## Data Sheet

## FEATURES

Wideband RF input frequency range: $\mathbf{2 4 ~ G H z}$ to $\mathbf{4 4} \mathbf{~ G H z}$
2 upconversion modes
Direct conversion from baseband I/Q to RF
Single-sideband upconversion from real IF
LO input frequency range: 5.4 GHz to 10.25 GHz
LO quadrupler for up to 41 GHz
Matched $50 \Omega$ single-ended RF output and IF inputs
Option between matched $100 \Omega$ balanced or $50 \Omega$ singleended LO inputs
$100 \Omega$ balanced baseband inputs
Sideband suppression and carrier feedthrough optimization
Variable attenuator for transceiver power control
Programmable via 4-wire SPI interface
40-terminal land grid array package (LGA)

## APPLICATIONS

## Point to point microwave radios

Radar, electronic warfare systems
Instrumentation, automatic test equipment (ATE)

## GENERAL DESCRIPTION

The ADMV1013 is a wideband, microwave upconverter optimized for point to point microwave radio designs operating in the 24 GHz to 44 GHz radio frequency (RF) range.

The upconverter offers two modes of frequency translation. The device is capable of direct conversion to RF from baseband in-phase quadrature (I/Q) input signals, as well as single-sideband (SSB) upconversion from complex intermediate frequency (IF) inputs. The baseband I/Q input path can be disabled and modulated complex IF signals, anywhere from 0.8 GHz to 6.0 GHz , can be inserted in the IF path and upconverted to 24 GHz to 44 GHz

while suppressing the unwanted sideband by typically better than 26 dBc . The serial port interface (SPI) allows adjustment of the quadrature phase and mixer gate voltage to allow optimum sideband suppression and local oscillator (LO) nulling. In addition, the SPI interface allows powering down the output envelope detector to reduce power consumption.

The ADMV 1013 upconverter comes in a 40-terminal land grid array package (LGA) package. The ADMV1013 operates over the $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ case temperature range.

Rev. B
Document Feedback

## ADMV1013

## TABLE OF CONTENTS

Features ..... 1
Applications. ..... 1
Functional Block Diagram .....  1
General Description .....  1
Revision History ..... 2
Specifications ..... 3
Serial Port Register Timing ..... 5
Absolute Maximum Ratings ..... 6
Thermal Resistance .....  .6
ESD Caution .....  6
Pin Configuration and Function Descriptions ..... 7
Typical Performance Characteristics ..... 9
I/Q Mode ..... 9
IF Mode. ..... 14
Envelope Detector Performance. ..... 19
Return Loss and Isolation ..... 21
$\mathrm{M} \times \mathrm{N}$ Spurious Performance ..... 24
Theory of Operation ..... 25
Start-Up Sequence ..... 25
Baseband Quadrature Modulation (I/Q Mode) ..... 25
Single-Sideband Upconversion (IF Mode) ..... 25
LO Input Path ..... 25
REVISION HISTORY
9/2019—Rev. A to Rev. B
Changes to Figure 1 ..... 1
Changes to Figure 3 and Table 5 ..... 7
4/2019—Rev. 0 to Rev. A
Changes to Figure 1 ..... 1
Changes to Frequency Ranges Parameter, Table 1 ..... 3
Changes to Thermal Resistance Section ..... 6
Changes to Figure 3 ..... 7
Changes to Table 5 ..... 8
Changes to Figure 50 Caption ..... 16
Sideband Suppression Optimization ..... 25
Carrier Feedthrough Nulling ..... 26
Envelope Detector ..... 26
Power Down and Reset ..... 26
Serial Port Interface (SPI) ..... 26
Applications Information ..... 28
Baseband Quadrature Modulation from Low Frequencies ..... 28
Performance at Different Quad Filter Settings ..... 28
VVA Temperature Compensation ..... 28
Performance Between Differential vs. Single-Ended LO Input ..... 29
Performance Across RF Frequency at Fixed Input Frequencies ..... 30
Performance Across Common-Mode Voltage in I/Q Mode ..... 31
Operating VCTRL1 and VCTRL2 Independently ..... 31
Recommended Land Pattern ..... 33
Evaluation Board Information ..... 33
Register Summary ..... 34
Register Details ..... 35
Outline Dimensions ..... 39
Ordering Guide ..... 39
Changes to Figure 58 Caption ..... 18
Change to Return Loss and Isolation Section. ..... 21
Moved Figure 70; Renumbered Sequentially ..... 21
Moved Figure 72 ..... 22
Moved Figure 77 ..... 22
Moved Figure 80 ..... 23
Changes to $\mathrm{M} \times \mathrm{N}$ Spurious Performance Section, I/Q Mode Section, and IF Mode Section ..... 24
Changes to Start-Up Sequence Section ..... 25
12/2018—Revision 0: Initial Version

## SPECIFICATIONS

IF and I/Q amplitude $=-20 \mathrm{dBm}$, VCC_DRV $=$ VCC2_DRV $=$ VCC_AMP2 $=$ VCC_ENV $=$ VCC_AMP1 $=$ VCC_BG2 $=$ VCC_MIXER $=$ VCC_BG = VCC_QUAD $=3.3 \mathrm{~V}, \mathrm{DVDD}=\mathrm{VCC}$ _VVA $=1.8 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, and set Register 0x0A to 0xE700, unless otherwise noted.
Measurements in IF mode performed with a $90^{\circ}$ hybrid, Register 0x03, Bit $7=1$, IF input frequency $\left(f_{\text {IF }}\right)=3.5 \mathrm{GHz}$.
Measurements in I/Q mode are measured as a composite of the I and Q channel performance, common-mode voltage $\left(\mathrm{V}_{\text {См }}\right)=0 \mathrm{~V}$, Register 0x03, Bit $7=0$, and Register 0x05, Bits[6:0] $=0 x 051$, unless otherwise noted. I/Q baseband frequency $\left(f_{B B}\right)=100 \mathrm{MHz}$.
VCTRL1 $=$ VCTRL2. $V_{\text {CTRL }}$ is the attenuation voltage at the VCTRL1 and VCTRL2 pins. $V_{\text {CTRL }}=1800 \mathrm{mV}$, unless otherwise specified.
Table 1.

\begin{tabular}{|c|c|c|c|c|c|}
\hline Parameter \& Test Conditions/Comments \& Min \& Typ \& Max \& Unit \\
\hline \begin{tabular}{l}
FREQUENCY RANGES \\
RF Output \\
LO Input \\
LO Quadrupler \\
IF Input \\
Baseband (BB) I/Q Input
\end{tabular} \& \& \[
\begin{aligned}
\& 24 \\
\& 5.4 \\
\& 21.6 \\
\& 0.8 \\
\& \text { DC } \\
\& \hline
\end{aligned}
\] \& \& \[
\begin{aligned}
\& 44 \\
\& 10.25 \\
\& 41 \\
\& 6.0 \\
\& 6.0 \\
\& \hline
\end{aligned}
\] \& \begin{tabular}{l}
GHz \\
GHz \\
GHz \\
GHz \\
GHz
\end{tabular} \\
\hline LO AMPLITUDE RANGE \& \& -6 \& 0 \& +6 \& dBm \\
\hline \begin{tabular}{l}
I/Q MODULATOR PERFORMANCE \\
Conversion Gain \\
24 GHz to 40 GHz \\
40 GHz to 44 GHz \\
Voltage Variable Attenuator (VVA) Control Range \\
Single-Sideband (SSB) Noise Figure \\
24 GHz to 40 GHz \\
40 GHz to 44 GHz \\
Output Third-Order Intercept (IP3) \\
24 GHz to 40 GHz \\
40 GHz to 44 GHz \\
Output 1 dB Compression Point (P1dB) \\
24 GHz to 40 GHz \\
40 GHz to 44 GHz \\
Sideband Rejection (SBR) Uncalibrated
\end{tabular} \& \begin{tabular}{l}
At maximum gain \\
\(\mathrm{f}_{\mathrm{BB}} \leq 3.5 \mathrm{GHz}\) \\
\(6 \mathrm{GHz}>\mathrm{f}_{\mathrm{BB}}>3.5 \mathrm{GHz}\) \\
At maximum gain \\
At maximum gain \\
At maximum gain \\
24 GHz to 44 GHz , at maximum gain
\end{tabular} \& 18

20

10 \& $$
\begin{aligned}
& 23 \\
& 21 \\
& 19 \\
& 35 \\
& 18 \\
& 19 \\
& 19 \\
& 23 \\
& 22 \\
& \\
& 13 \\
& 12
\end{aligned}
$$

\[
32

\] \& \& | dB |
| :--- |
| dB |
| dB |
| dB |
| dB |
| dBm |
| dBm |
| dBm |
| dBm |
| dBC | <br>


\hline | IF SINGLE-SIDEBAND UPCONVERSION PERFORMANCE |
| :--- |
| Conversion Gain |
| 24 GHz to 40 GHz |
| 40 GHz to 44 GHz |
| VVA Control Range |
| SSB Noise Figure |
| 24 GHz to 40 GHz |
| 40 GHz to 44 GHz |
| Output IP3 |
| 24 GHz to 40 GHz |
| 40 GHz to 44 GHz |
| Output P1dB |
| 24 GHz to 40 GHz |
| 40 GHz to 44 GHz |
| SBR |
| Uncalibrated |
| Calibrated | \& | At maximum gain |
| :--- |
| $\mathrm{f}_{\mathrm{FF}} \leq 3.5 \mathrm{GHz}$ |
| $6 \mathrm{GHz}>\mathrm{fiF}_{\mathrm{F}}>3.5 \mathrm{GHz}$ |
| At maximum gain |
| At maximum gain |
| At maximum gain |
| 24 GHz to 44 GHz , at maximum gain |
| Calibrated using LOAMP_PH_ADJ_ |
| Q_FINE and LOAMP_PH_ADJ_I_FINE bits | \& 13

20

10 \& $$
\begin{aligned}
& 18 \\
& 12 \\
& 14 \\
& 35 \\
& 25 \\
& 28 \\
& 23 \\
& 22 \\
& \\
& 13 \\
& 12
\end{aligned}
$$

$$
26
$$

\[
36

\] \& \& | dB |
| :--- |
| dB |
| dB |
| dB |
| dB |
| dBm |
| dBm |
| dBm |
| dBm |
| dBc |
| dBc | <br>

