

### FEATURES

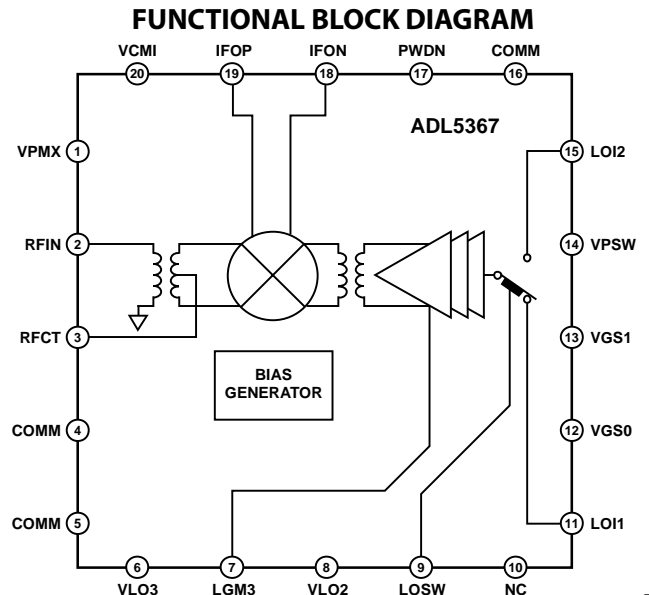
- RF frequency range of 500 MHz to 1700 MHz
- IF frequency range of 30 MHz to 450 MHz
- Power conversion loss: 7.7 dB
- SSB noise figure of 8.3 dB
- SSB noise figure with 5 dBm blocker of 21 dB
- Input IP3 of 34 dBm
- Typical LO drive of 0 dBm
- Single-ended, 50 Ω RF and LO input ports
- High isolation SPDT LO input switch
- Single-supply operation: 3.3 V to 5 V
- Exposed paddle 5 mm × 5 mm, 20-lead LFCSP
- 1500 V HBM/500 V FICDM ESD performance

### APPLICATIONS

- Cellular base station receivers
- Transmit observation receivers
- Radio link downconverters

### GENERAL DESCRIPTION

The [ADL5367](#) uses a highly linear, doubly balanced passive mixer core along with integrated RF and LO balancing circuitry to allow for single-ended operation. The [ADL5367](#) incorporates an RF balun, allowing optimal performance over a 500 MHz to 1700 MHz RF input frequency range. Performance is optimized for RF frequencies from 500 MHz to 1200 MHz using a high-side LO and for RF frequencies from 900 MHz to 1700 MHz using a low-side LO. The balanced passive mixer arrangement provides good LO to RF leakage, typically better than -35 dBm, and excellent intermodulation performance. The balanced mixer core also provides extremely high input linearity, allowing the device to be used in demanding cellular applications where in-band blocking signals may otherwise result in the degradation of dynamic performance. A high linearity IF buffer amplifier follows the passive mixer core to yield a typical power conversion loss of 7.7 dB and can be used with a wide range of output impedances.



NC = NO CONNECT

Figure 1.

The [ADL5367](#) provides two switched LO paths that can be used in TDD applications where it is desirable to rapidly switch between two local oscillators. LO current can be externally set using a resistor to minimize dc current commensurate with the desired level of performance. For low voltage applications, the [ADL5367](#) is capable of operation at voltages down to 3.3 V with substantially reduced current. Under low voltage operation, an additional logic pin is provided to power down (<200 μA) the circuit when desired.

The [ADL5367](#) is fabricated using a BiCMOS high performance IC process. The device is available in a 5 mm × 5 mm, 20-lead LFCSP and operates over a -40°C to +85°C temperature range. An evaluation board is also available.

Table 1. Passive Mixers

RF Frequency (MHz)	Single Mixer	Single Mixer and IF Amp	Dual Mixer and IF Amp
500 to 1700	<a href="#">ADL5367</a>	<a href="#">ADL5357</a>	<a href="#">ADL5358</a>
1200 to 2500	<a href="#">ADL5365</a>	<a href="#">ADL5355</a>	<a href="#">ADL5356</a>
2300 to 2900	<a href="#">ADL5363</a>	<a href="#">ADL5353</a>	<a href="#">ADL5354</a>

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## REVISION HISTORY

### 3/16—Rev. B to Rev. C

Added Thermal Resistance Section and Junction to Board Thermal Impedance Section .....	5
Changes to Figure 2 .....	6
Change to Evaluation Board Section and Figure 49 .....	20

### 2/15—Rev. A to Rev. B

Changes to Table 1 .....	1
Deleted Figure 37 and Figure 39 .....	13
Deleted Bias Resistor Selection Section .....	19
Changes to Figure 49 .....	20
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Updated Outline Dimensions .....	23
Changes to Ordering Guide .....	23

### 10/09—Revision 0: Initial Version

## SPECIFICATIONS

$V_S = 5\text{ V}$ ,  $I_S = 97\text{ mA}$ ,  $T_A = 25^\circ\text{C}$ ,  $f_{RF} = 900\text{ MHz}$ ,  $f_{LO} = 1103\text{ MHz}$ , LO power = 0 dBm,  $Z_O = 50\ \Omega$ , unless otherwise noted.

Table 2.

Parameter	Test Conditions/Comments	Min	Typ	Max	Unit
RF INPUT INTERFACE					
Return Loss	Tunable to >20 dB over a limited bandwidth		14		dB
Input Impedance			50		$\Omega$
RF Frequency Range		500		1700	MHz
OUTPUT INTERFACE					
Output Impedance	Differential impedance, $f = 200\text{ MHz}$		34  1.9		$\Omega$   pF
IF Frequency Range		30		450	MHz
DC Bias Voltage <sup>1</sup>	Externally generated	3.3	5.0	5.5	V
LO INTERFACE					
LO Power		-6	0	+10	dBm
Return Loss			12.6		dB
Input Impedance			50		$\Omega$
LO Frequency Range		730		1670	MHz
POWER-DOWN (PWDN) INTERFACE <sup>2</sup>					
PWDN Threshold			1.0		V
Logic 0 Level				0.4	V
Logic 1 Level		1.4			V
PWDN Response Time	Device enabled, IF output to 90% of the final level		160		ns
	Device disabled, supply current < 5 mA		220		ns
PWDN Input Bias Current	Device enabled		0.0		$\mu\text{A}$
	Device disabled		70		$\mu\text{A}$

<sup>1</sup> Apply the supply voltage from the external circuit through the choke inductors.

<sup>2</sup> PWDN function is intended for use with  $V_S \leq 3.6\text{ V}$  only.

**5 V PERFORMANCE**

$V_S = 5\text{ V}$ ,  $I_S = 97\text{ mA}$ ,  $T_A = 25^\circ\text{C}$ ,  $f_{RF} = 900\text{ MHz}$ ,  $f_{LO} = 1103\text{ MHz}$ , LO power = 0 dBm, VGS0 = VGS1 = 0 V, and  $Z_O = 50\ \Omega$ , unless otherwise noted.

**Table 3.**

Parameter	Test Conditions/Comments	Min	Typ	Max	Unit
<b>DYNAMIC PERFORMANCE</b>					
Power Conversion Loss	Including 1:1 IF port transformer and printed circuit board (PCB) loss	6.5	7.7	8.5	dB
Voltage Conversion Loss	$Z_{SOURCE} = 50\ \Omega$ , differential $Z_{LOAD} = 50\ \Omega$ differential		1.4		dB
SSB Noise Figure			8.3		dB
SSB Noise Figure Under Blocking	5 dBm blocker present $\pm 10\text{ MHz}$ from wanted RF input, LO source filtered		21		dB
Input Third-Order Intercept (IIP3)	$f_{RF1} = 899.5\text{ MHz}$ , $f_{RF2} = 900.5\text{ MHz}$ , $f_{LO} = 1103\text{ MHz}$ , each RF tone at 0 dBm	28	34		dBm
Input Second-Order Intercept (IIP2)	$f_{RF1} = 950\text{ MHz}$ , $f_{RF2} = 900\text{ MHz}$ , $f_{LO} = 1103\text{ MHz}$ , each RF tone at 0 dBm		80		dBm
Input 1 dB Compression Point (IP1dB) <sup>1</sup>	Exceeding 20 dBm RF power results in damage to the device		25		dBm
LO to IF Leakage	Unfiltered IF output		-15		dBm
LO to RF Leakage			-40		dBm
RF to IF Isolation			-47		dBc
IF/2 Spurious	0 dBm input power		-75		dBc
IF/3 Spurious	0 dBm input power		-72		dBc
<b>POWER SUPPLY</b>					
Positive Supply Voltage		4.5	5	5.5	V
Total Quiescent Current	$V_S = 5\text{ V}$		97		mA

<sup>1</sup> Exceeding 20 dBm RF power results in damage to the device.

**3.3 V PERFORMANCE**

$V_S = 3.3\text{ V}$ ,  $I_S = 56\text{ mA}$ ,  $T_A = 25^\circ\text{C}$ ,  $f_{RF} = 900\text{ MHz}$ ,  $f_{LO} = 1103\text{ MHz}$ , LO power = 0 dBm,  $R_9 = 226\ \Omega$ , VGS0 = VGS1 = 0 V, and  $Z_O = 50\ \Omega$ , unless otherwise noted.

**Table 4.**

Parameter	Test Conditions/Comments	Min	Typ	Max	Unit
<b>DYNAMIC PERFORMANCE</b>					
Power Conversion Loss	Including 4:1 IF port transformer and PCB loss		7.3		dB
Voltage Conversion Loss	$Z_{SOURCE} = 50\ \Omega$ , differential $Z_{LOAD} = 200\ \Omega$ differential		1		dB
SSB Noise Figure			8.1		dB
Input Third-Order Intercept (IIP3)	$f_{RF1} = 1949.5\text{ MHz}$ , $f_{RF2} = 1950.5\text{ MHz}$ , $f_{LO} = 1750\text{ MHz}$ , each RF tone at -10 dBm		28.5		dBm
Input Second-Order Intercept (IIP2)	$f_{RF1} = 1950\text{ MHz}$ , $f_{RF2} = 1900\text{ MHz}$ , $f_{LO} = 1750\text{ MHz}$ , each RF tone at -10 dBm		75		dBm
<b>POWER INTERFACE</b>					
Supply Voltage		3.0	3.3	3.6	V
Quiescent Current	Resistor programmable		56		mA
Power-Down Current	Device disabled		150		$\mu\text{A}$

## ABSOLUTE MAXIMUM RATINGS

Table 5.

