

# YNV12T10 DC-DC Converter

9.6 - 14 VDC Input; 0.7525 - 5.5 VDC  
Programmable @ 10 A



## Key Features & Benefits

- RoHS lead-free solder and lead-solder-exempted products are available
- Delivers up to 10 A (50 W)
- Industry-standard footprint and pinout
- Single-In-Line (SIP) Package: 2.0" x 0.575" x 0.327" (50.8 x 14.59 x 8.30 mm)
- Weight: 0.25 oz [7 g]
- Synchronous Buck Converter topology
- Start-up into pre-biased output
- No minimum load required
- Operating ambient temperature: -40 °C to 85 °C
- Remote output sense
- Remote ON/OFF (Positive or Negative)
- Fixed-frequency operation
- Auto-reset output overcurrent protection
- Auto-reset overtemperature protection
- High reliability, MTBF = 35.5 million hours
- All materials meet UL94, V-0 flammability rating
- Approved to the latest edition and amendment of ITE Safety standards, UL/CSA 60950-1 and IEC60950-1

Bel Power Solutions point-of-load converters are recommended for use with regulated bus converters in an Intermediate Bus Architecture (IBA). The YNV12T10 non-isolated DC-DC converters deliver up to 10 A of output current in an industry-standard through hole (SIP) package. The YNV12T10 converters operate from a 9.6-14 VDC input. These converters are ideal choices for Intermediate Bus Architectures where Point-of-Load power delivery is generally a requirement. They provide a resistor-programmable regulated output voltage of 0.7525 V to 5.5 V.

The YNV12T10 converters provide exceptional thermal performance, even in high temperature environments with minimal airflow. This is accomplished through the use of circuit, packaging and processing techniques to achieve ultra-high efficiency, excellent thermal management and a very sleek body profile.

The sleek body profile and the preclusion of heat sinks minimize impedance to system airflow, thus enhancing cooling for both upstream and downstream devices.

The use of 100% automation for assembly, coupled with advanced power electronics and thermal design, results in a product with extremely high reliability.

## Applications

- Intermediate Bus Architectures
- Telecommunications
- Data Communications
- Distributed Power Architectures
- Servers, Workstations

## Benefits

- High efficiency – no heat sink required
- Reduces Total Solution Board Area
- Minimizes Part Numbers in Inventory

## ELECTRICAL SPECIFICATIONS

Conditions:  $T_A = 25\text{ }^\circ\text{C}$ , Airflow = 200 LFM (1 m/s),  $V_{in} = 12\text{ VDC}$ ,  $V_{out} = 0.7525 - 5.0\text{ V}$ , unless otherwise specified.

PARAMETER	NOTES	MIN	TYP	MAX	UNITS
<b>ABSOLUTE MAXIMUM RATINGS</b>					
Input Voltage	Continuous	-0.3		15	VDC
Operating Ambient Temperature		-40		85	$^\circ\text{C}$
Storage Temperature		-55		125	$^\circ\text{C}$
<b>FEATURE CHARACTERISTICS</b>					
Switching Frequency			300		kHz
Output Voltage Programming Range <sup>1</sup>	By external resistor, See Trim Table 1	0.7525		5.5	VDC
Remote Sense Compensation				0.5	VDC
Turn-On Delay Time <sup>2</sup>	Full resistive load				
With $V_{in}$ (Converter Enabled, then $V_{in}$ applied)	From $V_{in} = V_{in}(\text{min})$ to $V_o = 0.1 * V_o(\text{nom})$		3.5		ms
With Enable ( $V_{in} = V_{in}(\text{nom})$ applied, then enabled)	From enable to $V_o = 0.1 * V_o(\text{nom})$		3.5		ms
Rise time <sup>2</sup>	From 10% to 90%, full resistive load		3.5		ms
ON/OFF Control (Positive Logic) <sup>3</sup>	Converter Off	-5		0.8	VDC
	Converter On	2.4		$V_{IN}$	VDC
ON/OFF Control (Negative Logic) <sup>3</sup>	Converter Off	2.4		$V_{IN}$	VDC
	Converter On	-5		0.8	VDC
<b>INPUT CHARACTERISTICS</b>					
Operating Input Voltage Range		9.6	12	14	VDC
Input Under Voltage Lockout	Turn-on Threshold		9.0		VDC
	Turn-off Threshold		8.5		VDC
Maximum Input Current	10 ADC Out @ 9.6 VDC In				
	$V_{OUT} = 5.0\text{ VDC}$			6.0	ADC
	$V_{OUT} = 3.3\text{ VDC}$			4.0	ADC
	$V_{OUT} = 2.5\text{ VDC}$			3.1	ADC
	$V_{OUT} = 2.0\text{ VDC}$			2.5	ADC
	$V_{OUT} = 1.8\text{ VDC}$			2.2	ADC
	$V_{OUT} = 1.5\text{ VDC}$			1.9	ADC
	$V_{OUT} = 1.2\text{ VDC}$			1.6	ADC
	$V_{OUT} = 1.0\text{ VDC}$			1.3	ADC
Input Stand-by Current (Converter disabled)			5		mA
Input No Load Current (Converter enabled)	$V_{OUT} = 5.0\text{ VDC}$		80		mA
	$V_{OUT} = 3.3\text{ VDC}$		60		mA
	$V_{OUT} = 2.5\text{ VDC}$		50		mA
	$V_{OUT} = 2.0\text{ VDC}$		45		mA
	$V_{OUT} = 1.8\text{ VDC}$		40		mA
	$V_{OUT} = 1.5\text{ VDC}$		37		mA
	$V_{OUT} = 1.2\text{ VDC}$		35		mA
	$V_{OUT} = 1.0\text{ VDC}$		33		mA
Input Reflected-Ripple Current - $i_s$	See Fig. E for setup. (BW = 20 MHz)		TBD		mA <sub>p-p</sub>
Input Voltage Ripple Rejection	120 Hz		72		dB

OUTPUT CHARACTERISTICS				
Output Voltage Set Point (no load)		-1.5	V <sub>out</sub>	+1.5 %V <sub>out</sub>
Output Regulation				
Over Line	Full resistive load		0.2	%V <sub>out</sub>
Over Load	From no load to full load		0.4	%V <sub>out</sub>
Output Voltage Range	(Overall operating input voltage, resistive load and temperature conditions until end of life)	-2.5		+2.5 %V <sub>out</sub>
Output Ripple and Noise - 20MHz bandwidth (Fig. E)				
Peak-to-Peak	V <sub>OUT</sub> = 1.0 VDC		10	20 mV <sub>P-P</sub>
Peak-to-Peak	V <sub>OUT</sub> = 5.0 VDC		25	40 mV <sub>P-P</sub>
External Load Capacitance Plus full load (resistive)				
Min. ESR > 1mΩ				1000 μF
Min. ESR > 10 mΩ				5000 μF
Output Current Range		0		10 ADC
Output Current Limit Inception (I <sub>OUT</sub> )			15	A
Output Short- Circuit Current	Short=10 mΩ, continuous		2	A <sub>rms</sub>
DYNAMIC RESPONSE				
load step from 5A to 10A with di/dt = 5 A/μS	Co = 100 μF ceramic		120 <sup>4</sup>	mV
Settling Time (V <sub>OUT</sub> < 10% peak deviation)			60	μs
load step change from 10A – 5A with di/dt = -5 A/μS	Co = 100 μF ceramic		120 <sup>4</sup>	mV
Settling Time (V <sub>OUT</sub> < 10% peak deviation)			60	μs
EFFICIENCY				
	Full load (10A)			
	V <sub>OUT</sub> = 5.0 VDC		94.0	%
	V <sub>OUT</sub> = 3.3 VDC		93.0	%
	V <sub>OUT</sub> = 2.5 VDC		92.0	%
	V <sub>OUT</sub> = 2.0 VDC		90.5	%
	V <sub>OUT</sub> = 1.8 VDC		90.0	%
	V <sub>OUT</sub> = 1.5 VDC		88.5	%
	V <sub>OUT</sub> = 1.2 VDC		87.0	%
	V <sub>OUT</sub> = 1.0 VDC		85.0	%

Notes:

- <sup>1</sup> The output voltage should not exceed 5.5V (taking into account both the programming and remote sense compensation).
- <sup>2</sup> Note that start-up time is the sum of turn-on delay time and rise time.
- <sup>3</sup> Converter is on if ON/OFF pin is left open.
- <sup>4</sup> See attached waveforms for dynamic response and settling time for different output voltages.



## OPERATIONS

### Input and Output Impedance

The YNV12T10 converter should be connected via a low impedance to DC power source. In many applications, the inductance associated with the distribution from the power source to the input of the converter can affect the stability of the converter. It is recommended to use decoupling capacitors in order to ensure stability of the converter and reduce input ripple voltage. Converter has internal input capacitance of 20  $\mu\text{F}$  with very low ESR ceramic capacitors. In a typical application, low - ESR tantalum or POS capacitors will be sufficient to provide adequate ripple voltage filtering and at the input of the converter. However, very low ESR ceramic capacitors 47 $\mu\text{F}$ -100 $\mu\text{F}$  are recommended at the input of the converter in order to minimize the input ripple voltage. They should be placed as close as possible to the input pins of the converter.

YNV12T10 has been designed for stable operation with or without external capacitance. Low ESR ceramic capacitors placed as close as possible to the load (Min 47 $\mu\text{F}$ ) are recommended for improved transient performance and lower output voltage ripple.

It is important to keep low resistance and low inductance PCB traces when connecting the load to the output pins of the converter in order to maintain good load regulation.

### ON/OFF (Pin 10)

The ON/OFF pin is used to turn the power converter on or off remotely via a system signal. There are two remote control options available, positive logic (standard option) and negative logic, and both are referenced to GND. Typical connections are shown in Fig. A.

The positive logic version turns the converter on when the ON/OFF pin is at a logic high or left open, and turns the converter off when at a logic low or shorted to GND.

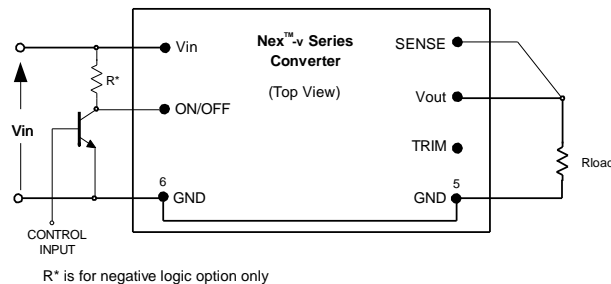


Fig. A: Circuit configuration for ON/OFF function.

The negative logic version turns the converter on when the ON/OFF pin is at a logic low or left open, and turns Converter off when the ON/OFF pin is at a logic high or connected to Vin.

