The QM Series of high current single output dc-dc converters sets new standards for thermal performance and power density in the quarter-brick package.

The QM48T/S25050 converters of the QM Series provide thermal performance in high temperature environments that is comparable to or exceeds the industry's leading 5 V half-bricks. This is accomplished through the use of patent pending circuit, packaging and processing techniques to achieve ultra-high efficiency, excellent thermal management, and a very low body profile.

Low body profile and the preclusion of heat sinks minimize impedance to system airflow, thus enhancing cooling for both upstream and downstream devices. The use of $100 \%$ automation for assembly, coupled with advanced electric and thermal design, results in a product with extremely high reliability.

Operating from a 36-75 V input, the QM Series converters provide outputs that can be trimmed from $-20 \%$ to $+10 \%$ of the nominal output voltage, thus providing outstanding design flexibility.


## Features

- RoHS lead-free solder and lead-solder-exempted products are available
- Delivers up to 25 A @ 5.0 V
- Industry-standard quarter brick pinout
- On-board input differential LC-filter
- High efficiency - no heat sink required
- Start-up into pre-biased output
- No minimum load required
- Available in through-hole and surface-mount packages
- Low profile: 0.28" [7.1 mm] SMT version, 0.31 " [7.9 mm] TH version
- Low weight: 1.1 oz [31.5 g] typical
- Meets Basic Insulation requirements of EN60950
- Withstands 100 V input transient for 100 ms
- Fixed-frequency operation
- Fully protected
- Remote output sense
- Output voltage trim range: $+10 \% /-20 \%$ with industry-standard trim equations
- High reliability: MTBF of 2.6 million hours, calculated per Telcordia TR-332, Method I Case 1
- Positive or negative logic ON/OFF option
- UL60950 recognized in US and Canada and DEMKO certified per IEC/EN60950
- Meets conducted emissions requirements of FCC Class B and EN 55022 Class B with external filter
- All materials meet UL94, V-0 flammability rating

36-75 VDC Input; 5 VDC @ 25 A Quarter-Brick
Changing the Shape of Power

## Electrical Specifications (QM48T25050 and QM48S25050)

Conditions: $T_{A}=25^{\circ} \mathrm{C}$, Airflow $=300$ LFM (1.5 m/s), Vin $=48$ VDC, unless otherwise specified.

