## Features

- 2-Phase 1 A Stepping Motor Driver
- Compensated Half Step Operation
- Chopper Current Control
- Unidirectional Single Wire Bus Interface with Error Feedback
- Intelligent Travel Operation Control
- Referencing by Extending or Retracting


## Application

- Dynamic Headlamp Adjustment


## Benefits

- Error Recognition with Feedback
- Short Circuit Protected Outputs
- Overtemperature Warning and Shut Off
- Supply Voltage Supervision

Electrostatic sensitive device. Observe precautions for handling.


## Description

The circuit serves to control a stepping motor for dynamic headlamp beam adjustment in automobiles. Two chopper-controlled H -bridges serve as the stepping motor driver. The circuit receives the commands to control the stepping motor by means of a unidirectional serial single-wire bus.
An integrated process control independently moves the stepping motor into the new desired position. This allows it to be automatically accelerated and slowed down. The stepping motor is operated in compensated half-step operation. The maximum clock frequency at which the stepping motor is operated depends on the supply voltage, the chip temperature, the operating mode, and position difference.

Intelligent Stepper Motor Driver

Figure 1. Block Diagram


## Pin Configuration

Figure 2. Pinning QFN 28


## Pin Description

| Pin | Symbol | Function |
| :---: | :---: | :---: |
| 1 | VBAT1A | Battery voltage |
| 2 | n.c. | Not connected |
| 3 | SM1A | Connection for stepping motor winding A |
| 4 | SRA | Sense resistor A connection |
| 5 | SM2A | Connection for stepping motor winding A |
| 6 | n.c. | Not connected |
| 7 | VBAT2A | Battery voltage |
| 8 | n.c. | Not connected |
| 9 | SCl1 | Test pin, please connect to ground for EMC reasons |
| 10 | SCO1 | Test pin, please connect to ground for EMC reasons |
| 11 | SCl2 | Test pin, please connect to ground for EMC reasons |
| 12 | SCO2 | Test pin, please connect to ground for EMC reasons |
| 13 | TA | Test pin, please connect to ground for EMC reasons |
| 14 | TTEMP | Test pin, please connect to ground for EMC reasons |
| 15 | VBAT2B | Battery voltage |
| 16 | n.c. | Not connected |
| 17 | SM2B | Connection for stepping motor winding B |
| 18 | SRB | Sense resistor B connection |
| 19 | SM1B | Connection for stepping motor winding B |
| 20 | n.c. | Not connected |
| 21 | VBAT1B | Battery voltage |
| 22 | BUS | Receives the control instructions via the single wire bus from the controller |
| 23 | VDD | 5 V supply voltage output |
| 24 | VSS | Digital signal ground |
| 25 | AGND | Analog signal ground |
| 26 | RSET | Reference current setting. Connected externally with a resistor to AGND. The value of the resistor determines all internal current sources and sinks. |
| 27 | COS | Oscillator pin, connected externally with a capacitor to AGND. The value of the capacitance determines the chopper frequency and the baud rate for data reception. |
| 28 | n.c. | Not connected |

## Functional Description

Analog Part

Figure 3. Analog Blocks


The circuit contains an integrated 5 V regulator to supply the internal logic and analog circuit blocks. The regulator uses an adjusted bandgap as voltage reference. Also all other parts that require an excellent voltage reference, such as the voltage monitoring block refer to the bandgap.
The bias generator derives its accurate currents from an external reference resistor. The oscillator is used for clocking the digital system. All timings like the baud rate, the step duration and the chopper frequency are determined from it. An external capacitor is used for generating the frequency.

The voltage monitoring enables the circuit to drive the stepping motor at different battery voltage levels. According to the battery voltage the stepping motor will be accelerated to a maximum step velocity. In case of under or over voltage the motor will shut off. A temperature monitoring is used for shut off at overtemperature conditions and current boost in case of low temperature.

## Digital Part

Figure 4. Digital Blocks


Figure 4 shows all digital blocks of the circuit. The stepping motor will be controlled by commands via the bus input pin. An analog comparator is used as a level shifter at the input. There is also a possibility of clamping the bus pin to ground. This will be used after detecting an error to feedback this to the microcontroller.

The next block is a UART. Its task is clock recovery and data recognition of the incoming bit stream. For clock recovery a special bitstream is used after each power on. The generated bitstream will be analyzed and after a correct parity check interpreted for execution.

A sophisticated cruise control generates all control signals for the two H-bridge drivers. It uses an internal step-time table for accelerating and decelerating the stepping motor depending on the actual and desired position and the temperature and voltage levels. Exception handling is integrated to interpret and react on the temperature, supply voltage, and coil-current signals from the analog part.

## Stepping Motor Driver

Figure 5. H-bridge Driver Stage


Figure 5 shows the diagram of one H-bridge driver stage. It consists of two NMOS and two PMOS power transistors. An external shunt is used for measuring the current flowing through the motor coil. Additional comparators and current sensing circuitry is integrated for error detection.

