# 40 MHz to 500 MHz VGA and I/Q Demodulator with 17 MHz Baseband Bandwidth 

## feATURES

- 17MHz I/Q Lowpass Output Noise Filters
- Wide Range 1.8 V to 5.25 V Supply Voltage
- Frequency Range: 40MHz to 500 MHz
- THD < 0.14\% (-57dBc)
at $800 \mathrm{~m} V_{\text {p.p. }}$ Differential Output Level
- IF Overload Detector
- Log Linear Gain Control Range: -7dB to 56dB
- Baseband I/Q Amplitude Imbalance: 0.2dB
- Baseband I/Q Phase Imbalance: $0.6^{\circ}$
- 7.8dB Noise Figure at Max Gain
- Input IP3 at Low Gain: -1dBm
- Low Supply Current: 24mA
- Low Delay Shift Over Gain Control Range: 2ps/dB
- Outputs Biased Up While in Standby
- 16-Lead QFN $4 \mathrm{~mm} \times 4 \mathrm{~mm}$ Package with Exposed Pad


## APPLICATIONS

- GPS IF Receivers
- Satellite IF Receivers
- VHF/UHF Receivers
- Wireless Local Loop


## DESCRIPTIOn

The $\mathrm{LT}^{\circledR} 5546$ is a 40 MHz to 500 MHz monolithic integrated quadrature demodulator with variable gain amplifier (VGA) and 17MHz I/Q baseband bandwidth designed for low voltage operation. It supports standards that use alinear modulation format. The chip consists of aVGA, quadrature downconverting mixers and 17MHz lowpass noise filters (LPF). The LO port consists of a divide-by-two stage and LO buffers. The IC provides all building blocks for IF downconversion to I and Q baseband signals with a single supply voltage of 1.8 V to 5.25 V . The VGA gain has a linear-in-dB relationship to the control input voltage. Hard-clipping amplifiers at the mixer outputs reduce the recovery time from a signal overload condition. The lowpass filters reduce the out-of-band noise and spurious frequency components. The -3 dB corner frequency of the noise filters is approximately 17 MHz and has a first order rolloff. The standby mode provides reduced supply current and fast transient response into the normal operating mode when the I/Q outputs are AC-coupled to a baseband chip.
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## TYPICAL APPLICATION



Total Harmonic Distortion vs IF Input Level at 1.8 V Supply


5546 TA01b

## ABSOLUTE MAXIMUM RATINGS

(Note 1)
Supply Voltage ..................................................... 5.5V
Differential Voltage Between $2 \times L 0^{+}$and $2 \times \mathrm{LO}^{-}$.......... 4 V
$\mathrm{IF}^{+}$, $\mathrm{IF}^{-}$ $\qquad$ -500 mV to 500 mV
$I_{\text {OUT }}{ }^{+}, I_{\text {OUT }}{ }^{-}$, Q $_{\text {OUT }}{ }^{+}$, Q $_{\text {OUT }}{ }^{-}$.................. $V_{\text {CC }}-1.8 \mathrm{~V}$ to $\mathrm{V}_{\text {CC }}$ Operating Ambient Temperature (Note 2) $\qquad$ $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$
Storage Temperature Range .................. $-65^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ Voltage on Any Pin
Not to Exceed $\qquad$ -500 mV to $\mathrm{V}_{\text {CC }}+500 \mathrm{mV}$

PACKAGE/ORDER INFORMATION

|  | ORDER PART NUMBER |
| :---: | :---: |
| GND 1 |  |
|  | LT5546EUF |
|  | UF PART MARKING |
|  |  |
|  | 5546 |
|  |  |
| $T_{\text {Jmax }}=125^{\circ} \mathrm{C}, \theta_{\mathrm{JA}}=37^{\circ} \mathrm{C} / \mathrm{W}$ EXPOSED PAD IS GND (PIN 17) (MUST BE SOLDERED TO PCB) |  |

Consult LTC Marketing for parts specified with wider operating temperature ranges.

