## Data Sheet

 ADA4051-1/ADA4051-2
## FEATURES

Very low supply current: $13 \mu \mathrm{~A}$ typical Low offset voltage: $\mathbf{1 5 \mu \mathrm { V } \text { maximum }}$
Offset voltage drift: $20 \mathrm{nV} /{ }^{\circ} \mathrm{C}$
Single-supply operation: 1.8 V to 5.5 V
High PSRR: 110 dB minimum
High CMRR: 110 dB minimum
Rail-to-rail input/output
Unity-gain stable
Extended industrial temperature range

## APPLICATIONS

Pressure and position sensors
Temperature measurements
Electronic scales
Medical instrumentation
Battery-powered equipment
Handheld test equipment

PIN CONFIGURATIONS


Figure 1.5-Lead SOT-23 (RJ-5)


Figure 2. 5-Lead SC-70 (KS-5)


Figure 3. 8-Lead MSOP (RM-8)


NOTES

1. IT IS RECOMMENDED THAT THE

EXPOSED PAD BE CONNECTED TO V-.
Figure 4. 8-Lead LFCSP (CP-8-13)

## GENERAL DESCRIPTION

The ADA4051-1/ADA4051-2 are CMOS, micropower, zerodrift operational amplifiers utilizing an innovative chopping technique. These amplifiers feature rail-to-rail input/output swing and extremely low offset voltage while operating from a 1.8 V to 5.5 V power supply. In addition, these amplifiers offer high power supply rejection ratio (PSRR) and common-mode rejection ratio (CMRR) while operating with a typical supply current of $13 \mu \mathrm{~A}$ per amplifier. This combination of features makes the ADA4051-1/ADA4051-2 amplifiers ideal choices for battery-powered applications where high precision and low power consumption are important.

The ADA4051-1/ADA4051-2 are specified for the extended industrial temperature range of $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The ADA4051-1 amplifier is available in 5-lead SOT-23 and 5-lead SC-70 packages. The ADA4051-2 amplifier is available in an 8-lead MSOP and an 8-lead LFCSP.

The ADA4051-1/ADA4051-2 are members of a growing series of zero-drift op amps offered by Analog Devices, Inc. Refer to Table 1 for a list of these devices.

Table 1. Op Amps

| Supply | Low Power, 5 V | 5 V | 16 V |
| :--- | :--- | :--- | :--- |
| Single | AD8538 | AD8628 | AD8638 |
| Dual | AD8539 | AD8629 | AD8639 |
| Quad |  | AD8630 |  |

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## SPECIFICATIONS

## ELECTRICAL CHARACTERISTICS-1.8 V OPERATION

$\mathrm{V}_{\mathrm{SY}}=1.8 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=\mathrm{V}_{\mathrm{SY}} / 2 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{L}}=100 \mathrm{k} \Omega$ to GND , unless otherwise noted.
Table 2.


| Parameter | Symbol | Test Conditions/Comments | Min | Typ | Max |
| :--- | :--- | :--- | :--- | :--- | :--- |
| NOISE PERFORMANCE |  |  |  |  |  |
| Voltage Noise | $\mathrm{e}_{\mathrm{n}} \mathrm{p}-\mathrm{p}$ | $\mathrm{f}=0.1 \mathrm{~Hz}$ to 10 Hz |  |  |  |
| Voltage Noise Density | $\mathrm{e}_{\mathrm{n}}$ | $\mathrm{f}=1 \mathrm{kHz}$ | 1.96 |  |  |
| Current Noise Density | $\mathrm{i}_{\mathrm{n}}$ | $\mathrm{f}=1 \mathrm{kHz}$ | 95 | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |  |

## ELECTRICAL CHARACTERISTICS—5 V OPERATION

$\mathrm{V}_{\text {SY }}=5.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=\mathrm{V}_{\mathrm{SY}} / 2 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{R}_{\mathrm{L}}=100 \mathrm{k} \Omega$ to GND , unless otherwise noted.

