

## High Linearity, Low Power Downconverting Mixer

### **FEATURES**

- Operation up to 2GHz
- Broadband RF, LO and IF Operation
- High Input IP3: +16.5dBm at 900MHz
- Typical Conversion Gain: 0.6dB at 900MHz
- SSB Noise Figure: 11dB at 900MHz
- On-Chip  $50\Omega$  LO Match
- Integrated LO Buffer: -5dBm Drive Level
- High LO-RF and LO-IF Isolation
- Low Supply Current: 28mA Typ
- Enable Function
- Single 5V Supply
- 16-Lead QFN (4mm × 4mm) Package

#### **APPLICATIONS**

- Point-to-Point Data Communication Systems
- Wireless Infrastructure
- Cable Downlink Infrastructure
- High Linearity Receiver Applications

### DESCRIPTION

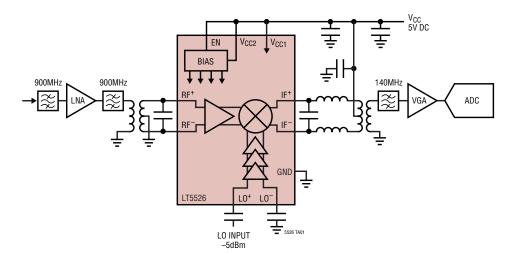
The LT®5526 is a low power broadband mixer optimized for high linearity applications such as point-to-point data transmission, cable infrastructure and wireless infrastructure systems. The device includes an internally matched high speed LO amplifier driving a double-balanced active mixer core. An integrated RF buffer amplifier provides excellent LO-RF isolation. The RF and IF ports can be easily matched across a broad range of frequencies for use in a wide variety of applications.

The LT5526 offers a high performance alternative to passive mixers. Unlike passive mixers which have conversion loss and require high LO drive levels, the LT5526 delivers conversion gain at significantly lower LO input levels and is much less sensitive to LO power level variations.

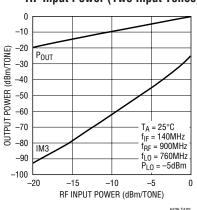
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## TYPICAL APPLICATION

#### High Signal Level Frequency Downconversion



### IF Output Power and IM3 vs RF Input Power (Two Input Tones)



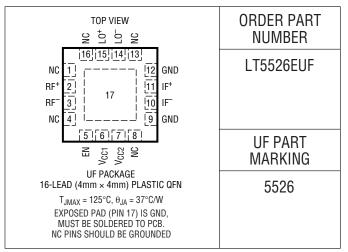
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## **ABSOLUTE MAXIMUM RATINGS**

| (Note 1)                               |                            |
|--|----------------------------|
| Supply Voltage                         | 5.5V                       |
| Enable Voltage                         | $-0.3V$ to $V_{CC} + 0.3V$ |
| LO Input Power                         | +10dBm                     |
| LO+ to LO- Differential DC Voltage .   | ±1V                        |
| RF Input Power                         | +10dBm                     |
| RF+ to RF- Differential DC Voltage     | ±0.7V                      |
| Operating Temperature Range            | – 40°C to 85°C             |
| Storage Temperature Range              | 65°C to 125°C              |
| Junction Temperature (T <sub>J</sub> ) | 125°C                      |

## PACKAGE/ORDER INFORMATION



Consult LTC Marketing for parts specified with wider operating temperature ranges.

## DC ELECTRICAL CHARACTERISTICS

 $V_{CC}$  = 5V, EN = 3V,  $T_A$  = 25°C (Note 3), unless otherwise noted. Test circuit shown in Figure 1.

| PARAMETER                                    | CONDITIONS           | MIN | TYP        | MAX | UNITS    |
|--|----------------------|-----|------------|-----|----------|
| Power Supply Requirements (V <sub>CC</sub> ) | ·                    |     |            |     |          |
| Supply Voltage                               |                      | 3.6 | 5          | 5.3 | V        |
| Supply Current                               | V <sub>CC</sub> = 5V |     | 28         | 33  | mA       |
| Shutdown Current                             | EN = Low             |     |            | 100 | μА       |
| Enable (EN) Low = Off, High = On             |                      | ·   |            |     |          |
| EN Input High Voltage (On)                   |                      | 3   |            |     | V        |
| EN Input Low Voltage (Off)                   |                      |     |            | 0.3 | V        |
| Enable Pin Input Current                     | EN = 5V<br>EN = 0V   |     | 55<br>0.01 |     | μΑ<br>μΑ |
| Turn-On Time (Note 5)                        |                      |     | 3          |     | μS       |
| Turn-Off Time (Note 5)                       |                      |     | 6          |     | μS       |

## AC ELECTRICAL CHARACTERISTICS (Notes 2, 3)

| PARAMETER                          | CONDITIONS           | MIN | TYP         | MAX | UNITS |
|------------------------------------|----------------------|-----|-------------|-----|-------|
| RF Input Frequency Range (Note 4)  | Requires RF Matching |     | 0.1 to 2000 |     | MHz   |
| LO Input Frequency Range (Note 4)  | Requires DC Blocks   |     | 0.1 to 2500 |     | MHz   |
| IF Output Frequency Range (Note 4) | Requires IF Matching |     | 0.1 to 1000 |     | MHz   |

#### $V_{CC}$ = 5V, EN = 3V, $T_A$ = 25°C. Test circuits shown in Figures 1 and 2. (Notes 2, 3)

| PARAMETER             | CONDITIONS                            | MIN | TYP      | MAX | UNITS |
|-----------------------|---------------------------------------|-----|----------|-----|-------|
| RF Input Return Loss  | $Z_0 = 50\Omega$ , External Match     |     | 15       |     | dB    |
| LO Input Return Loss  | $Z_0 = 50\Omega$ , External DC Blocks |     | 15       |     | dB    |
| IF Output Return Loss | $Z_0 = 50\Omega$ , External Match     |     | 15       |     | dB    |
| LO Input Power        |                                       |     | -10 to 0 |     | dBm   |



