# **QCPL-341H** 2.5 Amp Output Current IGBT Gate Drive Optocoupler



# **Preliminary Data Sheet**

## **Description**

The QCPL-341H contains an AlGaAs LED, which is optically coupled to an integrated circuit with a power output stage. This optocoupler is ideally suited for driving power IGBTs and MOSFETs used in motor control inverter applications. The high operating voltage range of the output stage provides the drive voltages required by gate controlled devices. The voltage and high peak output current supplied by this optocoupler make it ideally suited for direct driving IGBT with ratings up to 1200V/100A. For IGBTs with higher ratings, this optocoupler can be used to drive a discrete power stage which drives the IGBT gate. The QCPL-341H has the highest insulation voltage of V<sub>IORM</sub>= 630Vpeak in the IEC/ EN/DIN EN 60747-5-5.

## **Functional Diagram**



Note: Design Note: A 1 μF bypass capacitor must be connected between pins V<sub>CC</sub> and V<sub>EE</sub>.

## ssss **Truth Table**



## **Features**

- 2.5 A maximum peak output current
- 2.0 A minimum peak output current
- Rail-to-rail output voltage
- 300 ns maximum propagation delay
- 200 ns maximum propagation delay difference
- LED current input with hysteresis
- 25 kV/µs minimum Common Mode Rejection (CMR) at  $V_{CM}$  = 1500 V
- $\bullet$   $I_{\text{CC}}$  = 5.0 mA maximum supply current
- Under Voltage Lock-Out protection (UVLO) with hysteresis
- Wide operating  $V_{CC}$  Range: 15 to 30 V
- Industrial temperature range: -40 °C to 105 °C
- Safety Approval Pending
	- UL Recognized 3750/5000 VRMS for 1min.
	- CSA
	- IEC/EN/DIN EN 60747-5-5 VIORM = 630 Vpeak

## **Applications**

- IGBT/MOSFET gate drive
- AC and Brushless DC motor drives
- Renewable energy inverters
- Industrial inverters
- Switching power supp

**CAUTION: It is advised that normal static precautions be taken in handling and assembly of this component to prevent damage and/or degradation which may be induced by ESD.**

## **Ordering Information**

QCPL-341H is UL Recognized with 3750 VRMS for 1 minute per UL1577.



To order, choose a part number from the part number column and combine with the desired option from the option column to form an order entry.

Example 1:

QCPL-341H-560E to order product of 300 mil DIP Gull Wing Surface Mount package in Tape and Reel packaging with IEC/EN/DIN EN 60747-5-5 Safety Approval in RoHS compliant.

Example 2:

QCPL-341H-000E to order product of 300 mil DIP package in Tube packaging and RoHS compliant.

Option datasheets are available. Contact your Avago sales representative or authorized distributor for information.

## **Package Outline Drawings**

#### **QCPL-341H Outline Drawing (Standard DIP Package)**



#### **QCPL-341H Gull Wing Surface Mount Option 300 Outline Drawing**



NOTE: FLOATING LEAD PROTRUSION IS 0.25 mm (10 mils) MAX.

#### **Recommended Pb-Free IR Profile**

Recommended reflow condition as per JEDEC Standard, J-STD-020 (latest revision). Non- Halide Flux should be used.

#### **Regulatory Information**

The QCPL-341H is pending approval by the following organizations:

#### **UL**

Recognized under UL 1577, component recognition program, category, File E55361 up to V<sub>ISO</sub> = 3750 VRMS.

**CSA**

CSA Component Acceptance Notice #5, File CA 88324

#### **IEC/EN/DIN EN 60747-5-5 (Option 060 Only)**

Maximum Working Insulation Voltage V<sub>IORM</sub> = 630V<sub>peak</sub>

## **Table 1. IEC/EN/DIN EN 60747-5-5 Insulation Characteristics\* (Option 060 – Under Evaluation)**



\* Refer to the optocoupler section of the Isolation and Control Components Designer's Catalog, under Product Safety Regulations section, (IEC/EN/DIN EN 60747-5-5) for a detailed description of Method a and Method b partial discharge test profiles. **Note:** These optocouplers are suitable for "safe electrical isolation" only within the safety limit data. Maintenance of the safety data shall be ensured by means of protective circuits. Surface mount classification is Class A in accordance with CECC 00802.