\hline
\end{tabular}

\begin{tabular}{|c|c|c|c|c|c|}
\hline Parameter \& Test Conditions/Comments \& Min \& Typ \& Max \& Unit \\
\hline  \& \begin{tabular}{l}
For optimum performance \\
Measured with two tones with total power output (Pout) at RF \(=10 \mathrm{dBm}\) RF frequency \(\left(\mathrm{f}_{\mathrm{RF}}\right)=28 \mathrm{GHz}\)
\[
\mathrm{f}_{\mathrm{RF}}=28 \mathrm{GHz}
\]
\end{tabular} \& \& \[
\begin{aligned}
\& -45 \\
\& -20 \\
\& \\
\& 350 \\
\& 1
\end{aligned}
\] \& \& \begin{tabular}{l}
dBm \\
dBm \\
MHz \\
GHz
\end{tabular} \\
\hline \begin{tabular}{l}
RETURN LOSS \\
RF Output \\
LO Input \\
IF Input \\
BB Input \\
BB I/Q Input Impedance
\end{tabular} \& \(50 \Omega\) single-ended \(100 \Omega\) differential \(50 \Omega\) single-ended \(100 \Omega\) differential \& \& \[
\begin{aligned}
\& -8 \\
\& -12 \\
\& -12 \\
\& -10 \\
\& 100 \\
\& \hline
\end{aligned}
\] \& \& \[
\begin{aligned}
\& \mathrm{dB} \\
\& \mathrm{~dB} \\
\& \mathrm{~dB} \\
\& \mathrm{~dB} \\
\& \Omega
\end{aligned}
\] \\
\hline \begin{tabular}{l}
LEAKAGE \\
Fundamental LO to RF \(4 \times\) LO to RF 5.4 GHz to 6.8 GHz LO 6.8 GHz to 10.25 GHz LO 5.4 GHz to 10.25 GHz LO \\
\(5 \times \mathrm{LO}\) to RF Fundamental LO to IF Fundamental LO to I/Q
\end{tabular} \& \begin{tabular}{l}
At maximum gain \\
Uncalibrated \\
Uncalibrated \\
Calibrated using MXER_OFF_ADJ_I_N, \\
MXER_OFF_ADJ_I_P, MXER_OFF_ \\
ADJ_Q_N, MXER_OFF_ADJ_Q_P bits at \\
\(\mathrm{V}_{\text {CTRL }}=1800 \mathrm{mV}\), IF mode
\end{tabular} \& \& \[
\begin{aligned}
\& -80 \\
\& -12 \\
\& -20 \\
\& -45
\end{aligned}
\]
\[
\begin{aligned}
\& -55 \\
\& -70 \\
\& -75
\end{aligned}
\] \& \& \begin{tabular}{l}
dBm \\
dBm \\
dBm \\
dBm \\
dBm \\
dBm \\
dBm
\end{tabular} \\
\hline LOGIC INPUTS Input Voltage Range High, \(\mathrm{V}_{\text {INH }}\) Low, VINL Input Current, linh/linL Input Capacitance, \(\mathrm{C}_{\mathrm{IN}}\) \& \& \[
\begin{aligned}
\& \text { DVDD - } 0.4 \\
\& 0
\end{aligned}
\] \& \[
\begin{aligned}
\& 100 \\
\& 3 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& 1.8 \\
\& 0.4
\end{aligned}
\] \& \[
\begin{aligned}
\& \mathrm{V} \\
\& \mathrm{~V} \\
\& \mu \mathrm{~A} \\
\& \mathrm{pF}
\end{aligned}
\] \\
\hline \begin{tabular}{l}
LOGIC OUTPUTS \\
Output Voltage Range \\
High, Vон \\
Low, Vol \\
Output High Current, Іон
\end{tabular} \& \& \[
\begin{aligned}
\& \text { DVDD - } 0.4 \\
\& 0
\end{aligned}
\] \& \& \[
\begin{aligned}
\& 1.8 \\
\& 0.4 \\
\& 500
\end{aligned}
\] \& \[
\begin{aligned}
\& \text { V } \\
\& \text { V }
\end{aligned}
\]
\[
\mu \mathrm{A}
\] \\
\hline \begin{tabular}{l}
POWER INTERFACE \\
VCC_DRV, VCC2_DRV, VCC_AMP2, VCC_ENV, VCC_AMP1,VCC_BG2, VCC_MIXER, VCC_BG, VCC_QUAD \\
3.3 V Supply Current \\
DVDD, VCC_VVA \\
1.8 V Supply Current \\
Total Power Consumption Power-Down
\end{tabular} \& \begin{tabular}{l}
\(\mathrm{V}_{\text {CTRL }}=1.8 \mathrm{~V}\), no IF and I/Q or LO input signal \\
\(\mathrm{V}_{\text {CTRL }}=1.8 \mathrm{~V}\), no IF and I/Q or LO input signal
\end{tabular} \& \[
3.15
\]
\[
1.7
\] \& \[
\begin{aligned}
\& 3.3 \\
\& 550 \\
\& 1.8 \\
\& 3 \\
\& 1.9 \\
\& 77 \\
\& \hline
\end{aligned}
\] \& 3.45

1.9

136 \& | V |
| :--- |
| mA |
| V |
| mA |
| W |
| mW | <br>

\hline
\end{tabular}

## ADMV1013

## SERIAL PORT REGISTER TIMING

Table 2.

| Parameter | Description | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| tsdi, SETUP | Data to clock setup time | 10 |  |  | ns |
| tsDI, HOLD | Data to clock hold time | 10 |  |  | ns |
| $\mathrm{tsCLK}, \mathrm{HIGH}$ | Clock high duration | 40 to 60 |  |  | \% |
| tsCLK, LOW | Clock low duration | 40 to 60 |  |  | \% |
| $\mathrm{t}_{\text {SCLK, }}$ SEN/ $/$ SEN2_SETUP | Clock to $\overline{\mathrm{SEN}} / \overline{\mathrm{SEN}}$ 2 setup time | 30 |  |  | ns |
| $\mathrm{t}_{\text {SCLK, DOT }}$ | Clock to data out transition time |  |  | 10 | ns |
| tsclk, DOV | Clock to data out valid time |  |  | 10 | ns |
| $\mathrm{t}_{\text {SCLK, }}$ SEN/SEN2_INACTIVE | Clock to $\overline{\text { SEN }} / \overline{\text { SEN } 2}$ inactive | 20 |  |  | ns |
| $\mathrm{t}_{\text {SEN/SEN2_INACTIVE }}$ | Inactive $\overline{\text { SEN }} / \overline{S E N 2}$ (between two operations) | 80 |  |  | ns |

## Timing Diagram



## ABSOLUTE MAXIMUM RATINGS

Table 3.

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage |  |
| VCC_DRV, VCC2_DRV, VCC_AMP2, | 4.3 V |
| VCC_ENV, VCC_AMP1,VCC_BG2, |  |
| $\quad$ VCC_BG, VCC_MIXER | 2.3 V |
| DVDD, VCC_VVA | 5 dBm |
| IF Input Power | 5 dBm |
| I/Q Input Power | 9 dBm |
| LO Input Power | $125^{\circ} \mathrm{C}$ |
| Maximum Junction Temperature | 2.9 W |
| Maximum Power Dissipation ${ }^{1}$ | $1 \times 10^{6}$ hours |
| Lifetime at Maximum Junction Temperature (TJ) | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Operating Case Temperature Range | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Storage Temperature Range | $260^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering 60 sec) | $\mathrm{MSL3}$ |
| Moisture Sensitivity Level (MSL) Rating ${ }^{2}$ |  |
| Electrostatic Discharge (ESD) Sensitivity | 1250 V |
| Human Body Model (HBM) | 750 V |
| Field Induced Charged Device Model |  |
| $\quad$ (FICDM) |  |

${ }^{1}$ The maximum power dissipation is a theoretical number calculated by ( $\mathrm{T}_{\mathrm{J}}-85^{\circ} \mathrm{C}$ )/ $\theta_{\text {лс_- } \text { то } . ~}^{\text {. }}$
${ }^{2}$ Based on IPC/JEDEC J-STD-20 MSL classifications.
Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

## THERMAL RESISTANCE

Thermal performance is directly linked to printed circuit board (PCB) design and operating environment. Careful attention to PCB thermal design is required.
$\theta_{J A}$ is the natural convection junction to ambient thermal resistance measured in a one cubic foot sealed enclosure. $\theta_{\mathrm{JC}}$ is the junction to case thermal resistance.
$\theta_{\mathrm{JA}}$ and $\theta_{\mathrm{JC}}$ must only be used to compare the thermal performance of the different packages if all test conditions listed are similar to JEDEC specifications. Instead, $\Psi_{\mathrm{JT}}$ and $\Psi_{\mathrm{JB}}$ can be used to calculate the junction temperature of the device by using the following equations:

$$
\begin{equation*}
T_{J}=\left(P \times \Psi_{J T}\right)+T_{T O P} \tag{1}
\end{equation*}
$$

where:
$P$ refers to the total power dissipation in the chip (W).
$\Psi_{J T}$ refers to the junction to top thermal characterization number.
$T_{T O P}$ refers to the package top temperature $\left({ }^{\circ} \mathrm{C}\right)$ and is measured at the top center of the package.

$$
\begin{equation*}
T_{J}=\left(P \times \Psi_{J B}\right)+T_{B O A R D} \tag{2}
\end{equation*}
$$

where:
$P$ refers to the total power dissipation in the chip (W).
$\Psi_{J B}$ refers to the junction to board thermal characterization number.
$T_{B O A R D}$ refers to the board temperature measured on the midpoint of the longest side of the package, no more than 1 mm from the edge of the package body $\left({ }^{\circ} \mathrm{C}\right)$.
As stated in JEDEC51-12, Equation 1 and Equation 2 must be used when no heat sink/heat spreader is present. When a heat sink/heat spreader is added, estimating and calculating junction temperature can be achieved using $\theta_{\text {J__тор. }}$

Table 4. Thermal Resistance

| Package Type $^{\mathbf{1}}$ | $\boldsymbol{\theta}_{\mathrm{JA}}{ }^{\mathbf{2}}$ | $\boldsymbol{\theta}_{\mathrm{Jc} \_ \text {тор }}{ }^{\mathbf{3}}$ | $\boldsymbol{\theta}_{\mathrm{JB}}{ }^{4}$ | $\boldsymbol{\Psi}_{\mathrm{JT}}{ }^{5}$ | $\boldsymbol{\Psi}_{\mathrm{JB}}{ }^{6}$ | Unit |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{CC}-40-5$ | 28 | 13.8 | 11.1 | 6.4 | 13.8 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

${ }^{1}$ The thermal resistance values specified in Table 4 are simulated based on JEDEC specifications, unless specified otherwise, and must be used in compliance with JESD51-12.
${ }^{2} \theta_{\mathrm{JA}}$ is the junction to ambient thermal resistance in a natural convection, JEDEC environment.
${ }^{3} \theta_{\mathrm{Jc}}$ _Top is the junction to case (top) JEDEC thermal resistance.
${ }^{4} \theta_{\mathrm{J}}$ is the junction to board JEDEC thermal resistance.
${ }^{5} \Psi_{\text {Jт }}$ is the junction to top JEDEC thermal characterization parameter.
${ }^{6} \Psi_{J B}$ is the junction to board JEDEC thermal characterization parameter.

