bit 7 is used for toggling the protection feature on or off, and bits [6:0] are used for setting the alarm threshold. It is important to note that the binary codes in *Table 9* to *Table 11* are bits [6:0] when programming the registers for fault monitoring and does not include bit 7 in the calculations.

Follow the order of the subsequent steps to properly program threshold settings into the internal fault monitoring registers and turn on each fault monitoring feature:

- $\blacktriangleright$  Program bits [6:0] with the desired threshold code.
- **Program bit [7] to a value of a (1) to enable protection and rewrite to bits [6:0] with the desired threshold** code again.

## **SHUTDOWN CONTROL (SDN\_IO)**

The HV-HI output driver is disabled when SDN\_IO is high. As directed in the power-up section, it is recommended to power-up with SDN\_IO high so that the output driver is in shutdown mode and then bringing SDN\_IO low once the desired AD8460 configuration is written over SPI. Subsequently, floating the SDN\_IO pin enables the fault monitoring and protection feature while the AD8460 remains on. SDN\_IO sinks ~180 µA to override SDN\_IO's high state.

When SDN IO is floated, the driver is controlled by SPI commands. SDN IO has both input and output functionality. The user can drive the SDN\_IO pin to enable/disable the amplifier or monitoring the SDN\_IO. When SDN\_IO is floated or connected to a high impedance digital pin such as a microcontroller GPIO, SDN\_IO serves as a flag for any of the internal alarm conditions.

When SDN\_IO is pulled high, the AD8460's HVCC and HVEE supply currents are reduced to ~120 µA and the internal high voltage driver is disabled. The output goes to high impedance (~27 kΩ). The shutdown state is latched and the driver remains in shutdown even when SDN\_IO is floated. To enable the AD8460 from shutdown, pulling SDN\_IO low and following by floating the SDN\_IO is required to enable the shutdown protection features.

When SDN\_IO is held low, the output is continuously enabled, and shutdown is inhibited. Use caution in this case as the device is unprotected from overstress. Holding SDN\_IO low disables the shutdown protection features.

### **DELAYED SHUTDOWN**

The user may add delay to the AD8460's shutdown response time to improve noise immunity, by means of an external capacitor from SDN\_IO to ground. The capacitor value is chosen so that the desired delay equals the time required for the voltage on SDN\_IO to ramp from 0 V to its threshold voltage of 2.5 V under a constant current of 180 μA. The capacitor value  $C_{SDNIO}$  is calculated according to the relationship:

$$
C_{SDNIO} = \frac{(180 \,\mu A \times t)}{2.5 \,V}
$$

where, t is the desired delay time.

Note: The chosen delay applies to all internally-detected alarms (current, voltage, and temperature).

For example, to add a 5 μs delay so that short duration current or voltage spikes do not cause a shutdown, a capacitor is needed between SDN\_IO and ground, with value:

$$
C_{SDNIO} = \frac{(180 \ \mu A \times 5 \ \mu s)}{2.5 \ V} = 360 \ pF
$$

Note that parasitic capacitance on the PCB impacts the shutdown response time. The values seen in *Figure 65* are the total capacitance on the SDN\_IO pin, which includes the PCB's parasitic capacitance and added capacitor. In this example, any alarm condition shorter than 5 μs in duration does not trigger a shutdown. *Figure 65* shows the AD8460's shutdown response time vs. various capacitance.

Alarm latching is particularly useful when delayed shutdown is implemented. In the previous example, a fault of less than 5 μs duration does not trigger a shutdown, but the occurrence of a fault may be of interest for troubleshooting purposes. When the ALARM\_LATCH is true (1), the states of the corresponding ALARM flags may be polled through SPI to see if any faults are detected, even if the event is too short to force a shutdown.



*Figure 65. Shutdown Response Time vs. Various C<sub>SDN IO</sub>* 



*Figure 66. Shutdown Response Sequence*

### **MANUAL THERMAL SHUTDOWN**

The AD8460 features an optional manual thermal shutdown at T<sub>J</sub> = 150 °C without the need for SPI communication and programming. This manual shutdown feature is only valid for thermal shutdown. The overcurrent and overvoltage protection still require SPI communication and programming.