## ELECTRICAL CHARACTERIST|CS $V_{C C}=3 V, f_{2 \times L 0}=570 \mathrm{MHz}, \mathrm{P}_{2 \times L 0}=-5 \mathrm{dBm}$ (Note 5 ), $\mathrm{f}_{\mathrm{IF}}=284 \mathrm{MHz}$,

 $P_{\text {IF }}=-30 d B m$, I and $Q$ outputs $800 \mathrm{~m} V_{\text {P-p }}$ into $4 \mathrm{k} \Omega$ differential load, $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, E N=\mathrm{V}_{\mathrm{CC}}, S T B Y=V_{C C}$, unless otherwise noted. (Note 3)| SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX |
| :--- | :--- | :--- | :---: | :---: | :---: | UNITS

## Demodulator $/ / Q$ Output

|  | Nominal Voltage Swing | (Note 6) | 0.8 |  | $V_{\text {P-P }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Clipping Level | (Note 6) | 1.47 |  | $V_{\text {P-P }}$ |
|  | DC Common Mode Voltage |  | $\mathrm{V}_{\text {CC }}-1.19$ |  | V |
|  | I/Q Amplitude Imbalance | (Note 8) | 0.14 | 0.6 | dB |
|  | I/Q Phase Imbalance | (Note 8) | 0.6 | 3 | Deg |
|  | DC Offset | (Notes 6, 8) | 21 |  | mV |
|  | Output Driving Capability | Single Ended, $\mathrm{C}_{\text {LOAD }} \leq 10 \mathrm{pF}$ | 21.5 |  | k $\Omega$ |
| $\mathrm{r}_{0}$ | Small-Signal Output Impedance | (Note 6) | 180 |  | $\Omega$ |
|  | STBY to Turn-On Delay |  | 0.3 |  | $\mu \mathrm{S}$ |
|  | I/Q Output 1dB Compression |  | -10 |  | dBm |
|  | I/Q Output IM3 | $\begin{aligned} & \mathrm{P}_{\mathrm{IF}, 1}=-25.5 \mathrm{dBm}, 280 \mathrm{MHz} \\ & \mathrm{P}_{\mathrm{IF}, 2}=-25.5 \mathrm{dBm}, 280.1 \mathrm{MHz} \text { (Note } 7 \text { ) } \end{aligned}$ | -49 |  | dBc |

ELECTRICAL CHARACTERISTICS $v_{C C}=3 V, \mathrm{f}_{2 \times 10}=570 \mathrm{MHz}, \mathrm{P}_{2 \times 10}=-5 \mathrm{dBm}$ (Note 5), $\mathrm{f}_{\text {IF }}=284 \mathrm{MHz}$, $P_{\text {IF }}=-30 d B m$, I and $Q$ outputs $800 \mathrm{~m} V_{P-p}$ into $4 k \Omega$ differential load, $T_{A}=25^{\circ} \mathrm{C}, E N=V_{C C}, S T B Y=V_{\text {CC }}$, unless otherwise noted. (Note 3)

| SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX |
| :--- | :--- | :--- | :---: | :---: | :---: | UNITS

## Baseband Lowpass Filter (LPF)

|  | -3 dB Cutoff Frequency |  | 13 | 17 |
| :--- | :--- | :--- | ---: | ---: |
|  | Amplitude Roll-Off at 50 MHz |  | -9 | MHz |
|  | Group Delay Ripple |  | 1 | dB |

## 2xLO Input

| $\mathrm{f}_{2 \times L 0}$ | Frequency Range |  | 80 to 1000 | MHz |
| :--- | :--- | :--- | :---: | :---: |
| $\mathrm{P}_{2 \times L 0}$ | Input Power | $1: 2$ Transformer with 240 $\Omega$ Shunt Resistor (Note 5) | -20 | -5 |
|  | Input Power | LC Balun (Note 5) | -10 | dBm |
|  | Input Impedance | Differential Between 2xL0+ and 2xLO | dBm |  |
|  | DC Common Mode Voltage |  | $800 \Omega / / 0.4 \mathrm{pF}$ |  |
|  |  | $\mathrm{V}_{\text {CC }}-0.4$ | V |  |

## IF Detector

|  | IF Detector Range | Referred to IF Input | -30 to 8 | dBm |
| :--- | :--- | :--- | :---: | :---: |
|  | Output Voltage Range | For P PIF $=-30 \mathrm{dBm}$ to 8 dBm | 0.27 to 1.2 | V |
|  | Detector Response Time | With External 1.8pF Load, <br> Settling within 10\% of Final Value | 80 | ns |

