# 6.5 GHz, Ultrahigh Dynamic Range, Differential Amplifier 

## Data Sheet

## FEATURES

-3 dB bandwidth: 6.5 GHz typical
Preset $\mathbf{2 0 ~ d B ~ v o l t a g e ~ g a i n , ~ c a n ~ b e ~ r e d u c e d ~ b y ~ a d d i n g ~}$ external resistors
Differential or single-ended input to differential output Internally dc-coupled inputs and outputs Low noise input stage: $9.3 \mathbf{d B}$ noise figure at $2 \mathbf{~ G H z}$ Low distortion at 5 V supply and 2 V p-p output with $100 \Omega$ load 500 MHz : $\mathbf{7 8} \mathrm{dBc}$ (HD2), $\mathbf{- 7 1 \mathrm { dBc } ( H D 3 ) , - 8 0 \mathrm { dBc } \text { (IMD3) } ) ~}$
2 GHz: -64 dBc (HD2), -52 dBc (HD3), -65 dBc (IMD3)
Input voltage noise (NSD, RTI): $1.0 \mathrm{nV} / \sqrt{ } \mathrm{Hz}$ at 100 MHz
Single-supply operation: ac-coupled applications
Dual-supply operation: dc-coupled applications
Slew rate: $\mathbf{2 4 V / n s}$ at 2 V p-p output
DC power consumption: $\mathbf{8 6} \mathrm{mA}$ per amplifier at 5 V

## APPLICATIONS

Differential ADC drivers for GSPS ADCs
High speed data acquisition
Single-ended to differential conversion
DAC buffering
DC coupling and level shifting
RF/IF gain blocks
Balun alternative from dc to $\mathbf{4} \mathbf{~ G H z}$
SAW filter interfacing

## GENERAL DESCRIPTION

The ADL5569 is a high performance, dual, differential amplifier with 20 dB of voltage gain, optimized for applications spanning from dc to 6.5 GHz . The amplifier is available in a dual format, and it offers a low referred to input (RTI) noise spectral density (NSD) of $1.0 \mathrm{nV} / \sqrt{ } \mathrm{Hz}$ (at 100 MHz ) and excellent distortion performance over a wide frequency range, making it an ideal driver for high speed 12-bit to 16-bit analog-to-digital converters (ADCs). The ADL5569 is ideally suited for use in high performance zero intermediate frequency (IF) and complex IF receiver designs. In addition, this device has excellent low distortion for single-ended input driver applications.

Using two external series resistors for each amplifier expands the gain flexibility of the amplifier and allows any gain selection from 6 dB to 20 dB for a differential input. For a single-ended input, the gain can be adjusted from 6 dB to 17 dB with the addition of some external resistors. This device maintains low distortion through its output common-mode range of 2.0 V to

FUNCTIONAL BLOCK DIAGRAM


NOTES

1. $\mathrm{R}_{\mathrm{G}}$ IS THE SERIES RESISTANCE OF THE AMPLIFIER, AND $R_{F}$ IS THE FEEDBACK RESISTANCE OF THE AMPLIFIER.

Figure 1.
3.0 V, providing a flexible capability for driving ADCs with ac levels up to 2 V p-p.
Operating from a single 5 V supply, the quiescent current of the ADL5569 is typically 86 mA per amplifier. When disabled, the amplifiers consume only 8 mA per amplifier.

The device is optimized for wideband, low distortion, and low noise operation, giving it unprecedented second harmonic distortion (HD2) and third harmonic distortion (HD3) from dc to 4 GHz . These attributes, together with its adjustable gain capability, make this device the amplifier of choice for driving a wide variety of ADCs, mixers, pin diode attenuators, surface acoustic wave (SAW) filters, and a multitude of discrete radio frequency (RF) devices.

Fabricated on an Analog Devices, Inc., high speed silicon germanium ( SiGe ) process, the ADL5569 is supplied in a compact $2.5 \mathrm{~mm} \times 3 \mathrm{~mm}$, 16-lead LFCSP package and operates over the $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ temperature range.

Rev. C
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## 5/2018—Revision 0: Initial Version

ADL5569

## SPECIFICATIONS

Supply voltage $\left(\mathrm{V}_{s}\right)=5 \mathrm{~V}$, maximum gain, output common-mode voltage $\left(\mathrm{V}_{\text {сом }}\right)=\mathrm{V}_{s} / 2$, source impedance $\left(\mathrm{R}_{\mathrm{s}}\right)=100 \Omega$ differential, load impedance $\left(\mathrm{R}_{\mathrm{L}}\right)=100 \Omega$ differential, output voltage $\left(\mathrm{V}_{\text {out }}\right)=2 \mathrm{~V}$ p-p composite, frequency $=500 \mathrm{MHz}, \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, parameters specified for differential input and differential output, and signal spacing $=2 \mathrm{MHz}$ for two tone measurements, unless otherwise noted.

