Operational Amplifier

## Data Sheet

## FEATURES

Low input offset voltage: 0.2 mV typical
High output current drive: 30 mA
Wide range of operating voltage: $\pm 5 \mathrm{~V}$ to $\pm 50 \mathrm{~V}$
High slew rate: $20 \mathrm{~V} / \mu \mathrm{s}$ typical
High gain bandwidth product: 3.5 MHz typical
Thermal regulation at junction temperature $>145^{\circ} \mathrm{C}$
Ambient temperature range: $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Low input bias current $\leq \mathbf{1 5}$ nA typical

## APPLICATIONS

## Automated and bench top test equipment High voltage regulators and power amplifiers Data acquisition and signal conditioning Piezo drivers and predrivers <br> General-purpose current sensing

## GENERAL DESCRIPTION

The ADA4700-1 is a high voltage, precision, single-channel operational amplifier with a wide operating voltage range ( $\pm 5 \mathrm{~V}$ to $\pm 50 \mathrm{~V}$ ) and relatively high output current drive. Its advanced design combines low power ( 170 mW for a $\pm 50 \mathrm{~V}$ supply), high bandwidth ( 3.5 MHz ), and a high slew rate with unity-gain stability and phase inversion free performance. The ability to swing near rail to rail at the output enables designers to maximize signal-to-noise ratios (SNRs).

The ADA4700-1 is designed for applications requiring both ac and dc precision performance, making the ADA4700-1 useful in a wide variety of applications, including high voltage test equipment and instrumentation, high voltage regulators and power amplifiers, power supply control and protection, and as an amplifier or buffer for transducers with wide output ranges. It is particularly well suited for high intensity LED testing applications where it provides highly accurate voltage and current feedback as well as a predriver to provide accurate voltage and/or current sourcing stimulus to the LED string under test.
The ADA4700-1 is specified over the industrial temperature range of $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ and includes thermal regulation at a junction temperature greater than $145^{\circ} \mathrm{C}$ and an integrated current limit. The ADA4700-1 is available in a thermally enhanced, 8-lead SOIC package with an exposed pad.

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## REVISION HISTORY

## 8/13-Revision 0: Initial Version

## SPECIFICATIONS

## $\mathbf{V}_{\mathrm{sy}}= \pm \mathbf{5 0} \mathbf{V}$ ELECTRICAL CHARACTERISTICS

$\mathrm{V}_{\mathrm{SY}}= \pm 50 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise specified.
Table 1.


## ADA4700-1

| Parameter | Symbol | Test Conditions/Comments | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NOISE PERFORMANCE |  |  |  |  |  |  |
| Total Harmonic Distortion + Noise | THD + N | $\begin{aligned} & \mathrm{A}_{\mathrm{v}}=+1, \mathrm{~V}_{\mathrm{IN}}=10 \mathrm{~V} \text { p-p at } 1 \mathrm{kHz}, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega, \\ & \text { bandwidth }=80 \mathrm{kHz} \end{aligned}$ |  | 0.0002 |  | \% |
| Peak-to-Peak Noise | $\mathrm{e}_{\mathrm{n} p-\mathrm{p}}$ | $\mathrm{f}=0.1 \mathrm{~Hz}$ to 10 Hz |  | 800 |  | $\mathrm{n} V \mathrm{p}$-p |
| Voltage Noise Density | $\mathrm{e}_{\mathrm{n}}$ | $\mathrm{f}=1 \mathrm{kHz}$ |  | 14.7 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
|  |  | $\mathrm{f}=10 \mathrm{~Hz}$ |  | 27 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| Current Noise Density | $\mathrm{i}_{\mathrm{n}}$ | $\mathrm{f}=1 \mathrm{kHz}$ |  | 400 |  | $\mathrm{fA} / \sqrt{ } \mathrm{Hz}$ |

${ }^{1}$ See Figure 7 through Figure 9.
${ }^{2}$ Overshoot vs. temperature and capacitive load performance is shown in Figure 27 through Figure 30. Refer to the Driving Capacitive Loads section for recommendations on driving capacitive loads greater than 1 nF .
${ }^{3}$ Refer to the Safe Operating Area section.