| PARAMETER | NOTES | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ABSOLUTE MAXIMUM RATINGS |  |  |  |  |  |
| Input Voltage | Continuous | 0 |  | 80 | VDC |
| Operating Ambient Temperature |  | -40 |  | 85 | ${ }^{\circ} \mathrm{C}$ |
| Storage Temperature |  | -55 |  | 125 | ${ }^{\circ} \mathrm{C}$ |
| INPUT CHARACTERISTICS |  |  |  |  |  |
| Operating Input Voltage Range |  | 36 | 48 | 75 | VDC |
| Input Under Voltage Lockout Turn-on Threshold | Non-latching | 33 | 34 | 35 | VDC |
| Input Under Voltage Lockout Turn-off Threshold |  | 31 | 32 | 33 | VDC |
| Input Voltage Transient | 100 ms |  |  | 100 | VDC |
| Maximum Input Current | 25 ADC, 5 VDC Out @ 36 VDC In |  |  | 3.9 | ADC |
| Input Stand-by Current | $\mathrm{Vin}=48 \mathrm{~V}$, converter disabled |  | 2.65 |  | mADC |
| Input No Load Current (0 load on the output) | V in $=48 \mathrm{~V}$, converter enabled |  | 52 |  | mADC |
| Input Reflected-Ripple Current | 25 MHz bandwidth |  | 12.5 |  | mA PK-PK |
| Input Voltage Ripple Rejection | 120 Hz |  | TBD |  | dB |
| OUTPUT CHARACTERISTICS |  |  |  |  |  |
| External Load Capacitance | Plus full load (resistive) |  |  | 10,000 | $\mu \mathrm{F}$ |
| Output Current Range |  | 0 |  | 25 | ADC |
| Current Limit Inception | Non-latching | 26.25 | 30 | 33 | ADC |
| Peak Short-Circuit Current | Non-latching. Short $=10 \mathrm{~m} \Omega$. |  | 31 | 50 | A |
| RMS Short-Circuit Current | Non-latching |  |  | 6.5 | Arms |
| Output Voltage Set Point (no load) |  | 4.950 | 5.000 | 5.050 | VDC |
| Output Regulation Over Line |  |  | $\pm 2$ | $\pm 5$ | mV |
| Output Regulation Over Load |  |  | $\pm 2$ | $\pm 5$ | mV |
| Output Voltage Range | Over line, load and temperature ${ }^{2}$ | 4.925 |  | 5.075 | VDC |
| Output Ripple and Noise - 25 MHz bandwidth | Full load $+10 \mu \mathrm{~F}$ tantalum $+1 \mu \mathrm{~F}$ ceramic |  | 30 | 50 | $\mathrm{mV}_{\text {PK.PK }}$ |
| ISOLATION CHARACTERISTICS |  |  |  |  |  |
| I/O Isolation |  | 2000 |  |  | VDC |
| Isolation Capacitance |  |  | 1.4 |  | nF |
| Isolation Resistance |  | 10 |  |  | $\mathrm{M} \Omega$ |
| FEATURE CHARACTERISTICS |  |  |  |  |  |
| Switching Frequency |  |  | 340 |  | kHz |
| Output Voltage Trim Range ${ }^{1}$ | Industry-std. equations | -20 |  | +10 | \% |
| Remote Sense Compensation ${ }^{1}$ | Percent of $\mathrm{V}_{\text {Out }}$ (NOM) |  |  | +10 | \% |
| Output Over-Voltage Protection | Non-latching | 117 | 128 | 140 | \% |
| Auto-Restart Period | Applies to all protection features |  | 100 |  | ms |
| Turn-On Time |  |  | 4 |  | ms |
| ON/OFF Control (Positive Logic) |  |  |  |  |  |
| Converter Off |  | -20 |  | 0.8 | VDC |
| Converter On |  | 2.4 |  | 20 | VDC |
| ON/OFF Control (Negative Logic) |  |  |  |  |  |
| Converter Off |  | 2.4 |  | 20 | VDC |
| Converter On |  | -20 |  | 0.8 | VDC |
| DYNAMIC RESPONSE |  |  |  |  |  |
| Load Change $25 \%$ of lout Max, di/dt $=1 \mathrm{~A} / \mu \mathrm{s}$ | $\mathrm{Co}=470 \mu \mathrm{~F}$ tantalum $+1 \mu \mathrm{~F}$ ceramic |  | 120 |  | mV |
| Setting Time to 1\% |  |  | 40 |  | us |
| EFFICIENCY |  |  |  |  |  |
| 100\% Load |  |  | 89.5 |  | \% |
| 50\% Load |  |  | 90.5 |  | \% |

Notes: 1. Vout can be increased up to $10 \%$ via the sense leads or up to $10 \%$ via the trim function, however total output voltage trim from all sources should not exceed $10 \%$ of $\mathrm{V}_{\text {out }}(\mathrm{NOM})$, in order to insure specified operation of over-voltage protection circuitry.
2. $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$

## Operation

## Input and Output Impedance

These power converters have been designed to be stable with no external capacitors when used in low inductance input and output circuits.

However, in many applications, the inductance associated with the distribution from the power source to the input of the converter can affect the stability of the converter. The addition of a $33 \mu \mathrm{~F}$ electrolytic capacitor with an ESR < $1 \Omega$ across the input helps ensure stability of the converter. In many applications, the user has to use decoupling capacitance at the load. The power converter will exhibit stable operation with external load capacitance up to $2,200 \mu \mathrm{~F}$ on 5 V output.

## ON/OFF (Pin 2)

The ON/OFF pin is used to turn the power converter on or off remotely via a system signal. There are two remote control options available, positive logic and negative logic and both are referenced to Vin(-). Typical connections are shown in Fig. A.