## Data Communication

The circuit receives all commands for the stepping motor via a single wire bus. In idle mode the bus pin is pulled up by an internal current source near to VBAT voltage. During the transmission the external transmitter has to pull down the bus level to send information about data and clock timing. The used baud rate has to be about 2400 baud. Because of oscillator tolerances a synchronization sequence has to be sent at the beginning of data transfer.

Figure 6 shows the pattern used for this sequence. The circuit uses the 1-0-1-0 sequences for adjusting the internal bit time. Later on during data transfer every 1-0-1-0 sequence coming up randomly is used for resynchronization. Thus all tolerances that occur during operation will be eliminated.

To obtain a synchronization of up to $15 \%$ oscillator tolerance the pattern has to be sent at least 4 times.

Figure 6. Synchronization Sequence


Between two commands a pause has to be included. This is necessary for a clear recogition of a new message frame (command). Figure 7 shows the timing diagram of two commands.

Figure 7. Message Frame and Space


Every command consists of 16 bits. They will be sent with two bytes. Figure 8 shows the message frame. The high byte is sent first, immediately followed by the low byte. Every byte starts with a start bit and ends with a parity bit and a stop bit. The first start bit (level 0 ) after a pause (level 1) indicates the beginning of a new message frame. The value of the parity bit has to be odd, i.e., the crossfooting of the byte including the parity bit is odd. If a data packet is not recognized due to a transmission error (parity error), the entire command is rejected.

Figure 8. Command Bits


## Bus Commands

There are different commands for controlling the stepping motor. Table 1 shows a list of all implemented commands and their meanings. The first command, the synchronization sequence, is described above. The second group of commands are the reference commands. A reference run command causes the stepping motor to make an initial run. It is used to establish a defined start position for the following position commands. The way the reference run is executed will be described later. There are two reference run commands. The difference is the turn direction of the stepping motor. This makes the circuit more flexible for different applications. The turn direction is coded in the 4 identifier bits.

Table 1. Bus Commands

| Bus Command | High Byte |  |  |  |  |  |  |  | Low Byte |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Data |  | Mode |  | Identifier |  |  |  | Data |  |  |  |  |  |  |  |
|  | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| Synchronization | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 |
| Reference run (extend) | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reference run (retract) | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| New position (0 = full extension) | D8 | D9 | 0 | 0 | 1 | 0 | 0 | 1 | D0 | D1 | D2 | D3 | D4 | D5 | D6 | D7 |
| New position (0 = full retraction) | D8 | D9 | 0 | 0 | 0 | 1 | 1 | 0 | D0 | D1 | D2 | D3 | D4 | D5 | D6 | D7 |
| New position (testmode, $0=$ full extension) | D8 | D9 | 1 | 1 | 1 | 0 | 0 | 1 | D0 | D1 | D2 | D3 | D4 | D5 | D6 | D7 |
| New position (testmode, $0=$ full retraction) | D8 | D9 | 1 | 1 | 0 | 1 | 1 | 0 | D0 | D1 | D2 | D3 | D4 | D5 | D6 | D7 |

The last class of commands are the position commands. Every new position will be sent as an absolute value. This makes the transmission more safe in terms of losing a position command. The next received command tells the stepping motor the right position again. For the position data there are 10 bits available (D0 to D9).

The maximum possible step count to be coded with 10 bit is 1024. Though position commands up to 1024 will be executed, it's prohibited to use values higher than 698, as this is the step count of the reference run. For details see chapter "Reference Run".

There are 4 new position commands. They differ in the identifier and in the modus bits. The identifier fixes the turn direction. For test purposes there are new position commands with a different mode. In this mode the stepping motor works with a reduced coil current. This may be used for end tests in the production of the application.

Any command with modus or identifier different to the first reference run will be ignored. Thus it is also not possible to change modus or identifier by performing a second reference run.

## Power-up Sequence

After power-up the circuit has to be synchronized and a reference run has to be executed before a position command can be carried out. Figure 9 shows a timing diagram on how the necessary sequences follow each other.

Figure 9. Necessary Commands after Power-up


The first sequence is the synchronization sequence. Its pattern (Figure 6) should be sent at least 4 times to be sure that the following commands will be recognized. If there are distortions on the bus it is helpful to send this sequence more than 4 times. A RC lowpass filter at the bus pin (Figure 16) helps to reduce distortsions.

After synchronization the stepping motor has to make the reference run to initialize its zero position. The first reference run will only be executed if the circuit recognizes this command three times in series. This function is implemented contributing to the importance of the reference run. After the reference run the circuit will switch to normal operation. To perform a reference run during normal operation, the command has to be sent only once. Figure 10 shows the state diagram for the implemented sequence processor.