## **AC ELECTRICAL CHARACTERISTICS** $V_{CC} = 5V$ , EN = 3V, $T_A = 25^{\circ}C$ , $P_{RF} = -15 dBm$ (-15 dBm/tone for 2-tone IIP3 tests, $\Delta f = 1 MHz$ ), $P_{LO} = -5 dBm$ , unless otherwise noted. Test circuits shown in Figures 1 and 2. (Notes 2, 3)

| PARAMETER                        | CONDITIONS  | MIN TYP | MAX | UNITS |
|----------------------------------|---|---------|-----|-------|
| RF to LO Isolation               | f <sub>RF</sub> = 350MHz, f <sub>IF</sub> = 70MHz, f <sub>LO</sub> = 420MHz | 69      |     | dB    |
|                                  | $f_{RF} = 900MHz$ , $f_{IF} = 140MHz$ , $f_{LO} = 760MHz$                   | 55      |     | dB    |
|                                  | $f_{RF} = 1900MHz$ , $f_{IF} = 140MHz$ , $f_{LO} = 1760MHz$                 | 50      |     | dB    |
| Conversion Gain                  | $f_{RF} = 350MHz$ , $f_{IF} = 70MHz$ , $f_{LO} = 420MHz$                    | 0.6     |     | dB    |
|                                  | $f_{RF} = 900MHz$ , $f_{IF} = 140MHz$ , $f_{LO} = 760MHz$                   | 0.6     |     | dB    |
|                                  | $f_{RF} = 1900MHz$ , $f_{IF} = 140MHz$ , $f_{LO} = 1760MHz$                 | 0.4     |     | dB    |
| Conversion Gain vs Temperature   | $T_A = -40$ °C to 85°C  | -0.013  |     | dB/°C |
| Input 3rd Order Intercept        | $f_{RF} = 350MHz$ , $f_{IF} = 70MHz$ , $f_{LO} = 420MHz$                    | 15.2    |     | dBm   |
|                                  | $f_{RF} = 900MHz$ , $f_{IF} = 140MHz$ , $f_{LO} = 760MHz$                   | 16.5    |     | dBm   |
|                                  | $f_{RF} = 1900MHz$ , $f_{IF} = 140MHz$ , $f_{LO} = 1760MHz$                 | 14.1    |     | dBm   |
| Single Sideband Noise Figure     | $f_{RF} = 350MHz$ , $f_{IF} = 70MHz$ , $f_{LO} = 420MHz$                    | 12.7    |     | dB    |
|                                  | $f_{RF} = 900MHz$ , $f_{IF} = 140MHz$ , $f_{LO} = 760MHz$                   | 11.0    |     | dB    |
|                                  | $f_{RF} = 1900MHz$ , $f_{IF} = 140MHz$ , $f_{LO} = 1760MHz$                 | 13.7    |     | dB    |
| LO to RF Leakage                 | $f_{RF} = 350MHz$ , $f_{IF} = 70MHz$ , $f_{LO} = 420MHz$                    | -65     |     | dBm   |
|                                  | $f_{RF} = 900MHz$ , $f_{IF} = 140MHz$ , $f_{LO} = 760MHz$                   | -65     |     | dBm   |
|                                  | $f_{RF} = 1900MHz$ , $f_{IF} = 140MHz$ , $f_{LO} = 1760MHz$                 | -55     |     | dBm   |
| LO to IF Leakage                 | $f_{RF} = 350MHz$ , $f_{IF} = 70MHz$ , $f_{LO} = 420MHz$                    | -56     |     | dBm   |
|                                  | $f_{RF} = 900MHz$ , $f_{IF} = 140MHz$ , $f_{LO} = 760MHz$                   | -74     |     | dBm   |
|                                  | $f_{RF} = 1900MHz$ , $f_{IF} = 140MHz$ , $f_{LO} = 1760MHz$                 | -37     |     | dBm   |
| 2RF-2LO Output Spurious Product  | 350MHz: $f_{RF} = 385MHz$ at $-15dBm$ , $f_{LO} = 420MHz$                   | -75     |     | dBc   |
| $(f_{RF} = f_{LO} \pm f_{IF}/2)$ | 900MHZ: $f_{RF} = 830MHz$ at $-15dBm$ , $f_{LO} = 760MHz$                   | -72     |     | dBc   |
|                                  | 1900MHz: $f_{RF} = 1830MHz$ at $-15dBm$ , $f_{LO} = 1760MHz$                | -48     |     | dBc   |
| 3RF-3LO Output Spurious Product  | 350MHz: $f_{RF} = 396.67MHz$ at $-15dBm$ , $f_{LO} = 420MHz$                | -65     |     | dBc   |
| $(f_{RF} = f_{LO} \pm f_{IF}/3)$ | 900MHZ: $f_{RF} = 806.67MHz$ at $-15dBm$ , $f_{LO} = 760MHz$                | -68     |     | dBc   |
|                                  | 1900MHz: $f_{RF} = 1806.67MHz$ at $-15dBm$ , $f_{LO} = 1760MHz$             | -56     |     | dBc   |
| Input 1dB Compression            | $f_{RF} = 350MHz$ , $f_{IF} = 70MHz$ , $f_{LO} = 420MHz$                    | 5       |     | dBm   |
|                                  | $f_{RF} = 900MHz$ , $f_{IF} = 140MHz$ , $f_{LO} = 760MHz$                   | 5       |     | dBm   |
|                                  | $f_{RF} = 1900MHz$ , $f_{IF} = 140MHz$ , $f_{LO} = 1760MHz$                 | 1       |     | dBm   |

**Note 1:** Absolute Maximum Ratings are those values beyond which the life of a device may be impaired.

**Note 2:** The 900MHz and 1900MHz performance is measured with the test circuit shown in Figure 1. The 350MHz performance is measured using the test circuit in Figure 2.