ON/OFF pin is internally pulled up to Vin for positive logic version, and pulled down for negative logic version. A TTL or CMOS logic gate, open collector (open drain) transistor can be used to drive ON/OFF pin. When using open collector (open drain) transistor with a negative logic option, add a pull-up resistor ( $R^*$ ) of 75K to Vin as shown in Fig. A; This device must be capable of:

- sinking up to 0.2 mA at a low level voltage of  $\leq 0.8\text{V}$
- sourcing up to 0.25 mA at a high logic level of 2.3V – 5V
- sourcing up to 0.75 mA when connected to Vin.

### Remote Sense (Pin 3)

The remote sense feature of the converter compensates for voltage drops occurring only between Vout pins of the converter and the load. The SENSE pin (Pin 3) should be connected at the load or at the point where regulation is required (see Fig. B). There is no sense feature on the output GND return pin, where the solid ground plane should provide low voltage drop.

If remote sensing is not required, the SENSE pin must be connected to any of the Vout pins to ensure the converter will regulate at the specified output voltage. If these connections are not made, the converter will deliver an output voltage that is slightly higher than the specified value.

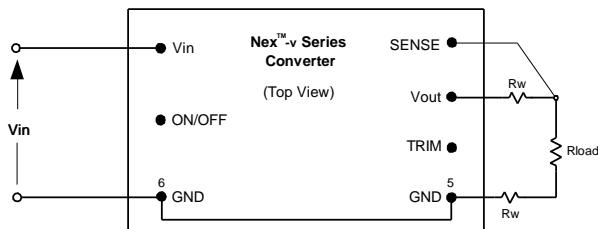


Fig. B: Remote sense circuit configuration.

Because the sense lead carries minimal current, large trace on the end-user board is not required. However, the sense trace should be located close to a ground plane to minimize system noise and insure optimum performance.

When utilizing the remote sense feature, care must be taken not to exceed the maximum allowable output power capability of the converter, equal to the product of the nominal output voltage and the allowable output current for the given conditions.

When using remote sense, the output voltage at the converter can be increased up to 0.5V above the nominal rating in order to maintain the required voltage across the load. Therefore, the designer must, if necessary, decrease the maximum current (originally obtained from the derating curves) by the same percentage to ensure the converter’s actual output power remains at or below the maximum allowable output power.

### Output Voltage Programming (Pin 9)

The output voltage can be programmed from 0.7525V to 5.5V by connecting an external resistor between the TRIM pin (Pin 9) and the GND pin (Pin 5); see Fig. C.

A trim resistor,  $R_{TRIM}$ , for a desired output voltage can be calculated using the following equation:

$$R_{TRIM} = \frac{10.5}{(V_{O-REQ} - 0.7525)} - 1 \quad [k\Omega]$$

where,

$R_{TRIM}$  = Required value of trim resistor [kΩ]

$V_{O-REQ}$  = Desired (trimmed) output voltage [V]

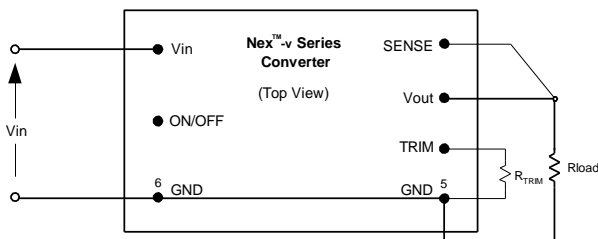


Fig. C: Configuration for programming output voltage.

Note that the tolerance of a trim resistor directly affects the output voltage tolerance. It is recommended to use standard 1% or 0.5% resistors; for tighter tolerance, two resistors in parallel are recommended rather than one standard value from Table 1.

The ground pin of the trim resistor should be connected directly to the converter GND pin (Pin 5) with no voltage drop in between. Table 1 provides the trim resistor values for popular output voltages.

V <sub>0-REG</sub> [V]	R <sub>TRIM</sub> [kΩ]	The Closest Standard Value [kΩ]
0.7525	open	
1.0	41.2	41.2
1.2	22.46	22.6
1.5	13.0	13.0
1.8	9.0	9.09
2.0	7.4	7.32
2.5	5.0	4.99
3.3	3.12	3.09
5.0	1.47	1.47
5.5	1.21	1.21

Table 1: Trim Resistor Value

The output voltage can also be programmed by an external voltage source. To make trimming less sensitive, a series external resistor (R<sub>EXT</sub>) is recommended between the TRIM pin and the programming voltage source. The control voltage can be calculated by the formula:

$$V_{CTRL} = 0.7 - \frac{(1 + R_{EXT})(V_{O-REQ} - 0.7525)}{15} \quad [V]$$

where,

V<sub>CTRL</sub> = Control voltage [V]

R<sub>EXT</sub> = External resistor between the TRIM pin and the voltage source; the value can be chosen depending on the required output voltage range [kΩ]

Control voltages with R<sub>EXT</sub> = 0 and R<sub>EXT</sub> = 15K are shown in Table 2.

V <sub>0-REG</sub> [V]	V <sub>CTRL</sub> (R <sub>EXT</sub> = 0)	V <sub>CTRL</sub> (R <sub>EXT</sub> = 15K)
0.7525	0.700	0.700
1.0	0.684	0.436
1.2	0.670	0.223
1.5	0.650	-0.097
1.8	0.630	-0.417
2.0	0.617	-0.631
2.5	0.584	-1.164
3.3	0.530	-2.017
5.0	0.417	-3.831
5.5	0.384	-4.364

Table 2: Control Voltage [VDC]

## PROTECTION FEATURES

### Input Undervoltage Lockout

Input undervoltage lockout is standard with this converter. The converter will shut down when the input voltage drops below a pre-determined voltage; it will start automatically when  $V_{in}$  returns to a specified range.

The input voltage must be at least 9.6V (typically 9V) for the converter to turn on. Once the converter has been turned on, it will shut off when the input voltage drops below typically 8.5V.

### Output Overcurrent Protection (OCP)

The converter is protected against over-current and short circuit conditions. Upon sensing an overcurrent condition, the converter will enter hiccup mode. Once over-load or short circuit condition is removed,  $V_{out}$  will return to nominal value.

### Overtemperature Protection (OTP)

The converter will shut down under an over-temperature condition to protect itself from overheating caused by operation outside the thermal derating curves, or operation in abnormal conditions such as system fan failure. After the converter has cooled to a safe operating temperature, it will automatically restart.

### Safety Requirements

Approved to the latest edition and amendment of ITE Safety standards, UL/CSA 60950-1 and IEC60950-1.

The maximum DC voltage between any two pins is  $V_{in}$  under all operating conditions. Therefore, the unit has ELV (extra low voltage) output; it meets SELV requirements under the condition that all input voltages are ELV.

The converter is not internally fused. To comply with safety agencies requirements, a recognized fuse with a maximum rating of 15 Amps must be used in series with the input line.

## CHARACTERIZATION

### General Information

The converter has been characterized for many operational aspects, to include thermal derating (maximum load current as a function of ambient temperature and airflow) for vertical and horizontal mounting, efficiency, start-up and shutdown parameters, output ripple and noise, transient response to load step-change, overload and short circuit.

The figures are numbered as Fig. x.y, where x indicates the different output voltages, and y associates with specific plots ( $y = 1$  for the vertical thermal derating, ...). For example, Fig. x.1 will refer to the vertical thermal derating for all the output voltages in general.

The following pages contain specific plots or waveforms associated with the converter. Additional comments for specific data are provided below.

### Test Conditions

All thermal and efficiency data presented were taken with the converter soldered to a test board, specifically a 0.060" thick printed wiring board (PWB) with four layers. The top and bottom layers were not metalized. The two inner layers, comprising two-ounce copper, were used to provide traces for connectivity to the converter.

The lack of metalization on the outer layers as well as the limited thermal connection ensured that heat transfer from the converter to the PWB was minimized. This provides a worst-case but consistent scenario for thermal derating purposes.

All measurements requiring airflow were made in di/dt's vertical and horizontal wind tunnel facilities using Infrared (IR) thermography and thermocouples for thermometry.

Ensuring components on the converter do not exceed their ratings is important to maintaining high reliability. If one anticipates operating the converter at or close to the maximum loads specified in the derating curves, it is prudent to check actual operating temperatures in the application. Thermographic imaging is preferable; if this capability is not

available, then thermocouples may be used. Bel Power Solutions recommends the use of AWG #40 gauge thermocouples to ensure measurement accuracy. Careful routing of the thermocouple leads will further minimize measurement error. Refer to Fig. D for optimum measuring thermocouple location.

### Thermal Derating

Load current vs. ambient temperature and airflow rates are given in Figs. x.1 to x.2 for maximum temperature of 120 °C. Ambient temperature was varied between 25 °C and 85 °C, with airflow rates from 30 to 500 LFM (0.15m/s to 2.5 m/s), and vertical and horizontal converter mounting. The airflow during the testing is parallel to the long axis of the converter, going from input pins to output pins.

For each set of conditions, the maximum load current was defined as the lowest of:

- (i) The output current at which any MOSFET temperature does not exceed a maximum specified temperature (120 °C) as indicated by the thermographic image, or
- (ii) The maximum current rating of the converter (10A)

During normal operation, derating curves with maximum FET temperature less than or equal to 120 °C should not be exceeded. Temperature on the PCB at the thermocouple location shown in Fig. D should not exceed 120 °C in order to operate inside the derating curves.

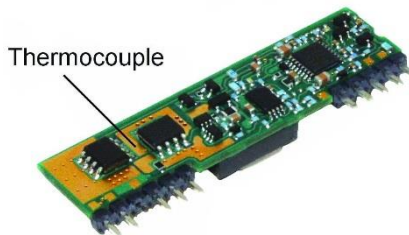


Fig. D: Location of the thermocouple for thermal testing.

### Efficiency

Figure x.3 shows the efficiency vs. load current plot for ambient temperature of 25 °C, airflow rate of 200 LFM (1 m/s) and input voltages of 9.6 V, 12 V and 14 V.

### Power Dissipation

Fig. x.4 shows the power dissipation vs. load current plot for  $T_a = 25$  °C, airflow rate of 200 LFM (1 m/s) with vertical mounting and input voltages of 9.6 V, 12 V and 14 V.

### Ripple and Noise

The output voltage ripple waveform is measured at full rated load current. Note that all output voltage waveforms are measured across a 1  $\mu$ F ceramic capacitor.

The output voltage ripple and input reflected ripple current waveforms are obtained using the test setup shown in Figure E.

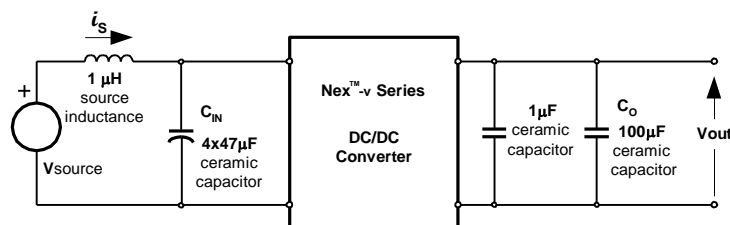


Fig. E: Test Set-up for measuring input reflected ripple currents,  $i_s$  and output voltage ripple.