## ESD CAUTION

ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



NOTES

1. DNC = DO NOT CONNECT. DO NOT CONNECT TO THIS PIN.
2. EXPOSED PAD. SOLDER THE EXPOSED PAD TO A LOW IMPEDANCE GROUND PLANE. 产

Figure 3. Pin Configuration

Table 5. Pin Function Descriptions

| Pin No. | Mnemonic | Description |
| :---: | :---: | :---: |
| 1 | RST | SPI Reset. Connect this pin to logic high for normal operation. The SPI logic is 1.8 V . |
| 2 | DVDD | 1.8 V SPI Digital Supply. |
| 3 | SCLK | SPI Clock Digital Input. |
| 4 | SDI | SPI Serial Data Input. |
| 5 | SDO | SPI Serial Data Output. |
| 6 | BG_RBIAS2 | Voltage Gain Amplifier (VGA) Chip Band Gap Circuit, External High Precision Resistor. Place a $1.1 \mathrm{k} \Omega$, high precision resistor shunt to ground close to this pin. |
| 7 | VCC_DRV | 3.3 V Power Supply for RF Driver. Place a 100 pF , a $0.01 \mu \mathrm{~F}$, and a $10 \mu \mathrm{~F}$ capacitor close to this pin. |
| 8, 10, 27, 36, 39 | GND | Ground. |
| 9 | RF | RF Output. This pin is dc-coupled internally to GND and matched to $50 \Omega$ single ended. |
| 11 | VCC2_DRV | 3.3 V Power Supply for RF Predriver. Place a 100 pF , a $0.01 \mu \mathrm{~F}$, and a $10 \mu \mathrm{~F}$ capacitor close to this pin. |
| 12, 13, 31 | DNC | Do Not Connect. Do not connect to this pin. |
| 14 | VCC_VVA | 1.8V Power Supply for VVA Control Circuit. Place a $100 \mathrm{pF}, 0.01 \mu \mathrm{~F}$, and a $10 \mu \mathrm{~F}$ capacitor close to this pin. |
| 15 | VCTRL1 | RF Voltage Variable Attenuator 1 (VVA1) Control Voltage. Place a $1 \mathrm{k} \Omega$ series resistor with this pin. |
| 16 | VCTRL2 | RF Voltage Variable Attenuator 2 (VVA2) Control Voltage. Place a $1 \mathrm{k} \Omega$ series resistor with this pin. |
| 17 | VCC_AMP2 | 3.3 V Power Supply for RF Amplifier 2 (AMP2). Place a 100 pF , a $0.01 \mu \mathrm{~F}$, and a $10 \mu \mathrm{~F}$ capacitor close to this pin. |
| 18 | $\overline{\text { SEN2 }}$ | SPI Serial Enable for VGA Chip. Connect this pin with Pin 40 ( $\overline{\text { SEN }}$ ). |
| 19 | VCC_ENV | 3.3V Power Supply for Envelope Detector. Place a 100 pF , a $0.01 \mu \mathrm{~F}$, and a $10 \mu \mathrm{~F}$ capacitor close to this pin. |
| 20 | VCC_AMP1 | 3.3 V Power Supply for RF Amplifier 1 (AMP1). Place a 100 pF , a $0.01 \mu \mathrm{~F}$, and a $10 \mu \mathrm{~F}$ capacitor close to this pin. |
| 21 | VENV_N | Negative Differential Envelope Detector Output. |
| 22 | VENV_P | Positive Differential Envelope Detector Output. |
| 23 | VCC_BG2 | 3.3V Power Supply for VGA Chip Band Gap Circuit. Place a 100 pF , a $0.01 \mu \mathrm{~F}$, and a $10 \mu \mathrm{~F}$ capacitor close to this pin. |
| 24,30 | IF_Q, IF_I | IF Single-Ended Complex Inputs. These pins are internally ac-coupled. When in IF mode, Pin 25 (Q_P), Pin 26 (Q_N), Pin 28 (I_P), and Pin 29 (I_N) must be kept floating. |
| 25, 26 | Q_N, Q_P | Differential Baseband Q Inputs. These pins are dc-coupled. Do not connect these pins in IF mode. |
| 28,29 | I_P, I_N | Differential Baseband I Inputs. These pins are dc-coupled. Do not connect these pins in IF mode. |


| Pin No. | Mnemonic | Description |
| :---: | :---: | :---: |
| 32 | VCC_MIXER | 3.3V Power Supply for Mixer. Place a 100 pF , a $0.01 \mu \mathrm{~F}$, and a $10 \mu \mathrm{~F}$ capacitor close to this pin. |
| 33 | VCC_BG | 3.3 V Power Supply for Mixer Chip Band Gap Circuit. Place a 100 pF , a $0.01 \mu \mathrm{~F}$, and a $10 \mu \mathrm{~F}$ capacitor close to this pin. |
| 34 | BG_RBIAS1 | Mixer Chip Band Gap Circuit, External High Precision Resistor. Place a $1.1 \mathrm{k} \Omega$, high precision resistor shunt to ground close to this pin. |
| 35 | VCC_QUAD | 3.3 V Power Supply for Quadruppler. Place a 100 pF , a $0.01 \mu \mathrm{~F}$, and a $10 \mu \mathrm{~F}$ capacitor close to this pin. |
| 37,38 | LON, LOP | Negative and Positive Differential Local Oscillator Input. This pin is dc-coupled internally to ground and matched to $100 \Omega$ differential or $50 \Omega$ single ended. If using the LO as single ended, terminate the unused LO port with $50 \Omega$ impedance to ground. |
| 40 | $\overline{\text { SEN }}$ | SPI Serial Enable for Mixer Chip. Connect this pin with Pin 18 ( (SEN2). |
|  | EPAD | Exposed Pad. Solder the exposed pad to a low impedance ground plane. |

## TYPICAL PERFORMANCE CHARACTERISTICS

## I/Q MODE

I/Q amplitude $=-20 \mathrm{dBm}$, VCC_DRV $=$ VCC2_DRV $=$ VCC_AMP2 $=$ VCC_ENV $=$ VCC_AMP1 $=$ VCC_BG2 $=$ VCC_MIXER $=$ VCC_BG $=$ VCC_QUAD $=3.3 \mathrm{~V}$, DVDD $=\mathrm{VCC}$ _VVA $=1.8 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, and set Register 0x0A to 0xE700, unless otherwise noted. VCTRL1 $=$ VCTRL2. $V_{\text {CTRL }}$ is the attenuation voltage at the VCTRL1 and VCTRL2 pins. $V_{\text {CTRL }}=1800 \mathrm{mV}$, unless otherwise specified. Measurements in I/Q mode are measured as a composite of the I and Q channel performance, $\mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}$, Register 0 x 03 , Bit $7=0$, and Register 0x05, Bits[6:0] = 0x051, unless otherwise noted. I/Q $\mathrm{f}_{\mathrm{BB}}=100 \mathrm{MHz}$.


Figure 4. Conversion Gain vs. RF Frequency ( $f_{R F}$ ) at Three Different Gain Settings for Various Temperatures, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 5. Conversion Gain vs. RF Frequency at for Various Supply
Voltages, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 6. Conversion Gain vs. RF Frequency at for Various LO Inputs, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 7. Conversion Gain vs. VCTRL at Various Temperatures and $f_{R F}=28 \mathrm{GHz}$ and $39 \mathrm{GHz}, f_{B B}=100 \mathrm{MHz}$


Figure 8. Conversion Gain vs. Baseband Frequency at $f_{\text {RF }}=28 \mathrm{GHz}$ and 39 GHz (Upper Sideband)


Figure 9. Conversion Gain vs. Baseband Frequency at $f_{\text {RF }}=28 \mathrm{GHz}$ and 39 GHz (Lower Sideband)


Figure 10. Output IP3 vs. RF Frequency at Maximum Gain for Various Temperatures, RF Amplitude $=-20 \mathrm{dBm}$ per Tone at 20 MHz Spacing, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 11. Output IP3 vs. RF Frequency at Maximum Gain for Supply Voltages, RF Amplitude $=-20 \mathrm{dBm}$ per Tone at 20 MHz Spacing, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 12. Output IP3 vs. RF Frequency at Maximum Gain for Various LO Inputs, RF Amplitude $=-20 \mathrm{dBm}$ per Tone at 20 MHz Spacing, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 13. Output IP3 vs. VCTRL, RF Amplitude $=-20 \mathrm{dBm}$ per Tone at 20 MHz Spacing, $f_{B B}=100 \mathrm{MHz}$ at $f_{R F}=28 \mathrm{GHz}$ and 39 GHz (Upper Sideband)


Figure 14. Output IP3 vs. Baseband Frequency at $f_{R F}=28 \mathrm{GHz}$ and 39 GHz at Maximum Gain, RFAmplitude $=-20 \mathrm{dBm}$ per Tone at 20 MHz Spacing (Upper Sideband and Lower Sideband)


Figure 15. Output IP3 vs. Total Input Power at 20 MHz Spacing, $f_{B B}=100 \mathrm{MHz}, f_{R F}=28 \mathrm{GHz}$ and 39 GHz (Upper Sideband)


Figure 16. Noise Figure vs. RF Frequency at Maximum Gain for Various Temperatures, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 17. Noise Figure vs. RF Frequency for Various Supply Voltages, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 18. Noise Figure vs. RF Frequency for Various LO Inputs, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 19. Noise Figure vs. V CTRL for Various Temperatures at $f_{R F}=28 \mathrm{GHz} 39 \mathrm{GHz}, f_{B B}=100 \mathrm{MHz}$