Figure 10. Flow Diagram for the Power-up Sequence


## Reference Run

## Cruise Control

In normal operation, new position commands are transmitted as absolute values. To drive the stepping motor to these absolute positions, the circuit has to know the motor's zero position. Therefore, the stepping motor has to perform a reference run after each power-up in which it is extended or retracted to its limit stop. Before the execution of the reference run, the motor is supplied with hold current.
As the actual position is not known at the beginning of the reference run the whole position range has to be passed. To optimize performance for smaller actuators, the reference run has been reduced to 698 steps. Therefore, it is prohibited to access positions higher than 698, because in a following reference run the stepping motor would not reach its zero position.

If it is necessary that the entire range up to position 1024 can be used, the reference run has to be executed twice. Since any command during reference run is ignored, the second reference command has to be sent about 2.4 s after the first command.

To avoid any possible mistake, e.g., the loss of a step during the reference run or the bouncing at the limit stop, there is a special run to be executed.
This is shown in Table 2.
Table 2. Reference Run Course

| Phase | Action |  | Int. Counter | Steptime |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Ramp up to 446 Hz step frequency | Drive <br> through <br> the whole | 704 | $3300 \mu \mathrm{~s}$ |
|  |  |  | 703 | $2895 \mu \mathrm{~s}$ |
|  |  |  | 702 | $2540 \mu \mathrm{~s}$ |
|  |  |  | 701 | $2240 \mu \mathrm{~s}$ |
|  | Drive at constant speed |  | 700 to 11 | $2240 \mu \mathrm{~s}$ |
|  | Ramp down to minimum step frequency ( 303 Hz ) | range <br> (698 <br> steps) | 10 | 2240 \% |
|  |  |  | 9 | $2549 \mu \mathrm{~s}$ |
| II |  |  | 8 | 2895 ¢ |
| III |  |  | 7 to 6 | $3300 \mu \mathrm{~s}$ |
| IV | Wait for $6 \times 3300 \mu \mathrm{~s}$ with the last coil current |  | 6 | $3300 \mu \mathrm{~s}$ |
| V | Perform another 6 steps with $3300 \mu$ s |  | 5 to 0 | $3300 \mu \mathrm{~s}$ |
| VI | Wait for $5 \times 3300 \mu \mathrm{~s}$ with the last coil current |  | 0 | $3300 \mu \mathrm{~s}$ |
| VII | Set current to hold current; normal operation |  | varied | varied |

The travel operation control independently moves the stepping motor into its new position. To reach the new position as fast as possible but without abrupt velocity changes, the stepping motor is accelerated or slowed down depending on the difference between actual and nominal position. If this difference is huge the stepping frequency will increase (acceleration). When the new position is nearly reached, the frequency will decrease again (deceleration). In the case of a new nominal position opposite to the direction of the motion being from the microcontroller, the stepping frequency will decrease to its starting value $(300 \mathrm{~Hz})$ before the direction can turn. The cruise control is shown in Figure 11.

The possible stepping frequencies for velocity control are shown in Table 3.

Figure 11. Dynamic Frequency Adaption


Table 3. Frequency Ramp

| Number | Step Frequency (Hz) | Step Time $(\boldsymbol{\mu s} \mathbf{)}$ |
| :---: | :---: | :---: |
| 1 | 303 | 3300 |
| 2 | 345 | 2895 |
| 3 | 394 | 2540 |
| 4 | 446 | 2240 |
| 5 | 493 | 2030 |
| 6 | 538 | 1860 |
| 7 | 575 | 1740 |
| 8 | 613 | 1630 |
| 9 | 649 | 1540 |
| 10 | 680 | 1470 |
| 11 | 714 | 1400 |
| 12 | 741 | 1350 |
| 13 | 769 | 1300 |
| 14 | 800 | 1250 |
| 15 | 826 | 1210 |
| 16 | 855 | 1170 |
| 17 | 877 | 1140 |
| 18 | 901 | 1110 |
| 19 | 926 | 1080 |
| 20 | 952 | 1050 |
| 21 | 980 | 1020 |
| 22 | 1000 | 1000 |

In addition to the actual step frequency there is a maximum step frequency up to which the actual step frequency can rise. To secure a correct operation at low supply voltages the maximum value for the stepping frequency is smaller at low voltages. If the supply voltage falls below the 9 V threshold, travel operation will suspend. To restart operation, the supply voltage has to rise above 10.5 V . The relation of the maximum step frequency and the supply voltage during operation is shown in Table 4.

If the chip temperature exceeds the overtemperature warning threshold, the step speed is reduced to 300 Hz . If the chip temperature rises further the output driver is shut off.