Parameter	Rating
Supply Voltage, $V_s$	5.5 V
RF Input Level	20 dBm
LO Input Level	13 dBm
IFOP, IFON Bias Voltage	6.0 V
VGS0, VGS1, LOSW, PWDN	5.5 V
Internal Power Dissipation	1.2 W
Maximum Junction Temperature	150°C
Operating Temperature Range	-40°C to +85°C
Storage Temperature Range	-65°C to +150°C
Lead Temperature Range (Soldering, 60 sec)	260°C

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

### THERMAL RESISTANCE

$\theta_{JA}$  is thermal resistance, junction to ambient (°C/W), and  $\theta_{JB}$  is thermal impedance, junction to board (°C/W).

Table 6. Thermal Resistance

Package Type	$\theta_{JA}$ <sup>1</sup>	$\theta_{JB}$ <sup>1</sup>	Unit
20-Lead LFCSP	25	14.74	°C/W

<sup>1</sup> See the JEDEC standard, JESD51-2, for information on optimizing thermal impedance (PCB with 3 × 3 vias).

### Junction to Board Thermal Impedance

The junction to board thermal impedance ( $\theta_{JB}$ ) is the thermal impedance from the die to or near the component lead of the ADL5367. For the ADL5367,  $\theta_{JB}$  is determined experimentally to 14.74°C/W with the device mounted on a 4-layer circuit board with two layers as ground planes in a configuration similar to the ADL5367-EVALZ evaluation board. Board size and complexity (number of layers) affect  $\theta_{JB}$ ; more layers tend to reduce the thermal impedance slightly.

If the board temperature is known, use the junction to board thermal impedance to calculate die temperature (also known as junction temperature) to ensure it does not exceed the specified limit of 150°C. For example if the board temperature is 85°C, the die temperature is given by the equation

$$T_j = T_B + (P_{DISS} \times \theta_{JB})$$

where  $T_j$  is the junction temperature.

$T_B$  is the board temperature measured at or near the component lead.

$P_{DISS}$  is the power dissipated from the device.

The typical worst case power dissipation for the ADL5367 is 605 mW (5.5 V × 110 mA). Therefore  $T_j$  is

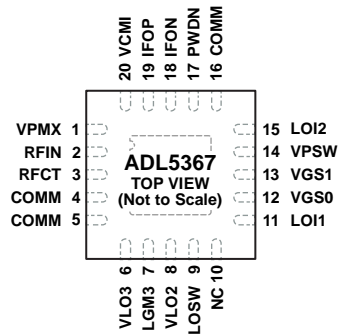
$$T_j = 85^\circ\text{C} + (0.605 \text{ W} \times 14.74^\circ\text{C/W}) = 93.91^\circ\text{C}$$

### ESD CAUTION



**ESD (electrostatic discharge) sensitive device.** Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



- NOTES  
 1. NC = NO CONNECT.  
 2. EXPOSED PAD. MUST BE SOLDERED TO GROUND.

08083-002

Figure 2. Pin Configuration

Table 7. Pin Function Descriptions

Pin No.	Mnemonic	Description
1	VPMX	Positive Supply Voltage for IF Amplifier.
2	RFIN	RF Input. This pin must be ac-coupled.
3	RFCT	RF Balun Center Tap (AC Ground).
4, 5, 16	COMM	Device Common (DC Ground).
6, 8	VLO3, VLO2	Positive Supply Voltages for LO Amplifier.
7	LGM3	LO Amplifier Bias Control.
9	LOSW	LO Switch. LOI1 selected for 0 V, or LOI2 selected for 3 V.
10	NC	No Connect.
11, 15	LOI1, LOI2	LO Inputs. This pin must be ac-coupled.
12, 13	VGS0, VGS1	Mixer Gate Bias Controls. 3 V logic. Ground these pins for nominal setting.
14	VPSW	Positive Supply Voltage for LO Switch.
17	PWDN	Power Down. Connect this pin to ground for normal operation or connect this pin to 3.0 V for disable mode.
18, 19	IFON, IFOP	Differential IF Outputs.
20	VCM1	No Connect. This pin can be grounded.
	EPAD (EP)	Exposed pad must be soldered to ground.

# TYPICAL PERFORMANCE CHARACTERISTICS

## 5 V PERFORMANCE

$V_S = 5\text{ V}$ ,  $I_S = 97\text{ mA}$ ,  $T_A = 25^\circ\text{C}$ ,  $f_{RF} = 900\text{ MHz}$ ,  $f_{LO} = 1103\text{ MHz}$ , LO power = 0 dBm,  $V_{GS0} = V_{GS1} = 0\text{ V}$ , and  $Z_O = 50\ \Omega$ , unless otherwise noted.

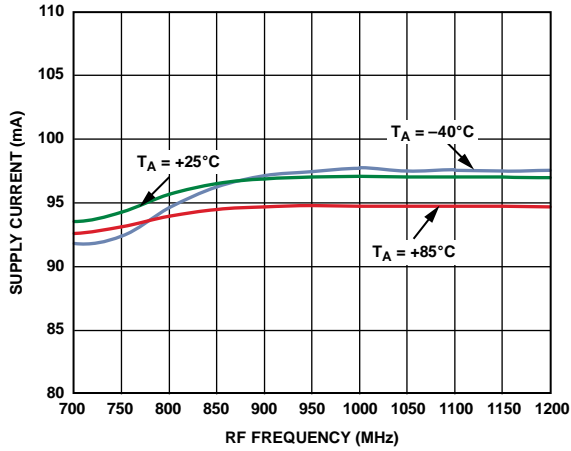


Figure 3. Supply Current vs. RF Frequency

06983-017

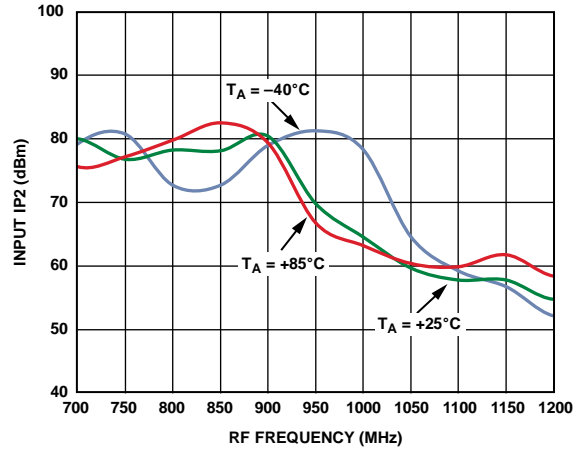


Figure 6. Input IP2 vs. RF Frequency

06983-023

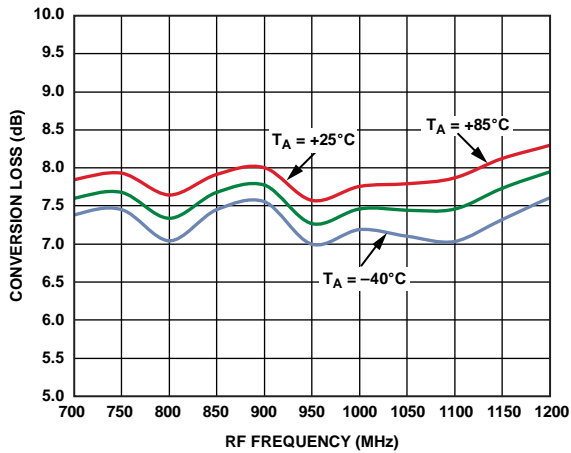


Figure 4. Power Conversion Loss vs. RF Frequency

06983-035

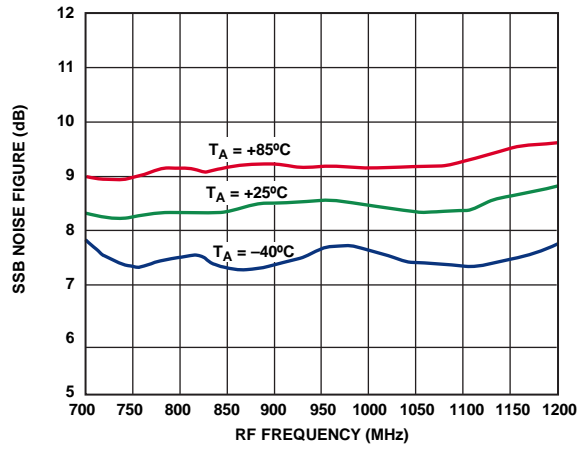


Figure 7. SSB Noise Figure vs. RF Frequency

06983-011

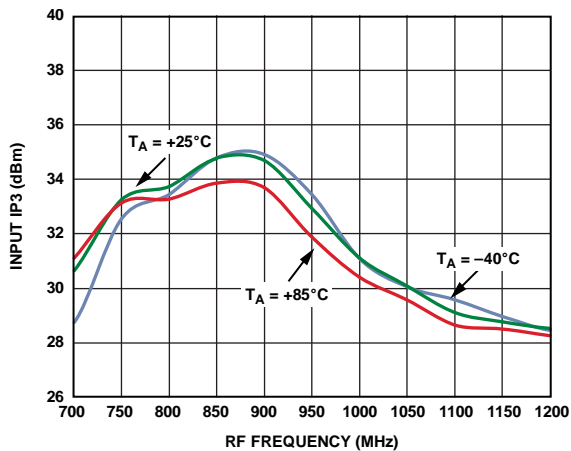


Figure 5. Input IP3 vs. RF Frequency

06983-028

$V_S = 5\text{ V}$ ,  $I_S = 97\text{ mA}$ ,  $T_A = 25^\circ\text{C}$ ,  $f_{RF} = 900\text{ MHz}$ ,  $f_{LO} = 1103\text{ MHz}$ , LO power = 0 dBm,  $V_{GS0} = V_{GS1} = 0\text{ V}$ , and  $Z_O = 50\ \Omega$ , unless otherwise noted.