Fig. A: Circuit configuration for ON/OFF function.
The positive logic version turns on when the ON/OFF pin is at logic high and turns off when at logic low. The converter is on when the ON/OFF pin is left open.
The negative logic version turns on when the pin is at logic low and turns off when the pin is at logic high. The ON/OFF pin can be hard wired directly to Vin(-) to enable automatic power up of the converter without the need of an external control signal.
ON/OFF pin is internally pulled-up to 5 V through a resistor. A mechanical switch, open collector transistor, or FET can be used to drive the input of the ON/OFF pin. The device must be capable of sinking up to 0.2 mA at a low level voltage of $\leq 0.8 \mathrm{~V}$. An external voltage source of $\pm 20 \mathrm{~V}$ max. may be connected directly to the ON/OFF input, in which case it should be capable of sourcing or sinking up to 1 mA depending on the signal polarity. See
the Start-up Information section for system timing waveforms associated with use of the ON/OFF pin.

## Remote Sense (Pins 5 and 7)

The remote sense feature of the converter compensates for voltage drops occurring between the output pins of the converter and the load. The $\operatorname{SENSE}(-)$ (Pin 5) and SENSE(+) (Pin 7) pins should be connected at the load or at the point where regulation is required (see Fig. B).


Fig. B: Remote sense circuit configuration.
If remote sensing is not required, the $\operatorname{SENSE}(-)$ pin must be connected to the Vout(-) pin (Pin 4), and the SENSE(+) pin must be connected to the Vout( + ) pin (Pin 8) to ensure the converter will regulate at the specified output voltage. If these connections are not made, the converter will deliver an output voltage that is slightly higher than the specified value.
Because the sense leads carry minimal current, large traces on the end-user board are not required. However, sense traces should be located close to a ground plane to minimize system noise and ensure optimum performance. When wiring discretely, twisted pair wires should be used to connect the sense lines to the load to reduce susceptibility to noise.

The converter's output overvoltage protection (OVP) senses the voltage across Vout(+) and Vout(-), and not across the sense lines, so the resistance (and resulting voltage drop) between the output pins of the converter and the load should be minimized to prevent unwanted triggering of the OVP.

When utilizing the remote sense feature, care must be taken not to exceed the maximum allowable output power capability of the converter, equal to the product of the nominal output voltage and the allowable output current for the given conditions.
When using remote sense, the output voltage at the converter can be increased by as much as $10 \%$ above the nominal rating in order to maintain the required voltage across the load. Therefore, the designer must, if necessary, decrease the maximum current (originally
obtained from the derating curves) by the same percentage to ensure the converter's actual output power remains at or below the maximum allowable output power.

## Output Voltage Adjust /TRIM (Pin 6)

The output voltage can be adjusted up $10 \%$ or down $20 \%$ relative to the rated output voltage by the addition of an externally connected resistor.

The TRIM pin should be left open if trimming is not being used. To minimize noise pickup, a $0.1 \mu \mathrm{~F}$ capacitor is connected internally between the TRIM and SENSE(-) pins.

To increase the output voltage, refer to Fig. C. A trim resistor, $\mathrm{R}_{\mathrm{T}-\mathrm{INCR}}$, should be connected between the TRIM (Pin 6) and SENSE(+) (Pin 7), with a value of:
$R_{\text {T-NCR }}=\frac{5.11(100+\Delta) \mathrm{Vo}_{\mathrm{oNOM}}-626}{1.225 \Delta}-10.22[\mathrm{k} \Omega]$
where,
Rt-INCR = Required value of trim-up resistor $k \Omega$ ]
Vo-nom $=$ Nominal value of output voltage [V]
$\Delta=\frac{(\text { Vo-ReQ }- \text { Vo-nom })}{\text { Vo-NOM }} \times 100$ [\%]

Vo-REQ $=$ Desired (trimmed) output voltage [V].
When trimming up, care must be taken not to exceed the converter's maximum allowable output power. See previous section for a complete discussion of this requirement.