## $\mathbf{V}_{\mathrm{sy}}=\mathbf{\pm 2 4}$ V ELECTRICAL CHARACTERISTICS

$\mathrm{V}_{\mathrm{SY}}= \pm 24 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise specified.
Table 2.


| Parameter | Symbol | Test Conditions/Comments | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NOISE PERFORMANCE |  |  |  |  |  |  |
| Total Harmonic Distortion + Noise | THD + N | $\begin{aligned} & \mathrm{A}_{\mathrm{v}}=+1, \mathrm{~V}_{\mathrm{IN}}=10 \mathrm{~V} \mathrm{p}-\mathrm{p} \text { at } 1 \mathrm{kHz}, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega, \\ & \text { bandwidth }=80 \mathrm{kHz} \end{aligned}$ |  | 0.0002 |  | \% |
| Peak-to-Peak Noise | $e_{\text {n } p \text {-p }}$ | $\mathrm{f}=0.1 \mathrm{~Hz}$ to 10 Hz |  | 800 |  | nV p-p |
| Voltage Noise Density | $\mathrm{e}_{\mathrm{n}}$ | $\mathrm{f}=1 \mathrm{kHz}$ |  | 14.7 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
|  |  | $\mathrm{f}=10 \mathrm{~Hz}$ |  | 27 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| Current Noise Density | $\mathrm{i}_{\mathrm{n}}$ | $\mathrm{f}=1 \mathrm{kHz}$ |  | 400 |  | $\mathrm{fA} / \sqrt{ } \mathrm{Hz}$ |

${ }^{1}$ See Figure 7 through Figure 9.
${ }^{2}$ Overshoot vs. temperature and capacitive load performance is shown in Figure 27 through Figure 30. Refer to the Driving Capacitive Loads section for recommendations on driving capacitive loads greater than 1 nF .
${ }^{3}$ Refer to the Safe Operating Area section.

## $\mathbf{V}_{\mathrm{sy}}= \pm \mathbf{5}$ V ELECTRICAL CHARATERISTICS

$\mathrm{V}_{\mathrm{SY}}= \pm 5 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise specified.
Table 3.


[^0]
## ABSOLUTE MAXIMUM RATINGS

Table 4.

| Parameter | Rating |
| :---: | :---: |
| Supply Voltage | 110 V |
| Input Voltage | $\mathrm{V}-\leq \mathrm{V}_{\text {IN }} \leq \mathrm{V}+$ |
| Input Current | $\pm 10 \mathrm{~mA}$ |
| Differential Input Voltage | $\mathrm{V}-\leq \mathrm{V}_{\mathrm{IN}} \leq \mathrm{V}+^{+}$ |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operating Temperature Range ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Junction Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 60 sec ) | $300^{\circ} \mathrm{C}$ |
| ESD |  |
| Charged Device Model (CDM) | 1250 V |
| Human Body Model (HBM) | 4500 V |
| Machine Model (MM) | 200 V |

${ }^{1}$ Refer to the Thermal Management section.
Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## THERMAL RESISTANCE

$\theta_{\text {IA }}$ is specified for the worst-case conditions, that is, a device soldered in a circuit board for surface-mount packages. The values in Table 5 were obtained per JEDEC standard JESD51.

Table 5. Thermal Resistance

| Package Type | $\boldsymbol{\theta}_{\mathrm{JA}}$ | $\boldsymbol{\theta}_{\boldsymbol{\prime c}}$ | Unit |
| :--- | :--- | :--- | :--- |
| 8-Lead SOIC_N_EP | 45 | 30 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

Board layout impacts thermal characteristics such as $\theta_{J A}$. When proper thermal management techniques are used, a better $\theta_{\text {JA }}$ can be achieved. Refer to the Thermal Management section for additional information.