To enable the manual thermal shutdown, tie TMP directly to SDN\_IO, as shown in *Figure 67.* In this configuration, the TMP pin's analog output voltage reaches the SDN\_IO's logic high threshold at approximately  $T_J = 150 °C$ , activating shutdown mode. The AD8460 does not self-reset when the die temperature has cooled below 150 °C. The AD8460 remains in shutdown until resequencing the power supplies or the SDN\_IO pin.



*Figure 67. TMP and SDN\_IO pin Configuration for Manual Thermal Shutdown*

# **POWER ON RESET (POR) AND RESET**

The AD8460 executes a digital reset upon power-on. Power-on-reset (POR) resets all digital registers to default, including all alarm thresholds while powering-on the AD8460. The protection system is inactive upon power-on by default. Use caution in operating the device before any alarm thresholds are set and the protection system is enabled. Reset to defaults can also be commanded at any time through the SOFT\_RESET register bit. See *Table 22* for more information on SOFT\_RESET.

The default power-on configuration is:

- **Driver output enabled**
- Protection system disabled
- Waveform generation mode set to AWG
- $\triangleright$  Simple demonstration pattern loaded in pattern memory
- Nominal quiescent current
- $\triangleright$  DAC in shutdown

Manual POR can be achieved by pulling RESET LOW and then HIGH, which resets all the digital registers to default.

# **SLEEP CONTROL AND OTHER REGISTER RELATED FEATURES**

### **SLEEP CONTROL**

HV\_SLEEP: Setting the HV\_SLEEP register (0x00, bit 4) LOW puts the high voltage driver into sleep mode. The HVCC and HVEE supply currents drop to ~120 µA and OUT goes to a high impedance state (~27 kΩ). The sleep mode is initiated through SPI command only. Setting the HV\_SLEEP register bit HIGH restores the driver to its active state. Note that the output stage is high impedance in the sleep mode. When driving a capacitive load, the output voltage drifts as the load capacitor discharges.

HVDAC\_SLEEP: This register allows the user to shut down the HVDAC to save power. The VCC\_5V supply currents drop to 10.5 mA, and the HVCC and HVEE supply currents drop to 120 µA. HVDAC\_SLEEP permits a modest amount of additional power savings over HV\_SLEEP alone when in sleep mode. The HVDAC is in sleep mode by default at initial power-on or start-up.

INHIBIT\_HVDAC\_SHUTDOWN: By default, the HVDAC shuts down with the HV driver when a shutdown is commanded. INHIBIT\_ HVDAC\_SHUTDOWN allows the option to keep the HVDAC powered-up in the event of a shutdown command.

## **OTHER FEATURES**

Other features implemented in the AD8460 that may be useful in certain applications are:

- ▶ CHIP\_ID: This read-only register contains the code 0x46.
- $\triangleright$  DIE\_REV: This 4-bit read-only register contains the code 0x4.

### **SLEW BOOST**

The AD8460's output amplifier employs a slew boosting architecture to enhance high-speed signal fidelity. Slew boost is a variable-enhancement mechanism that increases quiescent current in proportion to the instantaneous differential voltage sensed at the inputs to the operational amplifier within the HV driver. As with any voltagefeedback operational amplifier, the inputs are kept very nearly equal through negative feedback. In cases where the output is unable to keep up with a rapidly changing input (disrupting the feedback loop), the inputs momentarily begin to move apart. This differential signal induces the slew boost circuit to increase supply current, allowing the output to slew faster, and restores the disrupted feedback signal.

The additional current is typically needed for about 50 ns to 100 ns but increases power dissipation significantly during that time. The amount of additional self-heating that occurs as a result of this depends on the signal dynamics. For instance, for a 100 kHz square wave with a period of 10 µs, the slew boost is only active for 1% of the waveform's period, resulting in a small increase in overall power dissipation.

The dynamic safe operating area (SOA) is shown in the *SAFE OPERATING AREA* section. The dynamic SOA shows the connection between the output swing and the maximum input/output frequency for a pulse response. If slewboost is activated frequently, as a high-frequency square wave might require, power dissipation increases dramatically and may push the device outside its dynamic SOA. To expand the dynamic SOA curve, use additional thermal management or limit the input/output edge speed, which limits the current produced by the slew boosting circuit and reduces the internal power dissipation.