## Power Supply

| $V_{\text {CC }}$ | Supply Voltage |  | 1.8 | 5.25 | V |
| :--- | :--- | :--- | ---: | :---: | :---: |
| $I_{\text {CC }}$ | Supply Current | EN $=$ High, STBY = Low or High | 24 | 34 | mA |
| $I_{\text {OFF }}$ | Shutdown Current | EN, STBY $<350 \mathrm{mV}$ | 0.2 | 30 | $\mu \mathrm{~A}$ |
| $I_{\text {STBY }}$ | Standby Current | EN = Low; STBY = High | 3.6 | 6 | mA |

Mode

| Enable | Enable Pin Voltage | EN $=$ High | 1 | V |
| :--- | :--- | :--- | :--- | :---: |
| Disable | Enable Pin Voltage | EN = Low |  | 0.5 |
| Standby | Standby Pin Voltage | STBY = High | 1 | V |
| No Standby | Standby Pin Voltage | STBY = Low |  | V |

Note 1: Absolute Maximum Ratings are those values beyond which the life of a device may be impaired.
Note 2: Specifications over the $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ temperature range are assured by design, characterization and correlation with statistical process controls.
Note 3: Tests are performed as shown in the configuration of Figure 6. The IF input transformer loss is substracted from the measured values.
Note 4: Power gain is defined here as the I (or $Q$ ) output power into a $4 \mathrm{k} \Omega$ differential load, divided by the IF input power in dB. To calculate the voltage gain between the differential I output (or Q output) and the IF input, including ideal matching network, $10 \cdot \log (4 \mathrm{k} \Omega / 50)=19 \mathrm{~dB}$ has to be added to this power gain.

Note 5: If a narrow-band match is used in the $2 \times$ LO path instead of a 1:2 transformer with $240 \Omega$ shunt resistor, $2 \times$ LO input power can be reduced to -10 dBm , without degrading the phase imbalance. See Figure 11 and Figure 6.
Note 6: Differential between $\mathrm{I}_{\text {OUT }}{ }^{+}$and $\mathrm{I}_{\text {OUT }^{-}}$(or differential between $Q_{\text {OUT }}{ }^{+}$and $Q_{\text {OUT }^{-}}$).
Note 7: The gain control voltage $\mathrm{V}_{\text {CTRL }}$ is set in such a way that the differential output voltage between $\mathrm{I}_{\text {OUT }}{ }^{+}$and $\mathrm{I}_{\mathrm{OUT}^{-}}$(or differential between $Q_{\text {OUT }^{+}}$and $Q_{\text {OUT }}{ }^{-}$) is $800 \mathrm{~m} V_{\text {P-p }}$, with the given input power $\mathrm{P}_{\text {IF. }}$ IF frequencies are 280 MHz and 280.1 MHz , with $\mathrm{f}_{2 \times \mathrm{LO}}=570 \mathrm{MHz}$.
Note 8: The typical parameter is defined as the mean of the absolute values of the data distribution.
Note 9: IF frequency is 125 MHz , with $\mathrm{f}_{2 \times \mathrm{LO}}=502 \mathrm{MHz}$.

## TYPICAL PGRFORMANCE CHARACTERISTICS $\quad v_{c c=}=3 v, t_{2 \times 10}=570 \mathrm{NHz}, P_{2}=10=-5 d \mathrm{dm}$

(Note 5), $\mathrm{f}_{\mathrm{IF}}=284 \mathrm{MHz}, \mathrm{P}_{\mathrm{IF}}=-30 \mathrm{dBm}$, I and $Q$ outputs $800 \mathrm{~m} \mathrm{~V}_{\mathrm{P}-\mathrm{p}}$ into $4 \mathrm{k} \Omega$ differential load, $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{EN}=\mathrm{V}_{\mathrm{CC}}, \mathrm{STBY}=\mathrm{V}_{\mathrm{CC}}$, unless otherwise noted. (Note 3)


Gain and Noise Figure
vs Control Voltage at 1.8 V Supply


## Gain and Noise Figure vs Control Voltage and VCC



Gain and Noise Figure
vs Control Voltage at 3V Supply


Gain Flatness
vs Control Voltage at 3V Supply


5546 G04

## Gain and Noise Figure vs IF Frequency at 3V Supply



## 

(Note 5), $\mathrm{f}_{\mathrm{IF}}=284 \mathrm{MHz}, \mathrm{P}_{\mathrm{IF}}=-30 \mathrm{dBm}$, I and $Q$ outputs $800 \mathrm{~m} \mathrm{~V}_{\mathrm{P}-\mathrm{p}}$ into $4 \mathrm{k} \Omega$ differential load, $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{EN}=\mathrm{V}_{\mathrm{CC}}, \mathrm{STBY}=\mathrm{V}_{\mathrm{CC}}$, unless otherwise noted. (Note 3)