Although the exposed pad can be left floating, it must be connected to an external V - plane for proper thermal management.

## ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



Table 6. Pin Function Descriptions

| Pin No. | Mnemonic | Description |
| :--- | :--- | :--- |
| $1,5,8$ | NC | No Connect. Do not connect to these pins. |
| 2 | - IN | Inverting Input. |
| 3 | + IN | Noninverting Input. |
| 4 | V- | Negative Supply Voltage. |
| 6 | OUT | Output. |
| 7 | V+ | Positive Supply Voltage. |
| 9 | EPAD | Exposed Pad. Connect the exposed pad to V- or leave floating. The exposed pad is electrically connected to the device. |

## TYPICAL PERFORMANCE CHARACTERISTICS

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 4. Input Offset Voltage Distribution, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 5. Input Offset Voltage Distribution, $V_{S Y}= \pm 24 \mathrm{~V}$


Figure 6. Input Offset Voltage Distribution, $V_{s y}= \pm 50 \mathrm{~V}$


Figure 7. Input Offset Voltage Drift Distribution, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 8. Input Offset Voltage Drift Distribution, $V_{S Y}= \pm 24 \mathrm{~V}$


Figure 9. Input Offset Voltage Drift Distribution, $V_{S Y}= \pm 50 \mathrm{~V}$
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 10. Input Offset Voltage (Vos) vs. Common-Mode Voltage (VCM), $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 11. Input Offset Voltage (Vos) vs. Common-Mode Voltage (VCM), $V_{S Y}= \pm 15 \mathrm{~V}$


Figure 12. Input Offset Voltage (Vos) vs. Common-Mode Voltage (VCM), $V_{S Y}= \pm 50 \mathrm{~V}$


Figure 13. Input Bias Current $\left(I_{B}\right)$ vs. Common-Mode Voltage $\left(V_{C M}\right)$ and Temperature, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 14. Input Bias Current $\left(I_{B}\right)$ vs. Common-Mode Voltage $\left(V_{C M}\right)$ and Temperature, $V_{S Y}= \pm 15 \mathrm{~V}$


Figure 15. Input Bias Current ( $I_{B}$ ) vs. Common-Mode Voltage ( $V_{C M}$ ) and Temperature, $V_{s y}= \pm 50 \mathrm{~V}$
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 16. Output Voltage ( $\mathrm{V}_{\mathrm{OH}}$ ) to Supply Rail vs. Load Current, $V_{s Y}= \pm 5 \mathrm{~V}$ to $\pm 50 \mathrm{~V}$


Figure 17. Output Current Transient Settling Time (Sourcing), $V_{S Y}= \pm 50$ V, Refer to Figure 56 for the Test Circuit


Figure 18. Supply Current vs. Supply Voltage


Figure 19. Output Voltage (VoL) to Supply Rail vs. Load Current, $V_{s Y}= \pm 5 \mathrm{~V}$ to $\pm 50 \mathrm{~V}$


Figure 20. Output Current Transient Settling Time (Sinking), $V_{S Y}= \pm 50 \mathrm{~V}$, Refer to Figure 57 for the Test Circuit
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 21. Unity-Gain Bandwidth vs. Temperature, $V_{S Y}= \pm 50 \mathrm{~V}$


Figure 22. Open-Loop Gain and Phase vs. Frequency, $V_{S Y}= \pm 5 \mathrm{~V}$ to $\pm 50 \mathrm{~V}$


Figure 23. Closed-Loop Gain vs. Frequency, $V_{s y}= \pm 5 \mathrm{~V}$ to $\pm 50 \mathrm{~V}$


Figure 24. Unity-Gain Bandwidth vs. Load Capacitance and Temperature, $V_{S Y}= \pm 50 \mathrm{~V}$