### **THERMAL MONITORING (TMP)**

Monitoring die temperature in the AD8460 is accomplished by measuring its TMP pin voltage relative to GND. This pin's analog output voltage is proportional to die temperature and is converted to degrees Celsius using the formula:

$$
T(^0C) = \frac{(VTMP - 1.6 V)}{6 \frac{mV}{^0C}}
$$

More precise temperature readings can be achieved through a one-time room temperature calibration of the TMP pin.

The AD8460's thermal monitoring capability is independent of any overtemperature shutdown threshold and may be used whether or not TMP is strapped to SDN\_IO. Note: If TMP is monitored while strapped to SDN\_IO, a high impedance must be maintained by the user's monitoring circuit so that loading does not interfere with the shutdown function. Failure to maintain a high impedance on SDN\_IO may result in damage to the AD8460 by inhibiting thermal shutdown.

### **OUTPUT COMPENSATION (COMP\_H AND COMP\_L)**

Pulse response may be optimized for different capacitive loads by means of the COMP\_H and COMP\_L pins. Place a capacitor from both COMP\_H to OUT and COMP\_L to OUT to reduce overshoot in the step response. See *Figure 68* and *Figure 69* for information on selecting the compensation capacitors. Note that these must be high voltage types to withstand the full-scale range of the output signal; minimum 100 V capacitors are recommended when

running on the nominal ±50 V supplies. If supplies are brought up to ±55 V, the minimum voltage rating of capacitors used needs to be increased to 110 V accordingly.



*Figure 68. Large Signal Pulse Response Overshoot vs. CLOAD and CCOMP, Positive Overshoot*



*Figure 69. Large Signal Pulse Response Overshoot vs. CLOAD and CCOMP, Negative Overshoot*

# **THERMAL COMPENSATION (COMP\_T)**

Place a 0.1 μF capacitor from COMP\_T to ground. This compensation capacitor is required for stable output of TMP as junction temperature monitor.

# **PROGRAMMABLE QUIESCENT CURRENT**

Quiescent power dissipation may be reduced for applications that do not require maximum dynamic performance. Programming reduced supply current lowers power dissipation and lowers junction temperature at the expense of speed, slew rate, settling time, capacitive load drive, and noise.

This feature is controlled in CTRL\_REG\_04: SET\_IQ and allows for adjusting the supply current up or down relative to the nominal supply current. The MSB sets the polarity of the supply current adjust: (0) is a decrease in supply current, whereas (1) is an increase in supply current. The remaining bits [6:0] are a monotonic but nonlinear control of the supply current across the span of codes. From SET\_IQ = 0x00, the part is at nominal supply current, bits [6:0] can be increased up to limit SET\_IQ = 0x7F, where the part sees zero supply current, resulting in quiescent current

starved shutdown. From SET\_IQ = 0x80, the part is again at nominal supply current, and bits [6:0] can be increased up to SET\_IQ = 0xFF, where the part is at roughly double the nominal supply current. Exercise extreme caution if increasing supply current, noting the thermal effects of the increased supply current, where self-heating can increase junction temperature and must be monitored appropriately.



*Figure 70. Quiescent Current vs. Code*

# **APPLICATIONS INFORMATION**

# **Thermal Management PCB Thermal Design**

The AD8460's innovative EPAD-up package greatly reduces thermal management constraints on the PCB layout. Conventional EPAD-down packages require copper-filled vias or expensive solid copper coins pressed into the PCB for thermal conduction to a heat sink on the underside of the board. EPAD-up allows the heat sink to be mounted to the top of the AD8460, freeing up component space on the secondary side of the PCB, and eliminating the need for through-board thermal relief. Four small mounting holes are needed to secure the recommended heat sink to the PCB, and these are located outside of the AD8460's immediate area. Component heights on the primary side of the PCB in the area beneath the heat sink must be smaller than the minimum height of the AD8460, as illustrated in *Figure 71*.



*Figure 71.Component Height Restriction Beneath Heat Sink*

To maximize heat transfer, attach the heat sink to the EPAD, as shown in *Figure 71*, using a high conductivity thermal interface material (TIM).