Total Harmonic Distortion vs IF Input Power at 3V Supply and $800 \mathrm{mV} \mathrm{V}_{\text {p.p }}$ Differential Out


5546 G07
Total Harmonic Distortion vs IF Input Power and Supply Voltage


LPF Frequency Response vs Baseband Frequency and Supply Voltage


Total Harmonic Distortion vs IF Input Power and IF Frequency


5546 G08
Total Harmonic Distortion
vs IF Input Power at $500 \mathrm{mV} \mathrm{V}_{\mathrm{P}-\mathrm{p}}$ Differential Out


5546 G11
IF Detector Output Voltage vs IF Input CW Power at 3V Supply


Total Harmonic Distortion vs IF Input Power at 1.8 V Supply and $800 \mathrm{mV} \mathrm{V}_{\text {p-p }}$ Differential Out


5546 G09
LPF Frequency Response vs Baseband Frequency and Temperature


5546 G12
IF Detector Output Voltage vs IF Input CW Power at 1.8V Supply


TYPICAL PGRFORMANCE CHARACTERISTICS $v_{C C L}=3 v, t_{2 \times 10}=570 \mathrm{MHz}, P_{2 \times 10}=-5 d \mathrm{dm}$ (Note 5 ), $, \mathrm{f}_{\mathrm{IF}}=284 \mathrm{MHz}, \mathrm{P}_{\mathrm{IF}}=-30 \mathrm{dBm}, \mathrm{I}$ and Q outputs $800 \mathrm{~m} V_{\mathrm{P}-\mathrm{p}}$ into $4 \mathrm{k} \Omega$ differential load, $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{EN}=\mathrm{V}_{\mathrm{Cc}}, \mathrm{STBY}=\mathrm{V}_{\mathrm{CC}}$, unless otherwise noted. (Note 3)


## PIn functions

GND (Pins 1, 4 and 17): Ground. Pins 1 and 4 are connected to each other internally. The exposed pad (Pin 17) is not connected internally to Pins 1 and 4 . For chip functionality, the exposed pad and either Pin 1 or Pin 4 must be connected to ground. For best RF performance, Pin 1, Pin 4 and the exposed pad should be connected to RF ground.
IF+, IF- (Pins 2, 3): Differential Inputs for the IF Signal. Each pin must be DC grounded through an external inductor or RF transformer with central ground tap. This path should have a $D C$ resistance lower than $2 \Omega$ to ground.
$\mathrm{V}_{\text {cc }}$ (Pins 5 and 8): Power Supply. These pins should be decoupled to ground using 1000 pF and $0.1 \mu \mathrm{~F}$ capacitors.
$V_{\text {ctrl }}$ (Pin 6): VGA Gain Control Input. This pin controls the IF gain and its typical input voltage range is 0.2 V to 1.7 V . It is internally biased via a 25 k resistor to 0.2 V , setting a low gain if the $\mathrm{V}_{\text {CTRL }}$ pin is left floating.
IF DET (Pin 7): IF Detector Output. For strong IF input signals, the DC level at this pin is a function of the IF input signal level.

EN (Pin 9): Enable Input. When the enable pin voltage is higher than 1 V , the IC is completely turned on. When the input voltage is less than 0.5 V , the IC is turned off, except the part of the circuit associated with standby mode.
$2 \times L 0^{-}, 2 \times L 0^{+}$(Pins 10, 11): Differential Inputs for the 2xLO Input. The $2 x$ LO input frequency must be twice that of the IF frequency. The internal bias voltage is $\mathrm{V}_{C C}-0.4 \mathrm{~V}$.
STBY (Pin 12): Standby Input. When the STBY pin is higher than 1 V , the standby mode circuit is turned on to prebias the I/Q buffers. When the STBY pin is less than 0.5 V , the standby mode circuit is turned off.
$\mathrm{a}_{\mathrm{OUT}}{ }^{-}, \mathrm{Q}_{\text {OUT }^{+}}$(Pins 13, 14): Differential Baseband Outputs of the $Q$ Channel. Internally biased at $V_{C C}-1.19 \mathrm{~V}$.
$\mathrm{I}_{\text {OUT }^{-}}$, $\mathrm{I}_{\text {OUT }}{ }^{+}$(Pins 15, 16): Differential Baseband Outputs of the I Channel. Internally biased at $\mathrm{V}_{\mathrm{Cc}}-1.19 \mathrm{~V}$.