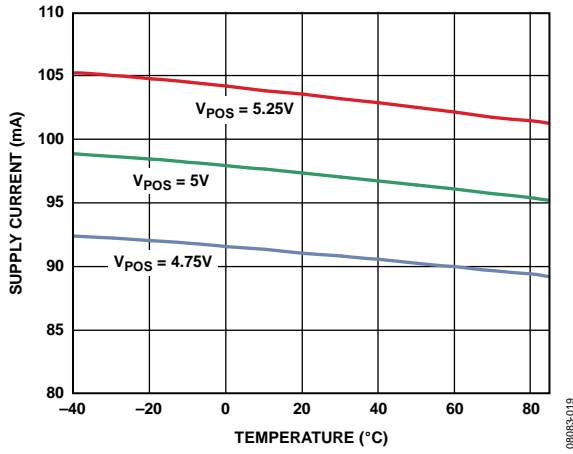


Figure 8. Supply Current vs. Temperature

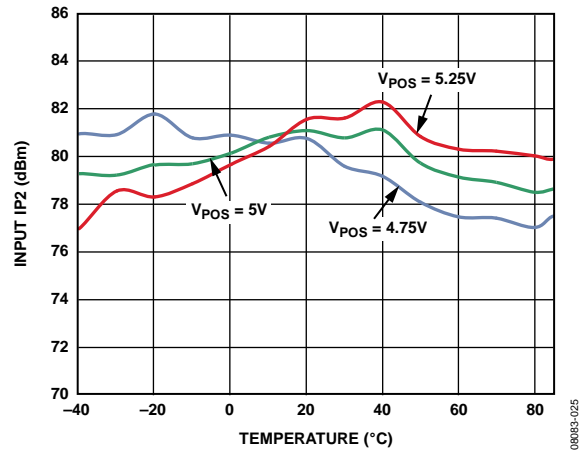


Figure 11. Input IP2 vs. Temperature

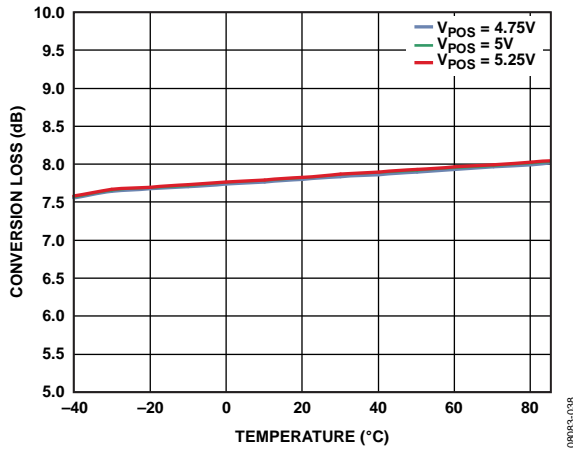


Figure 9. Power Conversion Loss vs. Temperature

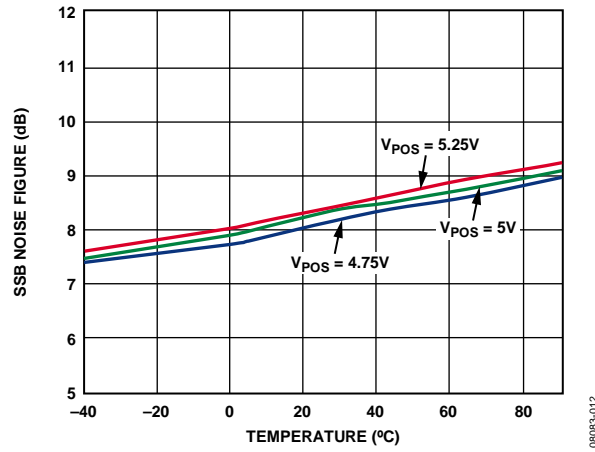


Figure 12. SSB Noise Figure vs. Temperature

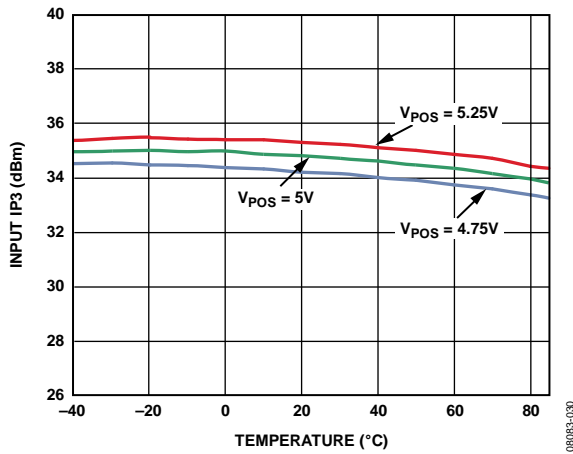


Figure 10. Input IP3 vs. Temperature



$V_S = 5\text{ V}$ ,  $I_S = 97\text{ mA}$ ,  $T_A = 25^\circ\text{C}$ ,  $f_{RF} = 900\text{ MHz}$ ,  $f_{LO} = 1103\text{ MHz}$ , LO power = 0 dBm,  $V_{GS0} = V_{GS1} = 0\text{ V}$ , and  $Z_O = 50\ \Omega$ , unless otherwise noted.

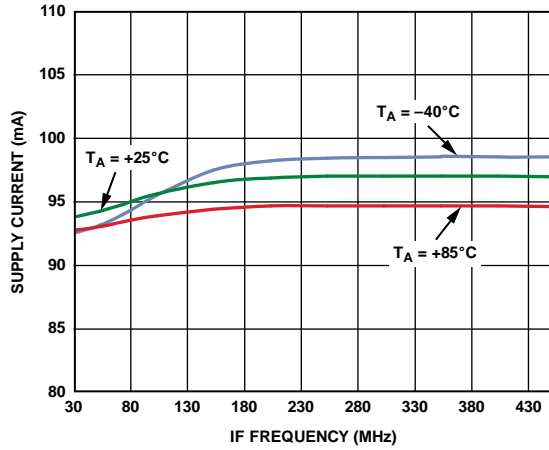


Figure 13. Supply Current vs. IF Frequency

08083-016

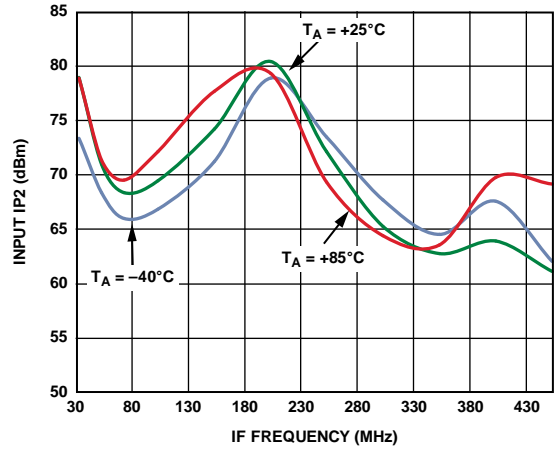


Figure 16. Input IP2 vs. IF Frequency

08083-021

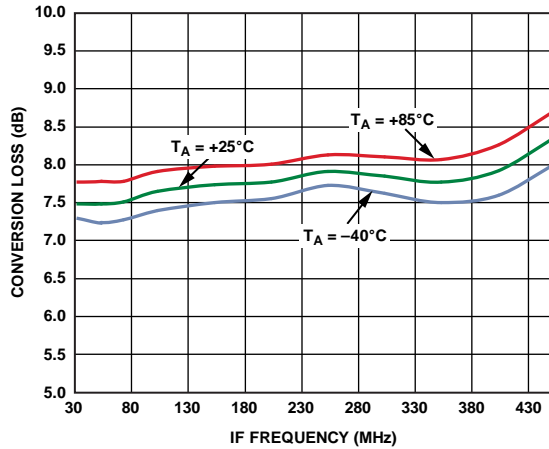


Figure 14. Power Conversion Loss vs. IF Frequency

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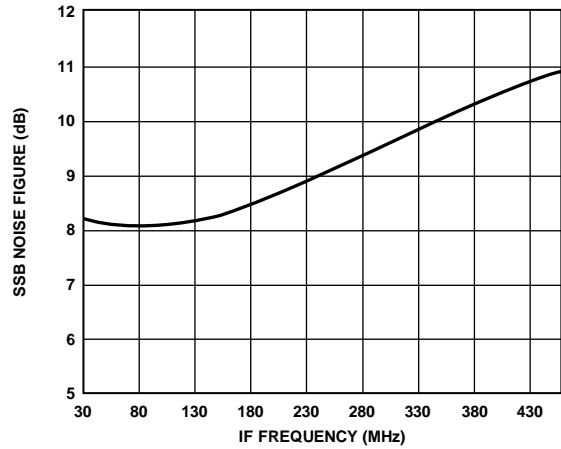


Figure 17. SSB Noise Figure vs. IF Frequency

08083-010

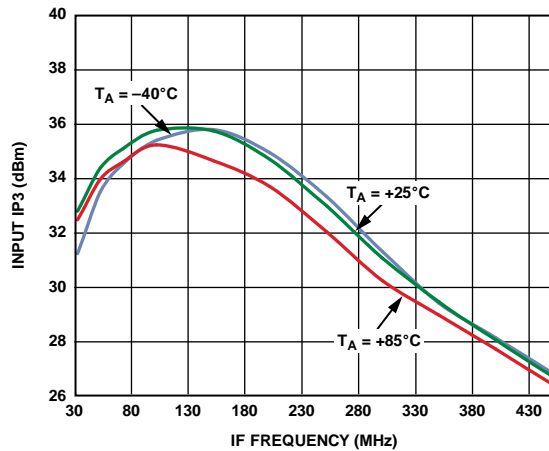


Figure 15. Input IP3 vs. IF Frequency

08083-028

$V_S = 5\text{ V}$ ,  $I_S = 97\text{ mA}$ ,  $T_A = 25^\circ\text{C}$ ,  $f_{RF} = 900\text{ MHz}$ ,  $f_{LO} = 1103\text{ MHz}$ , LO power = 0 dBm,  $V_{GS0} = V_{GS1} = 0\text{ V}$ , and  $Z_O = 50\ \Omega$ , unless otherwise noted.