Table 1.

| Parameter | Test Conditions/Comments | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| DYNAMIC PERFORMANCE |  |  |  |  |  |
| -3 dB Bandwidth ${ }^{1}$ | $V_{\text {OUT }} \leq 0.5 \mathrm{Vp}-\mathrm{p}$ |  | 6.5 |  | GHz |
| Bandwidth, 1.0 dB Flatness | $V_{\text {OUT }} \leq 1.0 \mathrm{~V}$ p-p |  | 4.8 |  | GHz |
| Voltage Gain (Av) |  |  |  |  |  |
| Differential Input | $\mathrm{R}_{\mathrm{L}}=\mathrm{open}$ |  | 20 |  | dB |
|  | $\mathrm{R}_{\mathrm{L}}=100 \Omega$ differential | 6 | 19 |  | dB |
| Single-Ended Input | $\mathrm{RL}=100 \Omega$ differential | 6 | 17 |  | dB |
| Gain Accuracy |  |  | $\pm 0.15$ |  | dB |
| Gain Supply Sensitivity | $\mathrm{V}_{\mathrm{s}} \pm 5 \%$ |  | 8.6 |  | $\mathrm{mdB} / \mathrm{V}$ |
| Gain Temperature Sensitivity | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |  | 4 |  | $\mathrm{mdB} /{ }^{\circ} \mathrm{C}$ |
| Slew Rate | Rising, $\mathrm{V}_{\text {out }}=2 \mathrm{~V}$ p-p step |  | 24 |  | V/ns |
|  | Falling, Vout $=2 \mathrm{~V}$ p-p step |  | 24 |  | V/ns |
| Settling Time | 2 V step to 1\% |  | 500 |  | ps |
| Overdrive Recovery Time | Differential input voltage step from 2 V to 0 V for $\mathrm{V}_{\text {out }} \leq \pm 20 \mathrm{mV}$ |  | 6 |  | ns |
| Reverse Isolation (SDD12) | PDB and PDB2 are high |  | -34 |  | dB |
| When Amplifier Disabled | PDB and PDB2 are low |  | -17.5 |  | dB |
| INPUT AND OUTPUT CHARACTERISTICS |  | 13 |  | 35 | V |
| Input Resistance |  |  |  |  |  |
| Differential |  |  | 100 |  | $\Omega$ |
| Single-Ended |  |  | 91.7 |  | $\Omega$ |
| Common-Mode Rejection Ratio (CMRR) |  |  | 47 |  | dB |
| Output Common-Mode Range | VCOM and VCOM2 | 2.0 |  | 3.0 | V |
| VCOM and VCOM2 Input Impedance |  |  | 2.5 |  | $\mathrm{k} \Omega$ |
| Output, Common Mode | Referenced to $\mathrm{V}_{\text {com }}\left(\mathrm{V}_{s} / 2\right)$ |  |  |  |  |
| Offset |  | -30 | $\pm 10$ | +30 | mV |
| Drift | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |  | 0.15 |  | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |
| Output, Differential Offset |  |  |  |  |  |
| Voltage |  | -10 | $\pm 1.5$ | +10 | mV |
| Drift | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |  | $\pm 6$ |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Output Resistance (Differential) |  |  | 14.0 |  | $\Omega$ |
| Maximum Output Voltage Swing | 1 dB compression point |  | 6.5 |  | $\checkmark \mathrm{p}$-p |
| POWER INTERFACE |  |  |  |  |  |
| Supply Voltage |  | 4.75 | 5 | 5.25 | V |
| Digital Input Voltage | PDB, PDB2 |  |  |  |  |
| Logic High ( $\mathrm{V}_{\mathbf{H}}$ ) |  | 2.1 |  | 3.45 | V |
| Logic Low ( $\mathrm{V}_{\mathrm{IL}}$ ) |  | 0 |  | 1.0 | V |
| PDB Input Current | $\mathrm{PDB}=3 \mathrm{~V}$ |  | -7 |  | $\mu \mathrm{A}$ |
|  | $\mathrm{PDB}=0 \mathrm{~V}$ |  | -70 |  | $\mu \mathrm{A}$ |
| Supply Current (Isupply) | Each amplifier |  |  |  |  |
| Quiescent, Each Amplifier | PDB is high |  | 86 |  | mA |
| Disabled (Powered Down), Each Amplifier | PDB is low |  | 8 |  | mA |


| Parameter | Test Conditions/Comments | Min Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: |
| NOISE/HARMONIC PERFORMANCE |  |  |  |  |
|  |  |  |  |  |
| Second Harmonic Distortion (HD2) |  | -89 |  | dBc |
| Third Harmonic Distortion (HD3) |  | -83 |  | dBc |
| Output Third-Order Intercept (OIP3) |  | 42 |  | dBm |
| Third-Order Intermodulation Distortion (IMD3) |  | -82 |  | dBC |
| Output Second-Order Intercept (OIP2) |  | 74 |  | dBm |
| Second-Order Intermodulation Distortion (IMD2) |  | -73 |  | dBC |
| Output 1 dB Compression Point (OP1dB) |  | 17.4 |  | dBm |
| Noise Figure ${ }^{2}$ |  | 5.4 |  | dB |
| Noise Spectral Density (NSD), RTI ${ }^{2}$ |  | 1.0 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| 500 MHz |  |  |  |  |
| HD2 |  | -78 |  | dBC |
| HD3 |  | -71 |  | dBC |
| OIP3 |  | 41 |  | dBm |
| IMD3 |  | -80 |  | dBc |
| OIP2 |  | 74 |  | dBm |
| IMD2 |  | -73 |  | dBc |
| OP1dB |  | 17.2 |  | dBm |
| $N F^{2}$ |  | 6.3 |  | dB |
| NSD, RT/ ${ }^{2}$ |  | 1.2 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| 1000 MHz |  |  |  |  |
| HD2 |  | -65 |  | dBc |
| HD3 |  | -58 |  | dBc |
| OIP3 |  | 39 |  | dBm |
| IMD3 |  | -76 |  | dBC |
| OIP2 |  | 71 |  | dBm |
| IMD2 |  | -70 |  | dBc |
| OP1dB |  | 17.7 |  | dBm |
| $\mathrm{NF}^{2}$ |  | 7.0 |  | dB |
| NSD, RTI ${ }^{2}$ |  | 1.3 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| 2000 MHz |  |  |  |  |
| HD2 |  | -64 |  | dBc |
| HD3 |  | -52 |  | dBc |
| OIP3 |  | 34 |  | dBm |
| IMD3 |  | -65 |  | dBc |
| OIP2 |  | 63 |  | dBm |
| IMD2 |  | -62 |  | dBc |
| OP1dB |  | 17.4 |  | dBm |
| $N{ }^{2}$ |  | 9.3 |  | dB |
| NSD, RT ${ }^{2}$ |  | 1.8 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| 3000 MHz |  |  |  |  |
| HD2 |  | -62 |  | dBc |
| HD3 |  | -46 |  | dBc |
| OIP3 |  | 30 |  | dBm |
| IMD3 |  | -58 |  | dBc |
| OIP2 |  | 57 |  | dBm |
| IMD2 |  | -56 |  | dBc |
| OP1dB |  | 16.2 |  | dBm |
| $\mathrm{NF}^{2}$ |  | 11.1 |  |  |
| NSD, RT ${ }^{2}$ |  | 2.2 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |

## ADL5569

| Parameter | Test Conditions/Comments | Min | Typ | Max |
| :--- | :--- | :--- | :--- | :--- |
| Unit |  |  |  |  |
| 4000 MHz |  |  |  |  |
| HD2 |  | -58 |  |  |
| HD3 |  | -48 |  |  |
| OIP3 |  | 25 | dBc |  |
| IMD3 |  | -48 | dBm |  |
| OIP2 |  | 59 | dBc |  |
| IMD2 |  | -58 | dBm |  |
| OP1dB |  | 14.3 | dBc |  |
| NF $^{2}$ |  | 12.1 | dBm |  |
| NSD, RTI |  | dB |  |  |

${ }^{1} S$ parameters are taken with the device under test (DUT) itself. The printed circuit board (PCB) is not used in the measurement.
${ }^{2}$ NSD RTI is calculated from the noise figure, as follows:
$N S D(R T I)=1 / 2 \times \sqrt{4 k T \times\left(10^{N F / 10}-1\right) \times R_{I N}}$
where:
$k$ is Boltzmann's constant, which equals $1.381 \times 10^{-23} \mathrm{~J} / \mathrm{K}$.
$T$ is the standard absolute temperature for evaluating noise figure, which equals 290 K .
$R_{I N}$ is the differential input impedance of each amplifier, which equals $100 \Omega$.

## ABSOLUTE MAXIMUM RATINGS

Table 2.

| Parameter | Rating |
| :--- | :--- |
| Output Voltage Swing $\times$ Bandwidth Product | $5 \mathrm{~V}-\mathrm{GHz}$ |
| Supply Voltage $\left(\mathrm{V}_{\mathrm{s}}\right)$ at VCC and VCC2 | 5.25 V |
| VIP, VIP2, VIN, and VIN2 | $\mathrm{V}_{\mathrm{s}}+0.5 \mathrm{~V}$ |
| PDB, PDB2 | 3.6 V |
| Maximum Output Current, lout (VIP, VIP2, | $\pm 30 \mathrm{~mA}$ |
| VIN, and VIN2 Pins) |  |
| Internal Power Dissipation | 1 W |
| Maximum Junction Temperature | $125^{\circ} \mathrm{C}$ |
| Operating Temperature Range | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

## THERMAL RESISTANCE

Thermal performance is directly linked to PCB design and operating environment. Careful attention to PCB thermal design is required.
$\theta_{\mathrm{JA}}$ is the natural convection junction to ambient thermal resistance measured in a one cubic foot sealed enclosure. $\theta_{\mathrm{JC}}$ is the junction to case thermal resistance.

Table 3. Thermal Resistance

| Package Type | $\boldsymbol{\theta}_{\mathrm{JA}}{ }^{\mathbf{1}}$ | $\boldsymbol{\theta}_{\mathbf{J c}}{ }^{\mathbf{2}}$ | Unit |
| :--- | :--- | :--- | :--- |
| $\mathrm{CP}-16-44$ | 90.5 | 20.9 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

${ }^{1}$ Measured on an Analog Devices evaluation board.
${ }^{2}$ Based on simulation with JEDEC standard JESD51.

## ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



Figure 2. Pin Configuration

Table 4. Pin Function Descriptions

| Pin No. | Mnemonic | Description |
| :---: | :---: | :---: |
| 1 | VIN | Negative Side of Balanced Differential Inputs for Amplifier 1. This pin is biased to the VCC voltage ( $\mathrm{V}_{\text {vcc }} / 2$, and is typically ac-coupled. |
| 2 | VIP | Positive Side of Balanced Differential Inputs for Amplifier 1. This pin is biased to Vvcc/2, and is typically ac-coupled. |
| 3,11 | GND | Ground. Ground reference for the entire chip. These pins must be soldered to a low impedance ground plane. |
| 4 | VIP2 | Positive Side of Balanced Differential Inputs for Amplifier 2. This pin is biased to the VCC2 voltage (Vvccz $) / 2$ and is typically ac-coupled. |
| 5 | VIN2 | Negative Side of Balanced Differential Inputs for Amplifier 2. This pin is biased to $\mathrm{V}_{\text {vcca }} / 2$ and is typically ac-coupled. |
| 6 | PDB2 | Power-Down Control (Active Low) for Amplifier 2. This pin is internally pulled up to approximately 2.8 V . A logic high on this pin ( 2.1 V < PDB2 voltage $\left(\mathrm{V}_{\mathrm{PDB} 2}\right)<3.3 \mathrm{~V}$ ) enables the device. |
| 7 | VCOM2 | Common-Mode Voltage Input for Amplifier 2. A voltage applied to this pin sets the common-mode voltage of the inputs and outputs of the amplifier. If left open, the VCOM 2 voltage $\left(\mathrm{V}_{\mathrm{Vcom} 2}\right)=\mathrm{V}_{\mathrm{CC2}} / 2$. Decouple this pin to ground with a $0.1 \mu \mathrm{~F}$ capacitor. |
| 8 | VCC2 | Positive Supply for Amplifier 2. |
| 9 | VON2 | Negative Side of Balanced Differential Outputs for Amplifier 2. This pin is biased to Vvcom2 and is typically ac-coupled. |
| 10 | VOP2 | Positive Side of Balanced Differential Outputs for Amplifier 2. This pin is biased to $\mathrm{V}_{\mathrm{vcom} 2}$ and is typically ac-coupled. |
| 12 | VOP | Positive Side of Balanced Differential Outputs for Amplifier 1. This pin is biased to Vvcom and is typically ac-coupled. |
| 13 | VON | Negative Side of Balanced Differential Outputs for Amplifier 1. This pin is biased to Vvcom and is typically ac-coupled. |
| 14 | VCC | Positive Supply for the Amplifier 1. |
| 15 | VCOM | Common-Mode Voltage Input for Amplifier 1. A voltage applied to this pin sets the common-mode voltage of the inputs and outputs of the amplifier. If left open, $\mathrm{V}_{\mathrm{vcom}}=\mathrm{V} v c c / 2$. Decouple this pin to ground with a $0.1 \mu \mathrm{~F}$ capacitor. |
| 16 | PDB | Power-Down Control (Active Low) for Amplifier 1. This pin is internally pulled up to approximately 2.8 V . A logic high on this pin ( 2.1 V < PDB voltage $\left(\mathrm{V}_{\mathrm{PDB}}\right)<3.3 \mathrm{~V}$ ) enables the device. |
|  | EPAD | Exposed Pad. The exposed pad is internally connected to GND and must be soldered to a low impedance ground plane. |

## TYPICAL PERFORMANCE CHARACTERISTICS

$\mathrm{V}_{\mathrm{S}}=5 \mathrm{~V}$, maximum gain, $\mathrm{V}_{\mathrm{CoM}}=\mathrm{V}_{\mathrm{s}} / 2, \mathrm{R}_{\mathrm{s}}=100 \Omega$ differential, $\mathrm{R}_{\mathrm{L}}=100 \Omega$ differential, $\mathrm{V}_{\text {out }}=2 \mathrm{~V}$ p-p, frequency $=500 \mathrm{MHz}, \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, parameters specified for differential input and differential output, and signal spacing $=2 \mathrm{MHz}$ for two-tone measurements, unless otherwise noted.


Figure 3. Gain vs. Frequency (S Parameters Taken with DUT, PCB Not Used in Measurement)


Figure 4. Gain vs. Frequency over Temperature


Figure 5. Gain Mismatch (Channel A to Channel B) vs. Frequency


Figure 6. Phase Mismatch (Channel A to Channel B) vs. Frequency


Figure 7. Output P1dB vs. Frequency over Temperature


Figure 8. Noise Figure vs. Frequency


Figure 9. Noise Spectral Density, Referred to Input vs. Frequency


Figure 10. Third-Order Intermodulation Distortion (IMD3) and Output Third-Order Intercept (OIP3) vs. Frequency


Figure 11. OIP3 vs. Frequency over Temperature


Figure 12. IMD3 vs. Frequency over Temperature


Figure 13. IMD3 vs. Frequency over RLOAD for Pout per Tone


Figure 14. Second-Order Intermodulation Distortion (IMD2) and Output Second-Order Intercept (OIP2) vs. Frequency


Figure 15. Second Harmonic Distortion (HD2) vs. Frequency


Figure 16. Third Harmonic Distortion (HD3) vs. Frequency


Figure 17. HD2 vs. Frequency over Temperature


Figure 18. HD3 vs. Frequency over Temperature


Figure 19. HD2 vs. Frequency for Various Output Voltages Swings


Figure 20. HD3 vs. Frequency for Various Voltages Swings


Figure 21. HD2 and HD3 vs. Output Common-Mode Voltage (Vсом)


Figure 22. IMD3 vs. Vсом


Figure 23. IMD3 vs. Frequency at Various Pout per Tones


Figure 24. HD2 and HD3 vs. Frequency for Various Supplies


Figure 25. Disable Time Response


Figure 26. HD2 vs. Frequency for a Single-Ended Input Circuit


Figure 27. HD3 vs. Frequency for a Single-Ended Input Circuit


Figure 28. IMD3 and OIP3 vs. Frequency for a Single-Ended Input Circuit


Figure 29. Enable Time Response


Figure 30. Large Signal Pulse Response, Output Voltage $\left(V_{\text {out }}\right)=4 \mathrm{Vp} p \mathrm{p}$


Figure 31. Common-Mode Rejection Ratio (CMRR) vs. Frequency


Figure 32. Group Delay vs. Frequency


Figure 33. Reverse Isolation (SDD12) vs. Frequency


Figure 34. Differential Input Reflection Coefficient (SDD11)


Figure 35. Supply Current vs. Temperature


Figure 36. Channel to Channel Isolation vs. Frequency


Figure 37. Differential Output Reflection Coefficient (SDD22)