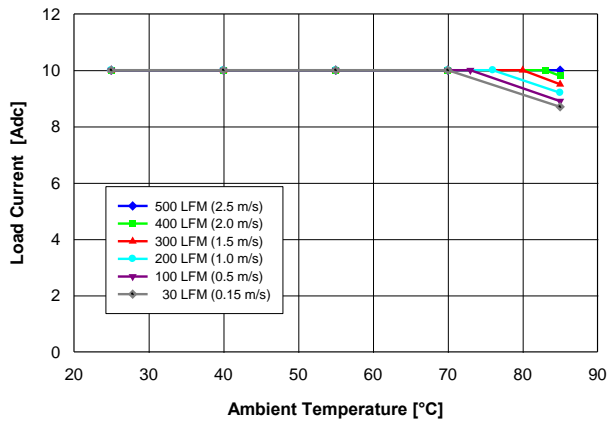


Fig. 5.0V.1: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 5.0V$  converter mounted vertically with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^{\circ}C$ .

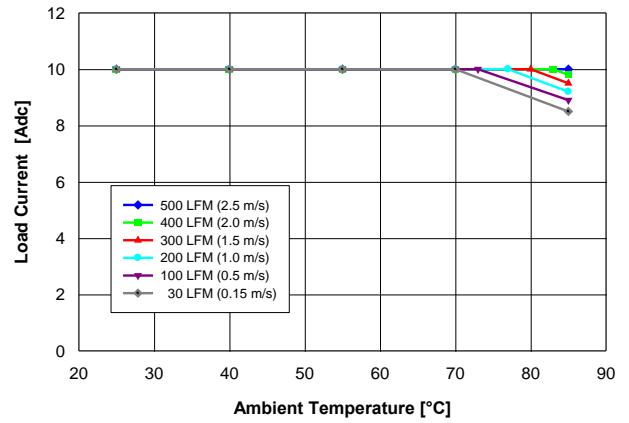


Fig. 5.0V.2: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 5.0V$  converter mounted horizontally with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^{\circ}C$ .

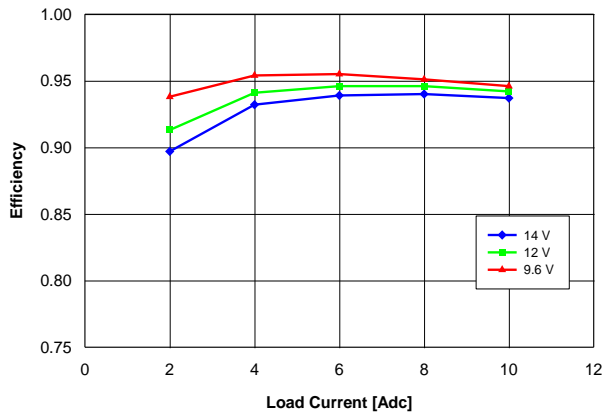


Fig. 5.0V.3: Efficiency vs. load current and input voltage for  $V_{out} = 5.0V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^{\circ}C$ .

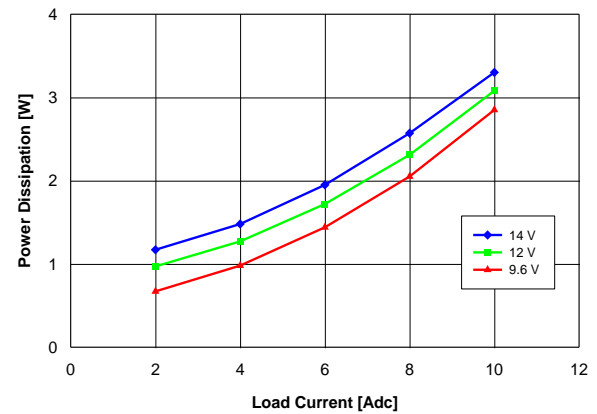


Fig. 5.0V.4: Power Loss vs. load current and input voltage for  $V_{out} = 5.0V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^{\circ}C$ .

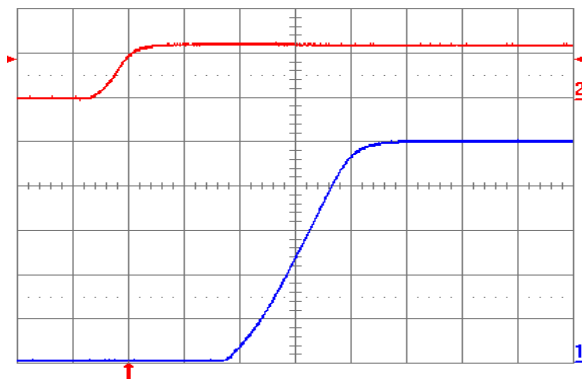


Fig. 5.0V.5: Turn-on transient for  $V_{out} = 5.0V$  with application of  $V_{in}$  at full rated load current (resistive) and  $100\mu F$  external capacitance at  $V_{in} = 12V$ . Top trace:  $V_{in}$  (10V/div.); Bottom trace: output voltage (1V/div.); Time scale: 2ms/div.

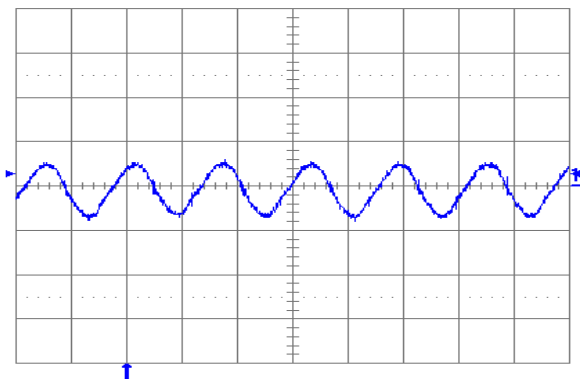


Fig. 5.0V.6: Output voltage ripple (20mV/div.) at full rated load current into a resistive load with external capacitance  $100\mu F$  ceramic and  $V_{in} = 12V$  for  $V_{out} = 5.0V$ . Time scale: 2µs/div.

# YNV12T10 DC-DC Converter

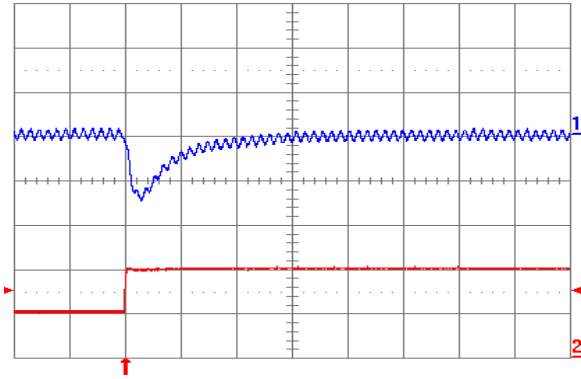


Fig. 5.0V.7: Output voltage response for  $V_{out} = 5.0V$  to positive load current step change from 5A to 10A with slew rate of  $5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale:  $20\mu s/div.$

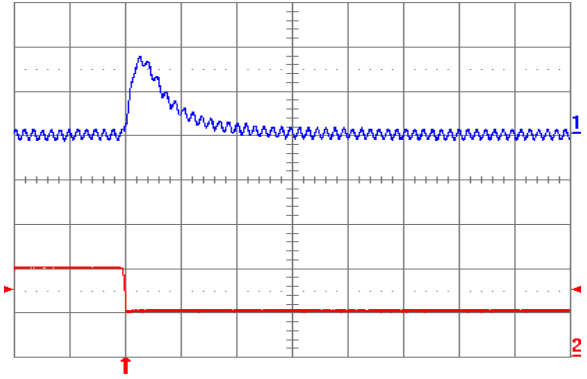


Fig. 5.0V.8: Output voltage response for  $V_{out} = 5.0V$  to negative load current step change from 10A to 5A with slew rate of  $-5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale:  $20\mu s/div.$

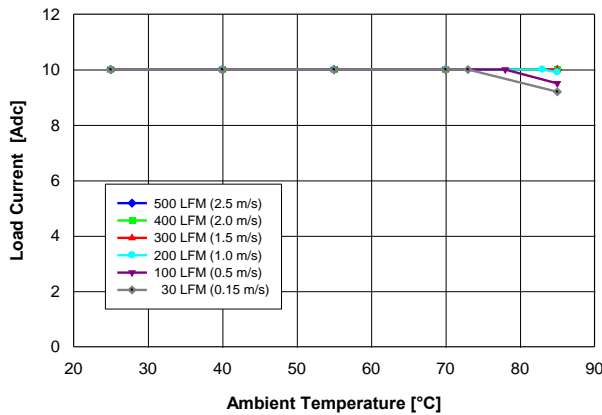


Fig. 3.3V.1: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 3.3V$  converter mounted vertically with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^\circ C$ .

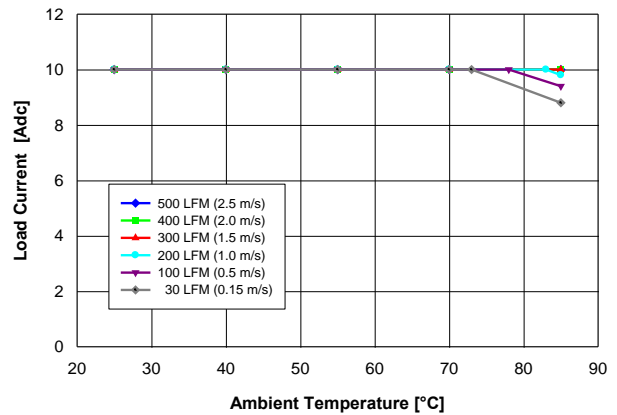


Fig. 3.3V.2: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 3.3V$  converter mounted horizontally with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^\circ C$ .

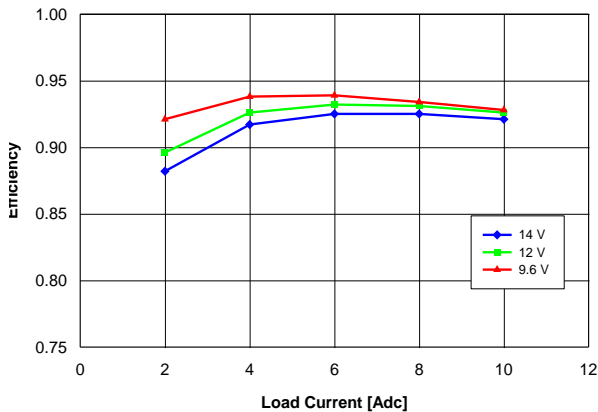


Fig. 3.3V.3: Efficiency vs. load current and input voltage for  $V_{out} = 3.3V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^\circ C$ .