Table 4. Maximum Step Frequency

| $\mathbf{V}_{\text {BAT }}$ | Maximum Step Frequency <br> at Rising Voltage | Maximum Step Frequency <br> $\left(\mathbf{V}_{\text {BAT once }}>10.5 \mathrm{~V}\right)$ |
| :--- | :--- | :--- |
| $<9 \mathrm{~V}$ | No operation | No operation |
| 9 V to 9.5 V | No operation | $300 \mathrm{~Hz}(3.33 \mathrm{~ms})$ |
| 9.5 V to 10 V | No operation | $500 \mathrm{~Hz}(2.03 \mathrm{~ms})$ |
| 10 V to 10.5 V | No operation | $680 \mathrm{~Hz}(1,47 \mathrm{~ms})$ |
| 10.5 V to 11 V | $850 \mathrm{~Hz}(1.17 \mathrm{~ms})$ | $850 \mathrm{~Hz}(1.17 \mathrm{~ms})$ |
| $>11 \mathrm{~V}$ | $1000 \mathrm{~Hz}(1 \mathrm{~ms})$ | $1000 \mathrm{~Hz}(1 \mathrm{~ms})$ |
| $>20 \mathrm{~V}$ | No operation | No operation |

## Step Operation

The stepping motor is operated in halfstep-compensation mode. The current for both coils is shown in Figure 12. The current levels are increased when the temperature is below $0^{\circ} \mathrm{C}$ to secure operation. For final tests at the end of the application production line the currents are reduced.

Figure 12. Compensated Halfstep Operation


## Bridge Current Control

The bridge current is controlled by a chopper current control, shown in Figure 13. The current is turned on every $40 \mu \mathrm{~s}$ ( 25 kHz chopper frequency). The current flow in the H bridge is shown in Figure 14a. After a blanking time of $2.5 \mu$ s to suppress turn-on peaks the current is measured via the shunt voltage. As soon as the current has reached its nominal value it is turned off again. The current flow in this state is shown in Figure 14b.

Figure 13. Chopper Current Control


Figure 14. Current Flow in Halfbridge


## Exception Handling

During operation, different exceptional states or errors can arise to which the circuit must correspondingly react. These are described below:

- Supply voltage below 9 V

Travel operation is suspended for the duration of the undervoltage. The output current will be set to zero. When the supply voltage rises above 10.5 V , travel operation restarts.

- Supply voltage above 20 V

Travel operation is suspended for the duration of the undervoltage. The output current will be set to zero. When the supply voltage falls below 20 V , travel operation restarts.

- Overtemperature warning

The maximum stepping speed is reduced to 300 Hz . This ensures a safe shut-off procedure if the temperature increases to shut-off temperature.

- Overtemperature shut-off

Travel operation is suspended when overtemperature is detected. An error signal is sent to the bus master via the bus. Operation can only restart after the supply voltage is shut off.

- Interruption of a stepping motor winding

The motor windings are only checked for interruption when supplied with hold current, not during drive operation. The corresponding output is shut off. The other coil winding is supplied with hold current. An error signal is sent. Operation can only restart after the supply voltage is shut off.

- Short circuit of a stepping motor winding

The corresponding output is shut off. The other coil winding is supplied with hold current. An error signal is sent. Operation can only restart after the supply voltage is shut off.

- Short circuit of an output to ground or $\mathrm{V}_{\mathrm{BAT}}$

The corresponding output is shut off. The other coil winding is supplied with hold current. An error signal is sent. Operation can only restart after the supply voltage is shut off.

An error signal is sent to the microcontroller by clamping the bus to ground for 3 seconds. If the error should occur during a data transmission, the above described reactions will happen immediately except for the clamping. This will take place about $200 \mu \mathrm{~s}$ after the end of the stopbit of the lowbyte to guarantee a correct command recognintion in the second headlamp. The error signal timing is shown in Figure 15.

Figure 15. Error Signal Timing


## Absolute Maximum Ratings

| Parameters | Symbol | Value | Unit |
| :--- | :---: | :---: | :---: |
| Power supply ( t 400 ms ) | $\mathrm{V}_{\text {BAT }}$ | -0.3 to +45 | V |
| DC power supply | $\mathrm{V}_{\text {BAT }}$ | -0.3 to +28 | V |
| DC output current | $\mathrm{I}_{\text {OUT }}$ | $\pm 1.1$ | A |
| BUS input voltage | $\mathrm{V}_{\text {BUS }}$ | -0.3 to $\mathrm{V}_{\text {BAT }}+0.3$ | V |
| Human body model | ESD | 2 | kV |
| Charged device model | ESD | 500 | V |
| Storage temperature | $\mathrm{T}_{\text {Stg }}$ | -55 to +150 | ${ }^{\circ} \mathrm{C}$ |
| Operating temperature | $\mathrm{T}_{\text {op }}$ | -40 to +105 | ${ }^{\circ} \mathrm{C}$ |
| Maximum junction temperature | $\mathrm{T}_{\text {jmax }}$ | +150 | ${ }^{\circ} \mathrm{C}$ |

## Thermal Resistance

| Parameters | Symbol | Value | Unit |
| :--- | :---: | :---: | :---: |
| Thermal resistance junction-case | $\mathrm{R}_{\mathrm{th} J \mathrm{C}}$ | 5 | $\mathrm{~K} / \mathrm{W}$ |
| Thermal resistance junction-ambient | $\mathrm{R}_{\mathrm{thJA}}$ | 35 | $\mathrm{~K} / \mathrm{W}$ |