Table 3.


| Parameter | Symbol | Test Conditions/Comments | Min | Typ | Max |
| :--- | :--- | :--- | :--- | :--- | :--- |
| NOISE PERFORMANCE |  |  |  |  |  |
| Voltage Noise | $\mathrm{e}_{\mathrm{n}} \mathrm{p}-\mathrm{p}$ | $\mathrm{f}=0.1 \mathrm{~Hz}$ to 10 Hz | 1.96 | $\mu \mathrm{p}-\mathrm{p}$ |  |
| Voltage Noise Density | $\mathrm{e}_{\mathrm{n}}$ | $\mathrm{f}=1 \mathrm{kHz}$ | 95 | $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ |  |
| Current Noise Density | $\mathrm{i}_{\mathrm{n}}$ | $\mathrm{f}=1 \mathrm{kHz}$ | 100 | $\mathrm{fA} / \sqrt{\mathrm{Hz}}$ |  |

## ABSOLUTE MAXIMUM RATINGS

Table 4.

| Parameter | Rating |
| :---: | :---: |
| Supply Voltage | 6 V |
| Input Voltage | $\pm \mathrm{V}_{S Y} \pm 0.3 \mathrm{~V}$ |
| Input Current ${ }^{1}$ | $\pm 10 \mathrm{~mA}$ |
| Differential Input Voltage ${ }^{2}$ | $\pm \mathrm{V}_{\text {SY }}$ |
| Output Short-Circuit Duration to GND | Indefinite |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operating Temperature Range | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Junction Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 60 sec ) | $300^{\circ} \mathrm{C}$ |
| ${ }^{1}$ The input pins have clamp diodes to the power supply pins. Limit the input current to 10 mA or less whenever input signals exceed the power supply rail by 0.3 V . |  |
| ${ }^{2}$ Inputs are protected against high differentia $1.33 \mathrm{k} \Omega$ resistors and back-to-back diode-co typical $\mathrm{V}_{\mathrm{T}}$ of 0.7 V for $\mathrm{V}_{\text {см }}$ of 0 V ). | voltages by internal series ected N-MOSFETs (with a |

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

## THERMAL RESISTANCE

$\theta_{\mathrm{JA}}$ is specified for the worst-case conditions, that is, a device soldered on a circuit board for surface-mount packages with its exposed paddle soldered to a pad, if applicable. Table 5 shows simulated thermal values for a 4-layer (2S2P) JEDEC standard thermal test board, unless otherwise specified.

Table 5. Thermal Resistance

| Package Type | $\boldsymbol{\theta}_{\mathrm{JA}}$ | Unit |
| :--- | :--- | :--- |
| 5-Lead SOT-23 (RJ-5) | 190 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 5-Lead SC-70 (KS-5) | 534 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 8-Lead MSOP (RM-8) | 142 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 8-Lead LFCSP (CP-8-13) |  |  |
| $\quad$ 1-Layer JEDEC Board | 272 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 2-Layer JEDEC Board | 145 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 2-Layer JEDEC Board with $2 \times 2$ Vias | 55 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

## POWER SEQUENCING

The op amp supplies must be established simultaneously with or before any input signals are applied. If this is not possible, the input current must be limited to 10 mA .

## ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## TYPICAL PERFORMANCE CHARACTERISTICS

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 5. Input Offset Voltage Distribution


Figure 6. Input Offset Voltage Drift Distribution with Temperature


Figure 7. Input Offset Voltage vs. Input Common-Mode Voltage


Figure 8. Input Offset Voltage Distribution


Figure 9. Input Offset Voltage Drift Distribution with Temperature


Figure 10. Input Offset Voltage vs. Input Common-Mode Voltage
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 11. Input Bias Current vs. Temperature


Figure 12. Input Bias Current vs. Common-Mode Voltage and Temperature


Figure 13. Output Voltage ( $\mathrm{V}_{\text {он }}$ ) to Supply Rail vs. Load Current and Temperature


Figure 14. Input Bias Current vs. Temperature


Figure 15. Input Bias Current vs. Common-Mode Voltage and Temperature


Figure 16. Output Voltage ( $\mathrm{VOH}^{\prime}$ ) to Supply Rail vs. Load Current and Temperature
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 17. Output Voltage (VoL) to Supply Rail vs. Load Current and Temperature


Figure 18. Output Voltage (VOH) vs. Temperature


Figure 19. Output Voltage (VoL) vs. Temperature


Figure 20. Output Voltage (Vol) to Supply Rail vs. Load Current and Temperature


Figure 21. Output Voltage ( $V_{\mathrm{OH}}$ ) vs. Temperature


Figure 22. Output Voltage (Vol) vs. Temperature
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 23. Total Supply Current vs. Supply Voltage


Figure 24. Open-Loop Gain and Phase vs. Frequency


Figure 25. Closed-Loop Gain vs. Frequency


Figure 26. Total Supply Current vs. Temperature


Figure 27. Open-Loop Gain and Phase vs. Frequency


Figure 28. Closed-Loop Gain vs. Frequency
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 29. Output Impedance vs. Frequency