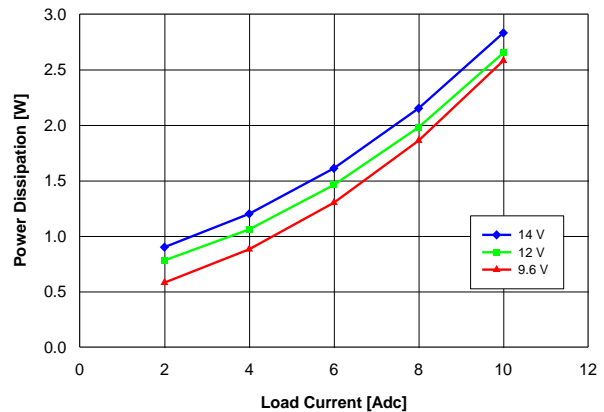


Fig. 3.3V.4: Power Loss vs. load current and input voltage for  $V_{out} = 3.3V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^\circ C$ .

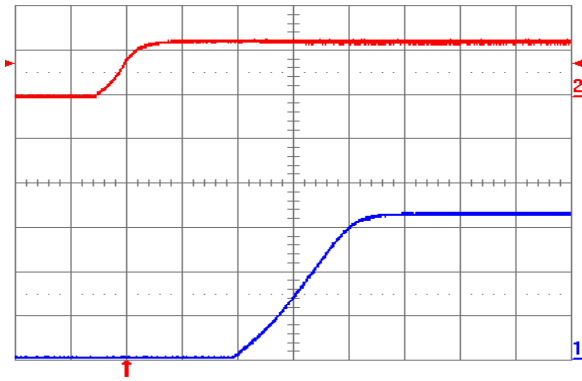


Fig. 3.3V.5: Turn-on transient for  $V_{out} = 3.3V$  with application of  $V_{in}$  at full rated load current (resistive) and  $100\mu F$  external capacitance at  $V_{in} = 12V$ . Top trace:  $V_{in}$  (10V/div.); Bottom trace: output voltage (1V/div.); Time scale: 2ms/div.

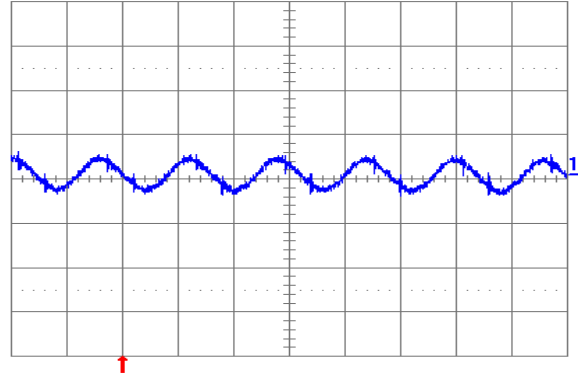


Fig. 3.3V.6: Output voltage ripple (20mV/div.) at full rated load current into a resistive load with external capacitance  $100\mu F$  ceramic and  $V_{in} = 12V$  for  $V_{out} = 3.3V$ . Time scale:  $2\mu s$ /div.

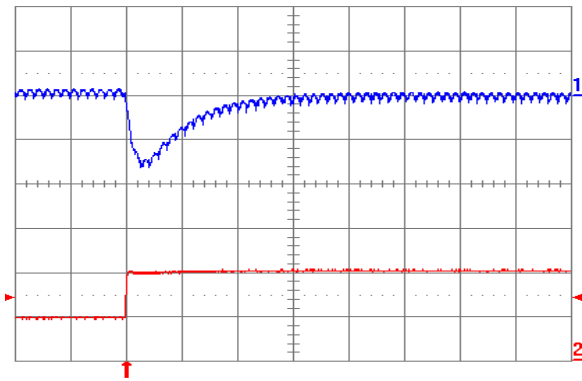


Fig. 3.3V.7: Output voltage response for  $V_{out} = 3.3V$  to positive load current step change from 5A to 10A with slew rate of  $5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale:  $20\mu s$ /div.

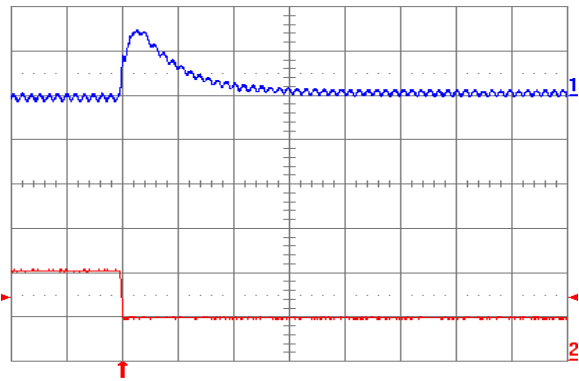


Fig. 3.3V.8: Output voltage response for  $V_{out} = 3.3V$  to negative load current step change from 10A to 5A with slew rate of  $-5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale:  $20\mu s$ /div.

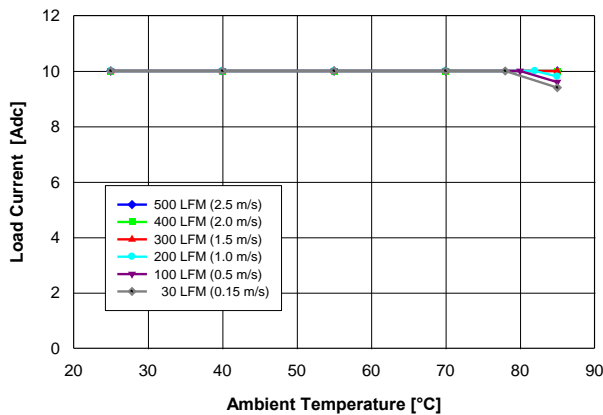


Fig. 2.5V.1: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 2.5V$  converter mounted vertically with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^\circ C$ .

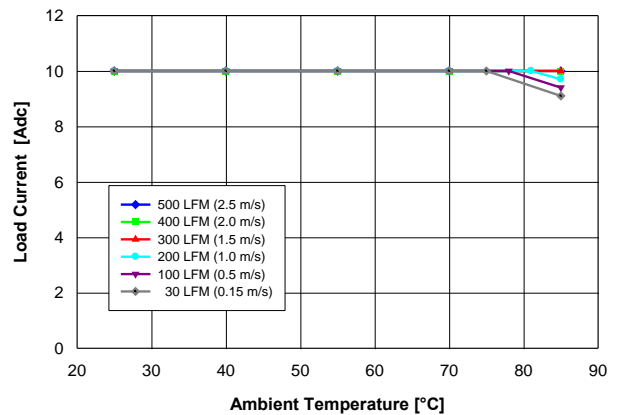


Fig. 2.5V.2: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 2.5V$  converter mounted horizontally with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^\circ C$ .

# YNV12T10 DC-DC Converter

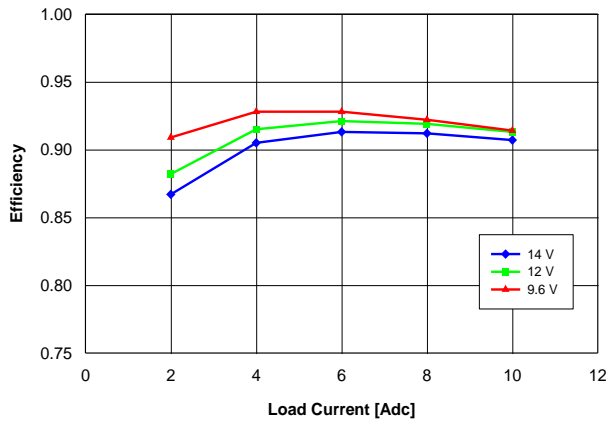


Fig. 2.5V.3: Efficiency vs. load current and input voltage for  $V_{out} = 2.5V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^{\circ}C$ .

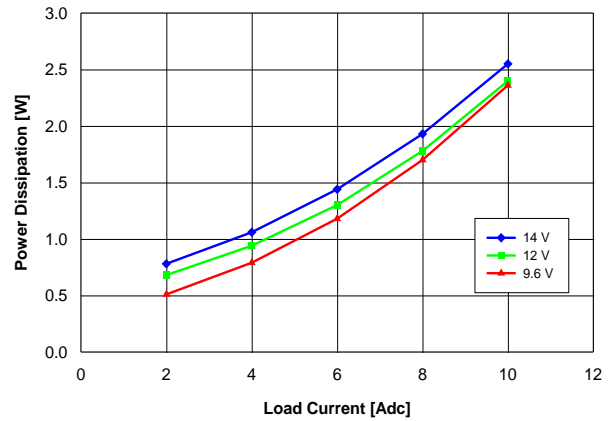


Fig. 2.5V.4: Power Loss vs. load current and input voltage for  $V_{out} = 2.5V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^{\circ}C$ .

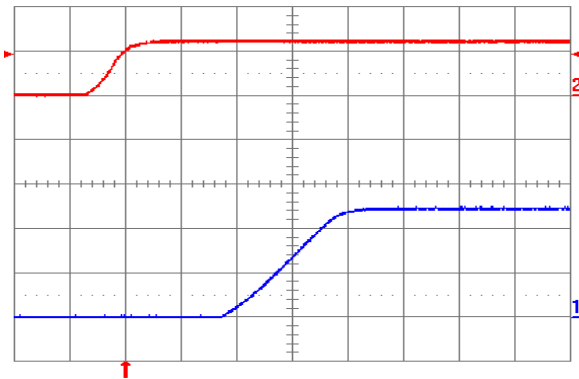


Fig. 2.5V.5: Turn-on transient for  $V_{out} = 2.5V$  with application of  $V_{in}$  at full rated load current (resistive) and  $100\mu F$  external capacitance at  $V_{in} = 12V$ . Top trace:  $V_{in}$  (10V/div.); Bottom trace: output voltage (1V/div.); Time scale: 2ms/div.

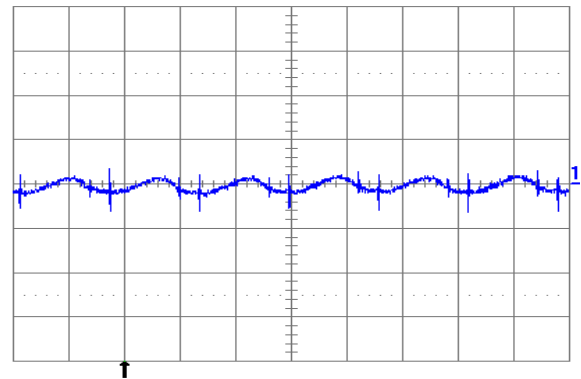


Fig. 2.5V.6: Output voltage ripple (20mV/div.) at full rated load current into a resistive load with external capacitance  $100\mu F$  ceramic and  $V_{in} = 12V$  for  $V_{out} = 2.5V$ . Time scale: 2 $\mu s$ /div.

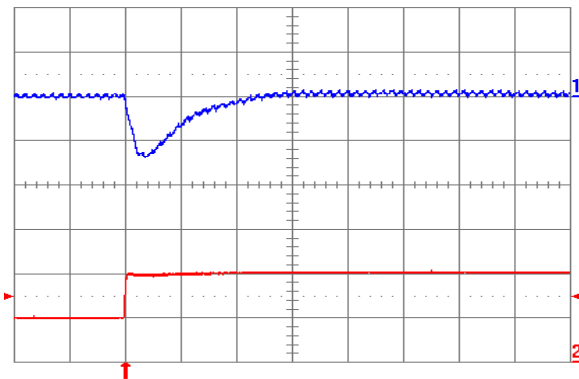


Fig. 2.5V.7: Output voltage response for  $V_{out} = 2.5V$  to positive load current step change from 5A to 10A with slew rate of  $5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale: 20 $\mu s$ /div.