Figure 25. Open-Loop Gain vs. Load Current for Various Supply Voltages


Figure 26. Open-Loop Gain vs. Temperature for Various Load Resistances, $V_{S Y}= \pm 50 \mathrm{~V}$
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 27. Small Signal Overshoot vs. Temperature for Various Capacitance Loads, $V_{s Y}= \pm 5 \mathrm{~V}$


Figure 28. Small Signal Overshoot vs. Temperature for Various Capacitance Loads, Vsy $= \pm 50 \mathrm{~V}$


Figure 29. Small Signal Overshoot vs. Temperature for Various Capacitance Loads, $V_{S Y}= \pm 15 \mathrm{~V}$


Figure 30. Small Signal Overshoot vs. Load Capacitance, Vsy $= \pm 5 \mathrm{~V}$ to $\pm 50 \mathrm{~V}$
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 31. Total Harmonic Distortion + Noise (THD + Noise) vs. Amplitude, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 32. Total Harmonic Distortion + Noise (THD + Noise) vs. Amplitude, $V_{S Y}= \pm 15 \mathrm{~V}$


Figure 33. Total Harmonic Distortion + Noise (THD + Noise) vs. Amplitude, $V_{S Y}= \pm 50 \mathrm{~V}$


Figure 34. Total Harmonic Distortion + Noise (THD + Noise) vs. Frequency, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 35. Total Harmonic Distortion + Noise (THD + Noise) vs. Frequency, $V_{s y}= \pm 15 \mathrm{~V}$


Figure 36. Total Harmonic Distortion + Noise (THD + Noise) vs. Frequency, $V_{S Y}= \pm 50 \mathrm{~V}$
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 37. Common-Mode Rejection Ratio (CMRR) vs. Frequency, $V_{s Y}= \pm 5 \mathrm{~V}$ to $\pm 50 \mathrm{~V}$


Figure 38. Power Supply Rejection Ratio (PSRR) vs. Frequency, $V S Y= \pm 5 \mathrm{~V}$ to $\pm 50 \mathrm{~V}$


Figure 39. Common-Mode Rejection Ratio (CMRR) vs. Temperature for Various Supply Voltages


Figure 40. Power Supply Rejection Ratio (PSRR) vs. Temperature
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 41. Closed-Loop Output Impedance (Zout) vs. Frequency, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 42. Positive Output Overload Recovery, $V_{S Y}= \pm 50 \mathrm{~V}$


Figure 43. No Phase Reversal, $V_{S Y}= \pm 50 \mathrm{~V}$


Figure 44. Closed-Loop Output Impedance (Zout) vs. Frequency, $V_{S Y}= \pm 50 \mathrm{~V}$


Figure 45. Negative Output Overload Recovery, $V_{s y}= \pm 50 \mathrm{~V}$
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 46. Input Voltage Noise Density vs. Frequency


Figure 47. 0.1 Hz to 10 Hz Noise, $V_{s y}= \pm 5 \mathrm{~V}$


Figure 48. Input Current Noise Density vs. Frequency


Figure 49. 0.1 Hz to 10 Hz Noise, $V_{s y}= \pm 50 \mathrm{~V}$
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 50. Small Signal Transient Response, $V_{S Y}= \pm 50 \mathrm{~V}$


Figure 51. Slew Rate (SR) vs. Temperature, $V_{s Y}= \pm 50 \mathrm{~V}$


Figure 52. $0.01 \%$ and $0.1 \%$ Settling Time vs. Step Size, $V_{S Y}= \pm 15 \mathrm{~V}$


Figure 53. Large Signal Transient Response, $V_{S Y}= \pm 50 \mathrm{~V}$


Figure 54. $0.01 \%$ and $0.1 \%$ Settling Time vs. Step Size, $V_{s Y}= \pm 5 \mathrm{~V}$


Figure 55. $0.01 \%$ and 0.1\% Settling Time vs. Step Size, $V_{s y}= \pm 50 \mathrm{~V}$

## TEST CIRCUITS



Figure 56. Test Circuit for Output Current Transient Settling Time (Sourcing) Shown in Figure 17