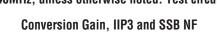
**Note 3:** Specifications over the  $-40^{\circ}$ C to  $85^{\circ}$ C temperature range are assured by design, characterization and correlation with statistical process controls.

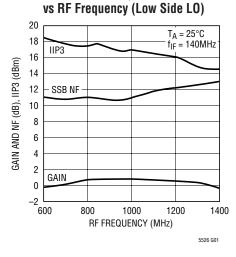
**Note 4:** Operation over a wider frequency range is possible with reduced performance. Consult the factory for information and assistance.

**Note 5:** Turn-on and turn-off times correspond to a change in the output level by 40dB.

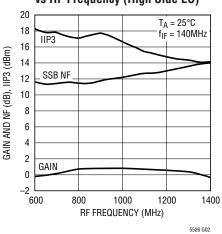


## **TYPICAL AC PERFORMANCE CHARACTERISTICS** 900MHz Application. $V_{CC}$ = 5V, EN = 3V, $T_A$ = 25°C, $P_{RF}$ = -15dB (-15dBm/tone for 2-tone IIP3 tests, $\Delta f$ = 1MHz), $f_{L0}$ = $f_{RF}$ - 140MHz, $P_{L0}$ = -5dBm, IF output measured at 140MHz, unless otherwise noted. Test circuit shown in Figure 1.

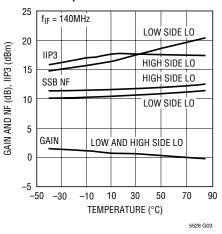




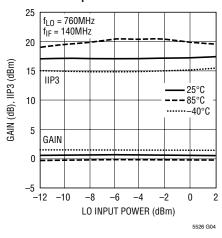
## Conversion Gain, IIP3 and SSB NF vs RF Frequency (High Side LO)



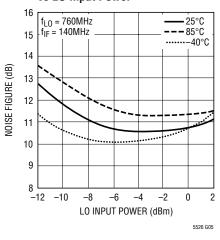
Conversion Gain, IIP3 and SSB NF vs Temperature



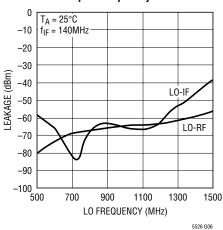
Conversion Gain and IIP3 vs LO Input Power



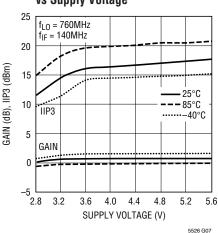
SSB Noise Figure vs LO Input Power



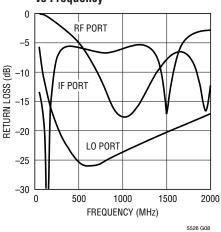
LO-IF and LO-RF Leakage vs LO Input Frequency



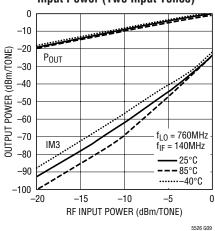
Conversion Gain and IIP3 vs Supply Voltage



RF, LO and IF Port Return Loss vs Frequency

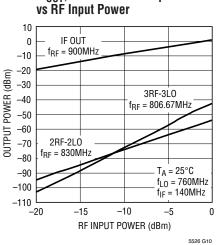


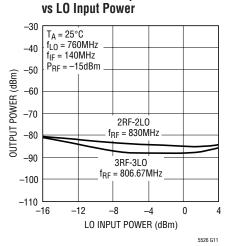
IF Output Power and IM3 vs RF Input Power (Two Input Tones)



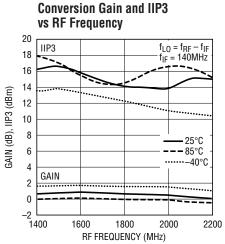
## TYPICAL AC PERFORMANCE CHARACTERISTICS 900MHz Application. $V_{CC}$ = 5V, EN = 3V, $T_A$ = 25°C, $P_{RF}$ = -15dB (-15dBm/tone for 2-tone IIP3 tests, $\Delta f$ = 1MHz), $f_{L0}$ = $f_{RF}$ - 140MHz, $P_{L0}$ = -5dBm, IF output measured at 140MHz, unless otherwise noted. Test circuit shown in Figure 1.

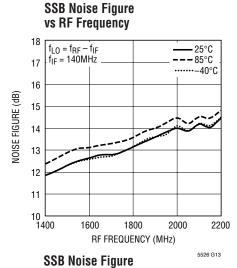
IF OUT,  $2 \times 2$  and  $3 \times 3$  Spurs  $2\times2$  and  $3\times3$  Spurs

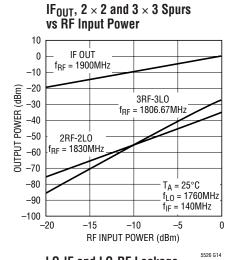


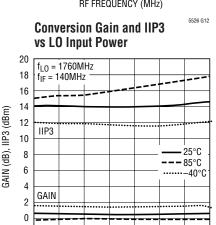


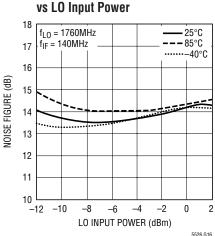
1900MHz Application.  $V_{CC}$  = 5V, EN = 3V,  $T_A$  = 25°C,  $P_{RF}$  = -15dB (-15dBm/tone for 2-tone IIP3 tests,  $\Delta f$  = 1MHz),  $f_{LO}$  =  $f_{RF}$  - 140MHz,  $P_{LO}$  = -5dBm, IF output measured at 140MHz, unless otherwise noted. Test circuit shown in Figure 1.