Figure 20. Noise Figure vs. Baseband Frequency at $f_{\text {RF }}=28 \mathrm{GHz}$ and 39 GHz (Upper Sideband)


Figure 21. Noise Figure vs. Baseband Frequency at $f_{\text {RF }}=28 \mathrm{GHz}$ and 39 GHz (Lower Sideband)


Figure 22. Sideband Rejection vs. RF Frequency at Maximum Gain for Various Temperatures, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 23. Sideband Rejection vs. RF Frequency at for Various Supply Voltages, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 24. Sideband Rejection vs. RF Frequency for Various LO Inputs, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 25. Sideband Rejection vs. $V_{\text {CTRL }}$ for Various Temperatures at $f_{R F}=28 \mathrm{GHz}$ and $39 \mathrm{GHz}, f_{B B}=100 \mathrm{MHz}$


Figure 26. Sideband Rejection vs. Baseband Frequency at $f_{R F}=28 \mathrm{GHz}$ and 39 GHz (Upper Sideband and Lower Sideband)


Figure 27. Output P1dB vs. RF Frequency at Maximum Gain for Various Temperatures, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 28. Output P1dB vs. RF Frequency for Various Supply Voltages, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 29. Output P1dB vs. RF Frequency for Various LO Inputs, $f_{B B}=100 \mathrm{MHz}$ (Upper Sideband)


Figure 30. Output P1dB vs. V ctrl for Various Temperatures at $f_{R F}=28 \mathrm{GHz}$ and $39 \mathrm{GHz}, f_{B B}=100 \mathrm{MHz}$


Figure 31. Output P1dB vs. Baseband Frequency at $f_{\text {RF }}=28 \mathrm{GHz}$ and 39 GHz (Upper Sideband)


Figure 32. Output P1dB vs. Baseband Frequency at $f_{R F}=28 \mathrm{GHz}$ and 39 GHz (Lower Sideband)

## ADMV1013

## IF MODE

IF amplitude $=-20 \mathrm{dBm}$, VCC_DRV $=$ VCC2_DRV $=$ VCC_AMP2 $=$ VCC_ENV $=$ VCC_AMP1 $=$ VCC_BG2 $=$ VCC_MIXER $=$ VCC_BG = VCC_QUAD $=3.3 \mathrm{~V}, \mathrm{DVDD}=\mathrm{VCC}$ VVA $=1.8 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, and set Register 0x0A to 0xE700, unless otherwise noted. VCTRL1 $=$ VCTRL2. $V_{\text {CTRL }}$ is the attenuation voltage at the VCTRL1 and VCTRL2 pins. $V_{\text {CTRL }}=1800 \mathrm{mV}$, unless otherwise specified. Measurements in IF mode performed with a $90^{\circ}$ hybrid, Register 0x03, Bit $7=1$, and $\mathrm{f}_{\mathrm{IF}}=3.5 \mathrm{GHz}$.


Figure 33. Conversion Gain vs. RF Frequency at Maximum Gain for Various Temperatures, $f_{I F}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 34. Conversion Gain vs. RF Frequency at Maximum Gain for Various Supply Voltages, $\mathrm{f}_{\text {IF }}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 35. Conversion Gain vs. RF Frequency at Maximum Gain for Various LO Inputs, $f_{\text {IF }}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 36. Conversion Gain vs. IF Frequency at $f_{R F}=28 \mathrm{GHz}$ and 39 GHz at Maximum Gain (Upper Sideband and Lower Sideband)


Figure 37. Conversion Gain vs. V CTRL at Various Temperatures at $f_{\text {RF }}=28 \mathrm{GHz}$ and $39 \mathrm{GHz}, f_{I F}=3.5 \mathrm{GHz}$ (Upper Sideband)


Figure 38. Conversion Gain vs. VCTRL at Various Temperatures at $f_{R F}=28 \mathrm{GHz}$ and $39 \mathrm{GHz}, f_{I F}=3.5 \mathrm{GHz}$ (Lower Sideband)


Figure 39. Output IP3 vs. RF Frequency at Maximum Gain for Various Temperatures, RF Amplitude $=-20 \mathrm{dBm}$ per Tone at 20 MHz Spacing,

$$
f_{\mathrm{IF}}=3.5 \mathrm{GHz} \text { (Upper Sideband and Lower Sideband) }
$$



Figure 40. Output IP3 vs. RF Frequency at Maximum Gain for Various Supply Voltages, RF Amplitude $=-20 \mathrm{dBm}$ per Tone at 20 MHz Spacing, $f_{I F}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 41. Output IP3 vs. RF Frequency at Maximum Gain for Various LO Inputs, RF Amplitude $=-20 \mathrm{dBm}$ per Tone at 20 MHz Spacing, $f_{\text {IF }}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 42. Output IP3 vs. $V_{\text {CTRL }}$ at $f_{\text {RF }}=28 \mathrm{GHz}$ and 39 GHz , RF Amplitude $=-20 \mathrm{dBm}$ per Tone at 20 MHz Spacing, $f_{\mathrm{IF}}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 43. Output IP3 vs. IF Frequency at $f_{R F}=28 \mathrm{GHz}$ and 39 GHz at Maximum Gain, RF Amplitude $=-20 \mathrm{dBm}$ per Tone at 20 MHz Spacing (Upper Sideband and Lower Sideband)


Figure 44. Output IP3 vs. Total Input Power at $f_{R F}=28 \mathrm{GHz}$ and 39 GHz at 20 MHz Spacing, $\mathrm{f}_{\mathrm{IF}}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 45. Noise Figure vs. RF Frequency at Maximum Gain for Various Temperatures, $f_{I F}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 46. Noise Figure vs. RF Frequency at Maximum Gain for Various Supply Voltages, $\mathrm{f}_{\text {IF }}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 47. Noise Figure vs. RF Frequency at Maximum Gain for Various LO Inputs, $f_{I F}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 48. Noise Figure vs. IF Frequency at $f_{R F}=28 \mathrm{GHz}$ and 39 GHz at Maximum Gain (Upper Sideband and Lower Sideband)


Figure 49. Noise Figure vs. VCTRL at Various Temperatures, $f_{I F}=3.5 \mathrm{GHz}$, (Upper Sideband and Lower Sideband)


Figure 50. Noise Figure vs. VCTRL for Various Temperatures at $f_{R F}=28 \mathrm{GHz}$ and $39 \mathrm{GHz}, \mathrm{f}_{\text {IF }}=3.5 \mathrm{GHz}$ (Lower Sideband)


Figure 51. Output P1dB vs. RF Frequency at Maximum Gain for Various Temperatures, $f_{I F}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 52. Output P1dB vs. RF Frequency at Maximum Gain for Various Supply Voltages, $f_{\text {IF }}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 53. Output P1dB vs. RF Frequency at Maximum Gain for Various LO Inputs, $\mathrm{f}_{\mathrm{IF}}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 54. Output P1dB vs. IF Frequency at $f_{R F}=28 \mathrm{GHz}$ and 39 GHz at Maximum Gain (Upper Sideband and Lower Sideband)


Figure 55. Output P1dB vs. V ствL for Various Temperatures at $f_{R F}=28 \mathrm{GHz}$ and $39 \mathrm{GHz}, f_{\text {IF }}=3.5 \mathrm{GHz}$ (Upper Sideband)


Figure 56. Output P1dB vs. V ctrl for Various Temperatures at $f_{\text {RF }}=28 \mathrm{GHz}$ and $39 \mathrm{GHz}, f_{I F}=3.5 \mathrm{GHz}$ (Lower Sideband)


Figure 57. Sideband Rejection vs. RF Frequency at Maximum Gain for Various Temperatures, $f_{I F}=3.5 \mathrm{GHz}$, Uncalibrated (Upper Sideband and Lower Sideband)


Figure 58. Sideband Rejection vs. RF Frequency at Maximum Gain for Various Temperatures, $f_{\text {IF }}=3.5 \mathrm{GHz}$, Calibrated at $25^{\circ} \mathrm{C}$ (Upper Sideband). Note: Calibrated Using LOAMP_PH_ADJ_Q_FINE and LOAMP_PH_ADJ_I_FINE Bits


Figure 59. Sideband Rejection vs. RF Frequency at Maximum Gain for Various Supply Voltages, $f_{\text {IF }}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 60. Sideband Rejection vs. RF Frequency at Maximum Gain for Various LO Inputs, $f_{I F}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)


Figure 61. Sideband Rejection vs. IF Frequency at $f_{R F}=28 \mathrm{GHz}$ and 39 GHz at Maximum Gain (Upper Sideband and Lower Sideband)


Figure 62. Sideband Rejection vs. $V_{C T R L}$ at $f_{R F}=28 \mathrm{GHz}$ and 39 GHz , $f_{\text {IF }}=3.5 \mathrm{GHz}$ (Upper Sideband and Lower Sideband)

## ENVELOPE DETECTOR PERFORMANCE

IF and I/Q amplitude $=-20 \mathrm{dBm}, \mathrm{VCC} \_\mathrm{DRV}=\mathrm{VCC} 2 \_D R V=$ VCC_AMP2 $=$ VCC_ENV $=$ VCC_AMP1 $=$ VCC_BG2 $=$ VCC_MIXER $=$ VCC_BG = VCC_QUAD $=3.3 \mathrm{~V}, \mathrm{DVDD}=\mathrm{VCC}, \mathrm{VVA}=1.8 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, and set Register 0 x 0 A to 0 xE 700 , unless otherwise noted.

Measurements in IF mode performed with a $90^{\circ}$ hybrid, Register 0x03, Bit $7=1$, IF $\mathrm{f}_{\mathrm{IF}}=3.5 \mathrm{GHz}$.
Measurements in I/Q mode are measured as a composite of the I and Q channel performance, $\mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}$, Register 0 x 03 , Bit $7=0$, and Register 0x05, Bits[6:0] $=0 \times 051$, unless otherwise noted. $\mathrm{I} / \mathrm{Q} \mathrm{f}_{\mathrm{BB}}=100 \mathrm{MHz}$.

VCTRL1 $=$ VCTRL2. $V_{\text {CTRL }}$ is the attenuation voltage at the VCTRL1 and VCTRL2 pins. $V_{\text {CTRL }}=1800 \mathrm{mV}$, unless otherwise specified.
Envelope detector measurements made with Register 0x03, Bit $5=1$.