## BLOCK DIAGRAM



## APPLICATIONS INFORMATION

The LT5546 consists of a variable gain amplifier (VGA), I/Q demodulator, quadrature LO generator, lowpass filters (LPFs), clipping amplifiers (clippers) and bias circuitry.

The IF signal is fed to the inputs of the VGA. The VGA gain is typically set by an external signal in such a way that the amplified IF signal delivered to the I/Q mixers is constant. The IF signal is then converted into I/Q baseband signals using the I/Q down-converting mixers. The quadrature LO signals that drive the mixers are internally generated from the on-chip divide-by-two circuit. The I/Q signals are passed through first-order low-pass filters and subsequently a pair of hard-clipping amplifiers (clippers). After externally setting the required gain, these amplifiers should not clip. However, in the event of overload, they reduce the settling time of any (optional) external AC coupling capacitors by preventing asymmetrical charging and discharging effects. The I/Q baseband outputs are buffered by output drivers.

## VGA and Input Matching

The VGA has a nominal 60dB gain control range with a frequency range of 40 MHz to 500 MHz . The inputs of the VGA must have a DC return to ground. This can be done using a transformer with a central tap (on the secondary) or an LC matching circuit with a matched impedance at the frequency of interest and near zero impedance at DC. The differential AC input impedance of the LT5546 is about $200 \Omega$, thus a $1: 4$ (impedance ratio) RF transformer with center tap can be used. In Figure 6, the evaluation board
schematic is shown using a 1:4 transformer. The measured input sensitivity of this board is about -80.5 dBm for a 10 dB signal-to-noise ratio. In the case of an L-C matching circuit, the circuit of Figure 1 can be used. In Table 1 the matching network component values are given for a range of IF frequencies. The matching circuit of Figure 1 approaches $180^{\circ}$ phase shift between $\mathrm{IF}^{+}$and $\mathrm{IF}^{-}$in a broad range around its center frequency. However, some amplitude mismatch occurs if the circuit is not tuned to the center frequency. This leads to reduced circuit linearity performance, because one of the inputs carries a higher signal compared to the perfectly balanced case. A 10\% frequency shift from the center frequency results in about a 2 dB gain difference between the $\mathrm{IF}^{+}$and $\mathrm{IF}^{-}$inputs. This results in a 1.5 dB higher IM3 contribution from the input stage which leads to a 0.75 dB drop in IIP3. Moreover, the IIP2 of the circuit is also reduced which can lead to a higher second order harmonic contribution. The circuit can be driven single ended, but this is not recommended because it leads to a 3dB drop in gain and a considerable increase in IM5 and IM7 components. The single-ended noise figure increases by 4 dB if one IF input is directly grounded and increases by 1.5 dB if one IF input is grounded via a $1 \mu \mathrm{H}$ inductor. An IF input cannot be left open or connected via a resistor to ground because this will disturb the internal biasing, reducing the gain, noise and linearity performance. For optimal performance, it is important to keep the DC impedance to ground of both IF inputs lower than $2 \Omega$. In the matching network of Figure 1, inductor L3 is used for supplying the DC bias current to the IF+ input.

## APPLICATIONS InfORMATION



Figure 1. Example L-C IF Input Matching Network at 280MHz

Table 1. The Component Values of Matching Network L1, L2, L3, C1, C2 and C3.

| $\mathbf{f}_{\mathbf{I F}}(\mathbf{M H z})$ | $\mathbf{L 1}, \mathbf{L 2}(\mathbf{n H})$ | $\mathbf{C 1}, \mathbf{C 2}(\mathbf{p F})$ | $\mathbf{L 3}(\mathbf{n H})$ | $\mathbf{C 3}(\mathbf{p F})$ |
| :---: | :---: | :---: | :---: | :---: |
| 50 | 340 | 34 | 1800 | 820 |
| 100 | 159 | 15.9 | 470 | 220 |
| 150 | 106 | 10.6 | 470 | 220 |
| 200 | 80 | 8.0 | 470 | 220 |
| 250 | 64 | 6.4 | 120 | 56 |
| 300 | 53 | 5.3 | 120 | 56 |
| 350 | 45 | 4.5 | 120 | 56 |
| 400 | 40 | 4.0 | 120 | 56 |
| 450 | 35 | 3.5 | 120 | 56 |
| 500 | 32 | 3.2 | 120 | 56 |