## THEORY OF OPERATION

The ADL5569 is a high gain, fully differential, dual amplifier and ADC driver that operates on a single power supply voltage $\left(\mathrm{V}_{\mathrm{s}}\right)$ of 5 V . Internal resistors preset the gain to 20 dB , and external resistors can be added to reduce this gain. The -3 dB bandwidth is 6.5 GHz , and the device has a differential input impedance of $100 \Omega$. The ADL5569 has a differential output impedance of $14 \Omega$ and an operating output commonmode voltage range of 2.0 V to 3.0 V with a 5 V supply.
The ADL5569 is composed of a pair of fully differential amplifiers with on-chip feedback and feedforward resistors. The gain is fixed at 20 dB but can be reduced by adding two resistors in series with the two inputs. The amplifier provides a high differential, open-loop gain and has an output common-mode circuit that enables the user to change the output common-mode voltage by applying a voltage to the VCOM or VCOM2 pin.
Each amplifier provides superior low distortion for frequencies near dc to beyond 2000 MHz , with low noise and low power consumption. This amplifier achieves an IMD3 of -82 dBc at 100 MHz , and -80 dBc IMD3 at 500 MHz for 2 V p-p operation. In addition, the ADL5569 can deliver 5 V p-p operation under heavy loads. The internal gain is set at 20 dB , and the device has a noise figure of 9.3 dB at 2 GHz . When comparing noise figure and distortion performance, this amplifier delivers the best in category spurious-free dynamic range (SFDR).

The ADL5569 features flexible input and output coupling. The device can be ac-coupled or dc-coupled. For dc coupling, the output common-mode voltage can be adjusted (using the VCOM and VCOM2 pins) from 2.5 V to 0.5 V for $\mathrm{V}_{\mathrm{s}}$ at 3.3 V and ground at -2.0 V .
The distortion performance as a function of output commonmode voltage is shown in Figure 21. Note that the VCOM and VCOM2 pins set the common-mode voltage at the outputs of the amplifier, the VOP, VOP2, VON, and VON2 pins, when configured for ac-coupled applications.

For ac-coupled applications with series capacitors at the inputs, as shown in Figure 38, the input common-mode level is set to the same as the voltage at VCOM or VCOM2.
Due to the wide input common-mode voltage range, this device can easily be dc-coupled to many types of mixers, demodulators, and amplifiers. If the outputs are ac-coupled, no external VCOM or VCOM2 voltage adjustment is required because the amplifier output common-mode level is set to $\mathrm{V}_{\mathrm{s}} / 2$.


Figure 38. Basic Structure

## APPLICATIONS INFORMATION BASIC CONNECTIONS

Figure 39 shows the basic connections for operating the ADL5569. Apply 5 V to the VCC and VCC2 pins and decouple with $0.1 \mu \mathrm{~F}$ and $10 \mu \mathrm{~F}$ surface-mount ceramic capacitors in parallel to ground.
Decouple the VCOM and VCOM2 pins (Pin 7 and Pin 15) using a $0.1 \mu \mathrm{~F}$ capacitor. The PDB and PDB2 pins (Pin 6 and Pin 16) are tied to logic high, respectively, to enable each amplifier. A differential signal is applied to Amplifier 1 through Pin 1 (VIN) and Pin 2 (VIP) and to Amplifier 2 through Pin 4 (VIP2) and Pin 5 (VIN2). Each amplifier has a gain of 20 dB .

The Amplifier 1 input pins, Pin 1 (VIN) and Pin 2 (VIP), and the output pins, Pin 13 (VON) and Pin 12 (VOP), are biased by applying a voltage to Pin 15 (VCOM). If VCOM is left open, VCOM equals $1 ⁄ 2$ of $\mathrm{V}_{\mathrm{s}}$. The Amplifier 2 input pins, Pin 4 (VIP2) and Pin 5 (VIN2), and the output pins, Pin 9 (VON2) and Pin 10 (VOP2), are biased by applying a voltage to Pin 7 (VCOM2). If VCOM2 is left open, VCOM2 equals $1 / 2$ of V .
The ADL5569 can be ac-coupled, as shown in Figure 39, or it can be dc-coupled if within the specified input and output common-mode voltage ranges. Pulling the PDB and PDB2 pins low puts the ADL5569 in sleep mode, reducing the current consumption to 16 mA at ambient temperature.


Figure 39. Basic Connections

## INPUT AND OUTPUT INTERFACING

The ADL5569 can be configured as a differential input to differential output driver, as shown in Figure 40 . The $50 \Omega$ resistors, R1 and R2, combined with the input balun, provide a $50 \Omega$ input match for the $100 \Omega$ input impedance. The input and output $0.1 \mu \mathrm{~F}$ capacitors isolate the $\mathrm{V}_{\mathrm{Vcc}} / \mathrm{V}_{\mathrm{VCC} 2}$ bias from the source and balanced load. The load is $100 \Omega$ to provide the expected ac performance (see the Specifications section).