Fig. C: Configuration for increasing output voltage.
To decrease the output voltage (Fig. D), a trim resistor, $\mathrm{R}_{\mathrm{T} \text {-DECR }}$, should be connected between the TRIM (Pin 6) and SENSE(-) (Pin 5), with a value of:
$R_{T-D E C R}=\frac{511}{|\Delta|}-10.22[\mathrm{~K} \Omega]$
where,
Rt-DECR $=$ Required value of trim-down resistor [ $\mathrm{k} \Omega$ ] and $\boldsymbol{\Delta}$ is as defined above.

Note: The above equations for calculation of trim resistor values match those typically used in conventional industrystandard quarter-bricks. More information can be found in Output Voltage Trim Feature Application Note.


Fig. D: Configuration for decreasing output voltage.
Trimming/sensing beyond $110 \%$ of the rated output voltage is not an acceptable design practice, as this condition could cause unwanted triggering of the output overvoltage protection (OVP) circuit. The designer should ensure that the difference between the voltages across the converter's output pins and its sense pins does not exceed 0.50 V , or:
$\left[\operatorname{Vou}(+)-\right.$ Vourf $\left._{(-)]}\right]\left[\mathrm{V}_{\text {sense }}(+)-\mathrm{V}_{\text {sense }}(-)\right] \leq 0.50[\mathrm{~V}]$
This equation is applicable for any condition of output sensing and/or output trim.

## Protection Features

## Input Undervoltage Lockout

Input undervoltage lockout is standard with this converter. The converter will shut down when the input voltage drops below a pre-determined voltage.

The input voltage must be at least 35 V for the converter to turn on. Once the converter has been turned on, it will shut off when the input voltage drops below 31 V . This feature is beneficial in preventing deep discharging of batteries used in telecom applications.

## Output Overcurrent Protection (OCP)

The converter is protected against overcurrent or shortcircuit conditions. Upon sensing an overcurrent condition, the converter will switch to constant current operation and thereby begin to reduce output voltage. When the output voltage drops below $60 \%$ of the nominal value of output voltage, the converter will shut down.
Once the converter has shut down, it will attempt to restart nominally every 100 ms with a typical $3 \%$ duty cycle. The attempted restart will continue indefinitely until the overload or short circuit conditions are removed or the output voltage rises above $60 \%$ of its nominal value.

## Output Overvoltage Protection (OVP)

The converter will shut down if the output voltage across Vout(+) (Pin 8) and Vout(-) (Pin 4) exceeds the threshold of the OVP circuitry. The OVP circuitry contains its own reference, independent of the output voltage regulation loop. Once the converter has shut down, it will attempt to restart every 100 ms until the OVP condition is removed.

## Overtemperature Protection (OTP)

The converter will shut down under an overtemperature condition to protect itself from overheating caused by operation outside the thermal derating curves, or operation in abnormal conditions such as system fan failure. After the converter has cooled to a safe operating temperature, it will automatically restart.

## Safety Requirements

The converters meet North American and International safety regulatory requirements per UL60950 and EN60950. Basic Insulation is provided between input and output.

To comply with safety agencies' requirements, an input line fuse must be used external to the converter. A fuse with rating of 7 A is recommended for use with this product.

## Electromagnetic Compatibility (EMC)

EMC requirements must be met at the end-product system level, as no specific standards dedicated to EMC characteristics of board mounted component dc-dc converters exist. However, Power-One tests their converters to several system level standards, primary of which is the more stringent EN55022, Information technology equipment - Radio disturbance characteristics Limits and methods of measurement.
Effective internal LC differential filter significantly reduces input reflected ripple current, and improves EMC.

With the addition of a simple external filter, all versions of the QM Series of converters pass the requirements of Class B conducted emissions per EN55022 and FCC, and meet at a minimum, Class A radiated emissions per EN 55022 and Class B per FCC Title 47CFR, Part 15-J. Please contact Power-One Applications Engineering for details of this testing.


Fig. H: Location of the thermocouple for thermal testing.

## Characterization

## General Information

The converter has been characterized for many operational aspects, to include thermal derating (maximum load current as a function of ambient temperature and airflow) for vertical and horizontal mounting, efficiency, start-up and shutdown parameters, output ripple and noise, transient response to load step-change, overload, and short circuit.