Figure 30. CMRR vs. Frequency


Figure 31. PSRR vs. Frequency


Figure 32. Output Impedance vs. Frequency


Figure 33. CMRR vs. Frequency


Figure 34. PSRR vs. Frequency
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 35. Small-Signal Overshoot vs. Load Capacitance


Figure 36. Large-Signal Transient Response


Figure 37. Small-Signal Transient Response


Figure 38. Small-Signal Overshoot vs. Load Capacitance


Figure 39. Large-Signal Transient Response


Figure 40. Small-Signal Transient Response
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 41. Input Voltage Noise, 0.1 Hz to 10 Hz


Figure 42. Voltage Noise Density vs. Frequency


Figure 43. Positive Overload Recovery


Figure 44. Input Voltage Noise, 0.1 Hz to 10 Hz


Figure 45. Voltage Noise Density vs. Frequency


Figure 46. Positive Overload Recovery
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 47. Negative Overload Recovery


Figure 50. Negative Overload Recovery


Figure 51. Positive Settling Time to 0.1\%


Figure 52. Negative Settling Time to $0.1 \%$
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 53. Channel Separation vs. Frequency


Figure 54. Output Swing vs. Frequency


Figure 55. No Phase Reversal


Figure 56. Channel Separation vs. Frequency


Figure 57. Output Swing vs. Frequency


Figure 58. No Phase Reversal

## THEORY OF OPERATION

The ADA4051-1/ADA4051-2 micropower chopper operational amplifiers feature a novel, patent-pending technique that suppresses offset-related ripple in a chopper amplifier. Instead of filtering the ripple in the ac domain, this technique nulls the initial offset of the amplifier in the dc domain, thus preventing ripple at the overall output.
Auto-zeroing and chopping are two techniques widely used in high precision CMOS amplifiers to achieve low offset, low offset drift, and no $1 / \mathrm{f}$ noise. Each of these techniques has pros and cons. Auto-zeroing results in more in-band noise due to aliasing introduced by sampling. On the other hand, chopping produces offset-related ripple because it modulates the initial offset associated with the amplifier up to its chopping frequency.
To accomplish the best noise vs. power trade-off, the chopping technique is the better approach when designing a low offset amplifier because there is no increased in-band noise. It is preferable to suppress the offset-related ripple inside a chopper amplifier because the offset-related ripple would otherwise need to be eliminated by an extra off-chip postfilter.

Figure 59 shows the block diagram design of the ADA4051-1/ ADA4051-2 chopper amplifiers employing a local feedback loop called autocorrection feedback (ACFB). The main signal path contains an input chopping switch network (CHOP1), a first transconductance amplifier (Gm1), an output chopping switch network (CHOP2), a second transconductance amplifier (Gm2), and a third transconductance amplifier (Gm3). CHOP1 and CHOP2 operate at 40 kHz of chopping frequency to modulate the initial offset and $1 / \mathrm{f}$ noise from Gm 1 up to the chopping frequency. A fourth transconductance amplifier (Gm4) in the ACFB senses the modulated ripple at the output of CHOP2, caused by the initial offset voltage of Gm 1 . Then, the ripple is demodulated down to a dc domain through a third chopping switch network (CHOP3), operating with the same chopping clock as CHOP1 and CHOP2. Finally, a null transconductance amplifier (Gm5) tries to null any dc component at the output of Gml that would otherwise appear in the overall output as ripple.
A switched-capacitor notch filter (NF) functions to selectively suppress the undesired offset-related ripple without disturbing the desired input signal from the overall input. The desired input dc signal appears as a dc signal at the output of CHOP2. Then, the initial offset is modulated up to the chopping frequency by CHOP3 and filtered out by the NF. Therefore, initial offset does not create any feedback and does not disturb the desired input signal. The NF is synchronized with the chopping clock to filter out the modulated component. In the same manner, the offset of Gm5 is filtered out by the combination of CHOP3 and the NF, enabling accurate ripple sensing at the output of CHOP2.
In parallel with the high dc gain path, a feedforward transconductance amplifier (Gm6) is added to bypass the phase shift introduced by the ACFB at the chopping frequency. Gm6 is designed to have the same transconductance as Gm 1 to avoid
pole-zero doublets. This design prevents any instability introduced by the ACFB in the overall feedback loop.