Figure 40. Differential Input to Differential Output Configuration
The differential gain of the ADL5569 is dependent on the source impedance and load, as shown in Figure 41. Determine the differential gain $\left(\mathrm{A}_{\mathrm{v}}\right)$ by

$$
\begin{equation*}
A_{V}=500 / 50 \tag{1}
\end{equation*}
$$



Figure 41. Differential Input Loading Circuit

## Single-Ended Input to Differential Output

The ADL5569 can also be configured in a single-ended input to differential output configuration, as shown in Figure 42. In this configuration, the gain of the device is reduced due to the application of the signal to only one side of the amplifier. The input and output $0.1 \mu \mathrm{~F}$ capacitors isolate the $\mathrm{V}_{\mathrm{VCC}} / \mathrm{V}_{\mathrm{VCC} 2}$ bias from the source and the balanced load.
The single-ended circuit configuration can be accomplished in three steps (see Figure 42), assuming a $50 \Omega$ Rs source. First, calculate the input resistance ( $\mathrm{R}_{\mathrm{IN}}$ ) of the amplifier using the following formula:

$$
\begin{equation*}
R_{I N}=\frac{R_{G}}{1-\left(\frac{R_{F}}{2 \times\left(R_{G}+R_{F}\right)}\right)} \tag{2}
\end{equation*}
$$

where:
$R_{G}$ is the series resistance internal to the amplifier.
$R_{F}$ is feedback resistance internal to the amplifier.
Thus, $\mathrm{R}_{\mathrm{IN}}=91.7 \Omega$.
The next step is to calculate the termination of Resistor R2 (see Figure 42). Because source impedance ( $\mathrm{R}_{\mathrm{s}}$ ) must be equal to the parallel equivalent resistance of R 2 and $\mathrm{R}_{\mathrm{IN}}$,

$$
R_{S}=\frac{R 2 \times R_{I N}}{R 2+R_{I N}}
$$

Thus,

$$
\begin{equation*}
R 2=R_{I N} \times R_{S} /\left(R_{I N}-R_{S}\right) \tag{3}
\end{equation*}
$$

When $\mathrm{R}_{\mathrm{S}}=50 \Omega$ and $\mathrm{R}_{\text {IN }}=91.7 \Omega, \mathrm{R} 2=109 \Omega$.
The last step is to calculate the gain path rebalancing resistor, R1 (see Figure 42), by using the following formula:

$$
\begin{equation*}
R 1=\frac{R_{S} \times R 2}{R_{S}+R 2} \tag{4}
\end{equation*}
$$

Thus, R1 $=34.0 \Omega$.


Figure 42. Single-Ended Input to Differential Output Configuration
See the AN-0990 Application Note, Terminating a Differential Amplifier in Single-Ended Input Applications, for more information on terminating single-ended inputs. The single-ended gain configuration of the ADL5569 is dependent on the source impedance and load, as shown in Figure 43.


Figure 43. Single-Ended Input Loading Circuit

Determine the single-ended gain ( $\mathrm{A}_{\mathrm{v}_{1}}$ ) using the following two equations:

$$
\begin{equation*}
R_{M A T C H}=\frac{R 2 \times R_{I N}}{R 2+R_{I N}} \tag{5}
\end{equation*}
$$

where $R_{\text {MATCH }}$ is the input resistance value that matches $\mathrm{R}_{\mathrm{s}}$, which is calculated as follows:

$$
\begin{align*}
& A_{V 1}= \\
& \frac{500}{50+\left(\frac{R_{S} \times R 2}{R_{S}+R 2}\right)} \times \frac{R 2}{R_{S}+R 2} \times \frac{R_{M A T C H}+R_{S}}{R_{M A T C H}} \times \frac{R_{L}}{10+R_{L}} \tag{6}
\end{align*}
$$

Figure 44. HD2 for Single-Ended and Differential Configurations vs. Frequency, Vout $=2$ V p-p

## GAIN ADJUSTMENT AND INTERFACING

The effective gain of the ADL5569 can be reduced by adding two resistors in series with the inputs to reduce the gain.


Figure 45. Gain Adjustment Using a Series Resistor
To find series resistor ( $\mathrm{R}_{\text {SERIIES }}$ ) for a given $\mathrm{A}_{\mathrm{V}}$ gain and $\mathrm{R}_{\mathrm{L}}$, use the following equation:

$$
\begin{equation*}
R_{\text {SERIES }}=\left(500 / A_{V}\right)-50 \tag{7}
\end{equation*}
$$

The necessary shunt component ( $\mathrm{R}_{\text {Shunt }}$ ) to match the source impedance, $\mathrm{R}_{\mathrm{s}}$, is expressed as

$$
\begin{equation*}
R_{\text {SHUNT }}=\frac{1}{\frac{1}{R_{S}}-\frac{1}{2 \times R_{\text {SERIES }}+100}} \tag{8}
\end{equation*}
$$

The shunt resistor values for multiple target voltage gains are listed in Table 5. The source resistance and input impedance need careful attention when using Equation 6. Consider the input impedance of the ADL5569 and the reactance of the ac coupling capacitors before assuming that the impedance and reactance of the capacitors make a negligible contribution.

To calculate the $\mathrm{A}_{\mathrm{v}}$ for a given Rseries, use the following equation:

$$
\begin{equation*}
A_{V}=\left(\frac{500}{R_{\text {SERIES }}+50}\right) \tag{9}
\end{equation*}
$$

Note that Equation 9 only gives the absolute gain and does not take into account that the circuit introduces a $180^{\circ}$ phase shift. To account for this phase shift, multiply the product of Equation 9 by -1 .