To keep the DC resistance of L 3 below $2 \Omega, 120 \mathrm{nH}$ is used. This disturbs the matching network slightly by causing the frequency where the S11 is minimal to be lower than the frequency where the amplitudes of IF+ and IF- are equal. To compensate for this, the value of coupling capacitor C3 is lowered and will contribute some correcting reactance. For low frequencies, it might not be possible to find any practical inductor value for L3 with DC resistance smaller than $2 \Omega$. In that case it is recommended to use a transformer with a center tap. The tolerance for the components in Figure 1 can be 10\% for a return loss higher than 16 dB and a gain reduction due to mismatch less than 0.3 dB .
It is possible to simplify the input matching circuit and compromise the performance. In Figure 2a, the simplified matching network is given.
This matching network can deliver equal amplitudes to the IF+ and IF- inputs for a narrow frequency region, but the phase difference between the inputs will not be exactly 180 degrees. In practice, the phase shift will be around 145


Figure 2a. Simplified IF Input Matching Network at 280MHz and Figure 2b. Simplified Circuit Schematic of the IF Inputs
degrees, depending on the quality factor of the network. This will result in a reduction in the gain. The higher the chosen quality factor, the closer the phase difference will approach 180 degrees. However, a higher quality factor will reduce bandwidth and create more loss in the matching network. For minimum board space, 0402 components are used. The measured noise figure for maximum gain with this matching network is about 9.4 dB , and the maximum gain is about 55dB. Assuming 0402 inductors with $Q=35$, the insertion loss of this network is about 2.5 dB . The tolerance for the components in Figure 2a can be $10 \%$ for a return loss higher than 10 dB and a gain reduction due to mismatch less than 0.5 dB . The measured input sensitivity for this matching network (see also Figure 11) is about -78.3 dBm for a 10 dB signal-to-noise ratio.

The gain of the VGA is set by the voltage at the $\mathrm{V}_{\text {CTRL }}$ pin. For high gain settings, both the noise figure and the input IP3 will be low. From a noise figure point of view, it is advantageous to work as closely as possible to the maximum gain point. However, if the voltage at the $\mathrm{V}_{\text {CTRL }}$ pin is increased beyond the maximum gain point (where additional increase in control voltage does not give an increase in gain), the response time of the gain control circuit is increased. If control speed is crucial, a few dB of gain margin should be allowed from the highest gain point to be sure that at all temperatures, the maximum gain setting is not crossed. At low gain settings, the noise figure and the input IP3 will be high. Optionally, the control voltage $\mathrm{V}_{\text {CTRL }}$ can be set lower than 0.2 V . The normal range is from $\mathrm{V}_{\text {CTRL }}=0.2 \mathrm{~V}$ to 1.7 V , which results in a nominal gain range from 1.6 dB to 56.8 dB . The linear-indB gain relation with the $\mathrm{V}_{\text {CTRL }}$ voltage still holds for control voltages as low as -0.35 V . This results in an

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extended gain control range of -23 dB to 57 dB . The $\mathrm{V}_{\text {CTRL }}$ pin is a very sensitive input because of its high input impedance and therefore should be well shielded. Signal pickup on the $V_{\text {CTRL }}$ pin can lead to spurs and increased noise floor in the I/Q baseband outputs. It can degrade the linearity performance and it can cause asymmetry in the two-tone test. If control speed is not important, $1 \mu \mathrm{~F}$ bypass capacitors are recommended between $\mathrm{V}_{\text {CTRL }}$ and ground.
A fast responding peak detector is connected to the VGA input, sensitive to signal levels above the signal levels where the VGA is operating in the linear range. It is active from -22dBm up to 5 dBm IF input signal levels. The DC output voltage of this detector (IF DET) can be used by the baseband controller to quickly determine the presence of a strong input level at the desired channel, and adjust gain accordingly. Figure 3a shows the simplified circuit schematic of the IF DET output.