The following pages contain specific plots or waveforms associated with the converter. Additional comments for specific data are provided below.

## Test Conditions

All data presented were taken with the converter soldered to a test board, specifically a 0.060 " thick printed wiring board (PWB) with four layers. The top and bottom layers were not metalized. The two inner layers, comprising twoounce copper, were used to provide traces for connectivity to the converter.

The lack of metalization on the outer layers as well as the limited thermal connection ensured that heat transfer from the converter to the PWB was minimized. This provides a worst-case but consistent scenario for thermal derating purposes.

All measurements requiring airflow were made in vertical and horizontal wind tunnel facilities using Infrared (IR) thermography and thermocouples for thermometry.

Ensuring components on the converter do not exceed their ratings is important to maintaining high reliability. If one anticipates operating the converter at or close to the maximum loads specified in the derating curves, it is prudent to check actual operating temperatures in the application. Thermographic imaging is preferable; if this capability is not available, then thermocouples may be used. Power-One recommends the use of AWG \#40 gauge thermocouples to ensure measurement accuracy. Careful routing of the thermocouple leads will further minimize measurement error. Refer to Figure H for optimum measuring thermocouple location.

## Thermal Derating

Load current vs. ambient temperature and airflow rates are given in Figs. 1-4 for vertical and horizontal converter mounting both through-hole and surface mount version. Ambient temperature was varied between $25^{\circ} \mathrm{C}$ and $85^{\circ} \mathrm{C}$, with airflow rates from 30 to 500 LFM ( 0.15 to $2.5 \mathrm{~m} / \mathrm{s}$ ).

For each set of conditions, the maximum load current was defined as the lowest of:
(i) The output current at which either any FET junction temperature did not exceed a maximum specified temperature $\left(120^{\circ} \mathrm{C}\right)$ as indicated by the thermographic image, or
(ii) The nominal rating of the converter (25 A)

During normal operation, derating curves with maximum FET temperature less than or equal to $120^{\circ} \mathrm{C}$ should not be exceeded. Temperature on the PCB at the thermocouple location shown in Fig. H should not exceed $118{ }^{\circ} \mathrm{C}$ in order to operate inside the derating curves.

## Efficiency

Fig. 5 shows the efficiency vs. load current plot for ambient temperature of $25^{\circ} \mathrm{C}$, airflow rate of $300 \mathrm{LFM}(1.5 \mathrm{~m} / \mathrm{s})$ with vertical mounting and input voltages of $36 \mathrm{~V}, 48 \mathrm{~V}$ and 72 V . Also, a plot of efficiency vs. load current, as a function of ambient temperature with Vin $=48 \mathrm{~V}$, airflow rate of 200 LFM ( $1 \mathrm{~m} / \mathrm{s}$ ) with vertical mounting is shown in Fig. 6.

## Power Dissipation

Fig. 7 shows the power dissipation vs. load current plot for $\mathrm{Ta}=25^{\circ} \mathrm{C}$, airflow rate of $300 \mathrm{LFM}(1.5 \mathrm{~m} / \mathrm{s})$ with vertical mounting and input voltages of $36 \mathrm{~V}, 48 \mathrm{~V}$ and 72 V . Also, a plot of power dissipation vs. load current, as a function of ambient temperature with Vin $=48 \mathrm{~V}$, airflow rate of 200 LFM (1 m/s) with vertical mounting is shown in Fig. 8.

## Start-up

Output voltage waveforms, during the turn-on transient using the ON/OFF pin for full rated load currents (resistive load) are shown without and with external load capacitance in Fig. 9 and Fig. 10, respectively.

## Ripple and Noise

Figure 12 shows the output voltage ripple waveform, measured at full rated load current with a $10 \mu \mathrm{~F}$ tantalum and $1 \mu \mathrm{~F}$ ceramic capacitor across the output. Note that all output voltage waveforms are measured across a $1 \mu \mathrm{~F}$ ceramic capacitor.