# **POWER DISSIPATION**

Under quiescent conditions and maximum supply voltage, with the default heat sink, the AD8460 dissipates ~2.475 W, which produces a 15.84 °C rise over ambient temperature.

Under heavier loading conditions, the increase in die temperature is greater. It is recommended that  $T_1$  be continuously monitored at the TMP pin to manage die temperature under different internal power dissipation levels. Alternatively, when operating at a constant power level, die temperature can be estimated based on the package's  $\theta_{JA}$  of 22.6 °C/watt when operating without a heatsink. Where the thermal setup of the AD8460 utilizes a heatsink, one should expect to have a junction-to-ambient thermal resistance  $\theta_{JA-SYSTEM}$  (with recommended heatsink Wakefield-Vette P/N 518-95AB and TIM GC Electronics type Z9 heat sink compound) of 6.4°C/watt. The following equation is the basic formula used for calculating junction temperature for a specific power dissipation and ambient temperature.

$$
T_J = \theta_{JA\_SYSTEM} * P_{DISS} + T_A
$$

For example, if dissipating 10 W internally at an ambient temperature of 25 °C with a heatsink and TIM in the thermal stackup for the EVAL-AD8460SDZ,  $T_J$  can be expected to climb to:  $25 °C + (6.4 °C/W \times 10 W) = 89 °C$ 

Note that ~19.5 W internal power dissipation pushes  $T<sub>J</sub>$  to its maximum rated value of 150 °C when using default heatsink in an environment with natural convection.

Thermal resistance values effectively show how much a certain portion of a thermal stackup heats up for a specified power dissipation. The equations below are the basic equations for determining the junction to ambient thermal resistance for a thermal stackup that uses thermal paste and heatsink. The  $\theta_{IA\; SYSTEM}$  should be designed to meet the user's thermal requirements. Using the junction-to-case thermal resistance ( $\theta_{\text{JC}}$ ) and thermal resistance of the thermal interface material ( $\theta_{TM}$ ), compute the thermal resistance ( $\theta_{HS}$ ) of the required heat sink with the following equation.

$$
\theta_{\rm HS} = (\frac{T_J - T_A}{P_{DISS}}) - \left(\theta_{JC} + \theta_{TIM}\right)
$$

$$
\theta_{JA\_SYSTEM} = \theta_{HS} + \theta_{JC} + \theta_{TIM}
$$

High-performance applications involving maximum power delivery at high duty cycles may require active cooling to effectively reduce  $\theta_{\text{JA\_SYSTEM}}$  and continuous monitoring of T $_{\text{J}}$ .

For lower power applications, or if forced air convection is used, a smaller heat sink may be sufficient.

*Table 12* shows the thermal resistances for different conditions when using the evaluation board, EVAL-AD8460SDZ at T<sub>A</sub> = 25 °C. The fan used is the Sunon Fans EE80251S2-1000U-999 with air flow of 37 CFM. The heatsink used is the Wakefield-Vette P/N 518-95AB. The TIM is the GC Electronics type Z9 heat sink compound.

<b>Heatsink</b>	<b>Air flow</b>	$\theta$ _(JA_SYSTEM) (°C/W)
No	No	22.6
Yes	No	6.4
	Yes	4.4

Table 12.  $\theta_{IA\; SYSTEM}$  for Different Thermal Stackups on the EVAL-AD8460SDZ

### **SAFE OPERATING AREA**

The safe operating area (SOA) represents the power handling capability of the device under various conditions. The power dissipation of the AD8460 occurs primarily from the slew boosting circuit and output stage. The SOA curves are unique to the conditions under which they are developed, such as PCB, heat sink, airflow, and ambient temperatures. In addition, all SOA curves are derated and are with respect to hotspots on the die. Typically, it is assumed the power dissipation is uniform across the whole die of a part, but, the reality is that the power dissipation is typically concentrated in certain areas based on the application. In high power applications, the output stage of an amplifier is where the hotspots commonly exist since the output stage transistors are where power is dissipated when driving a load. To preserve the lifespan of the silicon, it is recommended to utilize the SOA plots to estimate an optimal temperature for each specific application. Ensure that usage of the AD8460 remains within the published DC SOA and dynamic SOA curves, also monitoring the junction temperature using the TMP pin voltage ( $V_{TMP} \leq 2.5 V$ ).