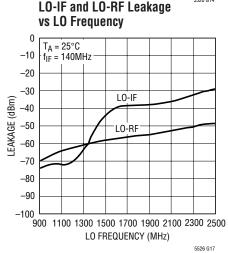












-10

-8

-6

LO INPUT POWER (dBm)

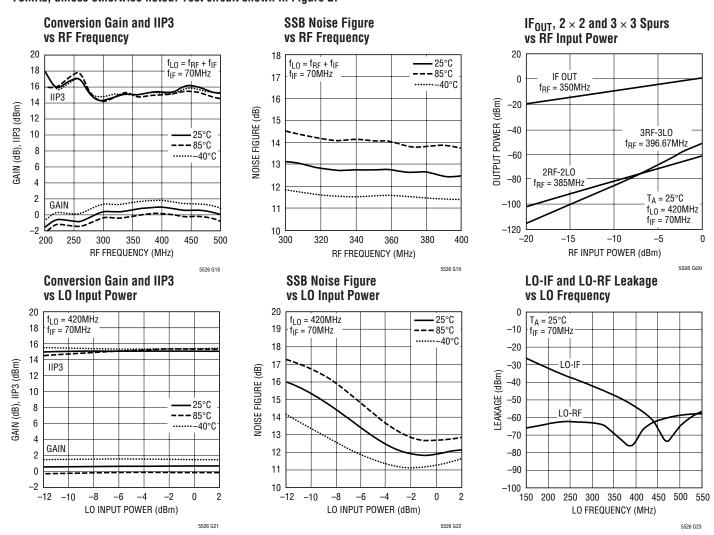
0 2

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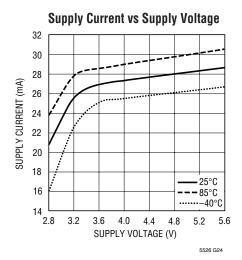
-2

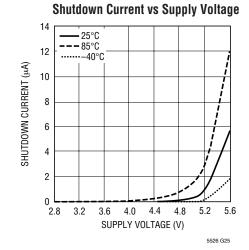
-12

# **TYPICAL AC PERFORMANCE CHARACTERISTICS** 350MHz Application. $V_{CC} = 5V$ , EN = 3V, $T_A = 25^{\circ}C$ , $P_{RF} = -15dB$ (-15dBm/tone for 2-tone IIP3 tests, $\triangle f = 1$ MHz), $f_{LO} = f_{RF} + 70$ MHz, $P_{LO} = -5dBm$ , IF output measured at 70MHz, unless otherwise noted. Test circuit shown in Figure 2.



## TYPICAL DC PERFORMANCE CHARACTERISTICS Test circuit shown in Figure 1.





TECHNOLOGY

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### PIN FUNCTIONS

**NC (Pins 1, 4, 8, 13, 16):** Not Connected Internally. These pins should be grounded on the circuit board for improved LO-to-RF and LO-to-IF isolation.

**RF**<sup>+</sup>, **RF**<sup>-</sup> (**Pins 2, 3**): Differential Inputs for the RF Signal. These pins must be driven with a differential signal. Each pin must also be connected to a DC ground capable of sinking 7.5mA (15mA total). This DC bias return can be accomplished through the center-tap of a balun or with shunt inductors. An impedance transformation is required to match the RF input to  $50\Omega$  (or  $75\Omega$ ).

**EN (Pin 5):** Enable Pin. When the input voltage is higher than 3V, the mixer circuits supplied through Pins 6, 7, 10 and 11 are enabled. When the input voltage is less than 0.3V, all circuits are disabled. Typical enable pin input current is  $55\mu$ A for EN = 5V and  $0.01\mu$ A when EN = 0V.

 $V_{CC1}$  (Pin 6): Power Supply Pin for the LO Buffer Circuits. Typical current consumption is 11mA. This pin should be externally connected to the other  $V_{CC}$  pins and decoupled with 100pF and 0.01 $\mu$ F capacitors.

 $V_{CC2}$  (Pin 7): Power Supply Pin for the Bias Circuits. Typical current consumption is 2.5mA. This pin should be externally connected to the other  $V_{CC}$  pins and decoupled with 100pF and 0.01 $\mu$ F capacitors.

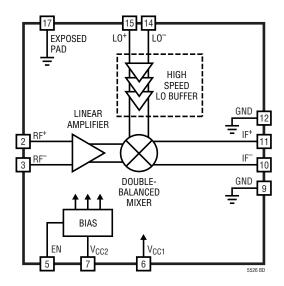
**GND** (Pins 9, 12): Ground. These pins are internally connected to the Exposed Pad for better isolation. They should be connected to ground on the circuit board, though they are not intended to replace the primary grounding through the Exposed Pad of the package.

**IF**<sup>-</sup> **and IF**<sup>+</sup> **(Pins 10, 11):** Differential Outputs for the IF Signal. An impedance transformation may be required to match the outputs. These pins must be connected to  $V_{CC}$  through impedance matching inductors, RF chokes or a transformer center-tap.

**LO**<sup>-</sup>, **LO**<sup>+</sup> (**Pins 14, 15**): Differential Inputs for the Local Oscillator Signal. The LO input is internally matched to  $50\Omega$ ; however, external DC blocking capacitors are required because these pins are internally biased to approximately 1.7V DC. Either LO input can be driven with a single-ended source while connecting the unused input to ground through a DC blocking capacitor.

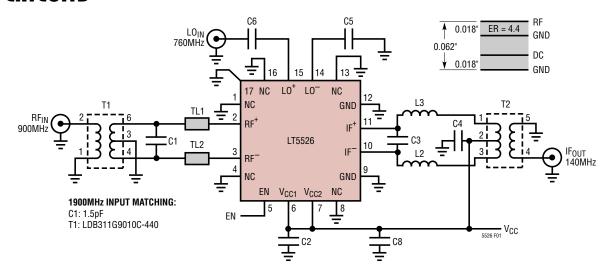
**Exposed Pad (Pin 17):** Circuit Ground Return for the Entire IC. This must be soldered to the printed circuit board ground plane.