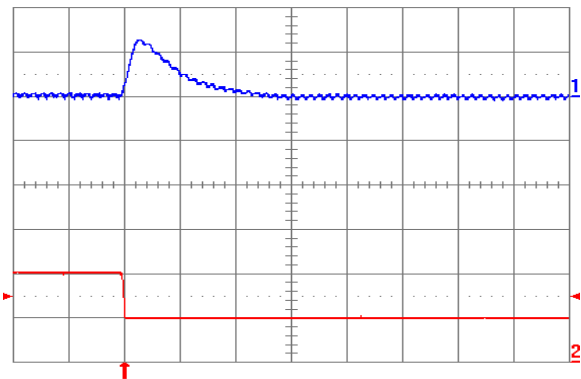


Fig. 2.5V.8: Output voltage response for  $V_{out} = 2.5V$  to negative load current step change from 10A to 5A with slew rate of  $-5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale: 20 $\mu s$ /div.

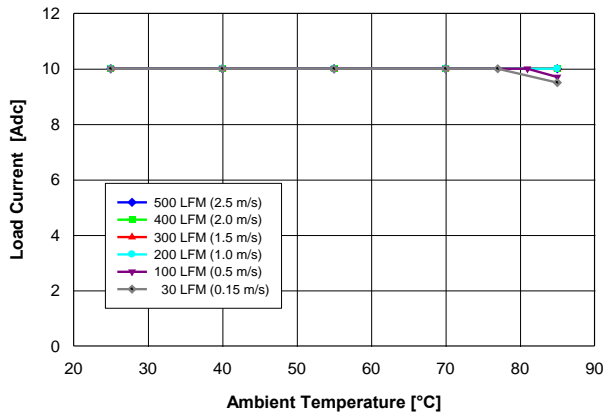


Fig. 2.0V.1: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 2.0V$  converter mounted vertically with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^{\circ}C$ .

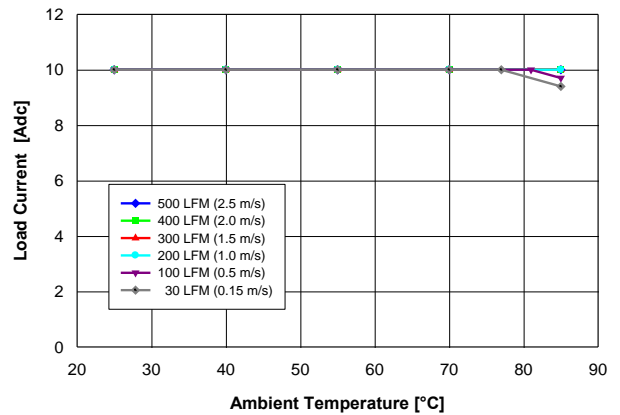


Fig. 2.0V.2: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 2.0V$  converter mounted horizontally with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^{\circ}C$ .

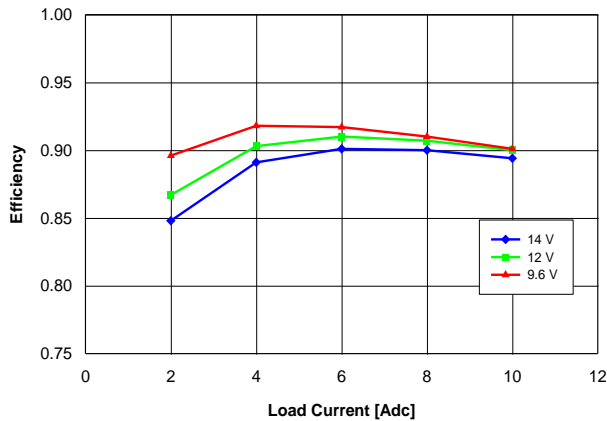


Fig. 2.0V.3: Efficiency vs. load current and input voltage for  $V_{out} = 2.0V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^{\circ}C$ .

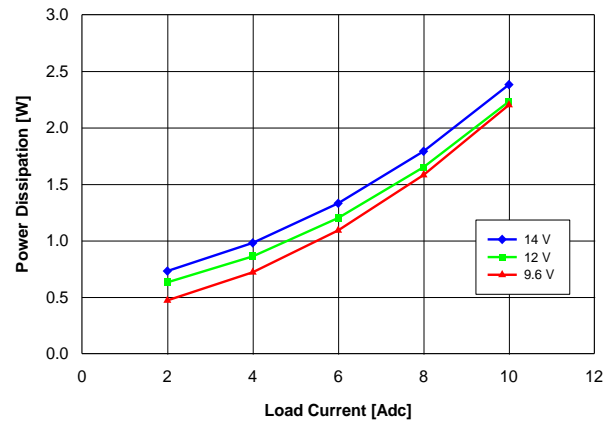


Fig. 2.0V.4: Power Loss vs. load current and input voltage for  $V_{out} = 2.0V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^{\circ}C$ .

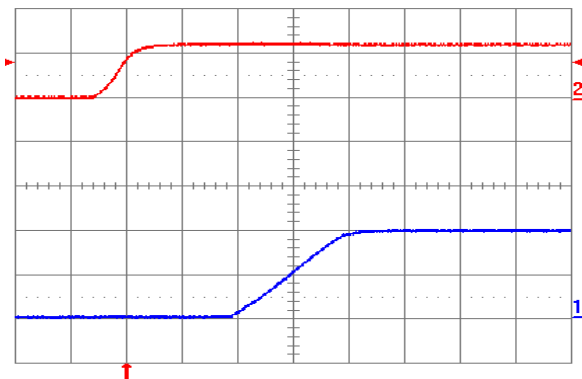


Fig. 2.0V.5: Turn-on transient for  $V_{out} = 2.0V$  with application of  $V_{in}$  at full rated load current (resistive) and  $100\mu F$  external capacitance at  $V_{in} = 12V$ . Top trace:  $V_{in}$  (10V/div.); Bottom trace: output voltage (1V/div.); Time scale: 2ms/div.

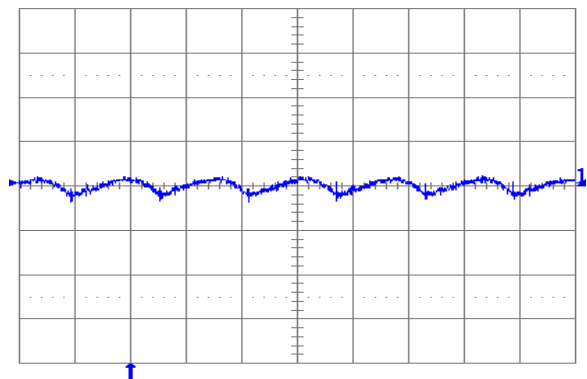


Fig. 2.0V.6: Output voltage ripple (20mV/div.) at full rated load current into a resistive load with external capacitance  $100\mu F$  ceramic and  $V_{in} = 12V$  for  $V_{out} = 2.0V$ . Time scale: 2μs/div.

# YNV12T10 DC-DC Converter

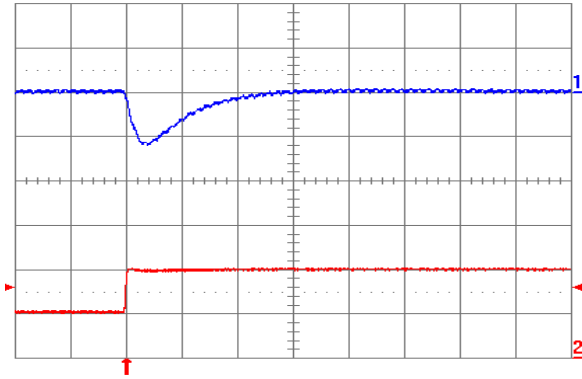


Fig. 2.0V.7: Output voltage response for  $V_{out} = 2.0V$  to positive load current step change from 5A to 10A with slew rate of  $5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale:  $20\mu s/div.$

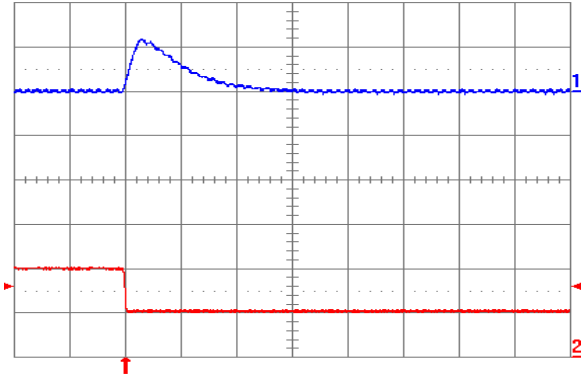


Fig. 2.0V.8: Output voltage response for  $V_{out} = 2.0V$  to negative load current step change from 10A to 5A with slew rate of  $-5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale:  $20\mu s/div.$

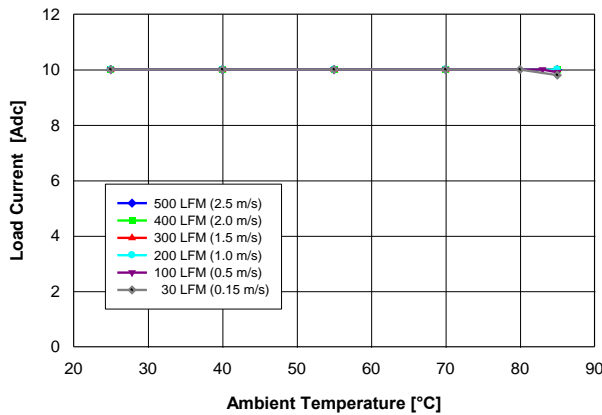


Fig. 1.8V.1: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 1.8V$  converter mounted vertically with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^\circ C$ .

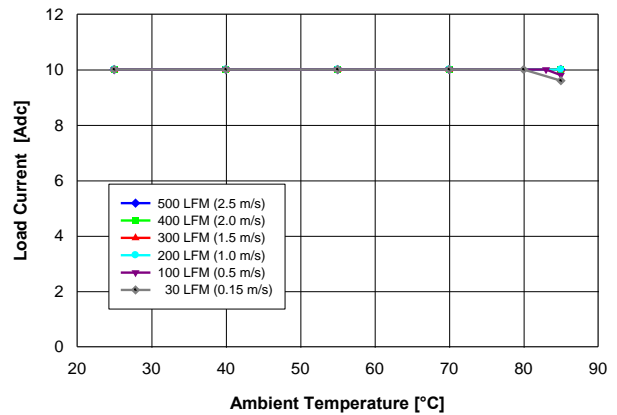


Fig. 1.8V.2: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 1.8V$  converter mounted horizontally with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^\circ C$ .