Figure 63. VENV_N/VENV_P Delta and Envelope Pout Delta vs. RF Frequency at Various Output Power Levels, Envelope Frequency $=100 \mathrm{MHz}, V_{C T R L}=1800 \mathrm{mV}$, $T_{A}=25^{\circ} \mathrm{C}, L O=0 \mathrm{dBm}, \mathrm{IF}=2 \mathrm{GHz}$ (Upper Sideband)


Figure 64. Output Level vs. Envelope Frequency for Normalized Harmonic Distortion (HD1), $1 \times$ and Normalized Harmonic Distortion(HD2), $2 \times$, $f_{R F}=28 \mathrm{GHz}, L O=0 \mathrm{dBm}$ at $25^{\circ} \mathrm{C}, \mathrm{HD} 1$ and HD2 Measurement Performed with Two Tones with Delta Equal to Envelope Frequency, HD2 Normalized to HD1 Level at 50 MHz


Figure 65. Pout and VENV_N/VENV_P Delta vs. Power In Total for Pout RF, Pout Envelope HD1, Pout Envelope HD2, and VENV_N/VENV_P Delta, Measurements Performed with Two Tones with 100 MHz Separation, $f_{R F}=28 \mathrm{GHz}, V_{C T R L}=1800 \mathrm{mV}$


Figure 66. HD1 Pout Envelope and VENV_N/VENV_P Delta vs. VCTRL $a t$ Various Total Input Power ( $P_{I N}$ ) Levels, Measurements Performed at 28 GHz with Two Input Tones with Separation of 100 MHz


Figure 67. Pout Envelope vs. Pout RF per Tone at Various Temperatures at $f_{R F}=33 \mathrm{GHz}$, Measurement Performed at 3.5 GHz IF with Two Tones at 100 MHz Spacing, $V_{\text {CTRL }}=1800 \mathrm{mV}$

## RETURN LOSS AND ISOLATION

IF and I/Q amplitude $=-20 \mathrm{dBm}$, VCC_DRV $=$ VCC2_DRV $=$ VCC_AMP2 $=$ VCC_ENV $=$ VCC_AMP1 $=$ VCC_BG2 $=$ VCC_MIXER $=$ VCC_BG $=$ VCC_QUAD $=3.3 \mathrm{~V}, \mathrm{DVDD}=\mathrm{VCC}$ _VVA $=1.8 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, and set Register 0 x 0 A to 0 xE 700 , unless otherwise noted.

Measurements in IF mode performed with a $90^{\circ}$ hybrid, Register 0x03, Bit $7=1$, and $\mathrm{f}_{\mathrm{IF}}=3.5 \mathrm{GHz}$.
Measurements in I/Q mode are measured as a composite of the I and Q channel performance, $\mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}$, Register 0 x 03 , Bit $7=0$, and Register 0x05, Bits[6:0] $=0 \times 051$, unless otherwise noted. $\mathrm{I} / \mathrm{Q} \mathrm{f}_{\mathrm{BB}}=100 \mathrm{MHz}$.
VCTRL1 $=$ VCTRL2. $V_{\text {CTRL }}$ is the attenuation voltage at the VCTRL1 and VCTRL2 pins. $V_{\text {CTRL }}=1800 \mathrm{mV}$, unless otherwise specified. Envelope detector measurements made with Register 0x03, Bit $5=1$.


Figure 68. RF Return Loss vs. RF Frequency at Various $V_{\text {CtRL }}$ Voltages


Figure 69. LO Return Loss vs. LO Frequency


Figure 70. IF Return Loss vs. IF Frequency (Taken Without Hybrid)


Figure 71. I/Q Differential Return Loss vs. Frequency (Taken Without Hybrids or Baluns)


Figure 72. LO to RF Leakage vs. LO Frequency for $4 \times L O, 5 \times L O$, and $1 \times L O$ at Various Temperatures (Uncalibrated)


Figure 73. $1 \times$ LO Leakage vs. LO Frequency at Different $V_{\text {ctrl }}$ Settings (Uncalibrated)


Figure $74.4 \times$ LO to RF Leakage vs. LO Frequency at Various Temperatures (Calibrated). Note: Calibrated at Each Frequency Using MXER_OFF_ADJ_I_N, MXER_OFF_ADJ_I_P,MXER_OFF_ADJ_Q_N, and MXER_OFF_ADJ_Q_PBits at $T_{A}=25^{\circ} \mathrm{C}$


Figure $75.5 \times$ LO Leakage vs. LO Frequency at Different VствL Settings (Uncalibrated)


Figure $76.4 \times$ LO Leakage vs. LO Frequency at Different $V_{\text {CtRL }}$ Settings (Uncalibrated)


Figure 77. $4 \times$ LO to RF Leakage vs. LO Frequency at Various V CTRL (Calibrated) Note: Calibrated at Each Frequency Using MXER_OFF_ADJ_I_N, MXER_OFF_ADJ_I_P,MXER_OFF_ADJ_Q_N, and MXER_OFF_ADJ_Q_P Bits at $V_{\text {CTRL }}=1800 \mathrm{mV}$


Figure 78. LO Leakage vs. LO Frequency at Various Temperatures at I_N, I_P, Q_N, and Q_P (Taken Without Hybrid(s))


Figure 79. Envelope Detector Differential Return Loss vs. Frequency


Figure 80. LO Leakage vs. LO Frequency at Various Temperatures at IF_I and IF_Q Ports(Taken Without Hybrid)

## M $\times$ N SPURIOUS PERFORMANCE

Mixer spurious products are measured in dBc from the RF output power level. Spurious frequencies are calculated by

$$
\begin{gathered}
|(\mathrm{M} \times \mathrm{IF})+(\mathrm{N} \times \mathrm{LO})|(\text { for IF Mode }) \\
|(\mathrm{M} \times \mathrm{IQ})+(\mathrm{N} \times \mathrm{LO})|(\text { for IQ Mode })
\end{gathered}
$$

N/A means not applicable. Blank cells in the spurious performance tables indicate that the frequency is above 50 GHz and is not measured. REF stands for reference RF output signal.
The LO frequencies are referred from the frequencies applied to the ADMV1013. IF and I/Q amplitude $=-20 \mathrm{dBm}$.
VCC_DRV $=$ VCC2_DRV $=$ VCC_AMP2 $=$ VCC_ENV $=$
VCC_AMP1 $=$ VCC_BG2 $=$ VCC_MIXER $=$ VCC_BG $=$
VCC_QUAD $=3.3 \mathrm{~V}$, DVDD $=\mathrm{VCC} \_V V A=1.8 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, and set Register 0x0A to 0xE700, unless otherwise noted.
Measurements in IF mode performed with a $90^{\circ}$ hybrid, Register $0 \times 03$, Bit $7=1$, and $\mathrm{f}_{\mathrm{IF}}=3.5 \mathrm{GHz}$.
Measurements in I/Q mode are measured as a composite of the I and Q channel performance, $\mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}$, Register $0 \times 03$, Bit $7=0$, and Register 0x05, Bits $[6: 0]=0 x 051$, unless otherwise noted. I/Q $\mathrm{f}_{\mathrm{BB}}=100 \mathrm{MHz}$.
VCTRL1 $=$ VCTRL2. $V_{\text {CTRL }}$ is the attenuation voltage at the VCTRL1 and VCTRL2 pins. $V_{\text {CTRL }}=1800 \mathrm{mV}$, unless otherwise specified.

## I/Q Mode

$\mathrm{f}_{\mathrm{BB}}=100 \mathrm{MHz}$ at $-20 \mathrm{dBm}, \mathrm{LO}=6.975 \mathrm{GHz}$ at +6 dBm .

|  |  | $\mathbf{N} \times \mathbf{L O}$ |  |  |  |  |  |  |  |  |  |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: | :---: |
|  |  | $\mathbf{0}$ | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ |  |  |
| $\mathbf{M} \times \mathbf{I Q}$ | $\mathbf{- 2}$ | 93 | 105 | 103 | 122 | 79 | 109 | 89 | 108 |  |  |
|  | $\mathbf{- 1}$ | 93 | 95 | 85 | 57 | 26 | 65 | 53 | 110 |  |  |
|  | $\mathbf{0}$ | N/A | 80 | 72 | 53 | 20 | 61 | 35 | 73 |  |  |
|  | $\mathbf{+ 1}$ | 93 | 96 | 74 | 32 | REF | 41 | 37 | 84 |  |  |
|  | $\mathbf{+ 2}$ | 93 | 107 | 86 | 91 | 57 | 89 | 91 | 83 |  |  |

$\mathrm{f}_{\mathrm{BB}}=100 \mathrm{MHz}$ at $-20 \mathrm{dBm}, \mathrm{LO}=9.725 \mathrm{GHz}$ at +6 dBm , and $\mathrm{f}_{\mathrm{RF}}=39 \mathrm{GHz}$.

|  |  | $\mathbf{N} \times$ LO |  |  |  |  |  |  |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: |
|  |  | $\mathbf{0}$ | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ |  |
| $\mathbf{M} \times \mathbf{I Q}$ | $\mathbf{- 2}$ | 97 | 116 | 95 | 116 | 89 | 113 |  |
|  | $\mathbf{- 1}$ | 101 | 100 | 37 | 62 | 26 | 90 |  |
|  | $\mathbf{0}$ | $\mathrm{~N} / \mathrm{A}$ | 77 | 40 | 63 | 20 | 77 |  |
|  | $\mathbf{+ 1}$ | 97 | 91 | 18 | 36 | REF | 68 |  |
|  | $\mathbf{+ 2}$ | 101 | 118 | 80 | 99 | 64 | 103 |  |

## IF Mode

$\mathrm{f}_{\mathrm{IF}}=3.5 \mathrm{GHz}$ at $-20 \mathrm{dBm}, \mathrm{LO}=6.125 \mathrm{GHz}$ at +6 dBm , and $\mathrm{f}_{\mathrm{RF}}=28 \mathrm{GHz}$.

|  |  | $\mathrm{N} \times \mathrm{LO}$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| $\mathbf{M} \times \mathbf{I F}$ | -2 | 76 | 117 | 120 | 109 | 77 | 92 | 90 | 84 | 45 |
|  | -1 | 68 | 90 | 80 | 77 | 23 | 46 | 56 | 53 | 44 |
|  | 0 | N/A | 71 | 71 | 26 | 9 | 34 | 24 | 20 | 30 |
|  | +1 | 76 | 92 | 58 | 18 | REF | 24 | 32 | 61 |  |
|  | +2 | 68 | 84 | 75 | 70 | 58 | 80 | 82 | 75 |  |