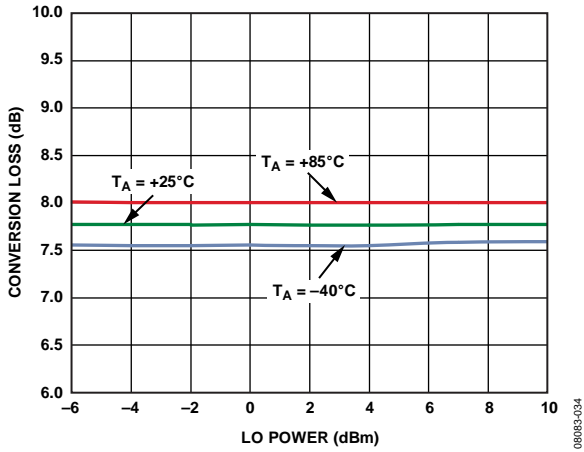


Figure 18. Power Conversion Loss vs. LO Power

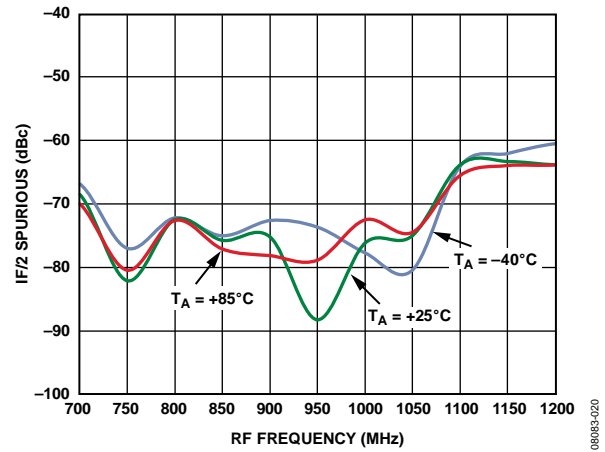


Figure 21. IF/2 Spurious vs. RF Frequency

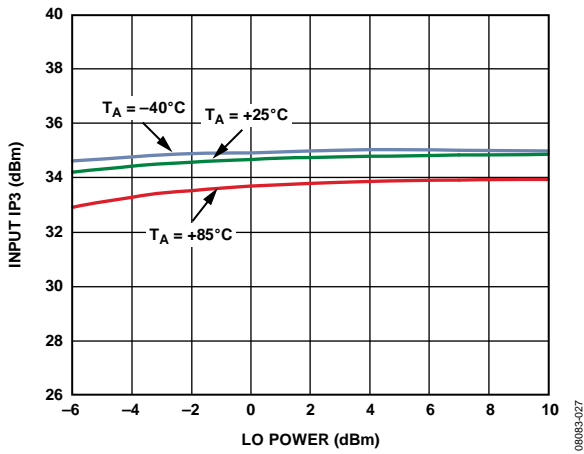


Figure 19. Input IP3 vs. LO Power

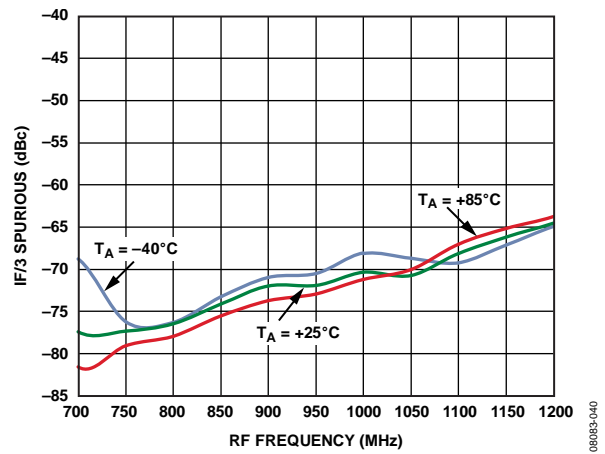


Figure 22. IF/3 Spurious vs. RF Frequency

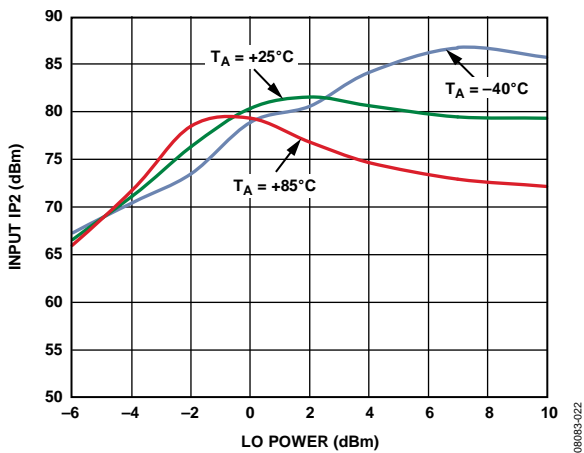


Figure 20. Input IP2 vs. LO Power

$V_S = 5\text{ V}$ ,  $I_S = 97\text{ mA}$ ,  $T_A = 25^\circ\text{C}$ ,  $f_{RF} = 900\text{ MHz}$ ,  $f_{LO} = 1103\text{ MHz}$ , LO power = 0 dBm,  $V_{GS0} = V_{GS1} = 0\text{ V}$ , and  $Z_O = 50\ \Omega$ , unless otherwise noted.

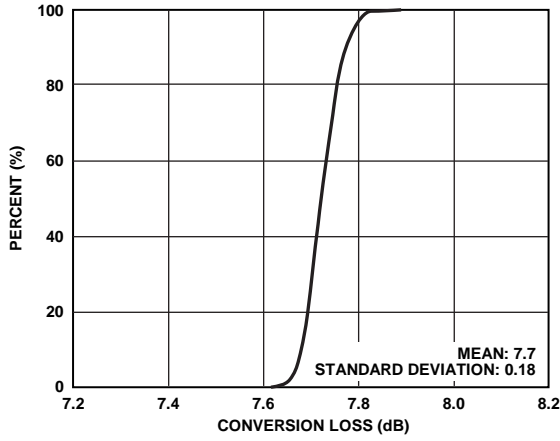


Figure 23. Conversion Loss Distribution

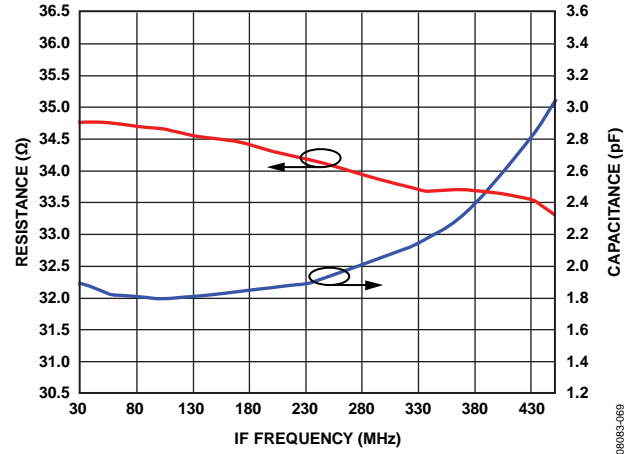


Figure 26. IF Port Return Loss

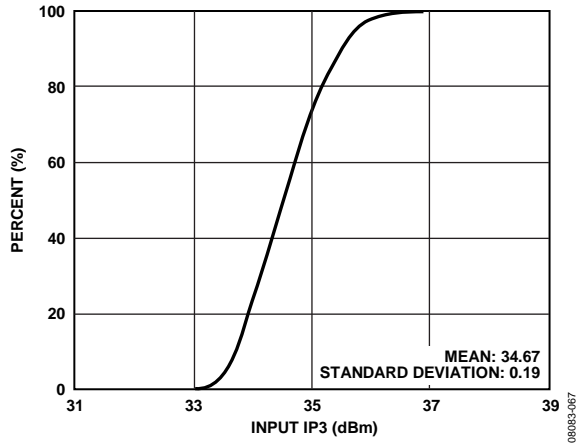


Figure 24. Input IP3 Distribution

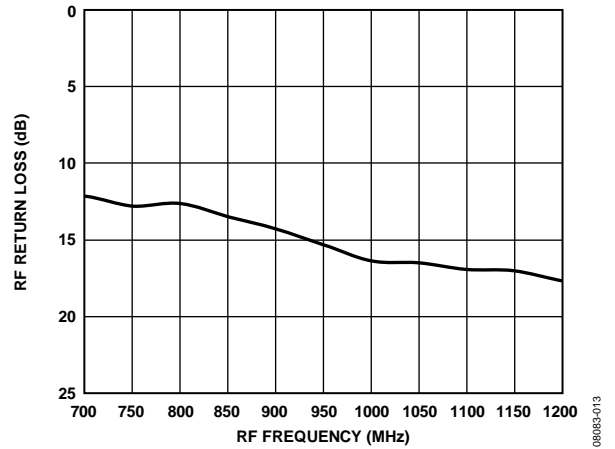


Figure 27. RF Port Return Loss, Fixed IF

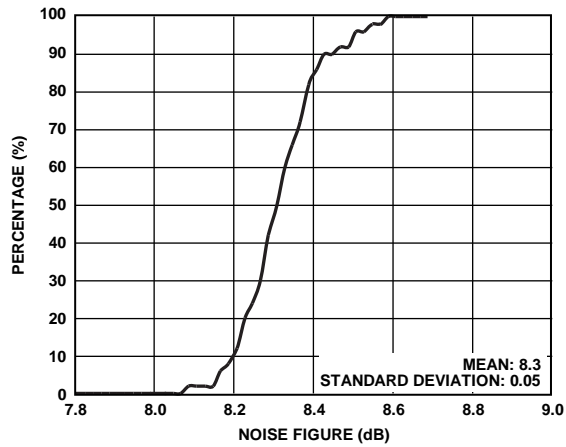


Figure 25. SSB Noise Figure Distribution

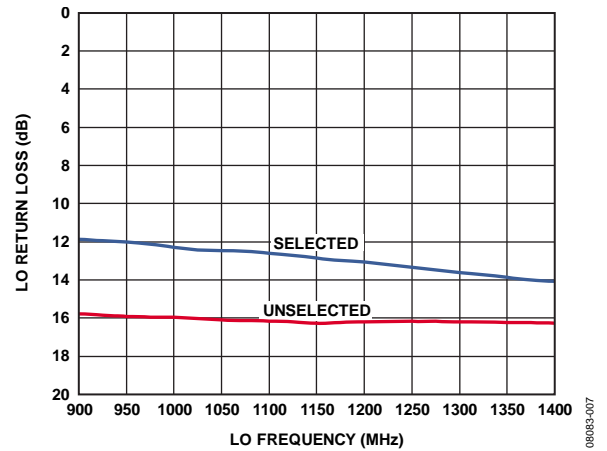


Figure 28. LO Return Loss, Selected and Unselected

$V_S = 5\text{ V}$ ,  $I_S = 97\text{ mA}$ ,  $T_A = 25^\circ\text{C}$ ,  $f_{RF} = 900\text{ MHz}$ ,  $f_{LO} = 1103\text{ MHz}$ , LO power = 0 dBm,  $V_{GS0} = V_{GS1} = 0\text{ V}$ , and  $Z_O = 50\ \Omega$ , unless otherwise noted.