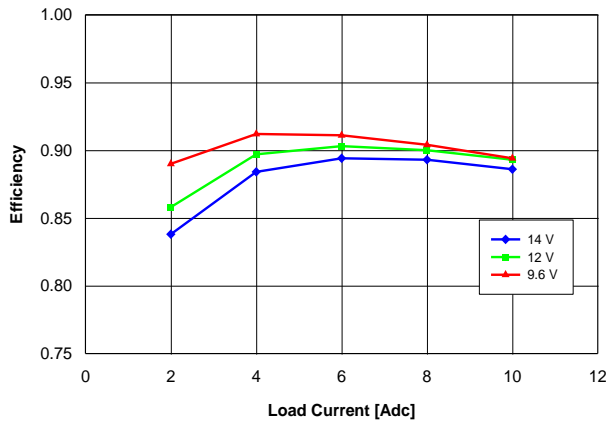


Fig. 1.8V.3: Efficiency vs. load current and input voltage for  $V_{out} = 1.8V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^\circ C$ .

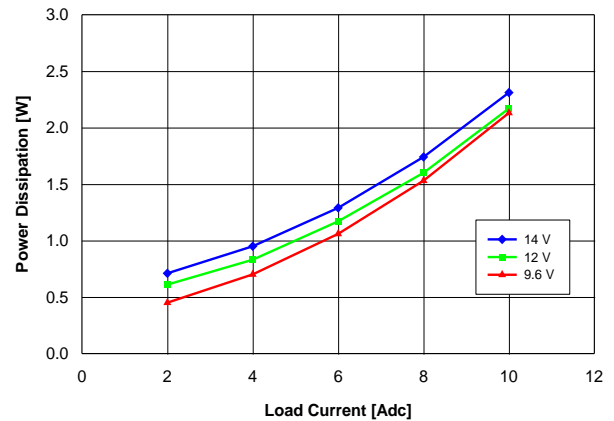


Fig. 1.8V.4: Power Loss vs. load current and input voltage for  $V_{out} = 1.8V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^\circ C$ .

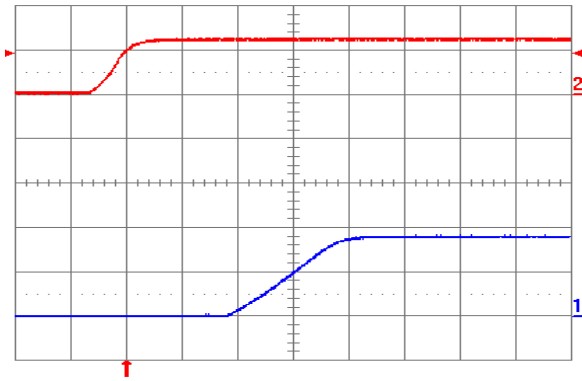


Fig. 1.8V.5: Turn-on transient for  $V_{out} = 1.8V$  with application of  $V_{in}$  at full rated load current (resistive) and  $100\mu F$  external capacitance at  $V_{in} = 12V$ . Top trace:  $V_{in}$  (10V/div.); Bottom trace: output voltage (1V/div.); Time scale: 2ms/div.

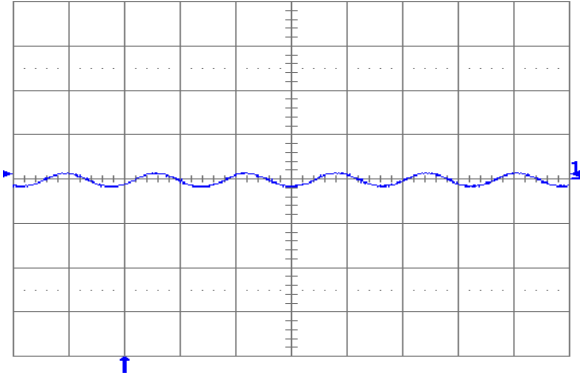


Fig. 1.8V.6: Output voltage ripple (20mV/div.) at full rated load current into a resistive load with external capacitance  $100\mu F$  ceramic and  $V_{in} = 12V$  for  $V_{out} = 1.8V$ . Time scale:  $2\mu s$ /div.

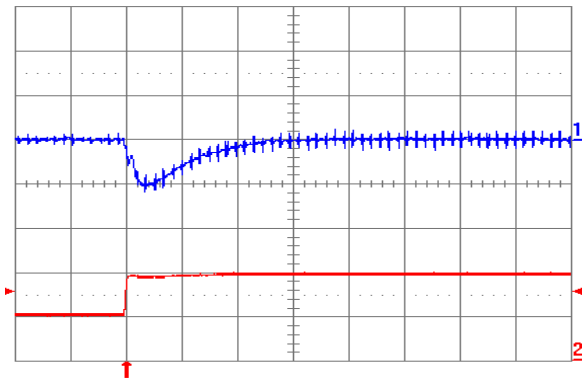


Fig. 1.8V.7: Output voltage response for  $V_{out} = 1.8V$  to positive load current step change from 5A to 10A with slew rate of  $5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale:  $20\mu s$ /div.

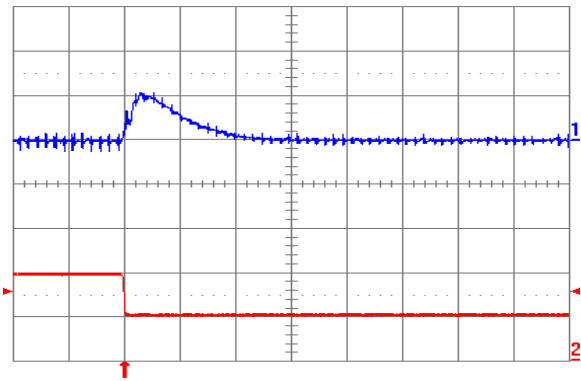


Fig. 1.8V.8: Output voltage response for  $V_{out} = 1.8V$  to negative load current step change from 10A to 5A with slew rate of  $-5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale:  $20\mu s$ /div.

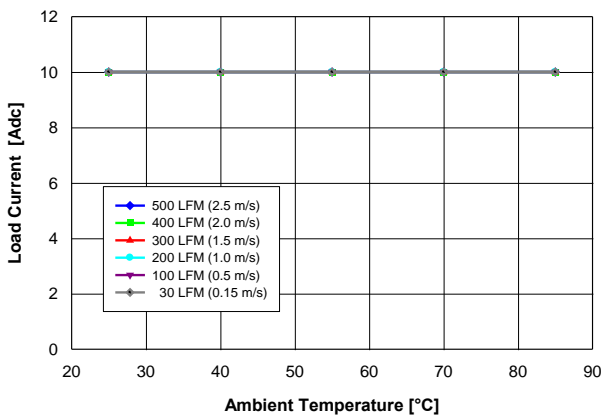


Fig. 1.5V.1: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 1.5V$  converter mounted vertically with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^\circ C$ .

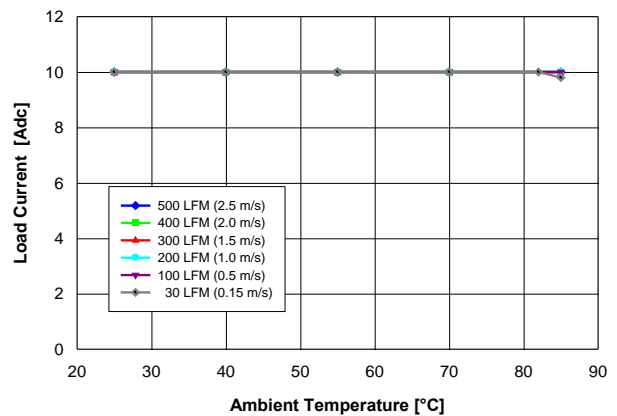


Fig. 1.5V.2: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 1.5V$  converter mounted horizontally with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^\circ C$ .



# YNV12T10 DC-DC Converter

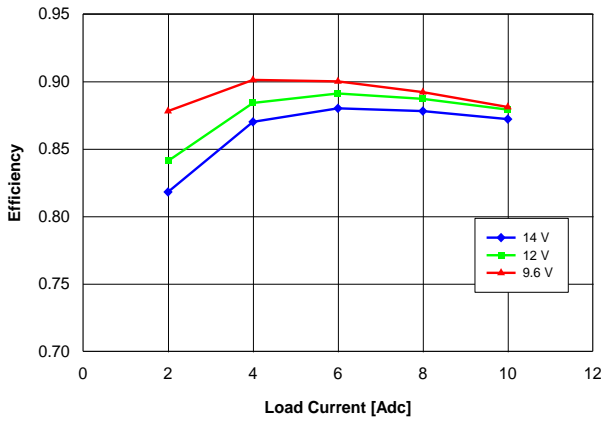


Fig. 1.5V.3: Efficiency vs. load current and input voltage for  $V_{out} = 1.5V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^{\circ}C$ .

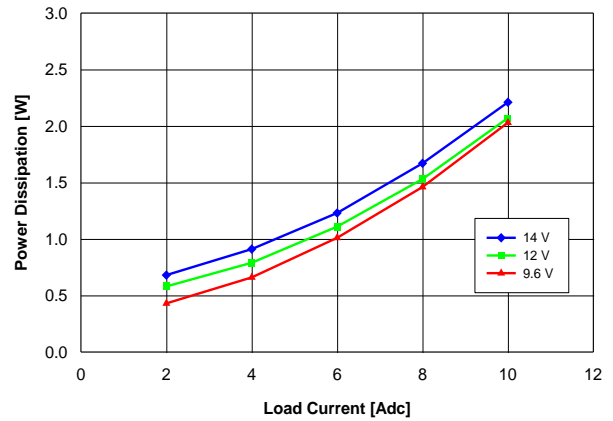


Fig. 1.5V.4: Power Loss vs. load current and input voltage for  $V_{out} = 1.5V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^{\circ}C$ .

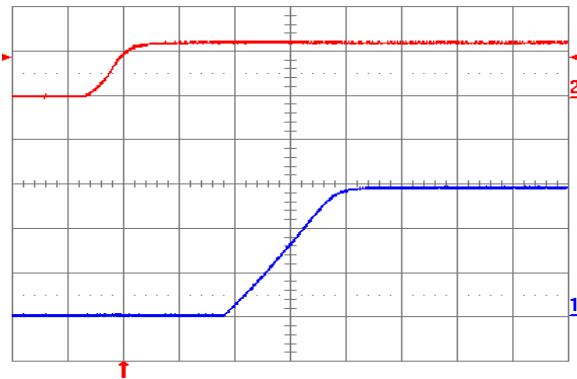


Fig. 1.5V.5: Turn-on transient for  $V_{out} = 1.5V$  with application of  $V_{in}$  at full rated load current (resistive) and  $100\mu F$  external capacitance at  $V_{in} = 12V$ . Top trace:  $V_{in}$  (10V/div.); Bottom trace: output voltage (0.5V/div.); Time scale: 2ms/div.