## I/Q Demodulators

The quadrature demodulators are double balanced mixers, down-converting the amplified IF signal from the VGA into I/Q baseband signals. The quadrature LO signals are generated internally from a double frequency external CW signal. The nominal output voltage of the differential I/Q baseband signals should be set to $0.8 \mathrm{~V}_{\text {P-p }}$ or lower, depending on the linearity requirements. The magnitudes of I and $Q$ are well matched and their phases are $90^{\circ}$ apart.

## Quadrature LO Generator

The quadrature LO generator consists of a divide-by-two circuit and LO buffers. An input signal (2xLO) with twice the desired IF signal frequency is used as the clock for the divide-by-two circuit, producing the quadrature LO signals for the demodulators. The outputs are buffered and then drive the down-converting mixers. With a fully differential approach, the quadrature LO signals are well matched. Second harmonic content (or higher order even harmonics) in the external $2 x L 0$ signal can degrade the $90^{\circ}$ phase shift between I and Q. Therefore, such content should be minimized. In disable or standby mode, the divide-by-two stage is powered down. After enabling the circuit, the phase relation between the IF signal and the baseband (I or Q) signals can be either $0^{\circ}$ or $180^{\circ}$, since the circuit cannot distinguish between the two subsequent identical sinusoi-


Figure 3a. Simplified Circuit Schematic of the IF DET Output and Figure 3b. The 2xLO Inputs


Figure 4. 2xLO Input Matching Networks for 4a) Narrow Band Tuned to 570 MHz , 4b) Wide Band, 4c) Single-Ended Wide Band
dal waveforms of the $2 \times L 0$ input signal. The phase relation between I and $Q$ is always $90^{\circ}$, i.e. I always leads $Q$ by $90^{\circ}$ forf $_{\text {IF }}>1 / 2 \bullet f_{2 x L 0}$. Figure 3b shows the simplified circuit schematic of the 2xLO inputs. Depending on the application, different $2 \times$ LO input matching networks can be chosen. In Figure 4, three examples are given. The first network provides the best $2 \times$ LO input sensitivity because it can boost the $2 x L 0$ differential input signal using a nar-row-band resonant approach. The second network gives a wide-band match, but the $2 x L 0$ input sensitivity is about 2 dB lower. The third network gives a simple and less expensive wide-band match, but 2xLO input sensitivity drops by about 9 dB . The IFinput sensitivity doesn't change significantly using any of the three $2 \times L 0$ matching networks.

## Baseband Circuit

The baseband circuit consists of I/Q low-pass filters, I/Q hard limiters (clippers) and I/Q output buffers. The hard limiters operate as linear amplifiers normally. However, if a high level input temporarily overloads a linear amplifier,

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then the circuit will limit symmetrically, which will help to prevent the output buffer from overloading. This speeds up recovery from an overload event, which can occur during the gain settling. The clipping level is approximately constant over temperature. The first order integrated lowpass filters are used for noise filtering of the down-converted baseband signals for both the I channel and the $Q$ channel. These filters are well matched in gain response. The -3 dB corner frequency is typically 17 MHz . The I/Q outputs can drive $2 \mathrm{k} \Omega$ in parallel with a maximum capacitive loading of 10 pF at 5 MHz , from all four pins to ground. The outputs are internally biased at $\mathrm{V}_{C C}-1.19 \mathrm{~V}$. Figure 5 shows the simplified output circuit schematic of the I channel or $Q$ channel.

The I/Q baseband outputs can be DC-coupled to the inputs of a baseband chip. For AC-coupled applications with large capacitors, the STBY pin can be used to pre-bias the outputs to nominal $\mathrm{V}_{\text {CC }}-1.19 \mathrm{~V}$ at much reduced current. This mode draws only 3.6 mA supply current. When the EN pin is then driven high ( $>1 \mathrm{~V}$ ), the chip is quickly switched to normal operating mode, avoiding the introduction of
large charging time constants. Table 2 shows the logic of the EN pin and STBY pin. In both normal operating mode and standby mode, the maximum discharging current is about $300 \mu \mathrm{~A}$, and the maximum charging current is more than 4 mA . In Figure 5 the simplified circuit schematic of the STBY (or EN) input is shown.