The input reflected ripple current waveforms are obtained using the test setup shown in Fig 13. The corresponding waveforms are shown in Figs. 14 and 15.

36-75 VDC Input; 5 VDC @ 25 A Quarter-Brick
Changing the Shape of Power

## Start-up Information (using negative ON/OFF)

## Scenario \#1: Initial Start-up From Bulk Supply

ON/OFF function enabled, converter started via application of $V_{\text {IN }}$. See Figure E.

## Time

## Comments

$t_{0} \quad$ ON/OFF pin is ON; system front end power is toggled on, $\mathrm{V}_{\text {IN }}$ to converter begins to rise.
$\mathrm{t}_{1} \quad \mathrm{~V}_{\text {IN }}$ crosses Under-Voltage Lockout protection circuit threshold; converter enabled.
$\mathrm{t}_{2} \quad$ Converter begins to respond to turn-on command (converter turn-on delay).
$t_{3} \quad$ Converter Vout reaches $100 \%$ of nominal value. For this example, the total converter start-up time ( $\mathrm{t}_{3}-\mathrm{t}_{1}$ ) is typically 4 ms .

## Scenario \#2: Initial Start-up Using ON/OFF Pin

With $\mathrm{V}_{\text {IN }}$ previously powered, converter started via ON/OFF pin. See Figure F.

| Time | Comments |
| :---: | :--- |
| $t_{0}$ | $V_{\text {Input }}$ at nominal value. |
| $t_{1}$ | Arbitrary time when ON/OFF pin is enabled (converter |
| enabled). |  |
| $t_{2}$ | End of converter turn-on delay. |
| $t_{3}$ | Converter Vout reaches 100\% of nominal value. |
| For this example, the total converter start-up time $\left(t_{3}-t_{1}\right)$ is |  |
| typically 4 ms. |  |

## Scenario \#3: Turn-off and Restart Using ON/OFF Pin

With $\mathrm{V}_{\text {IN }}$ previously powered, converter is disabled and then enabled via ON/OFF pin. See Figure G.

## Time

Comments
$t_{0} \quad V_{\text {IN }}$ and $V_{\text {OUt }}$ are at nominal values; ON/OFF pin ON.
$\mathrm{t}_{1} \quad$ ON/OFF pin arbitrarily disabled; converter output falls to zero; turn-on inhibit delay period ( 100 ms typical) is initiated, and ON/OFF pin action is internally inhibited.
$t_{2} \quad$ ON/OFF pin is externally re-enabled.
If $\left(\mathbf{t}_{\mathbf{2}} \mathbf{t}_{\mathbf{1}}\right) \leq \mathbf{1 0 0} \mathbf{~ m s}$, external action of ON/OFF pin is locked out by start-up inhibit timer.
If $\left(\mathrm{t}_{2}-\mathrm{t}_{1}\right)>\mathbf{1 0 0} \mathbf{~ m s}$, ON/OFF pin action is internally enabled.
$t_{3}$ Turn-on inhibit delay period ends. If ON/OFF pin is ON, converter begins turn-on; if off, converter awaits ON/OFF pin ON signal; see Figure F.
$\mathrm{t}_{4} \quad$ End of converter turn-on delay.
$t_{5} \quad$ Converter Vout reaches $100 \%$ of nominal value. For the condition, $\left(\mathbf{t}_{\mathbf{2}}-\mathbf{t}_{\mathbf{1}}\right) \leq \mathbf{1 0 0} \mathbf{~ m s}$, the total converter start-up time ( $\mathrm{t}_{5}-\mathrm{t}_{2}$ ) is typically 104 ms . For ( $\mathrm{t}_{2}-\mathrm{t}_{1}$ ) > $\mathbf{1 0 0} \mathbf{~ m s}$, start-up will be typically 4 ms after release of ON/OFF pin.


Fig. E: Start-up scenario \#1.


Fig. F: Start-up scenario \#2.


Fig. G: Start-up scenario \#3.


Fig. 1: Available load current vs. ambient air temperature and airflow rates for QM48T25050 converter with B height pins mounted vertically with air flowing from pin 3 to pin 1, MOSFET temperature $\leq 120^{\circ} \mathrm{C}$, Vin $=48 \mathrm{~V}$.