## Operating Range

| Parameters | Symbol | Value | Unit |
| :--- | :---: | :---: | :---: |
| Power supply range | $\mathrm{V}_{\text {BAT }}$ | 7 to 20 | V |
| Operating temperature range | $\mathrm{T}_{\text {op }}$ | -40 to +105 | ${ }^{\circ} \mathrm{C}$ |

## Electrical Characteristics

| No. | Parameters | Test Conditions | Pin | Symbol | Min. | Typ. | Max. | Unit | Type* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Supply |  |  |  |  |  |  |  |  |
| 1.1 | Supply current | $\begin{aligned} & \mathrm{V}_{\text {BAT }}=14 \mathrm{~V} \\ & \text { (no motor current) } \end{aligned}$ | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | I_total |  | 4 | 7 | mA | A |
| 1.2 | Supply voltage | Normal operation | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $V_{\text {BATsup }}$ | 7.0 |  | 20 | V | C |
| 1.3 | $\mathrm{V}_{\mathrm{DD}}$ voltage |  | 23 | $\mathrm{V}_{\text {VDD_13V }}$ | 4.9 | 5.0 | 5.1 | V | A |
| 1.4 | $\mathrm{V}_{\mathrm{DD}}$ voltage | $\mathrm{V}_{\text {BAT }}=7.0 \mathrm{~V}$ | 23 | $\mathrm{V}_{\text {VDD_7V }}$ | 4.8 | 5.0 | 5.1 | V | A |
| 2 | Bus Port |  |  |  |  |  |  |  |  |
| 2.1 | Threshold voltage | $\mathrm{V}_{\mathrm{BAT}}=12.0 \mathrm{~V}$, rising edge | 22 | $\mathrm{V}_{\text {LH_BUS_12 }}$ | 5.5 | 6.5 | 7.5 | V | A |
| 2.2 | Threshold voltage | $\begin{aligned} & V_{\text {BAT }}=12 \mathrm{~V} \text {, falling } \\ & \text { edge } \end{aligned}$ | 22 | $\mathrm{V}_{\text {HL_Bus_12 }}$ | 4.5 | 5.5 | 6.5 | V | A |
| 2.3 | Hysteresis |  | 22 | $\mathrm{V}_{\text {HYS_BUS12 }}$ |  | 1 |  | V | A |
| 2.4 | Input current | $\mathrm{V}_{\text {BUS }}=0 \mathrm{~V}$ | 22 | Iout_Bus_8 | -400 | -300 | -220 | $\mu \mathrm{A}$ | A |
| 2.5 | Saturation voltage | $\mathrm{I}_{\text {BUS }}=2 \mathrm{~mA}$, bus clamping | 22 | $\mathrm{V}_{\text {SAT_BUS_7 }}$ |  |  | 0.5 | V | A |
| 2.6 | Pulldown current | At error condition | 22 | $\mathrm{IPuldwn} \mathrm{\_7}$ | 2 |  |  | mA | A |
| 3 | Oscillator |  |  |  |  |  |  |  |  |
| 3.1 | Frequency | $\begin{aligned} & \mathrm{COS}=100 \mathrm{pF} \pm 5 \% \\ & \mathrm{R}_{\mathrm{SET}}=20 \mathrm{k} \Omega \pm 1 \% \end{aligned}$ | 27 | $\mathrm{F}_{\text {OSC_13 }}$ | 340 | 400 | 460 | kHz | A |
| 4 | Reference |  |  |  |  |  |  |  |  |
| 4.1 | Reference voltage | $\mathrm{R}_{\text {SET }}=20 \mathrm{k} \Omega \pm 1 \%$ | 26 | $\mathrm{V}_{\text {RSET_13V }}$ | 2.4 | 2.5 | 2.6 | V | A |
| 4.2 | Reference voltage | $\mathrm{V}_{\text {BAT }}=7 \mathrm{~V}$ | 26 | $\mathrm{V}_{\text {RSET_7V }}$ | 2.3 | 2.5 | 2.6 | V | A |
| 5 | Full Bridges |  |  |  |  |  |  |  |  |
| 5.1 | $\mathrm{R}_{\text {DSON }}$ | $\mathrm{R}_{\text {DSON }}$ of half-bridge | $\begin{gathered} 3,5, \\ 17,20 \end{gathered}$ | $\mathrm{R}_{\text {DSon }}$ |  | 1.2 | 1.7 | $\Omega$ | B |

*) Type means: $A=100 \%$ tested, $B=100 \%$ correlation tested, $C=$ Characterized on samples, $D=$ Design parameter Note: 1. cmd = command