Table 5. Differential Gain Adjustment Using Series Resistor

| Rs $\mathbf{( \Omega )}$ | Target Voltage Gain (dB) | RsERIEs ( $\mathbf{\Omega}$ ) | Rshunt $\mathbf{( \Omega )}$ |
| :--- | :--- | :--- | :--- |
| 50 | 6 | 169 | 56.2 |
| 50 | 7 | 147 | 57.6 |
| 50 | 8 | 124 | 59 |
| 50 | 9 | 105 | 59 |
| 50 | 10 | 88.7 | 60.4 |
| 50 | 11 | 73.2 | 63.4 |
| 50 | 12 | 60.4 | 64.9 |
| 50 | 13 | 48.7 | 66.5 |
| 50 | 14 | 37.4 | 69.8 |
| 50 | 15 | 28 | 73.2 |
| 50 | 16 | 19.6 | 78.7 |
| 50 | 17 | 12.1 | 84.5 |
| 50 | 18 | 5.23 | 90.9 |
| 100 | 6 | 169 | 130 |
| 100 | 7 | 147 | 133 |
| 100 | 8 | 124 | 140 |
| 100 | 9 | 105 | 147 |
| 100 | 10 | 88.7 | 158 |
| 100 | 11 | 73.2 | 169 |
| 100 | 12 | 60.4 | 182 |
| 100 | 13 | 48.7 | 205 |
| 100 | 14 | 37.4 | 232 |
| 100 | 15 | 28 | 280 |
| 100 | 16 | 19.6 | 357 |
| 100 | 17 | 12.1 | 511 |
| 100 | 18 | 5.23 | 1050 |
|  |  |  |  |

## EFFECT OF LOAD CAPACITANCE

Load capacitance, including stray capacitance from PCB traces, affects the bandwidth and flatness of the ADL5569 frequency response, resulting in excessive peaking. It is recommended to add $5 \Omega$ external series resistors to each output to isolate the load capacitance from the outputs and to effectively reduce peaking. Respective frequency responses resulting from the addition of a 0.5 pF to a 2.0 pF differential load capacitance are shown in Figure 46.


Figure 46. Frequency Response for Various Load Capacitances, $R_{L}=100 \Omega$

## GSPS ADC INTERFACING

A wideband data acquisition system using the ADL5569 together with the AD9689, a dual 14-bit ADC, was developed and tested as shown in Figure 49 for ac-coupled applications. The amplifier output common-mode voltage is set to AVDD/2 with the voltage divider formed by the two $10 \mathrm{k} \Omega$ resistors on the VCOM pin. However, the VCOM pin can be left open (with a decoupling capacitor as described in Table 4), because there is an internal divider to pull the node to VCC/2 in such cases. The resistor capacitor (RC) filter after the amplifier works with the pole formed by the ADC input capacitance to attenuate the broadband noise and out of band harmonics generated by the amplifier. The RC filter also blocks sharp switching pulses, that is, charge injection from the ADC internal sampling circuitry, from reaching the amplifier outputs and creating nonlinear effects. An additional band-pass filter, specific to the system rejection requirements, is also needed in front of the ADL5569 amplifier to prevent
unwanted signals from compressing the amplifier as well as from reaching the ADC. This filter is usually added during bench testing.
See the AN-835 Application Note, Understanding High Speed ADC Testing and Evaluation, for additional testing information and setups.

The signal-to-noise ratio (SNR) and SFDR with respect to full scale (FS) of the ADC system, is shown in Figure 47 and Figure 48.


Figure 47. ADC System SNR Referred to Full Scale (SNRFS) vs. Frequency


Figure 48. ADC System SFDR vs. Frequency


Figure 49. Wideband 3.2 GHz Bandwidth AC-Coupled ADC Interfacing Example: ADL5569 Driving the AD9689

Two tone intermodulation distortion performance (IMD2 and IMD3) is shown in Figure 50. The relative pass-band frequency response for this signal chain with a wideband antialiasing filter is shown in Figure 51.


Figure 50. Measured Two Tone IMD2/IMD3 Performance


Figure 51. Measured Relative Frequency Response

For dc applications, special requirements must be completed for the ADL5569 to accommodate a dc signal and level shift the amplifier to meet the common-mode voltage requirements of the companion converter. Figure 52 shows a 1.5 GHz design example of the ADL5569 using dual supplies of +3.3 V for the VCC and VCC2 pins and -2.0 V for the ground and exposed pad (EP) pins. By using these dual supplies, the internal logic of the power-down pins of the device (PDB and PDB2) is also level shifted to 1.0 V to enable the device.

The example shown in Figure 52 provides a single-ended input design, with an input common-mode voltage of 0.0 V . The output common-mode voltage is designed to accommodate 1.4 V to interface with the AD9689 analog inputs. The VCOM pin cannot be regarded as high-Z for the purposes of a voltage divider calculation for the $2 \mathrm{k} \Omega$ and $15.4 \mathrm{k} \Omega$ resistors. The 1.5 GHz bandwidth limitation of this design is not due to any of the passive components, but it is an inherent practical limitation of the ADL5569 and AD9689/AD9208 combination.

## ADL5569



Figure 52. 1.5 GHz Bandwidth, DC-Coupled ADC Interfacing Example: ADL5569 Driving the AD9689 and AD9208

## SOLDERING INFORMATION AND RECOMMENDED LAND PATTERN

Figure 53 shows the recommended land pattern for the ADL5569. The ADL5569 is contained in a $2.5 \mathrm{~mm} \times 3 \mathrm{~mm}$ LFCSP, which has an exposed ground pad (EPAD). This pad is internally connected to the ground of the chip. To minimize thermal impedance and ensure electrical performance, solder the pad to the low impedance ground plane on the PCB. To further reduce thermal impedance, it is recommended that the ground planes on all layers under the pad be stitched together with vias.
For more information on land pattern design and layout, refer to the AN-772 Application Note, A Design and Manufacturing Guide for the Lead Frame Chip Scale Package (LFCSP).
The land pattern on the ADL5569-EVALZ provides a simulated thermal resistance $\left(\theta_{J \mathrm{~A}}\right)$ of $90.5^{\circ} \mathrm{C} / \mathrm{W}$.