## **BLOCK DIAGRAM**



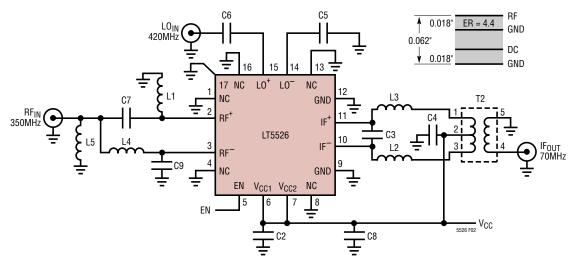


## **TEST CIRCUITS**



| REF DES    | VALUE  | SIZE | PART NUMBER               | REF DES  | VALUE               | SIZE       | PART NUMBER             |
|------------|--------|------|---------------------------|----------|---------------------|------------|-------------------------|
| C1         | 2.7pF  | 0402 | AVX 04025A2R7CAT          | L2, L3   | 150nH               | 1608       | Toko LL1608-FSR15J      |
| C2         | 0.01μF | 0402 | AVX 04023C103JAT          | T1       | 1:1                 | 1206       | Murata LDB31900M05C-417 |
| C3         | 1.2pF  | 0402 | AVX 04025A1R2BAT          | T2       | 4:1                 | SM-22      | M/A-COM ETC4-1-2        |
| C4, C5, C6 | 100pF  | 0402 | AVX 04025A101JAT          | TL1, TL2 | Z <sub>0</sub> = 80 | L = 1.25mm |                         |
| C8         | 1μF    | 0603 | Taiyo Yuden LMK107BJ105MA |          |                     |            |                         |

Figure 1. Test Schematic for 900MHz Application. For 1900MHz or Other Applications, Component Values Are as Indicated in Figure 1 and in Applications Section



| REF DES    | VALUE  | SIZE | PART NUMBER               | REF DES | VALUE | SIZE  | PART NUMBER        |
|------------|--------|------|---------------------------|---------|-------|-------|--------------------|
| C2         | 0.01pF | 0402 | AVX 04023C103JAT          | L1, L4  | 15nH  | 1005  | Toko LL1005-FH15NJ |
| C3         | 3.9pF  | 0402 | AVX 04025A3R9BAT          | L2, L3  | 270nH | 1608  | Toko LL1608-FSR27J |
| C4, C5, C6 | 100pF  | 0402 | AVX 04025A101JAT          | L5      | 100nH | 1005  | Toko LL1005-FHR10J |
| C8         | 1μF    | 0603 | Taiyo Yuden LMK107BJ105MA | T2      | 4:1   | SM-22 | M/A-COM ETC4-1-2   |
| C7, C9     | 10pF   | 0402 | AVX 04025A100JAT          |         |       |       |                    |

Figure 2. Test Schematic for 350MHz Applications

The LT5526 consists of a double-balanced mixer, RF buffer amplifier, high speed limiting LO buffer and bias/enable circuits. The IC has been optimized for downconverter applications with RF input signals to 2GHz and LO signals to 2.5GHz. With proper matching, the IF output can be tuned for operation at frequencies from 0.1MHz to 1GHz. Operation over a wider input frequency range is possible, though with reduced performance.

The RF, LO and IF ports are all differential, though the LO port is internally matched for single-ended drive (with external DC blocking capacitors). The LT5526 is characterized and production tested using single-ended LO drive. Low side or high side LO injection can be used.

#### **RF Input Port**

Figure 3 shows a simplified schematic of the internal RF input circuit and example external impedance matching components for a 900MHz application. Each RF input pin requires a low resistance DC return to ground capable of handling 7.5mA. The DC ground can be realized using the center-tap of an input transformer (T1), as shown, or through matching inductors or bias chokes connected from Pins 2 and 3 to ground.

A lowpass impedance matching network is used to transform the differential input impedance at Pins 2 and 3 to the optimum value for the balun output, as illustrated in Figures 3 and 4. To assist in matching, Table 1 lists the differential input impedance and reflection coefficient at Pins 2 and 3 for several RF frequencies. The following example demonstrates how to design a lowpass impedance transformation network for the RF input.

From Table 1, the differential input impedance at 900MHz is:  $R_{RF}$  +  $jX_{RF}$  = 31.3 +  $j8.41\Omega$ . The  $8.41\Omega$  reactance is divided into two halves, with one half on each side of the 31.3 $\Omega$  internal load resistor, as shown in Figure 4. The matching network consists of additional external series inductance and a capacitor (C1) in parallel with the desired source impedance ( $50\Omega$  in this example). The external capacitance and inductance are calculated as follows:

$$\begin{split} n &= R_S/R_{RF} = 50/31.3 = 1.597 \\ Q &= \sqrt{(n-1)} = 0.773 \\ X_C &= R_S/Q = 64.7\Omega \\ C1 &= 1/(\omega \bullet X_C) = 2.74 pF \\ X_L &= R_{RF} \bullet Q = 24.2\Omega \\ X_{EXT} &= X_L - X_{RF} = 15.8\Omega \\ L_{EXT} &= X_{EXT}/\omega = 2.79 nH \end{split}$$

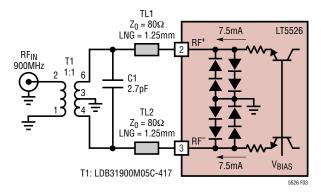


Figure 3. RF Input with External Matching for 900MHz Application



The external inductance is split in half (1.4nH), with each half connected between the pin and C1 as shown in Figure 4. The inductance may be realized with short, high impedance printed transmission lines, as in Figure 3, which provides a compact board layout and reduced component count. A 1:1 transformer (T1 in Figure 3) converts the  $50\Omega$  differential impedance to a  $50\Omega$  single-ended input.