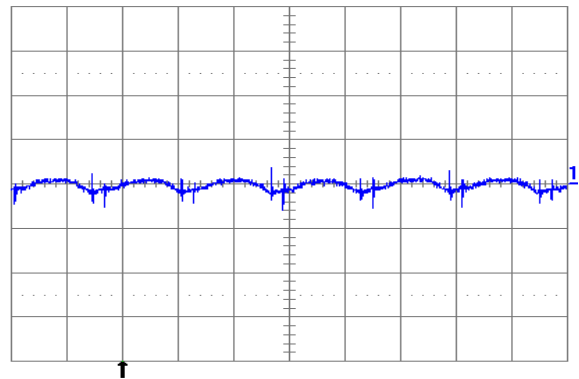


Fig. 1.5V.6: Output voltage ripple (20mV/div.) at full rated load current into a resistive load with external capacitance  $100\mu F$  ceramic and  $V_{in} = 12V$  for  $V_{out} = 1.5V$ . Time scale: 2 $\mu s$ /div.

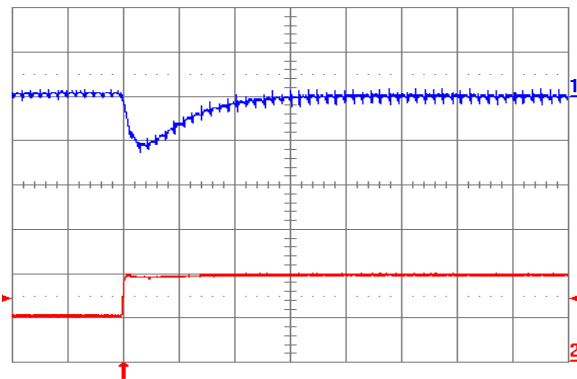


Fig. 1.5V.7: Output voltage response for  $V_{out} = 1.5V$  to positive load current step change from 5A to 10A with slew rate of  $5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale: 20 $\mu s$ /div.

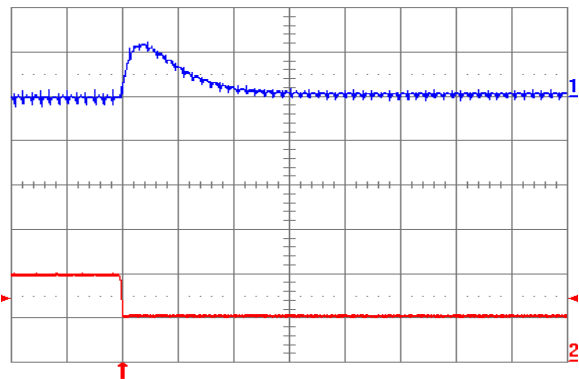


Fig. 1.5V.8: Output voltage response for  $V_{out} = 1.5V$  to negative load current step change from 10A to 5A with slew rate of  $-5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale: 20 $\mu s$ /div.



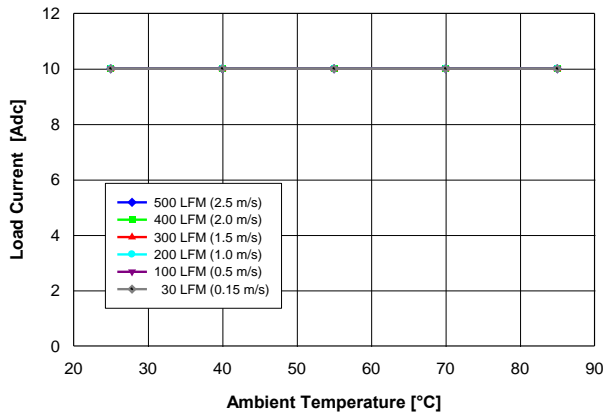


Fig. 1.2V.1: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 1.2V$  converter mounted vertically with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^{\circ}C$ .

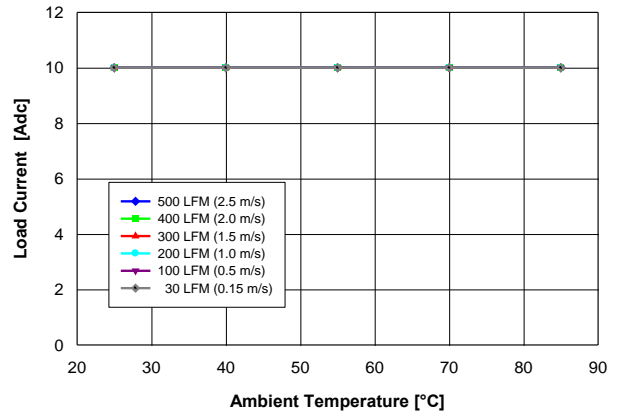


Fig. 1.2V.2: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 1.2V$  converter mounted horizontally with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^{\circ}C$ .

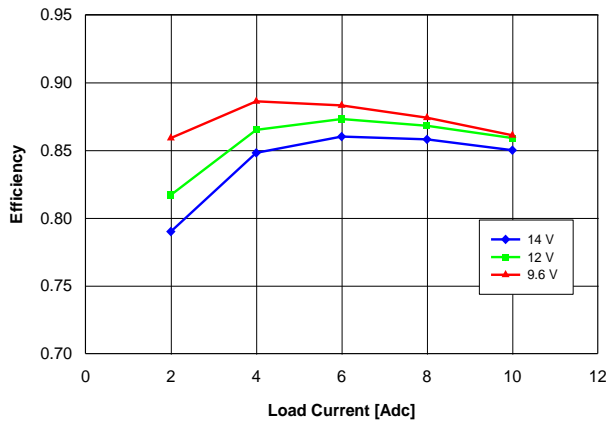


Fig. 1.2V.3: Efficiency vs. load current and input voltage for  $V_{out} = 1.2V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^{\circ}C$ .

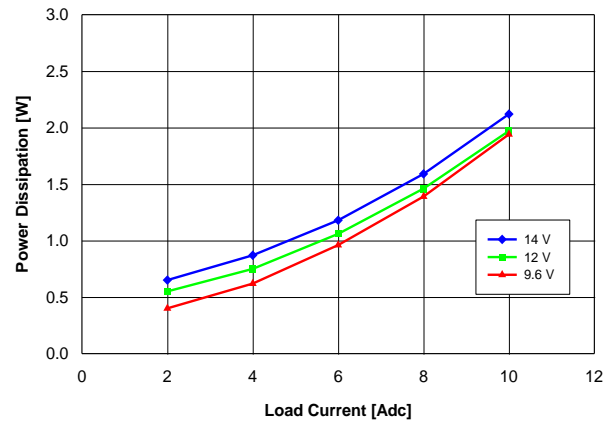


Fig. 1.2V.4: Power Loss vs. load current and input voltage for  $V_{out} = 1.2V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^{\circ}C$ .

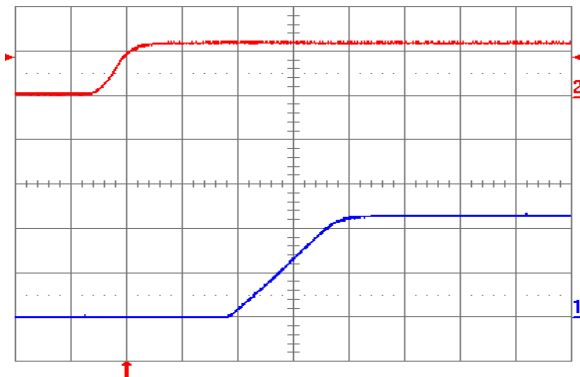


Fig. 1.2V.5: Turn-on transient for  $V_{out} = 1.2V$  with application of  $V_{in}$  at full rated load current (resistive) and  $100\mu F$  external capacitance at  $V_{in} = 12V$ . Top trace:  $V_{in}$  (10V/div.); Bottom trace: output voltage (0.5V/div.); Time scale: 2ms/div.

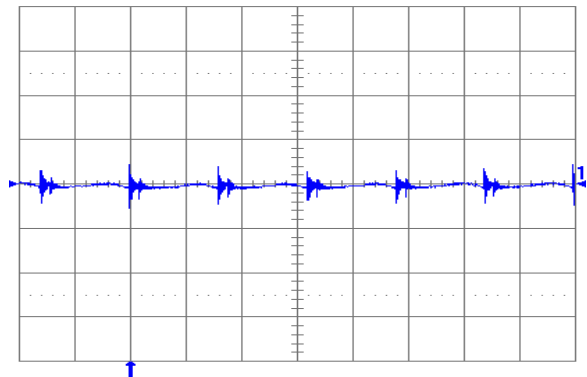


Fig. 1.2V.6: Output voltage ripple (20mV/div.) at full rated load current into a resistive load with external capacitance  $100\mu F$  ceramic and  $V_{in} = 12V$  for  $V_{out} = 1.2V$ . Time scale: 2µs/div.

# YNV12T10 DC-DC Converter

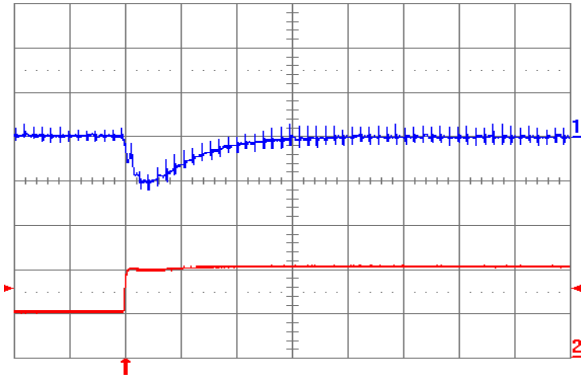


Fig. 1.2V.7: Output voltage response for  $V_{out} = 1.2V$  to positive load current step change from 5A to 10A with slew rate of  $5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale:  $20\mu s/div.$

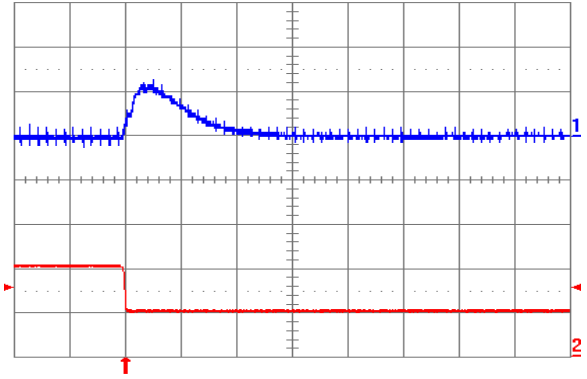


Fig. 1.2V.8: Output voltage response for  $V_{out} = 1.2V$  to negative load current step change from 10A to 5A with slew rate of  $-5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale:  $20\mu s/div.$

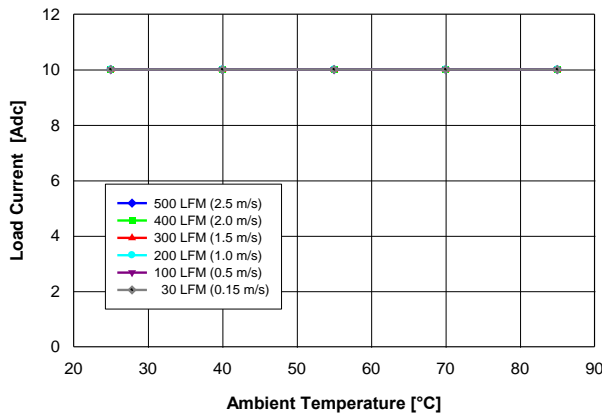


Fig. 1.0V.1: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 1.0V$  converter mounted vertically with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^\circ C$ .