Figure 53. Recommended Land Pattern

## EVALUATION BOARD

Figure 54 shows the general block diagram of the ADL5569EVALZ evaluation board. The schematic of the ADL5569EVALZ is shown in Figure 55 and has several options. The ADL5569-EVALZ is powered by a single 5 V supply. The power supply is decoupled by $10 \mu \mathrm{~F}$ and $0.1 \mu \mathrm{~F}$ capacitors. On-board regulators provide a 2.5 V common-mode voltage and 3 V logic supply voltage to enable and disable the power-down feature.

Several termination options are also provided to allow the user to terminate unused inputs and outputs of the amplifier for single-ended applications.
For more evaluation board options on the ADL5569, contact the Analog Devices sales.


Figure 54. General Block Diagram of the ADL5569-EVALZ Evaluation Board


Figure 55. ADL5569-EVALZ Evaluation Board Schematic

Table 6. Bill of Materials

| Qty. | Reference Designator | Description | Manufacturer | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| 1 | A1 | IC, dual-channel amplifier | Analog Devices | ADL5569 |
| 10 | C1 to C6, C8 to C11 | $0.01 \mu \mathrm{~F}$ capacitors, ceramic, X7R | Murata | GRM033R71A103KA01D |
| 6 | $\begin{aligned} & \mathrm{C} 12, \mathrm{C} 13, \mathrm{C} 16, \mathrm{C} 17, \mathrm{C} 20, \\ & \mathrm{C} 21 \end{aligned}$ | $4.7 \mu \mathrm{~F}$ capacitors, ceramic, X 5 R | Murata | GRM155R60J475ME87D |
| 2 | C14, C15 | $0.001 \mu \mathrm{~F}$ capacitors, ceramic, X7R | Murata | GRM033R71E102KA01D |
| 2 | C18, C19 | $1 \mu \mathrm{~F}$ capacitors, ceramic, X5R | Taiyo Yuden | AMK063ABJ105MP-F |
| 6 | C22, C23, C26 to C29 | $0.1 \mu \mathrm{~F}$ capacitors, ceramic, X5R | Murata | GRM033R60J104KE19D |
| 2 | C24, C25 | $10 \mu \mathrm{~F}$ capacitors, ceramic X5R | Taiyo Yuden | AMK105CBJ106MV-F |
| 1 | C7 | $10 \mu \mathrm{~F}$ capacitor ceramic, X5R | Murata | GRM21BR61C106KE15L |
| 1 | E1 | $120 \Omega$ at 100 MHz , ferrite bead, $0.07 \Omega, 1.5 \mathrm{~A}$ | Murata | BLM18SG121TN1D |
| 2 | E2, E3 | 33 nH , chip inductors, $0.06 \Omega, 1.3 \mathrm{~A}$ | Coilcraft, Inc. | 0402AF-330XJL |
| 8 | J1 to J8 | PCB SMA connectors, $50 \Omega$, end launch jack | Cinch Connectivity Solutions | 142-0701-851 |
| 2 | P1, P2 | Connector headers, straight, three position | Samtec | TSW-103-08-G-S |
| 1 | P3 | Connector PCB header, two position | Samtec | TSW-102-08-G-S |
| 8 | R1 to R4, R23 to R26 | $35.7 \mathrm{k} \Omega$ resistors, precision thick film chip | Panasonic | ERJ-1GEF3572C |
| 4 | R13, R14, R29, R30 | $0 \Omega$ resistors, 0201 | Panasonic | ERJ-1GEOROOC |
| 1 | R17 | $16.9 \mathrm{k} \Omega$ resistor, 0201 | Panasonic | ERJ-1GEF1692C |
| 1 | R19 | $10.7 \mathrm{k} \Omega$ resistor, 0402 | Vishay Precision Group | CRCW040210K7FKED |
| 2 | R21, R22 | $4.99 \mathrm{k} \Omega$ resistors, 0201 | Samsung | RC0603F4991CS |
| 4 | R5, R8, R18, R20 | $10 \mathrm{k} \Omega$ resistors, 0201 | Panasonic | ERJ-1GNF1002C |
| 4 | R6, R7, R9, R10 | $5.1 \Omega$ resistors, 0201 | Yageo | RC0201JR-075R1L |
| 3 | TP1, TP2, TP3 | Connector PCB pin test points | Mill-Max | 3137-1-00-15-00-00-08-0 |
| 2 | U1, U2 | IC ultralow noise, high PSRR, low dropout (LDO) regulators | Analog Devices | ADM7170ACPZ-5.0 |



Figure 56. Layout of the ADL5569-EVALZ Evaluation Board, Top Layer


Figure 57. Layout of the ADL5569-EVALZ Evaluation Board, Bottom Layer

## OUTLINE DIMENSIONS



Figure 58. 16-Lead Lead Frame Chip Scale Package [LFCSP]
$2.5 \mathrm{~mm} \times 3 \mathrm{~mm}$ Body and 0.55 mm Package Height (CP-16-44)
Dimensions shown in millimeters

ORDERING GUIDE

| Model $^{1}$ | Temperature Range | Package Description | Package Option | Marking Code |
| :--- | :--- | :--- | :--- | :--- |
| ADL5569BCPZ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 16-Lead Lead Frame Chip Scale Package [LFCSP] | CP-16-44 | ET |
| ADL5569BCPZ-R7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 16-Lead Lead Frame Chip Scale Package [LFCSP] | CP-16-44 | ET |
| ADL5569-EVALZ |  | Evaluation Board |  |  |

${ }^{1} Z=$ RoHS Compliant Part.

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