Figure 59. ADA4051-1/ADA4051-2 Chopper Amplifiers Block Diagram
The voltage noise density, which is equal to the thermal noise floor dominated by the Gm1, is essentially flat from dc to the chopping frequency because CHOP1 and CHOP2 eliminate the 1/f noise generated in Gm1 and the ACFB does not contribute any additional noise. Although the ACFB suppresses the ripple related to the chopping, there is a remaining voltage ripple. To further suppress the remaining ripple down to a desired level, it is recommended to have a postfilter at the output of the amplifier.
The remaining voltage ripple originates from two sources. The first type of ripple is due to the residual ripple associated with the initial offset of the Gm1. It is proportional to the magnitude of the initial offset and creates a spectrum at the chopping frequency ( $\mathrm{f}_{\text {Chop }}$ ). When the amplifier is configured as a unitygain buffer, this ripple has a typical value of $4.9 \mu \mathrm{~V} \mathrm{rms}$ and a maximum of $34.7 \mu \mathrm{~V} \mathrm{rms}$. The second type of ripple is due to the intermodulation between the high frequency input signal and the chopping frequency. This ripple depends on the input frequency ( $\mathrm{f}_{\mathrm{IN}}$ ) and creates a spectrum at frequencies equal to the difference between the chopping frequency and the input frequency $\left(f_{\text {CHOP }}-f_{\text {IN }}\right)$, as well as at frequencies equal to the summation of the chopping frequency and the input frequency $\left(f_{\text {Chop }}+f_{\text {IN }}\right)$. The magnitude of the ripple for different input frequencies is shown in Figure 60.


Figure 60. ADA4051-1/ADA4051-2 Modulated Output Ripple vs. Input Frequency

The design architecture of the ADA4051-1/ADA4051-2 specifically targets precision signal conditioning applications requiring accurate and stable performance from dc to 10 Hz bandwidth. In summary, the main features of the ADA4051-1/ ADA4051-2 chopper amplifiers are

- Considerable suppression of the offset-related ripple
- No effect on the desired input signal as long as its frequency is much lower than the chopping frequency shown in Figure 60
- Achievement of low offset similar to a conventional chopper amplifier
- No introduction of excess noise

The ADA4051-1/ADA4051-2 chopper amplifiers provide a rail-to-rail input range with a 1.8 V to 5.5 V supply voltage range and $20 \mu \mathrm{~A}$ supply current consumption over the $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ extended industrial temperature range. The gain bandwidth is 125 kHz as a unity-gain stable amplifier up to 100 pF load capacitance.

## INPUT VOLTAGE RANGE

The ADA4051-1/ADA4051-2 have internal ESD protection diodes. These diodes are connected between the inputs and each supply rail to protect the input MOSFETs from an electrical discharge event and are reversed-biased during normal operation. This protection scheme allows voltages as high as approximately 0.3 V beyond the supplies ( $\pm \mathrm{V}_{\mathrm{SY}} \pm 0.3 \mathrm{~V}$ ) to be applied at the input of either terminal without causing permanent damage.
If either input exceeds one of the supply rails by more than 0.3 V , these ESD diodes become forward-biased and large amounts of current begin to flow through them. Without current limiting, this excessive current would cause permanent damage to the device. If the inputs are expected to be subject to overvoltage conditions, install a resistor in series with each input to limit the input current to 10 mA maximum.

The ADA4051-1/ADA4051-2 also have internal circuitry that protects the input stage from high differential voltages. This circuitry is composed of internal $1.33 \mathrm{k} \Omega$ resistors in series with each input and back-to-back diode-connected N-MOSFET (with a typical $\mathrm{V}_{\mathrm{T}}$ of 0.7 V for a $\mathrm{V}_{\mathrm{CM}}$ of 0 V ) after these series resistors. With normal negative feedback operating conditions, the ADA4051-1/ ADA4051-2 amplifiers correct their output to ensure that the two inputs are at the same voltage. However, if the device is configured as a comparator or there are unusual operating conditions, the input voltages can be forced to different potentials, which may cause excessive current to flow through the internal diodeconnected N -MOSFETs.

Although the ADA4051-1/ADA4051-2 are rail-to-rail input amplifiers, take care to ensure that the potential difference between the inputs does not exceed $\pm \mathrm{V}_{\text {sy }}$ to avert permanent damage to the device.