## Electrical Characteristics (Continued)

| No. | Parameters | Test Conditions | Pin | Symbol | Min. | Typ. | Max. | Unit | Type* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5.2 | Output current | Output stage off | $\begin{gathered} \hline 3,5, \\ 17,20 \end{gathered}$ | $\mathrm{I}_{\text {LEAK }}$ |  |  | 10 | $\mu \mathrm{A}$ | A |
| 5.3 | Output current | Hold mode $\mathrm{R}_{\mathrm{SHUNT}}=240 \mathrm{~m} \Omega$ | $\begin{gathered} 3,5, \\ 17,20 \end{gathered}$ | $\mathrm{V}_{\text {SHUNT18 }}$ | 40 | 55 | 200 | mA | B |
| 5.4 | Output current | Test mode $\mathrm{R}_{\mathrm{SHUNT}}=240 \mathrm{~m} \Omega$ | $\begin{gathered} 3,5, \\ 17,20 \end{gathered}$ | $\mathrm{V}_{\text {SHUNT99 }}$ | 240 | 300 | 360 | mA | B |
| 5.5 | Output current | Normal mode $\mathrm{R}_{\mathrm{SHUNT}}=240 \mathrm{~m} \Omega$ | $\begin{gathered} 3,5, \\ 17,20 \end{gathered}$ | $\mathrm{V}_{\text {SHUNT182 }}$ | 500 | 550 | 600 | mA | B |
| 5.6 | Output current | $\begin{aligned} & \text { Normal mode } \\ & \left(\mathrm{T}<0^{\circ} \mathrm{C}\right) \\ & \mathrm{R}_{\mathrm{SHUNT}}=240 \mathrm{~m} \Omega \end{aligned}$ | $\begin{gathered} 3,5, \\ 17,20 \end{gathered}$ | $\mathrm{V}_{\text {SHUNT } 218}$ | 600 | 660 | 720 | mA | B |
| 5.7 | Output current | Halfstep compensation $\mathrm{R}_{\text {SHUNT }}=240 \mathrm{~m} \Omega$ | $\begin{gathered} 3,5, \\ 17,20 \end{gathered}$ | $\mathrm{V}_{\text {SHUNT257 }}$ | 700 | 780 | 860 | mA | B |
| 5.8 | Output current | Halfstep compensation ( $\mathrm{T}<0^{\circ} \mathrm{C}$ ) $\mathrm{R}_{\text {SHUNT }}=240 \mathrm{~m} \Omega$ | $\begin{gathered} 3,5, \\ 17,20 \end{gathered}$ | $\mathrm{V}_{\text {SHUNT309 }}$ | 840 | 936 | 1040 | mA | B |
| 5.9 | Overcurrent threshold | Highside switch | $\begin{gathered} 3,5, \\ 17,20 \end{gathered}$ | $\mathrm{l}_{\mathrm{OC} \_\mathrm{H}}$ |  | 1.6 |  | A | A |
| 5.10 | Overcurrent threshold | Lowside switch | $\begin{gathered} 3,5, \\ 17,20 \end{gathered}$ | $l_{\text {Oc_L }}$ |  | 1.6 |  | A | B |
| 5.11 | Chopper frequency |  |  |  |  | 1/16 |  | fcos | D |
| 6 | Voltage Comparators |  |  |  |  |  |  |  |  |
| 6.1 | Threshold voltage | 9.0 V comparator, rising edge | $\begin{gathered} 1,7 \\ 15,21 \end{gathered}$ | $\mathrm{V}_{\text {9_UP }}$ | 8.8 | 9.1 | 9.4 | V | A |
| 6.2 | Threshold voltage | 9.0 V comparator, falling edge | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | V9_Down | 8.6 | 8.9 | 9.2 | V | A |
| 6.3 | Hysteresis | 9.0 V comparator | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{V}_{9}$ _HYS | 60 | 200 | 340 | mV | A |
| 6.4 | Threshold voltage | 9.5 V comparator, rising edge | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{V}_{9 \text { _5_UP }}$ | 9.3 | 9.6 | 9.9 | V | A |
| 6.5 | Threshold voltage | 9.5 V comparator, falling edge | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{V}_{9 \text { _5_Down }}$ | 9.1 | 9.4 | 9.7 | V | A |
| 6.6 | Hysteresis | 9.5 V comparator | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{V}_{9 \_5}$ HYS | 60 | 200 | 340 | mV | A |
| 6.7 | Threshold voltage | 10.0 V comparator, rising edge | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{V}_{10 \_ \text {UP }}$ | 9.8 | 10.1 | 10.4 | V | A |
| 6.8 | Threshold voltage | 10.0 V comparator, falling edge | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{V}_{10 \_ \text {Down }}$ | 9.6 | 9.9 | 10.2 | V | A |
| 6.9 | Hysteresis | 10.0 V comparator | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{V}_{10 \_\mathrm{HYS}}$ | 60 | 200 | 340 | mV | A |
| 6.10 | Threshold voltage | 10.5 V comparator, rising edge | $\begin{gathered} 1,7 \\ 15,21 \end{gathered}$ | $\mathrm{V}_{10 \text { _5_UP }}$ | 10.35 | 10.65 | 10.95 | V | A |
| 6.11 | Threshold voltage | 10.5 V comparator, falling edge | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{V}_{10 \text { _5_Down }}$ | 10.15 | 10.45 | 10.75 | V | A |