Figure 57. Test Circuit for Output Current Transient Settling Time (Sinking) Shown in Figure 20

## THEORY OF OPERATION



Figure 58. Simplified Schematic of the ADA4700-1

The ADA4700-1 is a high voltage operational amplifier featuring a slew enhanced bipolar input stage that provides all of the voltage gain. Single stage amplifiers are noted for their excellent stability but poor open-loop gain; however, the advanced ADA4700-1 design provides gain comparable to multistage amplifiers and, therefore, combines the advantages of both.
Referring to Figure 58, the input stage is formed by Q5 to Q8 loaded by the current mirrors, Q9 to Q14. The output stage is of the complementary Darlington type formed by Q15 to Q18. Like other bipolar amplifiers, the input stage is internally clamped to prevent degradation with large differential inputs; however, the addition of Q1 and Q2 in conjunction with the high voltage diodes, D 1 and D 2 , maintain high differential input impedance even when the voltage between the inputs is equal to the supply voltage. This configuration makes the ADA4700-1 suitable for applications with unavoidable large differential voltages, such as rectifiers, peak detectors, and comparators.
The ADA4700-1 uses a single-pole compensation set by C3 and C4. The internal snubber networks, R1/C1 and R2/C2, further enhance the stability. This design enables large capacitive loads to be driven without the risk of oscillation.

The Q19 and Q20 transistors in conjunction with the R3 and R4 resistors provide output short-circuit protection. Additionally, a thermal regulating circuit (not shown in Figure 58) limits the die temperature to $145^{\circ} \mathrm{C}$ or greater to protect against excessive power dissipation.

With approximately equal split supplies up to $\pm 50 \mathrm{~V}$, the output can be shorted to ground unconditionally; however, operating this way is not recommended.
If the voltage between the output and either supply is more than 60 V , avoid a short circuit to the supply. Transient dissipation in the output transistors can exceed their safe operating area and cause subsequent destruction.

## THERMAL REGULATION

The circuitry for thermal regulation of the ADA4700-1 is dependent on the ambient temperature and time duration of the current drive. When thermal regulation of the ADA4700-1 is active, the supply current, $I_{\text {SY }}$, reduces from 1.7 mA to $300 \mu \mathrm{~A}$. The output stage remains biased during thermal regulation due to the parasitics of the output devices in conjunction with the elevated die temperature. For example, with a current drive, Iour, of 30 mA for 180 seconds and with an ambient temperature of $85^{\circ} \mathrm{C}$, the thermal regulation is triggered at a junction temperature of $145^{\circ} \mathrm{C}$ with an output current level of 22 mA . For additional information, refer to the Thermal Management section and the Safe Operating Area section.

## APPLICATIONS INFORMATION

## THERMAL MANAGEMENT

Thermal management of high power amplifiers such as the ADA4700-1 is an essential consideration in system design. Two conditions affect junction temperature ( $\mathrm{T}_{\mathrm{J}}$ ): power dissipation $\left(\mathrm{P}_{\mathrm{D}}\right)$ of the device and ambient temperature $\left(\mathrm{T}_{\mathrm{A}}\right)$ surrounding the package. This relationship is shown in Equation 1.

$$
\begin{equation*}
T_{J}=P_{D} \times \theta_{I A}+T_{A} \tag{1}
\end{equation*}
$$

where $\theta_{\text {IA }}$ is the thermal resistance between the die and the ambient environment. Power dissipation is the sum of quiescent power of the device and the power required to drive a load. Power dissipation for the sourcing current is shown in Equation 2.

$$
\begin{equation*}
P_{D}=((V+)-(V-)) \times I_{S Y}+\left((V+)-V_{\text {OUT }}\right) \times I_{O U T} \tag{2}
\end{equation*}
$$