Fig. 3: Available load current vs. ambient temperature and airflow rates for QM48S25050 converter mounted vertically with Vin $=48$ V , air flowing from pin 3 to pin 1 and maximum FET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 2: Available load current vs. ambient air temperature and airflow rates for QM48T25050 converter with B height pins mounted horizontally with air flowing from pin 3 to pin 1, MOSFET temperature $\leq 120^{\circ} \mathrm{C}$, $\mathrm{Vin}=48 \mathrm{~V}$.


Fig. 4: Available load current vs. ambient temperature and airflow rates for QM48S25050 converter mounted horizontally with Vin = 48 V , air flowing from pin 3 to pin 1 and maximum FET temperature $\leq 120^{\circ} \mathrm{C}$.


Fig. 5: Efficiency vs. load current and input voltage for converter mounted vertically with air flowing from pin 3 to pin 1 at a rate of $300 \mathrm{LFM}(1.5 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 7: Power dissipation vs. load current and input voltage for converter mounted vertically with air flowing from pin 3 to pin 1 at a rate of $300 \mathrm{LFM}(1.5 \mathrm{~m} / \mathrm{s})$ and $\mathrm{Ta}=25^{\circ} \mathrm{C}$.


Fig. 6: Efficiency vs. load current and ambient temperature for converter mounted vertically with Vin $=48 \mathrm{~V}$ and air flowing from pin 3 to pin 1 at a rate of 200 LFM ( $1.0 \mathrm{~m} / \mathrm{s}$ ).


Fig. 8: Power dissipation vs. load current and ambient temperature for converter mounted vertically with Vin $=48 \mathrm{~V}$ and air flowing from pin 3 to pin 1 at a rate of 200 LFM (1.0 $\mathrm{m} / \mathrm{s}$ ).


Fig. 9: Turn-on transient at full rated load current (resistive) with no output capacitor at Vin $=48 \mathrm{~V}$, triggered via ON/OFF pin. Top trace: ON/OFF signal ( $5 \mathrm{~V} / \mathrm{div}$.). Bottom trace: output voltage ( $2 \mathrm{~V} / \mathrm{div}$.) Time scale: $2 \mathrm{~ms} / \mathrm{div}$.


Fig. 11: Output voltage response to load current step-change (12.5 A - 18.75 A - 12.5 A) at Vin $=48 \mathrm{~V}$. Top trace: output voltage (100 mV/div.). Bottom trace: load current (5 A/div). Current slew rate: $1 \mathrm{~A} / \mu \mathrm{s}$. Co $=470 \mu \mathrm{~F}$ tantalum $+1 \mu \mathrm{~F}$ ceramic. Time scale: $0.2 \mathrm{~ms} / \mathrm{div}$.


Fig. 10: Turn-on transient at full rated load current (resistive) plus $10,000 \mu \mathrm{~F}$ at Vin $=48 \mathrm{~V}$, triggered via ON/OFF pin. Top trace: ON/OFF signal ( $5 \mathrm{~V} /$ div.). Bottom trace: output voltage (2 V/div.). Time scale: $2 \mathrm{~ms} / \mathrm{div}$.


Fig. 12: Output voltage ripple ( $20 \mathrm{mV} / \mathrm{div}$.) at full rated load current into a resistive load with $\mathrm{Co}=10 \mu \mathrm{~F}$ tantalum +1 uF ceramic and Vin $=48 \mathrm{~V}$. Time scale: $1 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 13: Test setup for measuring input reflected ripple currents, $\boldsymbol{i}_{c}$ and $\boldsymbol{i}_{s}$.


Fig. 14: Input reflected ripple current, $\boldsymbol{i}_{\text {S }}(10 \mathrm{~mA} / \mathrm{div})$, measured through $10 \mu \mathrm{H}$ at the source at full rated load current and Vin = 48 V . Refer to Fig. 13 for test setup. Time scale: $1 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 16: Output voltage vs. load current showing current limit point and converter shutdown point. Input voltage has almost no effect on current limit characteristic.