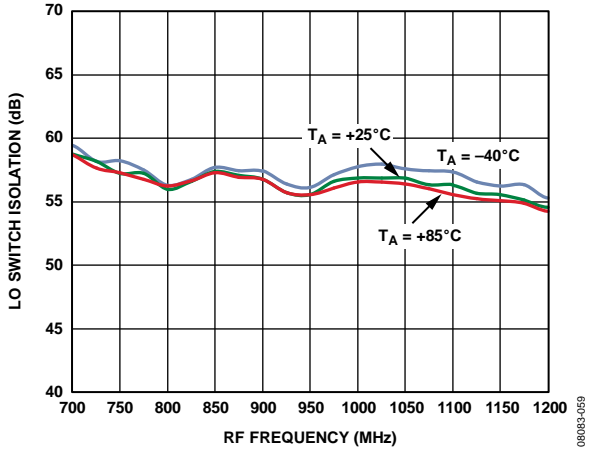


Figure 29. LO Switch Isolation vs. RF Frequency

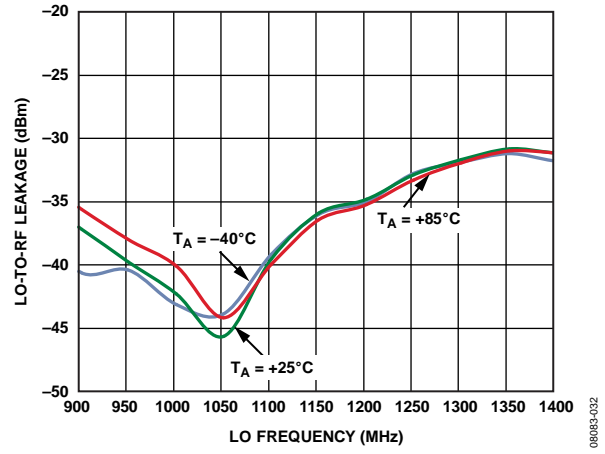


Figure 32. LO to RF Leakage vs. LO Frequency

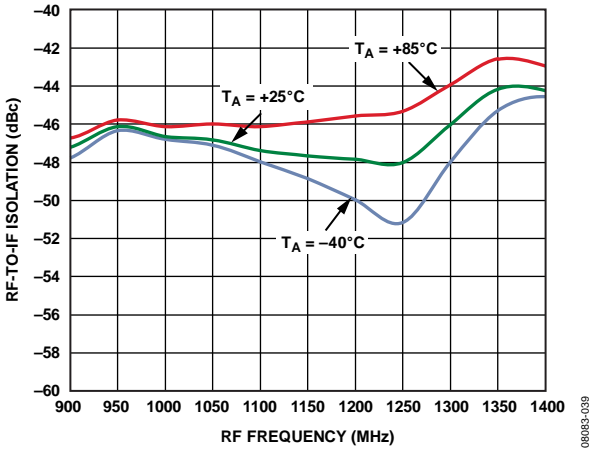


Figure 30. RF to IF Isolation vs. RF Frequency

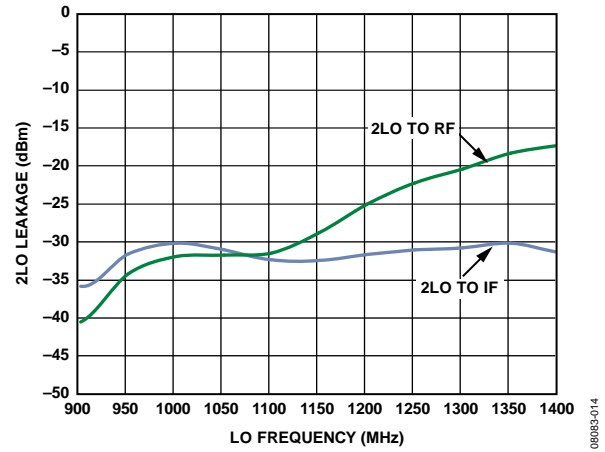


Figure 33. 2LO Leakage vs. LO Frequency

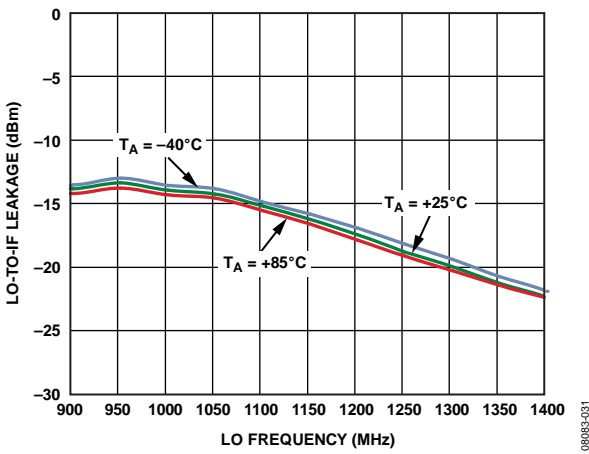


Figure 31. LO to IF Leakage vs. LO Frequency

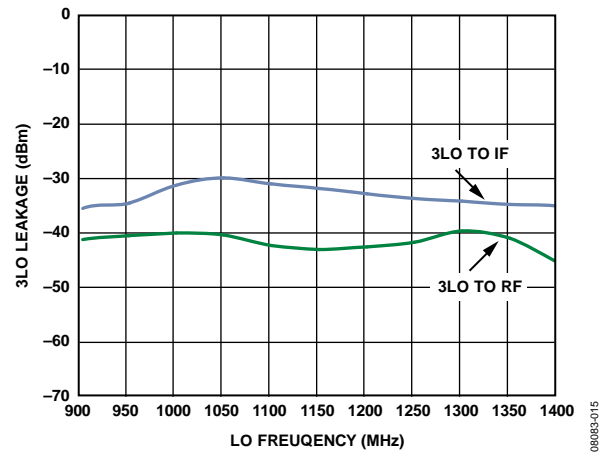


Figure 34. 3LO Leakage vs. LO Frequency

$V_S = 5\text{ V}$ ,  $I_S = 97\text{ mA}$ ,  $T_A = 25^\circ\text{C}$ ,  $f_{RF} = 900\text{ MHz}$ ,  $f_{LO} = 1103\text{ MHz}$ , LO power = 0 dBm,  $V_{GS0} = V_{GS1} = 0\text{ V}$ , and  $Z_O = 50\ \Omega$ , unless otherwise noted.

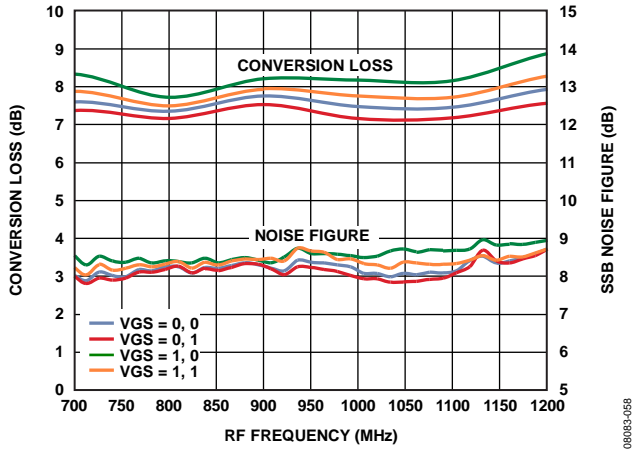


Figure 35. Power Conversion Loss and SSB Noise Figure vs. RF Frequency

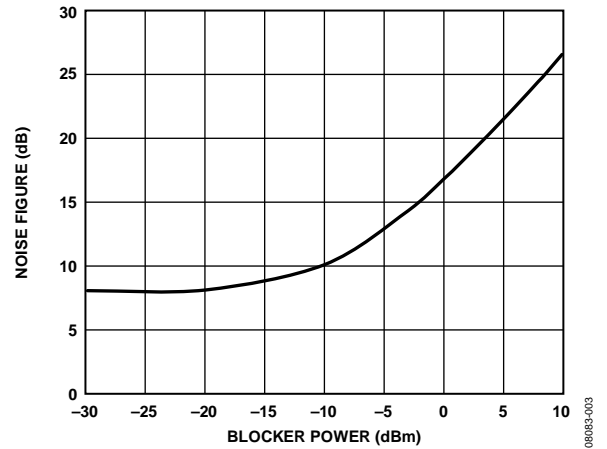


Figure 37. SSB Noise Figure vs. 10 MHz Offset Blocker Level

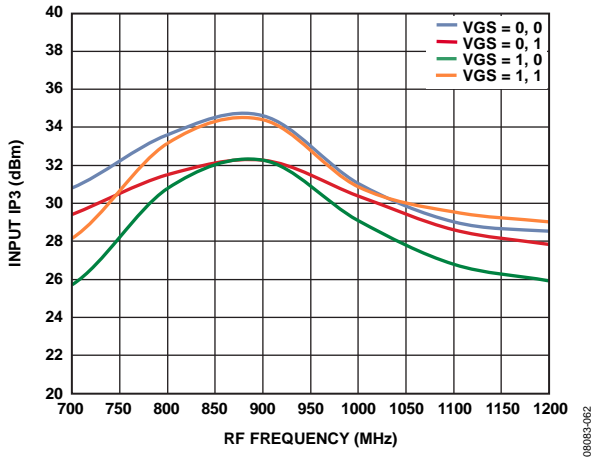


Figure 36. Input IP3 vs. RF Frequency

3.3 V PERFORMANCE

$V_S = 3.3\text{ V}$ ,  $I_S = 56\text{ mA}$ ,  $T_A = 25^\circ\text{C}$ ,  $f_{RF} = 900\text{ MHz}$ ,  $f_{LO} = 1103\text{ MHz}$ , LO power = 0 dBm,  $R_9 = 226\ \Omega$ ,  $V_{GS0} = V_{GS1} = 0\text{ V}$ , and  $Z_O = 50\ \Omega$ , unless otherwise noted.