Replace ((V+) - Vout) in Equation 2 with $\left((\mathrm{V}-)-\mathrm{V}_{\text {out }}\right)$ when sinking current.
The specified thermal resistance of the ADA4700-1 is $45^{\circ} \mathrm{C} / \mathrm{W}$. Printed circuit board (PCB) layout and an external heat sink can improve thermal performance by reducing $\theta_{\mathrm{JA}}$.
To reduce the thermal resistance between the junction and ambient environment, the exposed pad of the ADA4700-1 can be soldered to the V-plane layer of the PCB, which acts as a heat sink. By using the PCB layout shown in Figure 60, $\theta_{\mathrm{JA}}$ reduces to $26^{\circ} \mathrm{C} / \mathrm{W}$.
The ADA4700-1 guards the die from exceeding the absolute maximum temperature. When the die reaches a junction temperature greater than $145^{\circ} \mathrm{C}$, thermal regulation is triggered, the supply current is reduced, and the output load current is limited.

## SAFE OPERATING AREA

The safe operating area (SOA) of Figure 59 is the range of voltages, currents, and temperatures under which an amplifier can safely operate without failure. It is directly dependent on the ambient temperature and the thermal resistance. Figure 59 shows the SOA for the ADA4700-1 at steady state using the PCB shown in Figure 60. The duration of the 30 mA load driven is 180 seconds. Different time intervals produce alternate sets of curves. The guaranteed ambient temperature range of the ADA4700-1 is $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. The $125^{\circ} \mathrm{C}$ shown in Figure 59 is for reference only. To maintain normal operation, the ADA4700-1 must remain in the SOA (area under each curve) up to an ambient temperature of $85^{\circ} \mathrm{C}$.


Figure 59. Safe Operating Area with $\theta_{J A}=26^{\circ} \mathrm{C} / \mathrm{W}$


Figure 60. Thermal Landing and PCB Material Used to Obtain a $\theta_{J A}$ of $26^{\circ} \mathrm{C} / \mathrm{W}$

## DRIVING CAPACITIVE LOADS

Although the ADA4700-1 behaves well when driving capacitive loads, $C_{L}$, as seen in Figure 27 to Figure 30, extra compensation can improve the response when large capacitances need to be accommodated. The simplest way of accomplishing this is with a snubber network, as shown in Figure 61.


Figure 61. Snubber Network
For unity-gain applications and capacitive loads up to 1 nF , $R_{\text {SNUB }}=150 \Omega$ and $C_{\text {SNUB }}=10 \mathrm{nF}$ works well. Results for this circuit are shown in Figure 64. With higher closed-loop gains, lighter snubbing can be used. For capacitive loads up to 10 nF , the snubber must be larger. Figure 65 shows the results of using an Rssub $=22 \Omega$, Csnub $=100 \mathrm{nF}$, and $\mathrm{C}_{\mathrm{L}}=10 \mathrm{nF}$ with the ADA4700-1 in a gain of 10 . Because the snubber network places an ac load on the amplifier, snubbing does not work well when larger capacitive loads are used, or when large transients are present. A better approach is to use a bypass network in the feedback path, as shown in Figure 62.


Figure 62. Unity-Gain Configuration with Bypass Network
The bypass network in Figure 62 performs well with loads up to 100 nF . The resulting waveforms are shown in Figure 66 for various output amplitudes. For heavier loads, capacitive feedback, $\mathrm{C}_{\mathrm{FB}}$, must be increased. The configuration in Figure 62 can be modified to work with gains greater than 1 . Figure 63 shows a bypass network with a gain of 10 system, and results for various output amplitudes are shown in Figure 67.