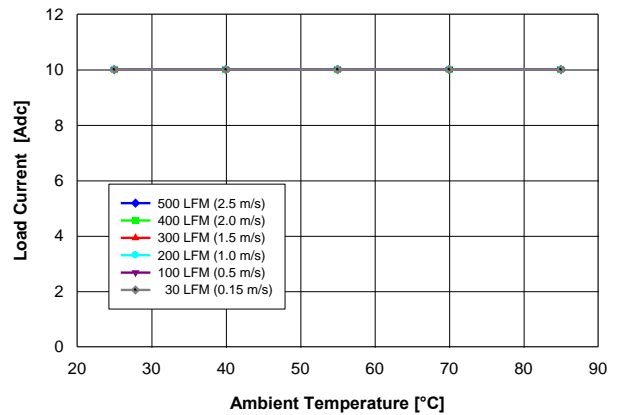


Fig. 1.0V.2: Available load current vs. ambient temperature and airflow rates for  $V_{out} = 1.0V$  converter mounted horizontally with  $V_{in} = 12V$ , and maximum MOSFET temperature  $\leq 120^\circ C$ .

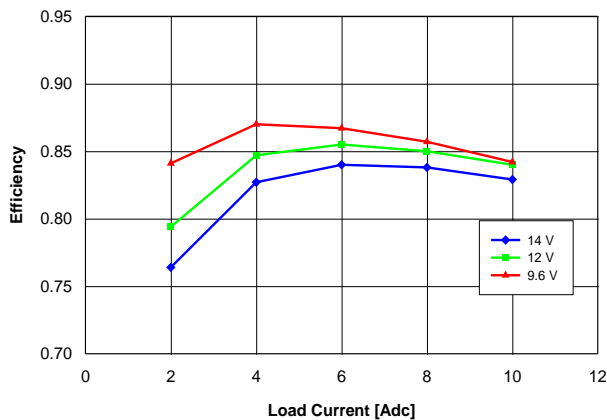


Fig. 1.0V.3: Efficiency vs. load current and input voltage for  $V_{out} = 1.0V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^\circ C$ .

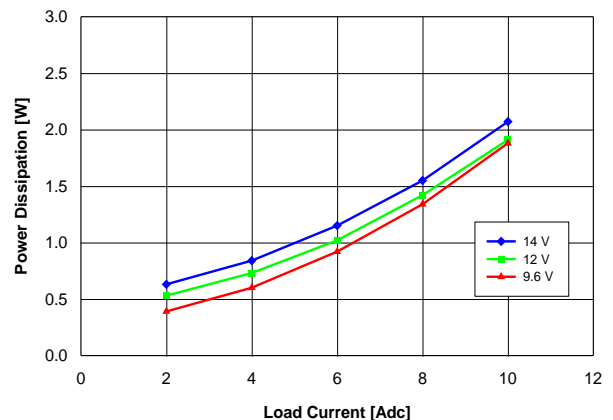


Fig. 1.0V.4: Power Loss vs. load current and input voltage for  $V_{out} = 1.0V$  converter mounted vertically with air flowing at a rate of 200 LFM (1 m/s) and  $T_a = 25^\circ C$ .

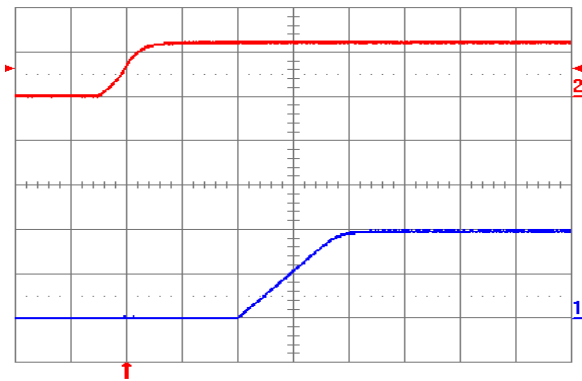


Fig. 1.0V.5: Turn-on transient for  $V_{out} = 1.0V$  with application of  $V_{in}$  at full rated load current (resistive) and  $100\mu F$  external capacitance at  $V_{in} = 12V$ . Top trace:  $V_{in}$  (10V/div.); Bottom trace: output voltage (0.5V/div.); Time scale: 2ms/div.

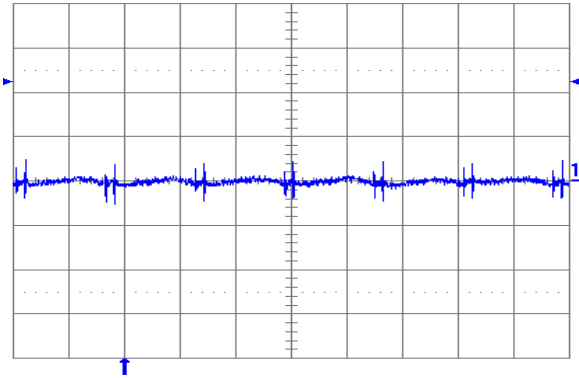


Fig. 1.0V.6: Output voltage ripple (20mV/div.) at full rated load current into a resistive load with external capacitance  $100\mu F$  ceramic and  $V_{in} = 12V$  for  $V_{out} = 1.0V$ . Time scale:  $2\mu s$ /div.

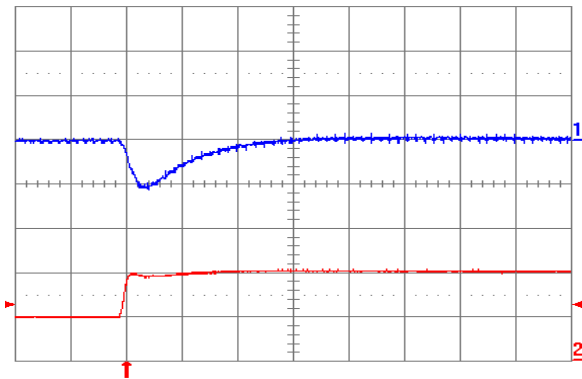


Fig. 1.0V.7: Output voltage response for  $V_{out} = 1.0V$  to positive load current step change from 5A to 10A with slew rate of  $5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale:  $20\mu s$ /div.

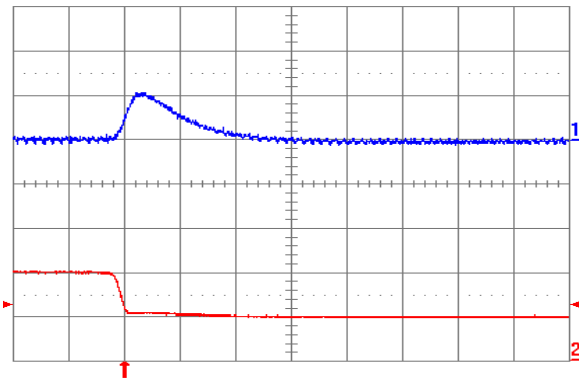
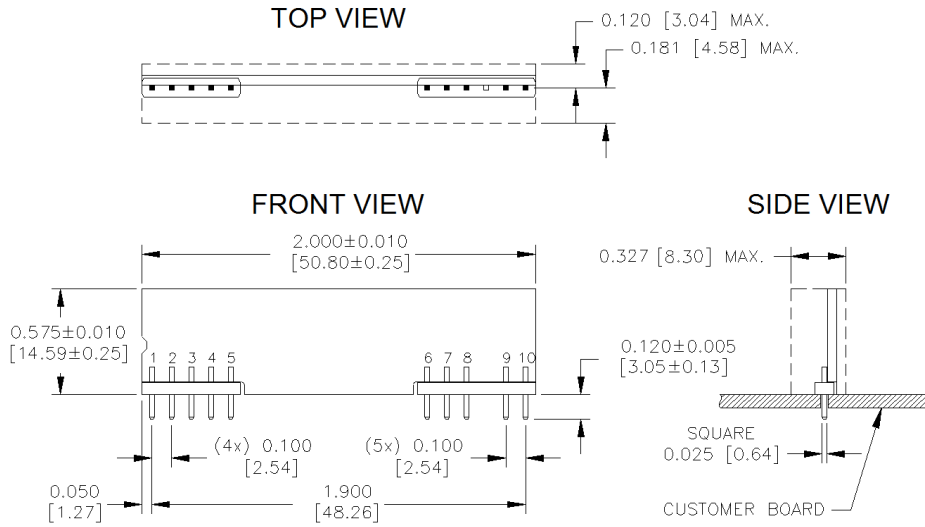


Fig. 1.0V.8: Output voltage response for  $V_{out} = 1.0V$  to negative load current step change from 10A to 5A with slew rate of  $-5A/\mu s$  at  $V_{in} = 12V$ . Top trace: output voltage (100mV/div.); Bottom trace: load current (5A/div.).  $C_o = 100\mu F$  ceramic. Time scale:  $20\mu s$ /div.

## PHYSICAL INFORMATION



**YNV12T10 Pinout (Through-Hole - SIP)**

PAD/PIN CONNECTIONS	
Pad/Pin #	Function
1	Vout
2	Vout
3	Vout SENSE
4	Vout
5	GND
6	GND
7	Vin
8	Vin
9	TRIM
10	ON/OFF

### YNV05T10 Platform Notes

- All dimensions are in inches [mm]
- Connector Material: Copper
- Connector Finish: Gold
- Converter Weight: 0.25 oz [7 g]
- Converter Height: 0.585" Max.
- Recommended Through Hole Via/Pad:  
Min. 0.043" X 0.064" [1.09 x 1.63]

## ORDERING INFORMATION

Product Series	Input Voltage	Mounting Scheme	Rated Load Current	Enable Logic	Environmental
YNV	12	T	10	-	
Y-Series	9.6 – 14 V	T ⇒ Through-Hole (SIP)	10 A (0.7525 to 5.5 V)	0 ⇒ Standard (Positive Logic) D ⇒ Opposite of Standard (Negative Logic)	No Suffix ⇒ RoHS lead-solder-exempt compliant G ⇒ RoHS compliant for all six substances

The example above describes P/N YNV12T10-0: 9.6 V – 14 V input, thru-hole (SIP), 10 A at 0.7525 V to 5.5 V output, standard enable logic, and lead-solder-exempt RoHS feature. Please consult factory regarding availability of a specific version.

**For more information on these products consult: [tech.support@psbel.com](mailto:tech.support@psbel.com)**

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**TECHNICAL REVISIONS** - The appearance of products, including safety agency certifications pictured on labels, may change depending on the date manufactured. Specifications are subject to change without notice.

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