Long-term usage of the AD8460 at or near maximum junction temperature of 150 °C may result in a reduction of expected lifespan of the product due to accelerated thermal stresses.

A thermal model for simulation of the AD8460 is forthcoming to enable customers to evaluate thermal performance of the AD8460 under different configurations.

### **DC SOA**

*Figure 72* shows that the DC safe operating area (SOA) is a curve of output current vs. output stage supply voltage differential (V<sub>s</sub> to V<sub>OUT</sub>), under which the amplifier can operate at a safe junction temperature (T<sub>J</sub>). The area under the curves of *Figure 72* shows the operational boundaries of the AD8460 for using the AD8460 evaluation board that maintains a T<sub>J</sub> ≤ 150°C.



*Figure 72. DC SOA without Heatsink, with Default Heatsink, with Default Heatsink and Fan, T<sub>A</sub> = 25 °C* 

All testing was done in the natural convection of a lab. Forced air convection in any of the test cases effectively lowers  $\theta_{IA}$  and moves the corresponding curve toward the upper right, expanding the SOA. For more information on the AD8460 evaluation board, refer to the AD8460 user guide. In *Figure 72*, the horizontal line at 1 A is the output current drive of the AD8460. The curved section maintains a fixed power dissipation that results in a junction temperature (TJ) of 150°C or less. Note that the x-axis is the output stage VCE (HVCC – V<sub>OUT</sub> or V<sub>OUT</sub> – HVEE) developed across the relevant output transistor and ends at a maximum VCE of 55 V.

# **Dynamic SOA**

*Figure 73* illustrates the maximum square-wave amplitude that can be generated continuously without exceeding absolute maximum temperature, plotted versus frequency with a specified capacitive load and specified heat sink.



*Figure 73. Dynamic SOA without Heatsink, with Default Heatsink, with Default Heatsink and Fan, CLOAD = 1 nF, T<sup>A</sup> = 25 °C*

The *Slew Boost* section discusses how the AD8460 consumes significant dynamic supply current during high-slew transitions. Above a particular frequency (load-dependent), the electrical power consumption required to slew ±full scale exceeds the device's ability to dissipate while remaining below absolute maximum junction temperature. Additional thermal management can be leveraged to expand the SOA.

# **Limiting Dynamic Peak Current for >1nF Loads**

The AD8460 can drive 1 A continuously by design, assuming appropriate thermal management as outlined in the *Thermal Management* section.

The AD8460 has also been qualified to drive 80 Vp-p square-wave pulses into a 1 nF load without external compensation or slew control. This corresponds to +2.6 A/−2.2 A peak, with a ~35 ns pulse width, as specified in the electrical characteristics.

If driving pulses into >1 nF loads, to remain within the qualified device conditions, the peak current should be limited to the continuous output current drive of 1 A. To ensure this, the user must implement digital slew rate control to limit the peak current when driving these loads.

The current into a capacitor can be calculated using the formula:

$$
I = C \frac{dV}{dt}
$$

This generates the following table of maximum slew rate that ensures a peak current of ≤ 1 A. Also outlined are the minimum  $f_{SYNC}$  frequencies required to drive 80 Vp-p as these slew rates digitally.

### **Table 13.Maximum Slew vs. Capacitive Load**



To implement a digital slew control, the number of steps needed during an edge event is calculated by:

$$
n_{STEPS} = \frac{Amplitude_{P-P} \times f_{SYNC}}{EDGE SPEED}
$$

For loads <47 nF, it is recommended to ensure each digital step is ≤5 V to limit the peak dynamic current. This corrosponds to a  $n_{STEPS} \ge 16$  for an 80 Vp-p  $Amplitude_{P-P}$ . *Table 13* shows the minimum  $f_{SYNC}$  frequencies to ensure at least 16 steps at the maximum edge speed. For loads >47 nF, a greater number of  $n_{s_{TEPS}}$  is recommended.

# **FULL-SCALE ADJUSTMENT**

Using HV supplies of ±50 V, the default configuration shown in *Figure 58* produces a 80 V span centered at zero volts. Modify the output voltage span in three different ways:

- ▶ Forcing REFIO\_1P2V externally with a user-supplied voltage reference.
- $\triangleright$  Changing the value of R<sub>SET</sub> to reduce the value of I<sub>REF</sub>.