Figure 63. Bypass Network with Gain of 10 System


Figure 64. Results from Snubber Network with $A_{v}=+1$ and $C_{L}=10 \mathrm{pF}$ to 1 nF


Figure 65. Results from Snubber Network with Higher Gains, $C_{L}=10 \mathrm{nF}$


Figure 66. Results of Bypass Network for Various Output Amplitudes, Unity Gain with $C_{L}=100 \mathrm{nF}$


Figure 67. Result of Bypass Network with $A_{v}=+10$ and $C_{L}=100 \mathrm{nF}$

## INCREASING CURRENT DRIVE

Extra output current can be obtained by adding external driver transistors. Crossover distortion is minimized by allowing the amplifier to drive the lower currents directly via the bypass resistor, as is shown in Figure 68. This circuit can provide a few hundred miliamps; however, keep the driver transistors within their safe operating area. For heavier loads (up to 5 A ), power Darlingtons can be used, as is shown in Figure 69.


Figure 68. Increasing Current Drive Using Discrete Transistors


Figure 69. Bilateral Current Source with Transfer Function $1 \mathrm{~mA} / \mathrm{V}$

## CONSTANT CURRENT APPLICATIONS

When a constant current with high compliance is needed, the ADA4700-1 can be used as a modified Howland current pump. The values shown in Figure 70 yield a transfer function of $1 \mathrm{~mA} / \mathrm{V}$. Applying this analysis to the modified Howland current pump in Figure 71 results in an output capability of $1 \mathrm{~A} / \mathrm{V}$.


Figure 70. Transfer Function of $1 \mathrm{~mA} / \mathrm{V}$


Figure 71. Modified Howland Current Pump

## OUTLINE DIMENSIONS



## ORDERING GUIDE

| Model $^{1}$ | Temperature Range | Package Description | Package Option |
| :--- | :--- | :--- | :--- |
| ADA4700-1ARDZ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package with Exposed Pad [SOIC_N_EP] | RD-8-2 |
| ADA4700-1ARDZ-R7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package with Exposed Pad [SOIC_N_EP] | RD-8-2 |
| ADA4700-1ARDZ-RL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package with Exposed Pad [SOIC_N_EP] | RD-8-2 |

[^1]NOTES
$\square$
Data Sheet
ADA4700-1
NOTES

## NOTES

## X-ON Electronics

Largest Supplier of Electrical and Electronic Components
Click to view similar products for Precision Amplifiers category:
Click to view products by Analog Devices manufacturer:
Other Similar products are found below :
561681F LT6005HGN\#PBF LT6238CGN\#PBF LT6238HGN\#PBF OP05CN8\#PBF LT6020IDD-1\#PBF LT1124CS8\#TR NCV20166SN2T1G NCS20166SN2T1G NCS21802MUTBG LT1637MPS8 LT1498IS8 LT1492CS8 TLC27L7CP TLV2473CDR LMP2234AMA/NOPB LMP7707MA/NOPB 5962-8859301M2A LMP2231AMAE/NOPB LMP2234AMTE/NOPB LMC6022IM/NOPB LMC6024IM/NOPB LMC6081IMX/NOPB LMP2011MA/NOPB LMP2231AMFE/NOPB LMP2232BMA/NOPB LMP2234AMAE/NOPB
LMP7717MAE/NOPB LMV2011MA/NOPB LT1013DDR TL034ACDR TLC2201AMDG4 TLE2024BMDWG4 TS9222IYDT
TLV2474AQDRG4Q1 TLV2472QDRQ1 TLC4502IDR TLC27M2ACP TLC2652Q-8DG4 OPA2107APG4 TL054AIDR AD8619WARZ-
R7 TLC272CD AD8539ARMZ LTC6084HDD\#PBF LTC1050CN8\#PBF LT1996AIDD\#PBF LT1112CN8\#PBF LTC6087CDD\#PBF
LT1078S8\#PBF


[^0]:    ${ }^{1}$ See Figure 7 through Figure 9.
    ${ }^{2}$ Overshoot vs. temperature and capacitive load performance is shown in Figure 27 through Figure 30. Refer to the Driving Capacitive Loads section for recommendations on driving capacitive loads greater than 1 nF .
    ${ }^{3}$ Refer to the Safe Operating Area section.

[^1]:    ${ }^{1} \mathrm{Z}=$ RoHS Compliant Part.