[^0]
## Electrical Characteristics (Continued)

| No. | Parameters | Test Conditions | Pin | Symbol | Min. | Typ. | Max. | Unit | Type* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6.12 | Hysteresis | 10.5 V comparator | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{V}_{10 \_5}$ _HYS | 60 | 200 | 340 | mV | A |
| 6.13 | Threshold voltage | 11.0 V comparator, rising edge | $\begin{gathered} 1,7 \\ 15,21 \end{gathered}$ | $\mathrm{V}_{11}$ UUP | 10.8 | 11.1 | 11.4 | V | A |
| 6.14 | Threshold voltage | 11.0 V comparator, falling edge | $\begin{gathered} 1,7 \\ 15,21 \end{gathered}$ | $\mathrm{V}_{11 \text { _Down }}$ | 10.6 | 10.9 | 11.2 | V | A |
| 6.15 | Hysteresis | 11.0 V comparator | $\begin{gathered} 1,7 \\ 15,21 \end{gathered}$ | $\mathrm{V}_{11 \text { _HYS }}$ | 60 | 200 | 340 | mV | A |
| 6.16 | Threshold voltage | 20.0 V comparator, rising edge | $\begin{gathered} 1,7 \\ 15,21 \end{gathered}$ | V ${ }_{\text {20_UP }}$ | 19.7 | 20.2 | 20.7 | V | A |
| 6.17 | Threshold voltage | 20.0 V comparator, falling edge | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{V}_{20 \_ \text {Down }}$ | 19.25 | 19.75 | 20.25 | V | A |
| 6.18 | Hysteresis | 20.0 V comparator | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{V}_{\text {20_HYS }}$ | 200 | 450 | 750 | mV | A |
| 6.19 | Threshold voltage | Motor disable (falling voltage) | $\begin{gathered} 1,7 \\ 15,21 \end{gathered}$ | $\mathrm{V}_{\text {9_Down }}$ | 8.6 | 8.9 | 9.2 | V | A |
| 6.20 | Threshold voltage | Motor enable (rising voltage) | $\begin{gathered} 1,7 \\ 15,21 \end{gathered}$ | $\mathrm{V}_{\text {10_5_UP }}$ | 10.35 | 10.65 | 10.95 | V | A |
| 6.21 | Hyteresis | Undervoltage turn off | $\begin{gathered} 1,7 \\ 15,21 \end{gathered}$ | $\mathrm{M}_{\text {DIS_HYS }}$ | 1.3 | 1.7 | 2.1 | V | A |
| 6.22 | Distance | 9.5 V to 9 V comparator rising edges | $\begin{gathered} 1,7 \\ 15,21 \end{gathered}$ | $\mathrm{D}_{9.5-9 \_R}$ | 300 | 500 | 700 | mV | A |
| 6.23 | Distance | 9.5 V to 9 V comparator falling edges | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{D}_{9.5-9 \mathrm{~F}}$ | 300 | 500 | 700 | mV | A |
| 6.24 | Distance | 10 V to 9.5 V comparator rising edges | $\begin{gathered} 1,7 \\ 15,21 \end{gathered}$ | $\mathrm{D}_{10-9.5 \mathrm{R}}$ | 300 | 500 | 700 | mV | A |
| 6.25 | Distance | 10 V to 9.5 V comparator falling edges | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{D}_{10-9.5 \mathrm{~F}}$ | 300 | 500 | 700 | mV | A |
| 6.26 | Distance | 10.5 V to 10 V comparator rising edges | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{D}_{10.5-10 \mathrm{R}}$ | 300 | 500 | 700 | mV | A |
| 6.27 | Distance | 10.5 V to 10 V comparator falling edges | $\begin{gathered} 1,7 \\ 15,21 \end{gathered}$ | $\mathrm{D}_{10.5-10 \mathrm{~F}}$ | 300 | 500 | 700 | mV | A |
| 6.28 | Distance | 11 V to 10.5 V comparator rising edges | $\begin{gathered} 1,7 \\ 15,21 \end{gathered}$ | $\mathrm{D}_{11-10.5 \mathrm{R}}$ | 300 | 500 | 700 | mV | A |
| 6.29 | Distance | 11 V to 10.5 V comparator falling edges | $\begin{gathered} 1,7, \\ 15,21 \end{gathered}$ | $\mathrm{D}_{11-10.5 \mathrm{~F}}$ | 300 | 500 | 700 | mV | A |