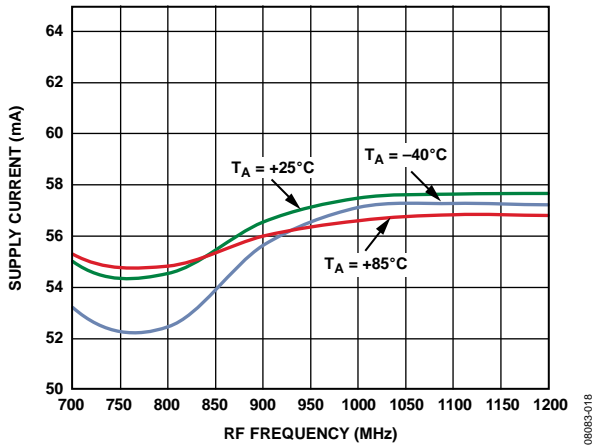


Figure 38. Supply Current vs. RF Frequency at 3.3 V

08083-018

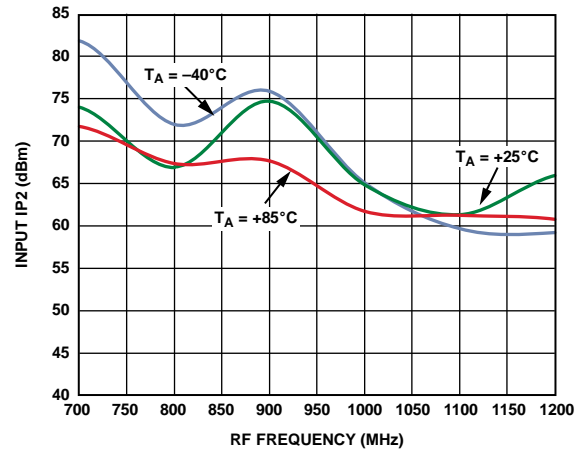


Figure 41. Input IP2 vs. RF Frequency at 3.3 V

08083-024

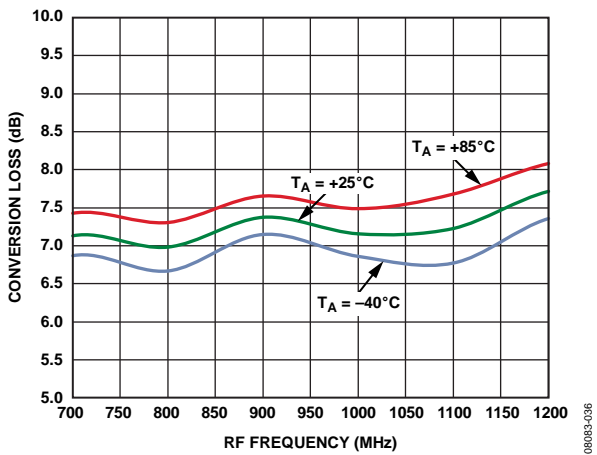


Figure 39. Power Conversion Loss vs. RF Frequency at 3.3 V

08083-036

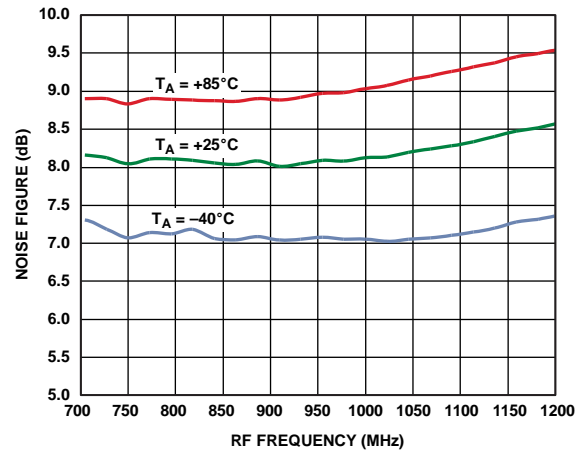


Figure 42. SSB Noise Figure vs. RF Frequency at 3.3 V

08083-064

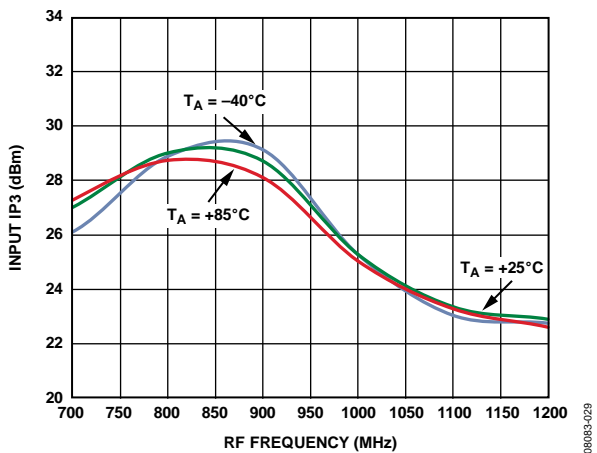


Figure 40. Input IP3 vs. RF Frequency at 3.3 V

08083-029

**UPCONVERSION**

$T_A = 25^\circ\text{C}$ ,  $f_{IF} = 153\text{ MHz}$ ,  $f_{LO} = 1697\text{ MHz}$ , LO power = 0 dBm, RF power = 0 dBm, VGS0 = VGS1 = 0 V, and  $Z_O = 50\ \Omega$ , unless otherwise noted.

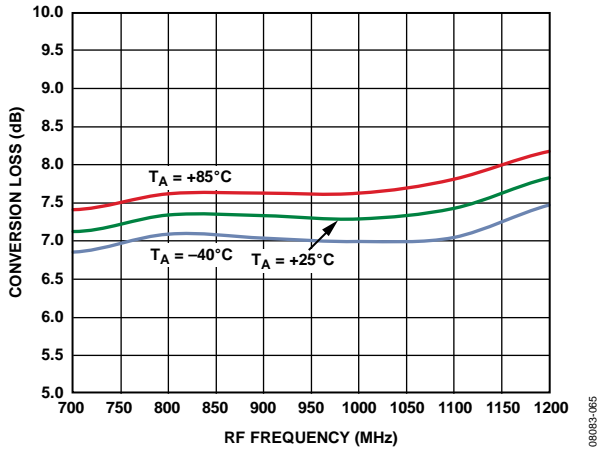


Figure 43. Power Conversion Loss vs. RF Frequency,  $V_s = 5\text{ V}$ , Upconversion

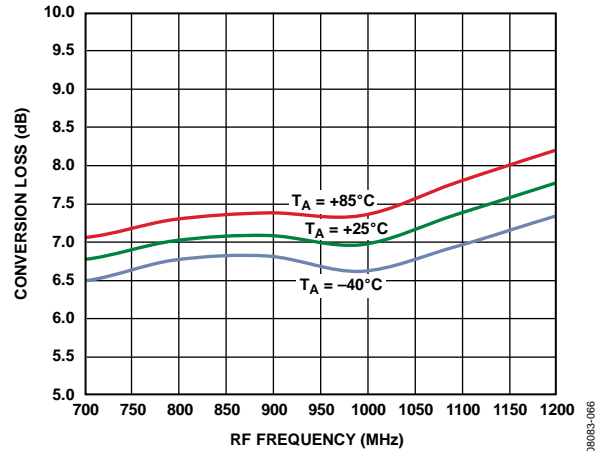


Figure 45. Power Conversion Loss vs. RF Frequency at 3.3 V, Upconversion

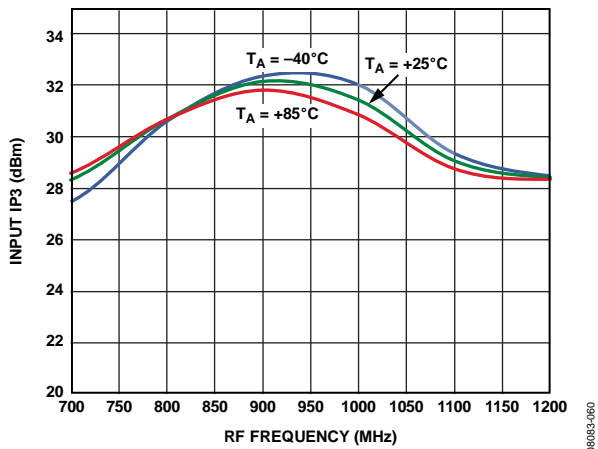


Figure 44. Input IP3 vs. RF Frequency,  $V_s = 5\text{ V}$ , Upconversion

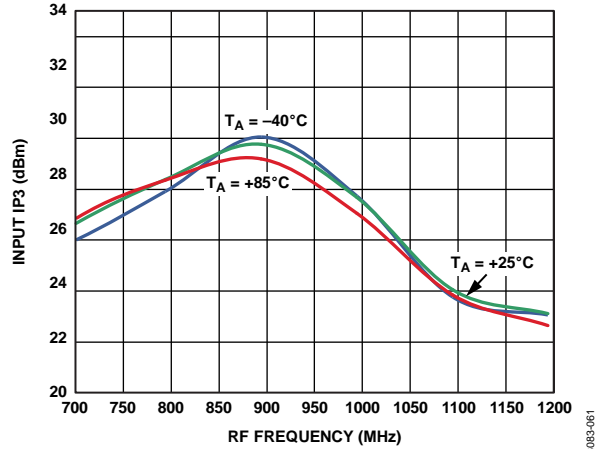


Figure 46. Input IP3 vs. RF Frequency at 3.3 V, Upconversion

**SPUR TABLES**

All spur tables are  $(N \times f_{RF}) - (M \times f_{LO})$  and were measured using the standard evaluation board. Mixer spurious products are measured in dBc from the IF output power level. Data was measured only for frequencies less than 6 GHz. Typical noise floor of the measurement system = -100 dBm.

**5 V Performance**

$V_S = 5\text{ V}$ ,  $I_S = 97\text{ mA}$ ,  $T_A = 25^\circ\text{C}$ ,  $f_{RF} = 900\text{ MHz}$ ,  $f_{LO} = 1103\text{ MHz}$ , LO power = 0 dBm, RF power = 0 dBm, VGS0 = VGS1 = 0 V, and  $Z_O = 50\ \Omega$ , unless otherwise noted.

		M														
		0	1	2	3	4	5	6	7	8	9	10	11	12	13	14
N	0		-7.8	-24.6	-35.7	-53.0	-47.4									
	1	-39.7	0.0	-45.0	-27.5	-53.0	-54.4	-71.8								
	2	-84.6	-68.8	-77.4	-72.8	-80.2	-80.9	-87.8	-96.8							
	3	<-100	-78.6	-95.5	-75.9	-97.9	-91.7	<-100	<-100							
	4	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100						
	5	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100					
	6	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100				
	7		<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100			
	8			<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100		
	9			<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	
	10				<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100
	11					<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100
	12						<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100
	13							<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100
	14								<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100
	15									<-100	<-100	<-100	<-100	<-100	<-100	<-100

**3.3 V Performance**

$V_S = 3.3\text{ V}$ ,  $I_S = 56\text{ mA}$ ,  $T_A = 25^\circ\text{C}$ ,  $f_{RF} = 900\text{ MHz}$ ,  $f_{LO} = 1103\text{ MHz}$ , LO power = 0 dBm, RF power = 0 dBm, R9 = 226  $\Omega$ , VGS0 = VGS1 = 0 V, and  $Z_O = 50\ \Omega$ , unless otherwise noted.

		M														
		0	1	2	3	4	5	6	7	8	9	10	11	12	13	14
N	0		-12.6	-28.8	-40.6	-43.0	-59.6									
	1	-40.5	0.0	-42.7	-27.1	-53.2	-50.7	-71.8								
	2	-78.6	-59.5	-64.8	-68.0	-65.9	-73.0	-75.4	-89.4							
	3	-93.9	-66.3	-90.1	-63.0	-90.5	-77.8	-96.4	-95.6							
	4	<-100	<-100	-95.6	-95.5	-97.0	<-100	<-100	<-100	<-100						
	5	<-100	<-100	<-100	<-100	<-100	-98.9	<-100	<-100	<-100	<-100					
	6	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100				
	7		<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100			
	8			<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100		
	9			<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	
	10				<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100
	11					<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100
	12						<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100
	13							<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100
	14								<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100
	15									<-100	<-100	<-100	<-100	<-100	<-100	<-100



## CIRCUIT DESCRIPTION

The **ADL5367** consists of two primary components: the radio frequency (RF) subsystem and the local oscillator (LO) subsystem. The combination of design, process, and packaging technology allows the functions of these subsystems to be integrated into a single die, using mature packaging and interconnection technologies to provide a high performance, low cost design with excellent electrical, mechanical, and thermal properties. In addition, the need for external components is minimized, optimizing cost and size.

The RF subsystem consists of an integrated, low loss RF balun, passive MOSFET mixer, sum termination network, and IF amplifier.

The LO subsystem consists of an SPDT terminated FET switch and a three-stage limiting LO amplifier. The purpose of the LO subsystem is to provide a large, fixed amplitude, balanced signal to drive the mixer independent of the level of the LO input.