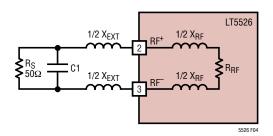


Figure 4. RF Input Impedance Matching Topology

Table 1. RF Input Differential Impedance

| FREQUENCY | INPUT        | REFLECTION | COEFFICIENT |
|-----------|--------------|------------|-------------|
| (MHz)     | IMPEDANCE    | MAG        | ANGLE       |
| 70        | 28.0 + j1.34 | 0.282      | 176         |
| 140       | 28.2 + j2.46 | 0.280      | 172         |
| 240       | 28.4 + j3.30 | 0.278      | 169         |
| 360       | 28.4 + j4.75 | 0.282      | 164         |
| 450       | 28.6 + j5.42 | 0.280      | 162         |
| 750       | 29.9 + j7.39 | 0.268      | 155         |
| 900       | 31.3 + j8.41 | 0.251      | 150         |
| 1500      | 38.3 + j17.9 | 0.237      | 112         |
| 1900      | 42.5 + j24.6 | 0.269      | 92.2        |

An alternative method of driving the RF input is to use a lumped-element balun configuration, as shown in Figure 5. This type of network may provide a more cost-effective solution for narrow band applications (fractional bandwidths < 30%). The actual balun is composed of components C7, C9, L1 and L4, and their values may be estimated as follows:

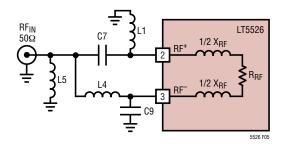


Figure 5. Schematic of Lumped Element Input Balun

$$L1 = L4 = \frac{\sqrt{R_S \cdot R_{RF}}}{\omega}$$

$$C7 = C9 = \frac{1}{\omega \sqrt{R_S \cdot R_{RF}}}$$

Where  $R_S$  is the source resistance (50 $\Omega$ ) and  $R_{RF}$  is the mixer input resistance from Table 1.

The computed values are only approximate, as they don't factor in the effects of  $X_{RF}$  or the parasitics of the external components. Actual component values for several frequencies are listed in Table 2, and measured return loss vs. frequency is plotted for each example in Figure 6.

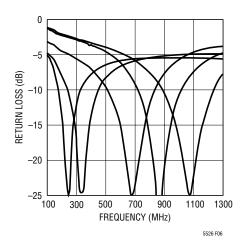


Figure 6. Input Return Loss with Lumped Element Baluns Using Values from Table 2

LINEAR

The purpose of L5 is to provide a DC return path for Pin 3. (Another possible placement for L5 would be across Pins 2 and 3, thus using L1 as part of the DC return path.) The inductance and resonant frequency of L5 should be large enough that they don't significantly affect the input impedance and performance of the balun. Either multilayer or wire-wound inductors may be used.

The impact of L5 on input matching can be reduced by adding a capacitor in parallel with it. In this case, the capacitor value should be the same as C7 and C9, while L5 should have the same value as L1 and L4.

Table 2. Component Values for Lumped Balun on RF Input

| FREQUENCY<br>(MHz) | L (nH) | C (pF) | L5 (nH) | BANDWIDTH<br>(MHz) |
|--------------------|--------|--------|---------|--------------------|
| 240                | 27     | 18     | 100     | 100                |
| 380                | 15     | 10     | 100     | 130                |
| 680                | 6.8    | 4.7    | 47      | 215                |
| 900                | 6.8    | 3.9    | 18      | 230                |
| 1100               | 3.9    | 2.7    | 15      | 230                |

#### **LO Input Port**

The LO buffer amplifier consists of high speed limiting differential amplifiers designed to drive the mixer core for high linearity. The LO+ and LO- pins are designed for single-ended drive, though differential drive can be used if desired. The LO input is internally matched to  $50\Omega$ ; however, external DC blocking capacitors are required because the LO pins are internally biased to approximately 1.7V DC. A simplified schematic for the LO input is shown in Figure 7.

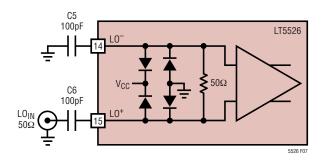


Figure 7. LO Input Schematic

External 100pF DC blocking capacitors provide a broadband match from about 110MHz to 2.7GHz, as shown in the plot of return loss vs frequency in Figure 8. The LO input match can be improved at lower frequencies by increasing the values of C5 and C6.

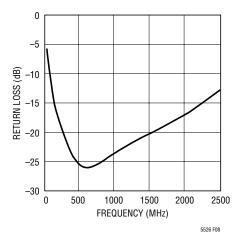


Figure 8. Typical LO Input Return Loss with 100pF DC Blocking Capacitors

Table 3. Single-Ended LO Input Impedance

| FREQUENCY | INPUT        | REFLECTION | COEFFICIENT |
|-----------|--------------|------------|-------------|
| (MHz)     | IMPEDANCE    | MAG        | ANGLE       |
| 400       | 63.4 – j12.0 | 0.158      | -35.8       |
| 600       | 61.6 – j8.38 | 0.128      | -31.5       |
| 800       | 61.8 – j6.86 | 0.122      | -26.6       |
| 1000      | 62.4 – j7.09 | 0.127      | -26.1       |
| 1200      | 62.8 – j8.32 | 0.135      | -28.8       |
| 1400      | 62.6 – j10.3 | 0.144      | -34.0       |
| 1600      | 61.9 – j12.6 | 0.154      | -40.3       |
| 1800      | 60.5 – j14.4 | 0.160      | -46.2       |

#### **IF Output Port**

A simplified schematic of the IF output circuit is shown in Figure 9. The output pins, IF<sup>+</sup> and IF<sup>-</sup>, are internally connected to the collectors of the mixer switching transistors. Both pins must be biased at the supply voltage, which can be applied through the center-tap of a transformer or



through impedance-matching inductors. Each IF pin draws about 7.5mA of supply current (15mA total). For optimum single-ended performance, these differential outputs must be combined externally through an IF transformer or balun.

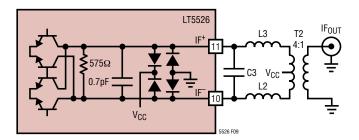


Figure 9. IF Output with External Matching

An equivalent small-signal model for the output is shown in Figure 10. The output impedance can be modeled as a  $575\Omega$  resistor in parallel with a 0.7pF capacitor. For most applications, the bond-wire inductance (0.7nH per side) can be ignored.