Note: The output span is defined by the HVDAC's external configuration and is unaffected by changes in HVCC and HVEE, provided there is sufficient headroom between HV supplies and programmed output range. See *Figure 43* for more information about headroom requirements. Insufficient HV supply headroom may result in output signal clipping.

## **FULL-SCALE REDUCTION**

For applications requiring dynamically-adjustable span, there are two methods to achieve a reduced programmable output voltage span.

Under the conventional setup,  $R_{TERM}$  = 50  $\Omega$ ,  $R_{SET}$  and REFIO\_1P2V can be adjusted to achieve a lower output voltage span. The output transfer function simplifies to:

$$
V_{OUT} = \left(80 \ V \times \left(\frac{DAC \ CODE}{2^{14}}\right) - 40 \ V\right) \times \left(\frac{2 \ k\Omega}{R_{SET}}\right) \times \left(\frac{V_{REFIO_{1P2V}}}{1.2 \ V}\right)
$$

The range of R<sub>SET</sub> is 2 kΩ to 20 kΩ, which can be used to change the output voltage range from +/−40 V to +/−4 V, respectively. Because  $R_{\text{SET}}$  is a hardware item, this is a good option for applications that do not require changes in span once the hardware configuration is implemented. Note that the AD8460's output voltage range cannot be increased by reducing R<sub>SET</sub>. See *Table 14* for a list of various RSET values for a specific output voltage span.

**Table 14.Typical Output Voltage Span for Constant REFIO\_1P2V with Various RSET values**

<b>Output Voltage Range (Vpp)</b>	RSET $(\Omega)$	<b>REFIO_1P2V (V)</b>
80	2000	1.2
60	2666.7	1.2
40	4000	1.2
20	8000	1.2
10	16000	$1.2\,$
8	20000	1.2

Alternatively, a reduced programmable voltage span may be implemented by forcing REFIO\_1P2V externally with a user-supplied voltage reference. This is done by driving REFIO\_1P2V with a voltage in the range of 1.2 V maximum to as low as 0.12 V, which can be used to change the output voltage range from +/−40 V to +/−4 V, respectively. This is the recommended option for applications requiring dynamically-adjustable span.





For precision applications, it is recommended to use a high precision 1.2 V to drive REFIO\_1P2V. This allows for the best dynamic performance when the device is under normal operation. The internal reference from REFIO\_1P2V can drift in performance with changes in temperature. See *Table 15* for a list of various REFIO\_1P2V values for a specific output voltage span.

# **LAYOUT**

When designing the PCB, it is important to incorporate thermal layout techniques in addition to the standard electrical layout practices. Thermal considerations involve attention to trace thickness, thermal vias, ground and power layers, and large copper areas for power supply areas. The high voltage power supply lines (HVCC, HVEE) should use as large a trace as possible to provide low impedance paths and reduce the effects of glitches on the power supply line. Decouple the power supply (HVCC, HVEE, AVDD\_3P3V, DVDD\_3P3V, VCC\_5V, and VREF\_5V) PCB entry points and the pins of the AD8460 with low ESR ceramic capacitors. The decoupling capacitors should be placed close to the AD8460 and connected using short and wide traces to provide low impedance paths and reduce the effect of glitches on the power supply lines. Lower ESR, ESL decoupling capacitors on HVCC, HVEE pins help reduce voltage ripple and glitches. For supplies with multiple pins (HVCC, HVEE), it is recommended that these pins be tied together and that each supply be decoupled only once. Place the smallest value capacitor on the same side of the board as the AD8460 and as close as possible to the amplifier power supply pins with the ground end of the capacitor directly to the ground plane.

Because this product has analog and digital functions, it is important to separate and confine the analog and digital sections to certain areas of the PCB proximal to the AD8460. Allow the analog ground plane to run under the AD8460 to avoid noise coupling. Avoid running digital lines under the AD8460 because these couple noise onto the die, unless there is a ground plane acting as shield. Fast switching digital signals such as SYNC or clock should be shielded with digital ground to avoid radiating noise to other parts of the board and should never be run near the analog traces. Traces on adjacent PCB layers should run at right angles to each other to reduce effects from coupling and feedthrough throughout the board. Avoid crossover of digital and analog signals. Use at least one ground plane, and it can be common or split between the digital and analog section. In the latter case, join the planes underneath the AD8460 devices.