Table 2. The Logic of Different Operating Modes

| EN | STBY | Comments |
| :--- | :--- | :--- |
| Low | Low | Shutdown Mode |
| Low | High | Standby Mode |
| High | Low or High | Normal Operation Mode |



Figure 5. Simplified Circuit Schematic of I Channel (or Q Channel) Outputs and STBY (or EN) Input


Figure 6. Evaluation Circuit Schematic with I/Q Output Buffers

## APPLICATIONS INFORMATION

## Evaluation Board

The evaluation circuit schematic is drawn in Figure 6. The components associated with buffers U 2 and U 3 are included to drive a $50 \Omega$ load for evaluation purposes only.

There is a unity voltage gain relationship for AC signals between the evaluation board outputs (I and $Q$ ) and the $\mathrm{I}_{\text {OUT }^{+}}, \mathrm{I}_{\text {OUT }}{ }^{-}$or Q OUT $^{+}$and $Q_{\text {OUT }}{ }^{-}$outputs of the LT5546 when the evaluation board outputs are terminated in $50 \Omega$.


Figure 7. Component Side Silkscreen of Evaluation Board


Figure 9. Bottom Side Silkscreen of Evaluation Board


Figure 8. Component Side Layout of Evaluation Board


Figure 10. Bottom Side Layout of Evaluation Board


Figure 11. 2.4GHz to 2.5 GHz Receiver Application (RX IF = 280MHz)

## PACKAGE DESCRIPTION

UF Package<br>16-Lead Plastic QFN (4mm $\times 4 \mathrm{~mm}$ )<br>(Reference LTC DWG \# 05-08-1692)



## RELATGD PARTS

| PART NUMBER | DESCRIPTION | COMMENTS |
| :---: | :---: | :---: |
| Infrastructure |  |  |
| LT5511 | High Signal Level Upconverting Mixer | RF Output to 3GHz, 17dBm IIP3, Integrated LO Buffer |
| LT5512 | High Signal Level Downconverting Mixer | DC-3GHz, 20dBm IIP3, Integrated LO Buffer |
| LT5515 | 1.5 GHz to 2.5 GHz Direct-Conversion Quadrature Demodulator | 20dBm IIP3, NF = 16.8dB, Integrated LO Quadrature Generator |
| LT5516 | 800MHz to 1.5 GHz Direct-Conversion Quadrature Demodulator | 4V to 5.25V Supply, 21.5dBm IIP3, NF = 12.8dB, Integrated LO Quadrature Generator |
| LT5522 | 600MHz to 2.7GHz High Signal Level Downconverting Mixer | 4.5V to 5.25V Supply, 25 dBm IIP3 at $900 \mathrm{MHz}, \mathrm{NF}=12.5 \mathrm{~dB}, 50 \Omega$ Single-Ended RF and LO Ports |
| RF Power Detectors |  |  |
| LT5504 | 800MHz to 2.7GHz RF Measuring Receiver | 2.7V to 5.25V Supply, 80dB Dynamic Range, Temperature Compensated |
| LTC5505 | RF Power Detectors with >40dB Dynamic Range | 2.7V to 6V Supply, 300MHz to 3.5GHz, Temperature Compensated |
| LTC5507 | 100kHz to 1000MHz RF Power Detector | 2.7V to 6V Supply, 48dB Dynamic Range, Temperature Compensated |
| LTC5508 | 0.3 GHz to 7GHz RF Power Detector | 2.7V to 6V Supply, 44dB Dynamic Range, Temperature Compensated |
| LTC5509 | 300 MHz to 3GHz RF Power Detector | -30dBm to 6dBm, 600 $\mu$ A Supply Current, Temperature Compensated |
| LTC5532 | 300MHz to 7GHz Precision RF Power Detector | Precision V ${ }_{\text {Out }}$ Offset Control, Adjustable Gain and Offset |
| RF Receiver Building Blocks |  |  |
| LT5500 | 1.8GHz to 2.7GHz Receiver Front End | 1.8 V to 5.25V Supply, Dual-Gain LNA, Mixer |
| LT5502 | 400MHz Quadrature IF Demodulator with RSSI | 1.8 V to 5.25V Supply, 70 MHz to 400MHz IF, 84dB Limiting Gain, 90dB RSSI Range |
| LT5503 | 1.2GHz to 2.7GHz Direct IQ Modulator and Mixer | 1.8 V to 5.25V Supply, Four Step RF Power Control, 120MHz Modulation Bandwidth |
| LT5506 | 40 MHz to 500 MHz Quadrature IF Demodulator with VGA | 1.8 V to 5.25V, I/Q Baseband Bandwidth 8.8MHz, -40dB to 57dB Linear Power Gain |

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