$\mathrm{f}_{\text {IF }}=3.5 \mathrm{GHz}$ at $-20 \mathrm{dBm}, \mathrm{LO}=8.875 \mathrm{GHz}$ at +6 dBm , and $\mathrm{f}_{\mathrm{RF}}=39 \mathrm{GHz}$.

|  |  | $\mathbf{N} \times \mathbf{L O}$ |  |  |  |  |  |  |  |  |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: | :---: |
|  |  | $\mathbf{0}$ | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ |  |  |
| $\mathbf{M} \times \mathbf{I F}$ | $\mathbf{- 2}$ | 83 | 132 | 109 | 96 | 68 | 99 | 107 |  |  |
|  | $\mathbf{- 1}$ | 69 | 95 | 76 | 54 | 25 | 57 | 83 |  |  |
|  | $\mathbf{0}$ | $\mathrm{~N} / \mathrm{A}$ | 69 | 44 | 53 | 16 | 52 |  |  |  |
|  | $\mathbf{+ 1}$ | 83 | 89 | 24 | 33 | REF | 58 |  |  |  |
|  | $\mathbf{+ 2}$ | 69 | 114 | 93 | 98 | 75 |  |  |  |  |

$\mathrm{f}_{\mathrm{IF}}=3.5 \mathrm{GHz}$ at $-20 \mathrm{dBm}, \mathrm{LO}=7.875 \mathrm{GHz}$ at +6 dBm , and $\mathrm{f}_{\mathrm{RF}}=28 \mathrm{GHz}$.

|  |  | $\mathrm{N} \times$ LO |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| $\mathbf{M} \times \mathbf{I F}$ | -2 | 82 | 140 | 115 | 107 | 69 | 99 | 97 | 95 |
|  | -1 | 65 | 120 | 91 | 41 | REF | 47 | 46 |  |
|  | 0 | N/A | 82 | 75 | 52 | 23 | 49 | 56 |  |
|  | +1 | 82 | 94 | 60 | 70 | 26 | 75 |  |  |
|  | +2 | 65 | 120 | 107 | 111 | 93 | 115 |  |  |

$\mathrm{f}_{\mathrm{IF}}=3.5 \mathrm{GHz}$ at $-20 \mathrm{dBm}, \mathrm{LO}=10.5 \mathrm{GHz}$ at +6 dBm , and $\mathrm{f}_{\mathrm{RF}}=39 \mathrm{GHz}$.

|  |  | $\mathbf{N} \times \mathbf{L O}$ |  |  |  |  |  |  |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: |
|  |  | $\mathbf{0}$ | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ |  |
| $\mathbf{M} \times$ IF | $\mathbf{- 2}$ | 96 | 122 | 99 | 91 | 70 | 94 |  |
|  | $\mathbf{- 1}$ | 80 | 85 | 28 | 26 | REF | 64 |  |
|  | $\mathbf{0}$ | $\mathrm{~N} / \mathrm{A}$ | 83 | 34 | 43 | 16 |  |  |
|  | $\mathbf{+ 1}$ | 97 | 95 | 45 | 49 | 41 |  |  |
|  | $\mathbf{+ 2}$ | 79 | 113 | 88 | 103 | 102 |  |  |

## THEORY OF OPERATION

The ADMV1013 is a wideband microwave upconverter optimized for microwave radio designs operating in the 24 GHz to 44 GHz RF frequency range. See Figure 1 for a functional block diagram of the device. The ADMV1013 digital settings are controlled via the SPI. The ADMV1013 has two modes of operation:

- Baseband quadrature modulation (I/Q mode)
- Single-sideband upconversion (IF mode)


## START-UP SEQUENCE

To use the voltage control RF VVA1 and RF VVA2, the VCC_VVA ( 1.8 V ) supply must be on. The VCTRL1 pin and VCTRL2 pin control the gain of the RF VVA1 and the RF VVA2. Similarly, to use the SPI control, it is necessary to first turn on DVDD and then perform a hard reset by toggling the RST pin to logic low and then to logic high.
The ADMV1013 SPI settings require the default settings to be changed during startup for optimum performance.

Set Register 0x0A to 0xE700 after each power-up or reset.

## BASEBAND QUADRATURE MODULATION (I/Q MODE)

In I/Q mode, the input impedance of the baseband pins (I_P, I_N, Q_P, and Q_N) are $100 \Omega$ differential. These inputs can be loaded with a dc-coupled $100 \Omega$ differential load. I_P and I_N are the differential baseband I inputs, and Q_P and Q_N are the differential baseband Q inputs. These inputs can operate from a $\mathrm{V}_{\mathrm{Cм}}$ of 0 V to 2.6 V . The baseband I/Q ports can operate from dc to 6.0 GHz at each I and Q channel.

To set the ADMV1013 in I/Q mode, set MIXER_IF_EN bit (Register 0x03, Bit 7) to 0 .

When changing the external $\mathrm{V}_{\mathrm{CM}}$, the internal mixer gate voltage also must be changed. To make this change, set the MIXER_VGATE bits (Register 0x05, Bits[6:0]). The MIXER_ VGATE value follows the $\mathrm{V}_{\mathrm{Cm}}$ such as, that for a 0 V to 1.8 V $\mathrm{V}_{\mathrm{CM}}$, MIXER_VGATE $=23.89 \mathrm{~V}_{\mathrm{CM}}+81$, and for $\mathrm{a}>1.8 \mathrm{~V}$ to $2.6 \mathrm{~V} \mathrm{~V}_{\text {См }}$, MIXER_VGATE $=23.75 \mathrm{~V}_{\text {См }}+1.25$.

## SINGLE-SIDEBAND UPCONVERSION (IF MODE)

The ADMV1013 features the ability to upconvert a real IF input anywhere from 0.8 GHz to 6.0 GHz while suppressing the unwanted sideband by typically better than 26 dBc . The IF inputs are quadrature to each other, $50 \Omega$ single ended, and are internally dc-coupled. IF_I and IF_Q are the quadrature IF inputs. An external $90^{\circ}$ hybrid is required to select the appropriate sideband. To configure the ADMV1013 in IF mode, set the MIXER_IF_EN bit (Register 0x03, Bit 7) to 1. The MIXER_IF_EN bit defaults to IF mode on SPI startup and reset.
In addition, the baseband pins (I_P, I_N, Q_P, and Q_N) must see an open load for optimum performance in IF mode.

## LO INPUT PATH

The LO input path operates from 5.4 GHz to 10.25 GHz with an LO amplitude range of -6 dBm to +6 dBm . The LO has an internal quadrupler ( $\times 4$ ) and a programmable band-pass filter. The LO band-pass filter is programmable using the QUAD_ FILTERS bits (Register 0x09, Bits[3:0]). See the Performance at Different Quad Filter Settings section for more information on the QUAD_FILTERS settings.

The LO path can operate either differentially or single ended. LOP and LON are the inputs to the LO path. The LO path can switch from differential to single-ended operation by setting the QUAD_SE_MODE bits (Register 0x09, Bits[9:6]). See the Performance Between Differential vs. Single-Ended LO Input section for more information. When using the LO as single ended, the unused LO input pin must be terminated with a $50 \Omega$ load.

Figure 81 shows a block diagram of the LO path.


Figure 81. LO Path Block Diagram
Enable the quadrupler by setting the QUAD_PD bits (Register 0x03, Bits[13:11]) to 0x0. To power down the quadrupler, set these bits to $0 \times 7$.

## SIDEBAND SUPPRESSION OPTIMIZATION

Unwanted sideband can be upconverted from the quadrature error by generating the quadrature LO signals and the external quadrature inputs. Deviation from ideal quadrature (that is, total sideband rejection and no sideband tone upconverts) on these signals limits the amount of achievable sideband rejection.
The ADMV 1013 offers approximately $25^{\circ}$ of quadrature phase adjustment in the LO path quadrature signals to suppress the sideband. Make these adjustments through the LOAMP_PH_ ADJ_I_FINE bits (Register 0x05, Bits[13:7]) and the LOAMP_ PH_ADJ_Q_FINE bits (Register 0x06, Bits[13:7]). These bits reject the unwanted sideband signal. To achieve the required sideband suppression, it may be necessary to adjust the amplitude difference between the quadrature inputs, as well externally.
In I/Q mode, the recommendation is to adjust the sideband suppression through the external transceiver digital-to-analog converter (DAC).

## CARRIER FEEDTHROUGH NULLING

Carrier feedthrough results from minute dc offsets that occur on the internal mixer. In an I/Q modulator, nonzero differential offsets mix with the LO and result in carrier feedthrough to the RF output. In addition to this effect, some of the signal power at the LO input couples directly to the RF output (this may be because of the bond wire to bond wire coupling or coupling through the silicon substrate). The net carrier feedthrough at the RF output is the vector combination of the signals that appear at the output because of these two effects.
The ADMV 1013 offers, in IF mode, LO feedthrough offset calibration adjustment in the LO path. Make these adjustments through the MXER_OFF_ADJ_I_N bits (Register 0x07, Bits[8:2], the MXER_OFF_ADJ_I_P bits (Register 0x07, Bits[15:9]), the MXER_OFF_ADJ_Q_N bits (Register 0x08, Bits[8:2]), and the MXER_OFF_ADJ_Q_P bits (Register 0x08, Bits[15:9] in order to reject the unwanted LO signal.

For I/Q mode, the LO feedthrough offset amplitude and phase calibration optimization can be adjusted externally through a transceiver DAC.

## ENVELOPE DETECTOR

The ADMV1013 features an envelope detector with a pseudo differential voltage output. The envelope detector output pins are VENV_P and VENV_N. The ADMV1013 turns on with the envelope detector turned off. To turn on the envelope detector, set the DET_EN bit (Bit 5, Register 0x03). The differential voltage output of the envelope detector rises linearly to the square of the input envelope voltage to the detector. The detector output ranges from -45 dBm to -20 dBm when the input two tone power ranges from -20 dBm to 0 dBm . The envelope detector has $350 \mathrm{MHz}, 3 \mathrm{~dB}$ envelope bandwidth and $1 \mathrm{GHz}, 10 \mathrm{~dB}$ envelope bandwidth. The envelope detector precedes the VVA and the output driver of the ADMV1013.