# **TOP LEVEL DIGITAL REGISTER ASSIGNMENT**

# **Table 16.Digital Register Map Instance Summary**



# **DEVICE CONTROL REGISTER SUMMARY AND MAP**

## **Table 17.Control Register Summary**



Note: R/W means read and write; R/CLR means read and clear. See the *FAULT MONITORING AND PROTECTION* section for a description of R/CLR.

## **Table 18. Control Register Map**





# **CONTROL REGISTER DETAILS**

# **Table 19.Bit Descriptions for CTRL\_REG\_00**



# **Table 20. Bit Descriptions for CTRL\_REG\_01**



# **Table 21. Bit Descriptions for CTRL\_REG\_02**



# **Table 22. Bit Descriptions for CTRL\_REG\_03**



# **Table 23. Bit Descriptions for CTRL\_REG\_04**



# **Table 24. Bit Descriptions for CTRL\_REG\_05**



# **Table 25. Bit Descriptions for CTRL\_REG\_08**



# **Table 26. Bit Descriptions for CTRL\_REG\_09**



# **Table 27. Bit Descriptions for CTRL\_REG\_10**



# **Table 28. Bit Descriptions for CTRL\_REG\_11**



# **Table 29. Bit Descriptions for CTRL\_REG\_12**



# **Table 30. Bit Descriptions for CTRL\_REG\_13**



# **Data Sheet AD8460**



# **Table 31. Bit Descriptions for CTRL\_REG\_14**



## **Table 32. Bit Descriptions for CTRL\_REG\_25**



## **Table 33. Bit Descriptions for CTRL\_REG\_26**



<sup>1</sup> CLR denotes that an alarm flag is cleared by writing a '1' to the corresponding register bit.

# **HVDAC DATA REGISTER (PATTERN MEMORY) SUMMARY**

## **Table 34.HVDAC Data Summary**





<sup>1</sup> Note that HVDAC\_DATA\_WORD\_00 through HVDAC\_DATA\_WORD\_03 default to non-zero codes, which produces a ½ scale triangle wave at a frequency defined by the SYNC clock rate in analog pattern generation mode. These values may be overwritten through SPI.









<sup>1</sup> Note that HVDAC\_DATA\_WORD\_00 through HVDAC\_DATA\_WORD\_03 default to non-zero codes, which produces a 4level staircase waveform at ±20 V (0 V, +20 V, 0 V, −20 V) without the need for user programming, with timing defined by the user-provided SYNC clock. These values may be overwritten through SPI for the user's own analog pattern.

# **HVDAC DATA REGISTER (PATTERN MEMORY) DETAILS**

HVDAC data, low-order byte of 14-bit analog pattern data.

### **Table 36. Bit Descriptions for HVDAC\_DATA\_BYTE\_00**



HVDAC data, high-order byte of 14-bit analog pattern data.

#### **Table 37. Bit Descriptions for HVDAC\_DATA\_BYTE\_01**



#### **Table 38. Bit Descriptions for HVDAC\_DATA\_BYTE\_02**



HVDAC data, high-order byte of 14-bit analog pattern data.

### **Table 39. Bit Descriptions for HVDAC\_DATA\_BYTE\_03**



HVDAC data, low-order byte of 14-bit analog pattern data.

#### **Table 40. Bit Descriptions for HVDAC\_DATA\_BYTE\_04**



HVDAC data, high-order byte of 14-bit analog pattern data.

### **Table 41. Bit Descriptions for HVDAC\_DATA\_BYTE\_05**



HVDAC data, low-order byte of 14-bit analog pattern data.

### **Table 42. Bit Descriptions for HVDAC\_DATA\_BYTE\_06**



HVDAC data, high-order byte of 14-bit analog pattern data.

### **Table 43. Bit Descriptions for HVDAC\_DATA\_BYTE\_07**



All remaining pattern memory registers (HVDAC\_DATA\_BYTE\_08 through HVDAC\_DATA\_BYTE\_31) follow the same format of low-order byte and high-order byte shown in *Table 39*. Note that the default value for these registers is 0x0.