Fig. 15: Input reflected ripple current, $i_{c}$ ( $200 \mathrm{~mA} / \mathrm{div}$ ), measured at input terminals at full rated load current and Vin = 48 V . Refer to Fig. 13 for test setup. Time scale: $1 \mu \mathrm{~s} / \mathrm{div}$.


Fig. 17: Load current (top trace, 20 A/div, $20 \mathrm{~ms} / \mathrm{div}$ ) into a 10 $\mathrm{m} \Omega$ short circuit during restart, at Vin $=48 \mathrm{~V}$. Bottom trace ( 20 A/div, $1 \mathrm{~ms} / \mathrm{div}$ ) is an expansion of the on-time portion of the top trace.

Physical Information


QM48S (Surface Mount)

| Pin Connections |  |
| :---: | :---: |
| Pin \# | Function |
| 1 | Vin ( + ) |
| 2 | ON/OFF |
| 3 | Vin (-) |
| 4 | Vout (-) |
| 5 | SENSE $(-)$ |
| 6 | TRIM |
| 7 | SENSE $(+)$ |
| 8 | $\operatorname{Vout}(+)$ |



## QM48T (Through-hole)

| Height <br> Option | HT <br> (Max. Height) | CL <br> (Min. Clearance) |
| :---: | :---: | :---: |
|  | $+0.000[+0.00]$ | $+0.016[+0.41]$ |
|  | $-0.038[-0.97]$ | $-0.000[-0.00]$ |
| A | $0.325[8.26]$ | $0.030[0.77]$ |
| B | $0.358[9.09]$ | $0.063[1.60]$ |
| D | $0.422[10.72]$ | $0.127[3.23]$ |


| Pin <br> Option | PL <br> Pin Length |
| :---: | :---: |
|  | $\pm 0.005[ \pm 0.13]$ |
| A | $0.188[4.77]$ |
| B | $0.145[3.68]$ |
| C | $0.110[2.79]$ |

## Converter Part Numbering/Ordering Information

| Product Series | Input <br> Voltage | Mounting Scheme | Rated Load Current | Output Voltage |  | ON/OFF Logic | Maximum Height [HT] | Pin Length $[\mathrm{PL}]$ | Special Features | RoHS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| QM | 48 | T | 25 | 050 | - | N | B | A | 0 |  |
| $1 / 4^{\text {th }}$ <br> Brick <br> Format | $36-75 \mathrm{~V}$ | $\mathrm{S} \Rightarrow$ <br> Surface <br> Mount <br> $\mathrm{T} \Rightarrow$ <br> Throughhole | 25 ADC | $050 \Rightarrow 5.0 \mathrm{~V}$ |  | $N \Rightarrow$ Negative $P \Rightarrow$ <br> Positive | $\begin{gathered} \stackrel{\text { SMT }}{\Rightarrow 0.295^{\prime \prime}} \\ \\ \text { Through hole } \\ \hline A \Rightarrow 0.325^{\prime \prime} \\ B \Rightarrow 0.358^{\prime \prime} \\ D \Rightarrow 0.422^{\prime \prime} \end{gathered}$ | $\begin{gathered} 0 \stackrel{\text { SMT }}{\Rightarrow 0.00^{\prime \prime}} \\ \frac{\text { Through }}{\text { hole }} \\ A \Rightarrow 0.188^{\prime \prime} \\ B \Rightarrow 0.145^{\prime \prime} \\ C \Rightarrow 0.110^{\prime \prime} \end{gathered}$ | $0 \Rightarrow$ STD | No Suffix $\Rightarrow$ RoHS lead-solderexemption compliant <br> $\mathrm{G} \Rightarrow \mathrm{RoHS}$ compliant for all six substances |

The example above describes P/N QM48T25050-NBAO: 36-75 V input, through-hole, 25 A @ 5 V output, negative ON/OFF logic, a maximum height of 0.358 ", a through the board pin length of 0.188 ", and RoHS lead-solder-exemption compliancy. Please consult factory regarding availability of a specific version.

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