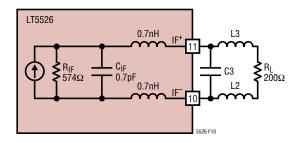


Figure 10. IF Output Small-Signal Model

The external components, C3, L2 and L3 form an impedance transformation network to match the mixer output impedance to the input impedance of transformer T2. The values for these components can be estimated using the same equations that were used for the input matching

network, along with the impedance values listed in Table 4. As an example, at an IF frequency of 140MHz and  $R_L = 200\Omega$  (using a 4:1 transformer for T2),

$$n = R_{IF}/R_{L} = 574/200 = 2.87$$

$$Q = \sqrt{(n-1)} = 1.368$$

$$X_{C} = R_{IF}/Q = 420\Omega$$

$$C = 1/(\omega \cdot X_{C}) = 2.71pF$$

$$C3 = C - C_{IF} = 2.01pF$$

$$X_{L} = R_{L} \cdot Q = 274\Omega$$

$$L2 = L3 = X_{I}/2\omega = 156nH$$

Table 4. IF Differential Impedance (Parallel Equivalent)

| FREQUENCY | OUTPUT         | REFLECTION | COEFFICIENT |
|-----------|----------------|------------|-------------|
| (MHz)     | IMPEDANCE      | MAG        | ANGLE       |
| 70        | 575   – j3.39k | 0.840      | -1.8        |
| 140       | 574   – j1.67k | 0.840      | -3.5        |
| 240       | 572   – j977   | 0.840      | -5.9        |
| 450       | 561   – j519   | 0.838      | -11.1       |
| 750       | 537   - j309   | 0.834      | -18.6       |
| 860       | 525   - j267   | 0.831      | -21.3       |
| 1000      | 509   - j229   | 0.829      | -24.8       |
| 1250      | 474   – j181   | 0.822      | -31.3       |
| 1500      | 435   - j147   | 0.814      | -38.0       |

#### **Low Cost Output Match**

For low cost applications in which the required fractional bandwidth of the IF output is less than 25%, it may be possible to replace the output transformer with a lumped-element network similar to that discussed earlier for the RF input. This circuit is shown in Figure 11, where L11, L12, C11 and C12 form a narrowband bridge balun. These element values are selected to realize a 180° phase shift at the desired IF frequency and can be estimated by using the equations below. In this case,  $R_{\rm IF}$  is the mixer output resistance and  $R_{\rm I}$  is the load resistance (50 $\Omega$ ).



$$\begin{aligned} &L11 = L12 = \frac{\sqrt{R_{IF} \bullet R_{L}}}{\omega} \\ &C11 = C12 = \frac{1}{\omega \sqrt{R_{IF} \bullet R_{L}}} \end{aligned}$$

Inductors L13 and L14 provide a DC path between  $V_{CC}$  and the IF<sup>+</sup> pin. Only one of these inductors is required. Low cost multilayer chip inductors are adequate for L11, L12 and L13. If L14 is used instead of L13, a larger value is usually required, which may require the use of a wirewound inductor. Capacitor C13 is a DC block which can also be used to adjust the impedance match. Capacitor C14 is a bypass capacitor.

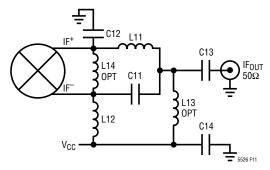


Figure 11. Narrowband Bridge IF Balun

Typical return loss of the IF output port is plotted versus frequency in Figure 12 for a 240MHz balun design. For this example, L11 = L12 = 100nH, C11 = C12 = 3.9pF, L14 = 560nH and C13 = 100pF. Performance versus IF output frequency is shown in Figure 13 in the case of a 1900MHz RF input. These results show that the usable IF bandwidth is greater than 60MHz, assuming tight tolerance matching components. Contact the factory for applications assistance with this circuit.

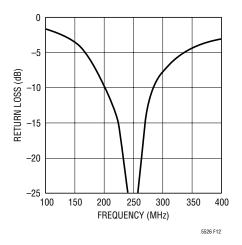


Figure 12. Typical Return Loss Performance with a 240MHz Narrowband Bridge IF Balun (Swept IF)

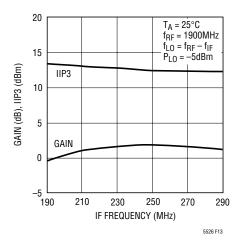
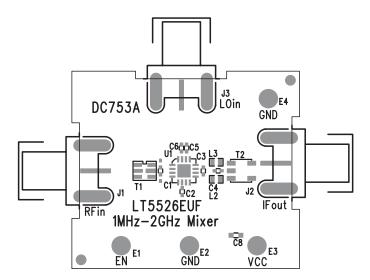


Figure 13. Typical Gain and IIP3 Performance with a 240MHz Narrowband Bridge IF Balun (Swept IF)

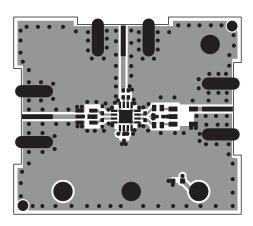
## TYPICAL APPLICATIONS

## **Evaluation Board Layouts**

Top Layer Silkscreen



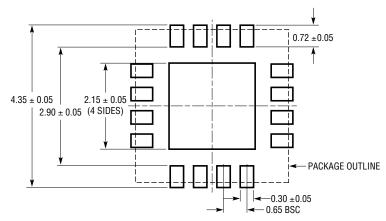
Top Layer Metal



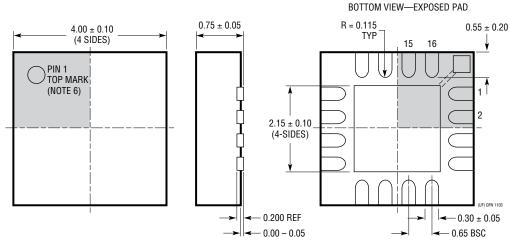
## PACKAGE DESCRIPTION

#### **UF Package** 16-Lead Plastic QFN (4mm × 4mm)

(Reference LTC DWG # 05-08-1692)