HVDAC data, low-order byte of 14-bit analog pattern data.

### **Table 44. Bit Descriptions for HVDAC\_DATA\_BYTE\_08**



HVDAC data, high-order byte of 14-bit analog pattern data.

### **Table 45. Bit Descriptions for HVDAC\_DATA\_BYTE\_09**



HVDAC data, low-order byte of 14-bit analog pattern data.

### **Table 46. Bit Descriptions for HVDAC\_DATA\_BYTE\_10**



HVDAC data, high-order byte of 14-bit analog pattern data.

### **Table 47. Bit Descriptions for HVDAC\_DATA\_BYTE\_11**



HVDAC data, low-order byte of 14-bit analog pattern data.

### **Table 48. Bit Descriptions for HVDAC\_DATA\_BYTE\_12**



HVDAC data, high-order byte of 14-bit analog pattern data.

### **Table 49. Bit Descriptions for HVDAC\_DATA\_BYTE\_13**



HVDAC data, low-order byte of 14-bit analog pattern data.

### **Table 50. Bit Descriptions for HVDAC\_DATA\_BYTE\_14**



HVDAC data, high-order byte of 14-bit analog pattern data.

### **Table 51. Bit Descriptions for HVDAC\_DATA\_BYTE\_15**



HVDAC data, low-order byte of 14-bit analog pattern data.

### **Table 52. Bit Descriptions for HVDAC\_DATA\_BYTE\_16**



HVDAC data, high-order byte of 14-bit analog pattern data.

### **Table 53. Bit Descriptions for HVDAC\_DATA\_BYTE\_17**



HVDAC data, low-order byte of 14-bit analog pattern data.

### **Table 54. Bit Descriptions for HVDAC\_DATA\_BYTE\_18**



HVDAC data, high-order byte of 14-bit analog pattern data.

### **Table 55. Bit Descriptions for HVDAC\_DATA\_BYTE\_19**



HVDAC data, low-order byte of 14-bit analog pattern data.

### **Table 56. Bit Descriptions for HVDAC\_DATA\_BYTE\_20**



HVDAC data, high-order byte of 14-bit analog pattern data.

### **Table 57. Bit Descriptions for HVDAC\_DATA\_BYTE\_21**



HVDAC data, low-order byte of 14-bit analog pattern data.

### **Table 58. Bit Descriptions for HVDAC\_DATA\_BYTE\_22**



HVDAC data, high-order byte of 14-bit analog pattern data.

### **Table 59. Bit Descriptions for HVDAC\_DATA\_BYTE\_23**



HVDAC data, low-order byte of 14-bit analog pattern data.

### **Table 60. Bit Descriptions for HVDAC\_DATA\_BYTE\_24**



HVDAC data, high-order byte of 14-bit analog pattern data.

### **Table 61. Bit Descriptions for HVDAC\_DATA\_BYTE\_25**



HVDAC data, low-order byte of 14-bit analog pattern data.

### **Table 62. Bit Descriptions for HVDAC\_DATA\_BYTE\_26**



HVDAC data, high-order byte of 14-bit analog pattern data.

### **Table 63. Bit Descriptions for HVDAC\_DATA\_BYTE\_27**



HVDAC data, low-order byte of 14-bit analog pattern data.

#### **Table 64. Bit Descriptions for HVDAC\_DATA\_BYTE\_28**


HVDAC data, high-order byte of 14-bit analog pattern data.

#### **Table 65. Bit Descriptions for HVDAC\_DATA\_BYTE\_29**



HVDAC data, low-order byte of 14-bit analog pattern data.

### **Table 66. Bit Descriptions for HVDAC\_DATA\_BYTE\_30**



HVDAC data, high-order byte of 14-bit analog pattern data.

### **Table 67. Bit Descriptions for HVDAC\_DATA\_BYTE\_31**



# **OUTLINE DIMENSIONS**



*Figure 74. 80-Lead Thin Quad Flat Package, Exposed Pad TQFP, SV-80-7, Dimensions shown in milimeters*

## **ORDERING GUIDE**



## **EVALUATION BOARD**



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