## OUTPUT PHASE REVERSAL

Although output phase reversal can occur with other amplifiers when the input common-mode voltage range is exceeded, the ADA4051-1/ADA4051-2 amplifiers are designed to prevent any output phase reversal, provided both inputs are maintained approximately within 0.3 V above and below the supply voltages $\left( \pm \mathrm{V}_{\mathrm{sy}} \pm 0.3 \mathrm{~V}\right.$ ).
With other amplifiers, the outputs may jump in the opposite direction to the supply rail when a common-mode voltage moves outside the common-mode range. This usually occurs when one of the internal stages of the amplifier no longer has sufficient bias voltage across it and subsequently turns off.
However, with the ADA4051-1/ADA4051-2 amplifiers, if one or both inputs exceed the input voltage range but remain within the $\pm \mathrm{V}_{\mathrm{sy}} \pm 0.3 \mathrm{~V}$ range, an internal loop opens and the output remains in saturation mode, without phase reversal, until the input voltage is brought back to within the input voltage range limits as shown in Figure 55 and Figure 58.

## OUTLINE DIMENSIONS




COMPLIANT TO JEDEC STANDARDS MO-187-AA
Figure 63. 8-Lead Mini Small Outline Package [MSOP] (RM-8)
Dimensions shown in millimeters


COMPLIANT TO JEDEC STANDARDS MO-229-WEED
Figure 64. 8-Lead Lead Frame Chip Scale Package [LFCSP]
$3 \mathrm{~mm} \times 3 \mathrm{~mm}$ Body and 0.75 mm Package Height
(CP-8-13)
Dimensions shown in millimeters

## ORDERING GUIDE

| Model ${ }^{1}$ | Temperature Range | Package Description | Package Option | Branding |
| :---: | :---: | :---: | :---: | :---: |
| ADA4051-1ARJZ-R2 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead Small Outline Transistor Package [SOT-23] | RJ-5 | AOU |
| ADA4051-1ARJZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead Small Outline Transistor Package [SOT-23] | RJ-5 | AOU |
| ADA4051-1ARJZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead Small Outline Transistor Package [SOT-23] | RJ-5 | AOU |
| ADA4051-1AKSZ-R2 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead Thin Shrink Small Outline Transistor Package [SC-70] | KS-5 | AOU |
| ADA4051-1AKSZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead Thin Shrink Small Outline Transistor Package [SC-70] | KS-5 | AOU |
| ADA4051-1AKSZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead Thin Shrink Small Outline Transistor Package [SC-70] | KS-5 | AOU |
| ADA4051-2ACPZ-R2 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Lead Frame Chip Scale Package [LFCSP] | CP-8-13 | A2M |
| ADA4051-2ACPZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Lead Frame Chip Scale Package [LFCSP] | CP-8-13 | A2M |
| ADA4051-2ACPZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Lead Frame Chip Scale Package [LFCSP] | CP-8-13 | A2M |
| ADA4051-2ARMZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Mini Small Outline Package [MSOP] | RM-8 | A2M |
| ADA4051-2ARMZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Mini Small Outline Package [MSOP] | RM-8 | A2M |
| ADA4051-2ARMZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Mini Small Outline Package [MSOP] | RM-8 | A2M |

${ }^{1} Z=$ RoHS Compliant Part.
$\square$ ADA4051-1/ADA4051-2

NOTES

## NOTES

## X-ON Electronics

Largest Supplier of Electrical and Electronic Components
Click to view similar products for Precision Amplifiers category:
Click to view products by Analog Devices manufacturer:
Other Similar products are found below :
561681F LT6005HGN\#PBF LT6238CGN\#PBF LT6238HGN\#PBF OP05CN8\#PBF OP227GN\#PBF LT6020IDD-1\#PBF LT1124CS8\#TR NCV20166SN2T1G NCS21802MUTBG LT1637MPS8 LT1498IS8 LT1492CS8 TLC27L7CP TLV2473CDR LMP2234AMA/NOPB LMP7707MA/NOPB 5962-8859301M2A LMP2231AMAE/NOPB LMP2234AMTE/NOPB LMC6022IM/NOPB LMC6024IM/NOPB LMC6081IMX/NOPB LMP2011MA/NOPB LMP2231AMFE/NOPB LMP2232BMA/NOPB LMP2234AMAE/NOPB LMP7715MFE/NOPB LMP7717MAE/NOPB LMV2011MA/NOPB TLC2201AMDG4 TLE2024BMDWG4 TLV2474AQDRG4Q1 TLV2472QDRQ1 TLC4502IDR TLC27M2ACP TLC2652Q-8DG4 OPA2107APG4 TL054AIDR TLC272CD AD8539ARMZ LTC6084HDD\#PBF LTC1050CN8\#PBF LT1112ACN8\#PBF LT1996AIDD\#PBF LT1112CN8\#PBF LTC6087CDD\#PBF LT1078S8\#PBF LT1079ACN\#PBF LTC6242HVCDHC\#PBF