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#### NOTE:

- 1. DRAWING CONFORMS TO JEDEC PACKAGE OUTLINE MO-220 VARIATION (WGGC)
  2. DRAWING NOT TO SCALE

- 3. ALL DIMENSIONS ARE IN MILLIMETERS
  4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15mm ON ANY SIDE
- 5. EXPOSED PAD SHALL BE SOLDER PLATED
- 6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE TOP AND BOTTOM OF PACKAGE



## **RELATED PARTS**

| PART NUMBER    | DESCRIPTION   | COMMENTS  |
|----------------|---|---|
| Infrastructure | ,   |   |
| LT5511         | High Linearity Upconverting Mixer   | RF Output to 3GHz, 17dBm IIP3, Integrated LO Buffer   |
| LT5512         | DC-3GHz High Signal Level Downconverting Mixer                              | DC to 3GHz, 21dBm IIP3, Integrated LO Buffer  |
| LT5514         | Ultralow Distortion, IF Amplifier/ADC Driver with Digitally Controlled Gain | 850MHz Bandwidth, 47dBm OIP3 at 100MHz, 10.5dB to 33dB Gain Control Range   |
| LT5515         | 1.5GHz to 2.5GHz Direct Conversion Quadrature Demodulator                   | 20dBm IIP3, Integrated LO Quadrature Generator  |
| LT5516         | 0.8GHz to 1.5GHz Direct Conversion Quadrature Demodulator                   | 21.5dBm IIP3, Integrated LO Quadrature Generator  |
| LT5517         | 40MHz to 900MHz Quadrature Demodulator                                      | 21dBm IIP3, Integrated LO Quadrature Generator  |
| LT5519         | 0.7GHz to 1.4GHz High Linearity Upconverting Mixer                          | 17.1dBm IIP3 at 1GHz, Integrated RF Output Transformer with $50\Omega$ Matching, Single-Ended LO and RF Ports Operation |
| LT5520         | 1.3GHz to 2.3GHz High Linearity Upconverting Mixer                          | 15.9dBm IIP3 at 1.9GHz, Integrated RF Output Transformer with 50Ω Matching, Single-Ended LO and RF Ports Operation      |
| LT5521         | 3.7GHz Very High Linearity Mixer  | 24.2dBm IIP3 at 1.95GHz, 12.5dB SSBNF, -42dBm LO Leakage, Supply Voltage = 3.15V to 5.25V                               |
| LT5522         | 600MHz to 2.7GHz High Signal Level Downconverting Mixer                     | 4.5V to 5.25V Supply, 25dBm IIP3 at 900MHz, NF = 12.5dB, $50\Omega$ Single-Ended RF and LO Ports                        |
| RF Power Detec | tors  |   |
| LT5504         | 800MHz to 2.7GHz RF Measuring Receiver                                      | 80dB Dynamic Range, Temperature Compensated, 2.7V to 5.25V Supply   |
| LTC®5505       | RF Power Detectors with >40dB Dynamic Range                                 | 300MHz to 3GHz, Temperature Compensated, 2.7V to 6V Supply  |
| LTC5507        | 100kHz to 1000MHz RF Power Detector   | 100kHz to 1GHz, Temperature Compensated, 2.7V to 6V Supply  |
| LTC5508        | 300MHz to 7GHz RF Power Detector  | 44dB Dynamic Range, Temperature Compensated, SC70 Package   |
| LTC5509        | 300MHz to 3GHz RF Power Detector  | 36dB Dynamic Range, Low Power Consumption, SC70 Package   |
| LTC5530        | 300MHz to 7GHz Precision RF Power Detector                                  | Precision V <sub>OUT</sub> Offset Control, Shutdown, Adjustable Gain  |
| LTC5531        | 300MHz to 7GHz Precision RF Power Detector                                  | Precision V <sub>OUT</sub> Offset Control, Shutdown, Adjustable Offset  |
| LTC5532        | 300MHz to 7GHz Precision RF Power Detector                                  | Precision V <sub>OUT</sub> Offset Control, Adjustable Gain and Offset   |
| LT5534         | 50MHz to 3GHz RF Power Detector with 60dB Dynamic Range                     | ±1dB Output Variation over Temperature, 38ns Response Time  |
| Low Voltage RF | Building Blocks   |   |
| LT5500         | 1.8GHz to 2.7GHz Receiver Front End   | 1.8V to 5.25V Supply, Dual-Gain LNA, Mixer, LO Buffer   |
| LT5502         | 400MHz Quadrature IF Demodulator with RSSI                                  | 1.8V to 5.25V Supply, 70MHz to 400MHz IF, 84dB Limiting Gain, 90dB RSSI Range   |
| LT5503         | 1.2GHz to 2.7GHz Direct IQ Modulator and Upconverting Mixer                 | 1.8V to 5.25V Supply, Four-Step RF Power Control,<br>120MHz Modulation Bandwidth  |
| LT5506         | 500MHz Quadrature IF Demodulator with VGA                                   | 1.8V to 5.25V Supply, 40MHz to 500MHz IF, -4dB to 57dB<br>Linear Power Gain, 8.8MHz Baseband Bandwidth                  |
| LT5546         | 500MHz Ouadrature IF Demodulator with VGA and 17MHz Baseband Bandwidth      | 17MHz Baseband Bandwidth, 40MHz to 500MHz IF, 1.8V to 5.25V Supply, -7dB to 56dB Linear Power Gain                      |
| Wide Bandwidth | ADCs  |   |
| LT1749         | 12-Bit, 80Msps  | 500MHz BW S/H, 71.8dB SNR, 87dB SFDR  |
| LT1750         | 14-Bit, 80Msps  | 500MHz BW S/H, 75.5dB SNR, 90dB SFDR, 2.25V <sub>P-P</sub> or 1.35V <sub>P-P</sub> Input Ranges                         |

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