*) Type means: $A=100 \%$ tested, $B=100 \%$ correlation tested, $C=$ Characterized on samples, $D=$ Design parameter
Note: 1. cmd = command

## Electrical Characteristics (Continued)

| No. | Parameters | Test Conditions | Pin | Symbol | Min. | Typ. | Max. | Unit | Type* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7 | Timing |  |  |  |  |  |  |  |  |
| 7.1 | Baud rate | $\mathrm{f}_{\mathrm{cos}}=340 \text { to } 460 \mathrm{kHz} \text {, }$ <br> full synchronization | 22 | Baud | 2350 | 2400 | 2450 | Baud | C, D |
| 7.2 | Delay time | 2 following commands | 22 | T ${ }_{\text {D }}$ | 5 |  |  | ms | C, D |
| 7.3 | Pause time | Between high and low byte | 22 | $\mathrm{T}_{\mathrm{P}}$ |  |  | 0 | $\mu \mathrm{s}$ | C, D |
| 7.4 | Clamping time | Bus error clamping | 22 | Tcl |  | 3 |  | s | C, D |
| 8 | Logic |  |  |  |  |  |  |  |  |
| 8.1 | Reference run detection | Commands in series to execute first reference run |  | Ref3 | 3 | 3 | 3 | cmd ${ }^{(1)}$ | D |
| 8.2 | Synchronization | 15\% oscillator tolerance |  | Sync | 4 |  |  | cmd ${ }^{(1)}$ | D |
| 9 | Thermal Values |  |  |  |  |  |  |  |  |
| 9.1 | Thermal prewarning |  |  | T_150 |  | 150 |  | ${ }^{\circ} \mathrm{C}$ | B |
| 9.2 | Hysteresis | Thermal prewarning |  | T_150 ${ }_{\text {HYS }}$ |  | 10 |  | ${ }^{\circ} \mathrm{C}$ | B |
| 9.3 | Thermal shut down |  |  | T_160 |  | 160 |  | ${ }^{\circ} \mathrm{C}$ | B |
| 9.5 | Thermal current boost |  |  | T_0 |  | 0 |  | ${ }^{\circ} \mathrm{C}$ | B |
| 9.6 | Hysteresis | Thermal currrent boost |  | T_O_HYS |  | 10 |  | ${ }^{\circ} \mathrm{C}$ | B |

${ }^{*}$ ) Type means: $A=100 \%$ tested, $B=100 \%$ correlation tested, $C=$ Characterized on samples, $D=$ Design parameter Note: 1. cmd = command

## Soldering Recommendations

| Parameters | Symbol | Value | Unit |
| :--- | :---: | :---: | :---: |
| Maximum heating rate | $\mathrm{T}_{\mathrm{D}}$ | 1 to 3 | ${ }^{\circ} \mathrm{C} / \mathrm{s}$ |
| Peak temperature in preheat zone | $\mathrm{T}_{\text {PH }}$ | 100 to 140 | ${ }^{\circ} \mathrm{C}$ |
| Duration of time above melting point of solder | $\mathrm{t}_{\mathrm{MP}}$ | minimum 10 <br> maximum 75 | s |
| Peak reflow temperature | $\mathrm{T}_{\text {Peak }}$ | 220 to 225 | ${ }^{\circ} \mathrm{C}$ |
| Maximum cooling rate | $\mathrm{T}_{\text {Peak }}$ | 2 to 4 | ${ }^{\circ} \mathrm{C} / \mathrm{s}$ |

Figure 16. Application Circuit


Table 5. Bill of Material

| Reference | Component | Value |
| :--- | :--- | :--- |
| C1 | Oscillator capacitor | $100 \mathrm{pF}, 5 \%$ |
| C2 | Bus input capacitor | 1 nF |
| C3 | Ceramic capacitor | 100 nF |
| C4 | Capacitor | $10 \mu \mathrm{~F}$ |
| C5 | Capacitor | $100 \mu \mathrm{~F}$ |
| C6 | Capacitor | 100 nF |
| D1 | Rectifier | - |
| R1 | Reference resistor | $20 \mathrm{k} \Omega, 1 \%$ |
| R2 | Bus input resistor | $1 \mathrm{k} \Omega, 5 \%$ |
| R3 | Shunt resistor side A | $0.24 \Omega, 5 \%$ |
| R4 | Shunt resistor side A | $0.24 \Omega, 5 \%$ |

## Ordering Information

| Extended Type Number | Package | Remarks |
| :--- | :---: | :--- |
| ATA6830-PKH | QFN 28 | $7 \mathrm{~mm} \times 7 \mathrm{~mm}$ |

## Package Information

The package is a thermal power package MLF $7 \times 7$ with a soldered leadframe and 28 pins. The overall size is $7 \times 7 \mathrm{~mm}^{2}$.


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[^0]:    *) Type means: $A=100 \%$ tested, $B=100 \%$ correlation tested, $C=$ Characterized on samples, $D=$ Design parameter
    Note: 1. cmd = command