## POWER DOWN AND RESET

The SPI of the ADMV1013 allows the user to power down the device circuits and reduce power consumption to typically 77 mW . To turn off the entire chip, set the BG_PD bit (Register 0x03, Bit 10) to 1 . In addition, individual blocks of the circuit can be powered down individually. To power down the quadrupler, set the QUAD_PD bits (Register 0x03, Bits[13:11]) to 0x7. To power down the VGA, set the VGA_PD bit (Register 0x03, Bit 15) to 1 . To power down the mixer, set the MIXER_PD bit (Register 0x03, Bit 14) to 1 . To power down the detector, set the DET_EN bit (Register 0x03, Bit 5) to 0.

## SERIAL PORT INTERFACE (SPI)

The SPI of the ADMV1013 allows the user to configure the device for specific functions or operations via a 4 -wire SPI port. This interface provides users with added flexibility and customization. The SPI consists of four control lines: SCLK, SDI, SDO, and active low chip select lines, $\overline{\mathrm{SEN}} / \overline{\mathrm{SEN} 2}$. $\overline{\mathrm{SEN}}$ and $\overline{\mathrm{SEN} 2}$ must be connected together.

The ADMV1013 protocol consists of a write/read bit followed by six register address bits, 16 data bits, and a parity bit. Both the address and data fields are organized MSB first and end with the LSB. For a write, set the first bit to 0 . For a read, set the first bit to 1 .

The write cycle sampling must be performed on the rising edge. The 16 bits of the serial write data are shifted in, MSB to lower sideband. The ADMV1013 input logic level for the write cycle supports a 1.8 V interface.
For a read cycle, up to 16 bits of serial read data are shifted out, MSB first. After the 16 bits of data shift out, the parity bit shifts out. The output logic level for a read cycle is 1.8 V .
The parity bit always follows the direction of the data. If parity is not used, the transmitting end transmits zero instead of parity. The parity is odd, which means that the total number of ones transmitted during a command, including the read/write bit, the address bit, the data bit, and the parity bit, must be odd.
Figure 82 and Figure 83 show the SPI write and read protocol, respectively.



## APPLICATIONS INFORMATION

## BASEBAND QUADRATURE MODULATION FROM LOW FREQUENCIES

Figure 84 shows the I/Q mode performance at low baseband input frequencies. The measurements were performed at 28 $\mathrm{GHz},-10 \mathrm{dBm}$ input power, $\mathrm{V}_{\mathrm{CM}}=0 \mathrm{~V}$, Register 0x03, Bit $7=0$, 0 dBm LO input power, and $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.


Figure 84. Conversion Gain and Sideband Rejection vs. Baseband Frequency

## PERFORMANCE AT DIFFERENT QUAD FILTER SETTINGS

Figure 85 shows the conversion gain vs. RF frequency in IF mode at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ and LO input power $=0 \mathrm{dBm}$ for different QUAD_FILTERS settings.


Figure 85. Conversion Gain vs. RF Frequency for Four Different QUAD_FILTERS Settings, $\mathrm{f}_{\mathrm{IF}}=3.5 \mathrm{GHz}$ (Upper Sideband)

Figure 86 shows the $4 \times$ LO to RF leakage vs. $4 \times$ LO frequency at different quad filter settings.


Figure $86.4 \times$ LO to RF Leakage vs. $4 \times$ LO Frequency for Four Different QUAD_FILTERS Settings

## VVA TEMPERATURE COMPENSATION

Figure 87 shows the conversion gain vs. RF frequency at two different Register $0 x 0 \mathrm{~A}$ settings, the recommended setting ( 0 xE 700 ) and a setting for higher gain, and three different temperatures for IF mode. The recommended value suggested in the Start-Up Sequence section provides the least variation in conversion gain over temperature. If the priority is to increase the conversion gain, Register $0 x 0 \mathrm{~A}$ can be set to 0 xFA 00 . However, at this value, the conversion gain variation over temperature can increase by 2 dB .


Figure 87. Conversion Gain vs. RF Frequency at Maximum Gain for Various Temperatures and Register 0x0A Settings (Recommended and Higher Gain Setting), $f_{I F}=3.5 \mathrm{GHz}$

Figure 88 shows the conversion gain vs. RF frequency at two different Register 0x0A settings, the recommended setting and the default setting, and three different temperatures for IF mode. The default values provides slightly less gain and a larger gain variation across temperature compared to the recommended setting.


Figure 88. Conversion Gain vs. RF Frequency at Maximum Gain for Various Temperatures and Register 0x0A Settings (Default and Recommended Register 0x0A Settings), $f_{I F}=2$ GHz

## PERFORMANCE BETWEEN DIFFERENTIAL vs. SINGLE-ENDED LO INPUT

Figure 89 to Figure 91 show the conversion gain, output IP3, and sideband rejection performance for operating the ADMV1013 LO input as differential vs. single ended. The measurements were performed with 0 dBm LO input power, IF mode, with an IF frequency of 3.5 GHz , upper sideband, and $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.


Figure 89. Conversion Gain vs. RF Frequency for Three Different LO Mode Settings, $f_{\text {IF }}=3.5 \mathrm{GHz}$ (Upper Sideband)


Figure 90. Output IP3 vs. RF Frequency for Three Different LO Mode Settings, RF Amplitude $=-20 \mathrm{dBm}$ per Tone at 20 MHz Spacing, $f_{\text {IF }}=3.5 \mathrm{GHz}$ (Upper Sideband)


Figure 91. Sideband Rejection vs. RF Frequency for Three Different LO Mode Settings, RF Amplitude $=-30 \mathrm{dBm}$ per Tone at 20 MHz Spacing, $f_{\text {IF }}=3.5 \mathrm{GHz}$ (Upper Sideband)

## PERFORMANCE ACROSS RF FREQUENCY AT FIXED INPUT FREQUENCIES

The ADMV1013 quadrupler operates from 21.6 GHz to 41 GHz . When using the lower sideband, the conversion gain starts rolling off gradually after the quadrupler frequency reaches 41 GHz . When using the upper sideband, the conversion gain starts rolling off when the quadrupler frequency is 21.6 GHz .

Figure 92 and Figure 93 show the conversion gain vs. RF frequency in IF mode for fixed IF frequencies $\left(\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{LO}=0 \mathrm{dBm}\right.$ ) for the upper sideband and lower sideband, respectively.


Figure 92. Conversion Gain vs. RF Frequency for Multiple IF Frequency Settings (Upper Sideband)


Figure 93. Conversion Gain vs. RF Frequency at Multiple IF Frequency Settings (Lower Sideband)

Figure 94 and Figure 95 show the conversion gain vs. RF frequency in I/Q mode for multiple baseband (BB) frequencies ( $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{LO}=0 \mathrm{dBm}$ ) for upper sideband and lower sideband, respectively.


Figure 94. Conversion Gain vs. RF Frequency for Multiple Baseband Frequency Settings (Upper Sideband)


Figure 95. Conversion Gain vs. RF Frequency at Multiple Baseband Frequency Settings (Lower Sideband)

## PERFORMANCE ACROSS COMMON-MODE VOLTAGE IN I/Q MODE

Figure 96, Figure 97, and Figure 98 show the performance at various common-mode voltages in I/Q mode. For each common-mode voltage, the mixer gate voltage was changed based on the equation described in the Baseband Quadrature Modulation (I/Q Mode) section.


Figure 96. Conversion Gain vs. RF Frequency at Multiple Common-Mode Voltages in I/Q Mode ( $f_{B B}=100 \mathrm{MHz}, L O=0 \mathrm{dBm}, T_{A}=25^{\circ} \mathrm{C}$ )


Figure 97. Output IP3 vs. RF Frequency at Multiple Common-Mode Voltages in $I / Q$ Mode ( $f_{B B}=100 \mathrm{MHz}, L O=0 \mathrm{dBm}, T_{A}=25^{\circ} \mathrm{C}$ )


Figure 98. Output P1dB vs. RF Frequency at Multiple Common-Mode Voltages in I/Q Mode ( $f_{B B}=100 \mathrm{MHz}, L O=0 \mathrm{dBm}, T_{A}=25^{\circ} \mathrm{C}$ )

## OPERATING VCTRL1 AND VCTRL2 INDEPENDENTLY

The data shown in the Specifications section and the Typical Performance Characteristics section is based on the VCTRL1 and VCTRL2 voltages being equal. Finer gain regulation can be obtained if VCTRL1 and VCTRL2 are used separately. Operating VCTRL1 and VCTRL2 also allows either maintaining IP3 or noise figure performance while attenuating the RF output.

Figure 99, Figure 102, and Figure 105 show the conversion gain, input IP3, and noise figure vs. the RF frequency, respectively ( $\mathrm{IF}=$ 2 GHz , upper sideband, $\mathrm{LO}=0 \mathrm{dBm}$ at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ), when VCTRL1 is equal to VCTRL2.
Figure 100, Figure 103, and Figure 106 show the conversion gain, input IP3, and noise figure vs. the RF frequency, respectively ( $\mathrm{IF}=2 \mathrm{GHz}$, upper sideband, $\mathrm{LO}=0 \mathrm{dBm}$ at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ), when VCTRL2 is held at a minimum attenuation and VCTRL1 is changed.
Figure 101, Figure 104, and Figure 107 show the conversion gain, input IP3, and noise figure vs. the RF frequency, respectively ( $\mathrm{IF}=2 \mathrm{GHz}$, upper sideband, $\mathrm{LO}=0 \mathrm{dBm}$ at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ), when VCTRL1 is held at minimum attenuation and VCTRL2 is changed.