A block diagram of the device is shown in Figure 47.

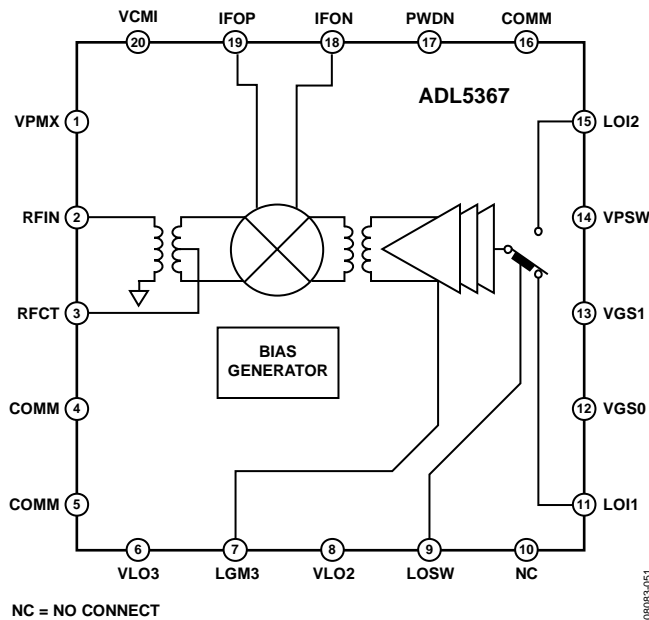


Figure 47. Simplified Schematic

### RF SUBSYSTEM

The single-ended, 50  $\Omega$  RF input is internally transformed to a balanced signal using a low loss (<1 dB) unbalanced to balanced (balun) transformer. This transformer is made possible by an extremely low loss metal stack, which provides both excellent balance and dc isolation for the RF port. Although the port can be dc connected, it is recommended that a blocking capacitor be used to avoid running excessive dc current through the device. The RF balun can easily support an RF input frequency range of 500 MHz to 1700 MHz.

The resulting balanced RF signal is applied to a passive mixer that commutates the RF input with the output of the LO subsystem. The passive mixer is essentially a balanced, low loss switch that adds minimum noise to the frequency translation. The only noise contribution from the mixer is due to the resistive loss of the switches, which is in the order of a few ohms.

Because the mixer is inherently broadband and bidirectional, it is necessary to properly terminate all the idler ( $M \times N$  product) frequencies generated by the mixing process. Terminating the mixer avoids the generation of unwanted intermodulation products and reduces the level of unwanted signals at the IF output. This termination is accomplished by the addition of a sum network between the IF output and the mixer.

Additionally, dc current can be saved by reducing the dc supply voltage to as low as 3.3 V, further reducing the dissipated power of the device. (Note that no performance enhancement is obtained by reducing the value of these resistors and excessive dc power dissipation may result.)

### LO SUBSYSTEM

The LO amplifier is designed to provide a large signal level to the mixer to obtain optimum intermodulation performance. The resulting amplifier provides extremely high performance centered on an operating frequency of 1100 MHz. The best operation is achieved with either high-side LO injection for RF signals in the 500 MHz to 1200 MHz range or low-side injection for RF signals in the 900 MHz to 1700 MHz range. Operation outside these ranges is permissible, and conversion loss is extremely wideband, easily spanning 500 MHz to 1700 MHz, but intermodulation is optimal over the aforementioned ranges.

The **ADL5367** has two LO inputs permitting multiple synthesizers to be rapidly switched with extremely short switching times (<40 ns) for frequency agile applications. The two inputs are applied to a high isolation SPDT switch that provides a constant input impedance, regardless of whether the port is selected, to avoid pulling the LO sources. This multiple section switch also ensures high isolation to the off input, minimizing any leakage from the unwanted LO input that may result in undesired IF responses.

The single-ended LO input is converted to a fixed amplitude differential signal using a multistage, limiting LO amplifier. This results in consistent performance over a range of LO input power. Optimum performance is achieved from  $-6$  dBm to  $+10$  dBm, but the circuit continues to function at considerably lower levels of LO input power.

The performance of this amplifier is critical in achieving a high intercept passive mixer without degrading the noise floor of the system. This is a critical requirement in an interferer rich environment, such as cellular infrastructure, where blocking interferers can limit mixer performance. The bandwidth of the intermodulation performance is somewhat influenced by the current in the LO amplifier chain. For dc current sensitive applications, it is permissible to reduce the current in the LO amplifier by raising the value of the external bias control resistor. For dc current critical applications, the LO chain can operate with a supply voltage as low as 3.3 V, resulting in substantial dc power savings.

In addition, when operating with supply voltages below 3.6 V, the [ADL5367](#) has a power-down mode that permits the dc current to drop to <200  $\mu$ A.

All of the logic inputs are designed to work with any logic family that provides a Logic 0 input level of less than 0.4 V and a Logic 1 input level that exceeds 1.4 V. All logic inputs are high impedance up to Logic 1 levels of 3.3 V. At levels exceeding 3.3 V, protection circuitry permits operation up to 5.5 V, although a small bias current is drawn.

# APPLICATIONS INFORMATION

## BASIC CONNECTIONS

The ADL5367 mixer is designed to upconvert or downconvert between radio frequencies (RF) from 500 MHz to 1700 MHz and intermediate frequencies (IF) from dc to 450 MHz. Figure 48 depicts the basic connections of the mixer. It is recommended to ac-couple the RF and LO input ports to prevent nonzero dc voltages from damaging the RF balun or LO input circuit. The RFIN capacitor value of 8 pF is recommended to provide the optimized RF input return loss for the desired frequency band.

For upconversion, the IF input, Pin 18 (IFON) and Pin 19 (IFOP), must be driven differentially or using a 1:1 ratio transformer for single ended operation. An 8 pF capacitor is recommended for the RF output, Pin 2 (RFIN).

## IF PORT

The real part of the output impedance is approximately 50 Ω, as seen in Figure 26, which matches many commonly used SAW filters without the need for a transformer. This results in a voltage conversion loss that is approximately the same as the power conversion loss, as shown in Table 3.

## MIXER VGS CONTROL DAC

The ADL5367 features two logic control pins, Pin 12 (VGS0) and Pin 13 (VGS1), that allow programmability for internal gate to source voltages for optimizing mixer performance over desired frequency bands. The evaluation board defaults both VGS0 and VGS1 to ground. Power conversion loss, NF, and IIP3 can be optimized, as shown in Figure 35 and Figure 36.

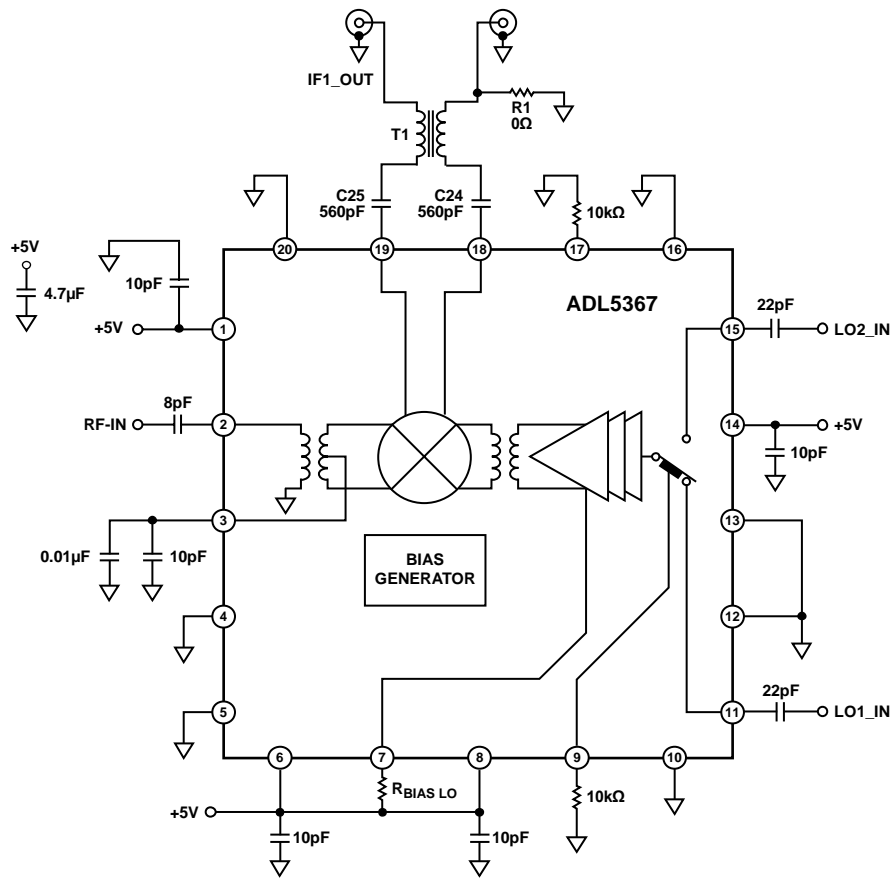


Figure 48. Typical Application Circuit

09002-2652

### EVALUATION BOARD

An evaluation board is available for the family of double balanced mixers. The standard evaluation board schematic is shown in Figure 49. The evaluation board, [ADL5367-EVALZ](#), is fabricated using Rogers® RO3003 material.

Table 8 describes the various configuration options of the evaluation board. The evaluation board layout is shown in Figure 50 to Figure 53.