Figure 99. Conversion Gain vs. RF Frequency at Various VCTRL Voltages (VCTRL1 = VCTRL2), IF Mode, IF Frequency $=2$ GHz, Upper Sideband


Figure 100. Conversion Gain vs. RF Frequency at Various VCTRL1 Voltages (VCTRL2 $=1.8$ V), IF Mode, IF Frequency $=2 \mathrm{GHz}$, Upper Sideband


Figure 101. Conversion Gain vs. RF Frequency at Various VCTRL2 Voltages (VCTRL1 = 1.8 V), IF Mode, IF Frequency $=2$ GHz, Upper Sideband


Figure 102. Input IP3 vs. RF Frequency at Various V CTRL Voltages (VCTRL1 $=$ VCTRL2), IIF Mode, IF Frequency $=2 \mathrm{GHz}$, Upper Sideband


Figure 103. Input IP3 vs. RF Frequency at Various VCTRL1 Voltages (VCTRL2 $=$ 1.8 V), IF Mode, IF Frequency = 2 GHz, Upper Sideband


Figure 104. Input IP3 vs. RF Frequency at Various VCTRL2 Voltages (VCTRL1 $=$ 1.8 V), IF Mode, IF Frequency $=2$ GHz, Upper Sideband


Figure 105. Noise Figure vs. RF Frequency at Various $V_{\text {CTRL }}$ Voltages $($ VCTRL $1=$ VCTRL2), IF Mode, IF Frequency $=2$ GHz, Upper Sideband


Figure 106. Noise Figure vs. RF Frequency at Various VCTRL 1 Voltages (VCTRL2 $=1.8$ V), IF Mode, IF Frequency $=2 \mathrm{GHz}$, Upper Sideband


Figure 107. Noise Figure vs. RF Frequency at Various VCTRL2 Voltages (VCTRL1 = 1.8 V), IF Mode, IF Frequency $=2 \mathrm{GHz}$, Upper Sideband

## RECOMMENDED LAND PATTERN

Solder the exposed pad on the underside of the ADMV1013 to a low thermal and electrical impedance ground plane. This pad is typically soldered to an exposed opening in the solder mask on the evaluation board. Connect these ground vias to all other ground layers on the evaluation board to maximize heat dissipation from the device package.


Figure 108. Evaluation Board Layout for the LGA Package

## EVALUATION BOARD INFORMATION

For more information about the ADMV1013 evaluation board, refer to the ADMV1013-EVALZ user guide.

## ADMV1013

## REGISTER SUMMARY

Table 6.


## REGISTER DETAILS

Address: 0x00, Reset: 0x00A4, Name: SPI_CONTROL


Table 7. Bit Descriptions for SPI_CONTROL

| Bits | Bit Name | Settings | Description | Reset | Access |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 15 | PARITY_EN |  | Enable the Parity for Write Execution | $0 \times 0$ | R/W |
| 14 | SPI_SOFT_RESET |  | SPI Soft Reset | $0 \times 0$ | R/W |
| $[13: 12]$ | RESERVED |  | Reserved | Chip ID | $0 \times 0$ |
| $[11: 4]$ | CHIP_ID |  | Revision ID | R |  |
| $[3: 0]$ | REVISION |  | $0 \times 4$ | R |  |

Address: 0x01, Reset: 0x0000, Name: ALARM


Table 8. Bit Descriptions for ALARM

| Bits | Bit Name | Settings | Description | Reset | Access |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 15 | PARITY_ERROR |  | Parity Error | $0 \times 0$ | R |
| 14 | TOO_FEW_ERRORS |  | Too Few Errors | $0 \times 0$ | R |
| 13 | TOO_MANY_ERRORS |  | Too Many Errors | $0 \times 0$ | R |
| 12 | ADDRESS_RANGE_ERRO <br> R | Address Range Error | $0 \times 0$ | R |  |
| $[11: 0]$ | RESERVED |  | Reserved | $0 \times 0$ | R |

Address: 0x02, Reset: 0xFFFF, Name: ALARM_MASKS


Table 9. Bit Descriptions for ALARM_MASKS

| Bits | Bit Name | Settings | Description | Reset | Access |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 15 | PARITY_ERROR_MASK |  | Parity Error Mask | R/W |  |
| 14 | TOO_FEW_ERRORS_MASK |  | Too Few Errors Mask | $0 \times 1$ | $0 \times 1$ |
| 13 | TOO_MANY_ERRORS_MASK |  | Too Many Errors Mask | R/W |  |
| 12 | ADDRESS_RANGE_ERROR_MASK |  | Address Range Error Mask | R/W |  |
| $[11: 0]$ | RESERVED |  | Reserved | R/W |  |

## ADMV1013

## Address: 0x03, Reset: 0x01D7, Name: ENABLE



Table 10. Bit Descriptions for ENABLE

| Bits | Bit Name | Settings | Description | Reset | Access |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | VGA_PD |  | Power Down the VGA Circuit | 0x0 | R/W |
| 14 | MIXER_PD |  | Power Down the Mixer Circuit | 0x0 | R/W |
| [13:11] | QUAD_PD | $\begin{aligned} & 000 \\ & 111 \end{aligned}$ | Power Down the Quad Enable LO Quad Circuit Disable LO Quad Circuit | 0x0 | R/W |
| 10 | BG_PD |  | Power Down the Transmitter Band Gap | 0x0 | R/W |
| [9:8] | RESERVED |  | Reserved | 0x0 | R |
| 7 | MIXER_IF_EN |  | Enable the IF Mode | 0x1 | R/W |
| 6 | RESERVED |  | Reserved | 0x1 | R |
| 5 | DET_EN |  | Enable the Envelope Detector | 0x0 | R/W |
| [4:0] | RESERVED |  | Reserved | $0 \times 17$ | R |

Address: 0x05, Reset: 0x5051, Name: LO_AMP_I

| 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | 1 | 0 |  | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 |




Table 11. Bit Descriptions for LO_AMP_I

| Bits | Bit Name | Settings | Description | Reset | Access |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $[15: 14]$ | RESERVED |  | Reserved. | $0 \times 1$ | R |
| $[13: 7]$ | LOAMP_PH_ADJ_I_FINE |  | Mixer Image Rejection Calibration. | $0 \times 20$ | R/W |
| $[6: 0]$ | MIXER_VGATE |  | Control Mixer Gate Voltage. For 0 V to 1.8V, MIXER_VGATE $=23.89 \times$ <br> Common-Mode Voltage + 81, and for 1.8 V to 2.6 V, MIXER_VGATE $=$ <br> $23.75 \times$ Common-Mode Voltage +1.25. | $0 \times 51$ | R/W |

Address: 0x06, Reset: $0 \times 5000$, Name: LO_AMP_Q


Table 12. Bit Descriptions for LO_AMP_Q

| Bits | Bit Name | Settings | Description | Reset | Access |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $[15: 14]$ | RESERVED |  | Reserved | $0 \times 1$ | R |
| $[13: 7]$ | LOAMP_PH_ADJ_Q_FINE |  | Mixer Image Rejection Calibration | $0 \times 20$ | R/W |
| $[6: 0]$ | RESERVED |  | Reserved | $0 \times 0$ | R |

Address: 0x07, Reset: 0xFFFC, Name: OFFSET_ADJUST_I


Table 13. Bit Descriptions for OFFSET_ADJUST_I

| Bits | Bit Name | Settings | Description | Reset | Access |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $[15: 9]$ | MXER_OFF_ADJ_I_P |  | LO Feedthrough Offset Calibration I Positive for IF Mode | 0x7F | R/W |
| $[8: 2]$ | MXER_OFF_ADJ_I_N |  | LO Feedthrough Offset Calibration I Negative for IF Mode | $0 \times 7 \mathrm{~F}$ | R/W |
| $[1: 0]$ | RESERVED |  | Reserved | $0 \times 0$ | R |

Address: 0x08, Reset: 0xFFFC, Name: OFFSET_ADJUST_Q


Table 14. Bit Descriptions for OFFSET_ADJUST_Q

| Bits | Bit Name | Settings | Description | Reset | Access |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $[15: 9]$ | MXER_OFF_ADJ_Q_P |  | LO Feedthrough Offset Calibration Q Positive for IF Mode | $0 \times 7 \mathrm{~F}$ | R/W |
| $[8: 2]$ | MXER_OFF_ADJ_Q_N |  | LO Feedthrough Offset Calibration Q Negative for IF Mode | $0 \times 7 \mathrm{~F}$ | R/W |
| $[1: 0]$ | RESERVED |  | Reserved | $0 \times 0$ | R |

Address: 0x09, Reset: 0x5700, Name: QUAD


Table 15. Bit Descriptions for QUAD

| Bits | Bit Name | Settings | Description | Reset | Access |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $[15: 10]$ | RESERVED |  | Reserved. | 0x15 | R |
| $[9: 6]$ | QUAD_SE_MODE |  | Switch Differential/Single-Ended Modes. | OxC | R/W |
|  |  | 0110 | Single-Ended Mode, Negative Side Disable. <br> Single-Ended Mode, Positive Side Disable. <br>  | 1001 | 1100 |
|  |  | Differential Mode. |  |  |  |
| $[5: 4]$ | RESERVED |  | LO Filters Bandwidth Selection. | $0 \times 0$ | R |
| $[3: 0]$ | QUAD_FILTERS | 0000 | LO Frequency Bandwidth: 8.62 GHz to 10.25 GHz. | $0 \times 0$ | R/W |
|  |  | 0101 | LO Frequency Bandwidth: 6.6 GHz to 9.2 GHz. |  |  |
|  |  | 1010 | LO Frequency Bandwidth: 5.4 GHz to 8 GHz. |  |  |
|  |  | 1111 | LO Frequency Bandwidth: 5.4 GHz to 7 GHz. |  |  |

## ADMV1013

Address: 0x0A, Reset: 0x0000, Name: VVA_TEMPERATURE_COMPENSATION


Table 16. Bit Descriptions for VVA_TEMPERATURE_COMPENSATION

| Bits | Bit Name | Settings | Description | Reset | Access |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $[15: 0]$ | VVA_TEMPERATURE_COMPENSATION |  | VVA Temperature Compensation. PARITY_EN must be <br> disabled when updating the VVA temperature <br> compensation. Set to 0xE700 on startup. | 0x0 | R/W |

## OUTLINE DIMENSIONS



Figure 109. 40-Terminal Land Grid Array Package [LGA]
$6 \mathrm{~mm} \times 6 \mathrm{~mm}$ Body and 0.67 mm Package Height (CC-40-5)
Dimensions shown in millimeters

ORDERING GUIDE

| Model $^{1}$ | Temperature Range | Package Description | Package Option |
| :--- | :--- | :--- | :--- |
| ADMV1013ACCZ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 40 -Terminal Land Grid Array Package [LGA] | CC-40-5 |
| ADMV1013ACCZ-R7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 40 -Terminal Land Grid Array Package [LGA] | CC-40-5 |
| ADMV1013-EVALZ |  | Evaluation Board |  |

[^0]
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AD9957BSVZ AD9957BSVZ-REEL ADMV1009AEZ ADMV1010AEZ ADMV1011AEZ ADMV1012AEZ ADRF6658BCPZ
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HMC967LP4E HMC977LP4E AD6634BBC HMC6505ALC5 MAUC-011003-TR0500 MAX9996ETP+T MAX19996AETP+
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[^0]:    ${ }^{1} Z=$ RoHS Compliant Part.