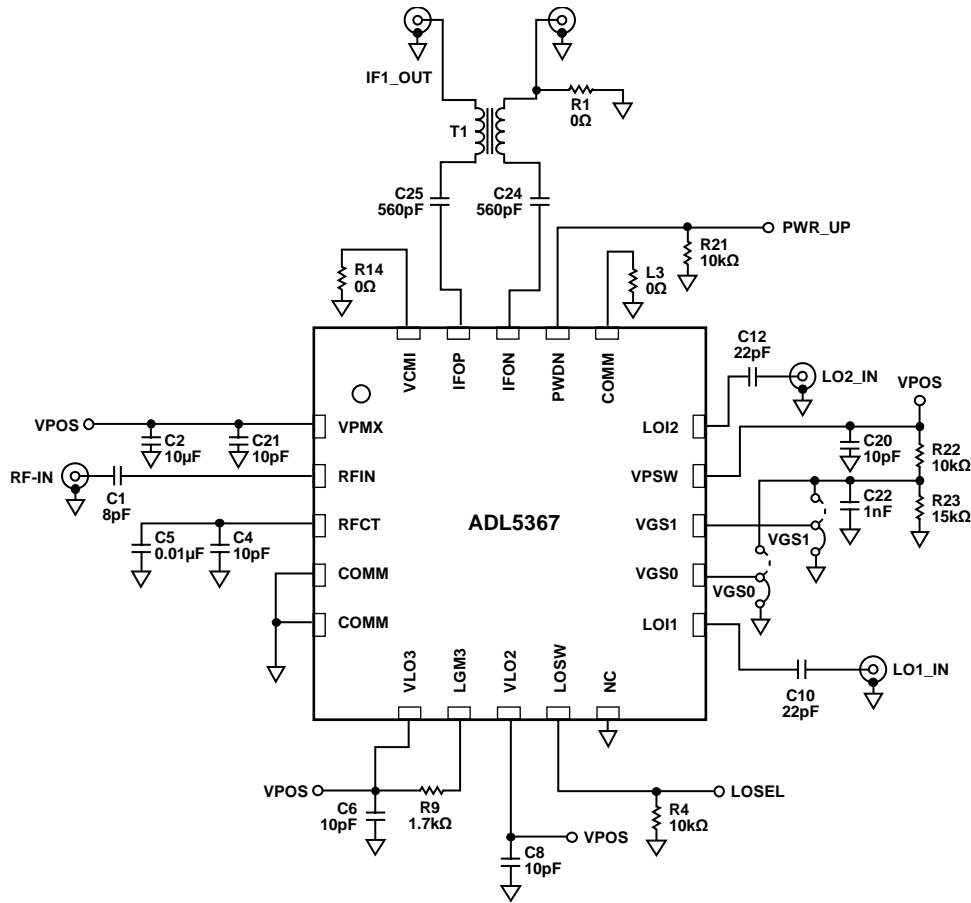


Figure 49. Evaluation Board Schematic

08082-053

Table 8. Evaluation Board Configuration

Components	Description	Default Conditions
C2, C6, C8, C20, C21	Power Supply Decoupling. Nominal supply decoupling consists of a 10 $\mu$ F capacitor to ground in parallel with a 10 pF capacitor to ground positioned as close to the device as possible.	C2 = 10 $\mu$ F (Size 0603), C6, C8, C20, C21 = 10 pF (Size 0402)
C1, C4, C5	RF Input Interface. The input channels are ac-coupled through C1. C4 and C5 provide bypassing for the center taps of the RF input baluns.	C1 = 3 pF (Size 0402), C4 = 10 pF (Size 0402), C5 = 0.01 $\mu$ F (Size 0402)
T1, R1, C24, C25	IF Output Interface. T1 is a 1:1 impedance transformer that provides a single-ended IF output interface. Remove R1 for balanced output operation. C24 and C25 block the dc bias at the IF ports.	T1 = TC1-1-13M+ (Mini-Circuits), R1 = 0 $\Omega$ (Size 0402), C24, C25 = 560 pF (Size 0402)
C10, C12, R4	LO Interface. C10 and C12 provide ac coupling for the LO1_IN and LO2_IN local oscillator inputs. LOSEL selects the appropriate LO input for both mixer cores. R4 provides a pull-down to ensure that LO1_IN is enabled when the LOSEL test point is logic low. LO2_IN is enabled when LOSEL is pulled to logic high.	C10, C12 = 22 pF (Size 0402), R4 = 10 k $\Omega$ (Size 0402)
R21	PWDN Interface. R21 pulls the PWDN logic low and enables the device. The PWR_UP test point allows the PWDN interface to be exercised using the an external logic generator. Grounding the PWDN pin for nominal operation is allowed. Using the PWDN pin when supply voltages exceed 3.3 V is not allowed.	R21 = 10 k $\Omega$ (Size 0402)
C22, L3, R9, R14, R22, R23, VGS0, VGS1	Bias Control. R22 and R23 form a voltage divider to provide 3 V for logic control, bypassed to ground through C22. VGS0 and VGS1 jumpers provide programmability at the VGS0 and VGS1 pins. It is recommended to pull these two pins to ground for nominal operation. R9 sets the bias point for the internal LO buffers. R14 sets the bias point for the internal IF amplifier.	C22 = 1 nF (Size 0402), L3 = 0 $\Omega$ (Size 0603), R9 = 1.7 k $\Omega$ (Size 0402), R14 = 0 $\Omega$ (Size 0402), R22 = 10 k $\Omega$ (Size 0402), R23 = 15 k $\Omega$ (Size 0402), VGS0 = VGS1 = 3-pin shunt

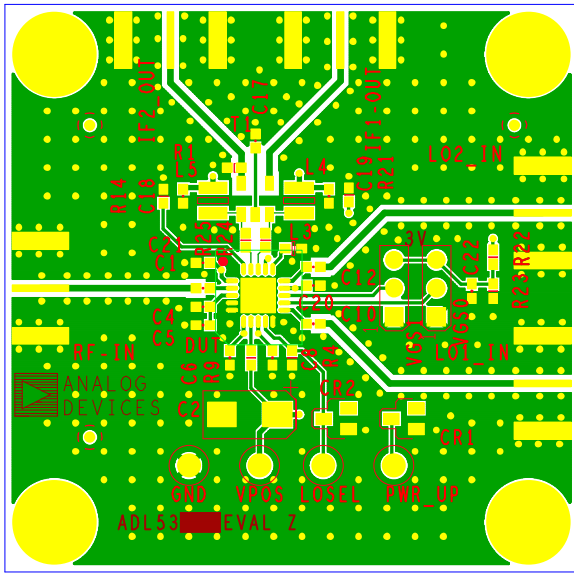


Figure 50. Evaluation Board Top Layer

08083-054

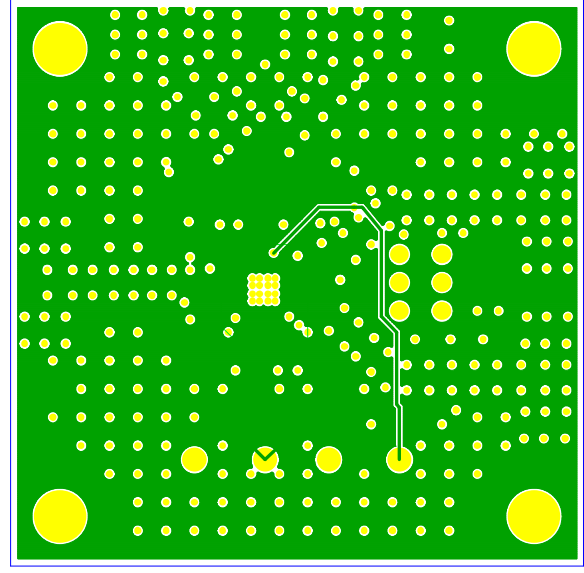


Figure 52. Evaluation Board Power Plane, Internal Layer 2

08083-056

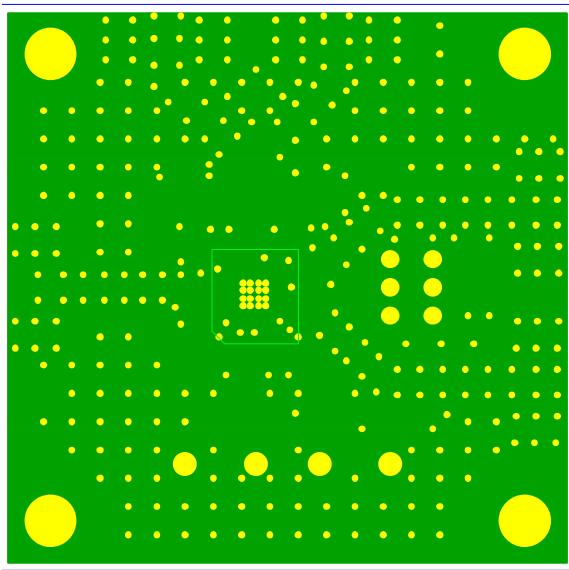


Figure 51. Evaluation Board Ground Plane, Internal Layer 1

08083-065

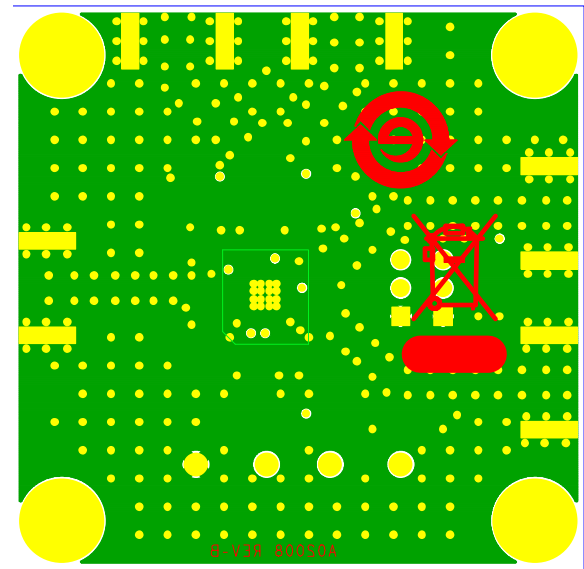
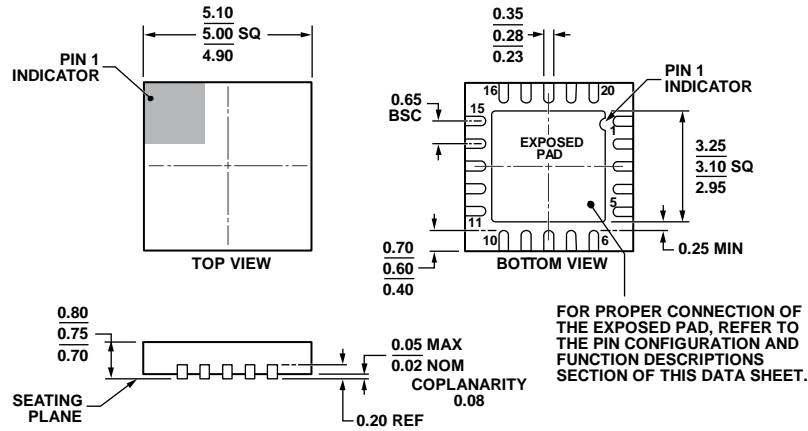


Figure 53. Evaluation Board Bottom Layer

08083-067

# OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARDS MO-220-WHHC.

Figure 54. 20-Lead Lead Frame Chip Scale Package [LFCSP\_WQ]  
 5 mm × 5 mm Body, Very Very Thin Quad  
 (CP-20-9)

Dimensions shown in millimeters

111808-A

## ORDERING GUIDE

Model <sup>1</sup>	Temperature Range	Package Description	Package Option	Ordering Quantity
ADL5367ACPZ-R7	-40°C to +85°C	20-Lead Lead Frame Chip Scale Package [LFCSP_WQ], 7" Tape and Reel	CP-20-9	1,500
ADL5367-EVALZ		Evaluation Board		1

<sup>1</sup> Z = RoHS Compliant Part.

**NOTES**



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[SX](#) [HMC129](#) [HMC143](#) [HMC400MS8ETR](#)