## **Table 2. Insulation and Safety Related Specifications**



Notes:

1. All Avago data sheets report the creepage and clearance inherent to the optocoupler component itself. These dimensions are needed as a starting point for the equipment designer when determining the circuit insulation requirements. However, once mounted on a printed circuit board, minimum creepage and clearance requirements must be met as specified for individual equipment standards. For creepage, the shortest distance path along the surface of a printed circuit board between the solder fillets of the input and output leads must be considered (the recommended Land Pattern does not necessarily meet the minimum creepage of the device). There are recommended techniques such as grooves and ribs which may be used on a printed circuit board to

achieve desired creepage and clearances. Creepage and clearance distances will also change depending on factors such as pollution degree and insulation level.

## **Table 3. Absolute Maximum Ratings**



## **Table 4. Recommended Operating Conditions**



## **Table 5. Electrical Specifications (DC)**

Unless otherwise noted, all typical values are at TA = 25 °C, Vcc - VEE = 30 V, VEE = Ground; all minimum and maximum specifications are at recommended operating conditions (TA = -40 to 105 °C,  $I_{F(ON)} = 7$  to 16 mA,  $V_{F(OFF)} = -3.6$  to 0.8 V,  $V_{EE} =$  Ground,  $V_{CC} = 15$  to 30 V).



## **Table 6. Switching Specifications (AC)**

Unless otherwise noted, all typical values are at TA = 25 °C, Vcc - VEE = 30 V, VEE = Ground; all minimum and maximum specifications are at recommended operating conditions (TA = -40 to 105 °C,  $I_{F(ON)}$  = 7 to 16 mA,  $V_{F(OFF)}$  = -3.6 to 0.8 V, VEE = Ground, Vcc = 15 to 30 V).



## **Table 7. Package Characteristics**

Unless otherwise noted, all typical values are at  $T_A = 25 °C$ ; all minimum/maximum specifications are at recommended operating conditions.



\* The Input-Output Momentary Withstand Voltage is a dielectric voltage rating that should not be interpreted as an input-output continuous voltage rating. For the continuous voltage rating, refer to your equipment level safety specification or Avago Technologies Application Note 1074 entitled "Optocoupler Input-Output Endurance Voltage."

#### **Notes:**

- 1. Derate linearly above 70 °C free-air temperature at a rate of 0.3 mA/ °C.
- 2. Maximum pulse width = 10 us. This value is intended to allow for component tolerances for designs with lo peak minimum = 2.0 A. See applications section for additional details on limiting I<sub>OH</sub> peak.
- 3. Derate linearly above 70 °C free-air temperature at a rate of 4.8 mW/ °C.
- 4. Derate linearly above 70 °C free-air temperature at a rate of 5.4 mW/ °C. The maximum LED junction temperature should not exceed 125 $\degree$ C.
- 5. Maximum pulse width =  $50 \mu s$ .
- 6. Output is sourced at -2.0 A with a maximum pulse width = 10  $\mu$ s. V $_{\text{CC}}$ -V<sub>o</sub> is measured to ensure 15 V or below.
- 7. Output is sourced at 2.0 A with a maximum pulse width = 10  $\mu$ s. V<sub>O</sub>-V<sub>EE</sub> is measured to ensure 15 V or below.
- 8. Output is sourced at -2.0 A/2.0 A with a maximum pulse width = 10 µs.
- 9. In this test V<sub>OH</sub> is measured with a dc load current. When driving capacitive loads, V<sub>OH</sub> will approach V<sub>CC</sub> as  $I_{\text{OH}}$  approaches zero amps.
- 10. Maximum pulse width = 1 ms.
- 11. Pulse Width Distortion (PWD) is defined as |t<sub>PHL-tPLH</sub>| for any given device.
- 12. The difference between t<sub>PHL</sub> and t<sub>PLH</sub> between any two QCPL-341H parts under the same test condition.
- 13. Pin 1 and 4 need to be connected to LED common.
- 14. Common mode transient immunity in the high state is the maximum tolerable dV<sub>CM</sub>/dt of the common mode pulse, V<sub>CM</sub>, to assure that the output will remain in the high state (i.e.,  $V_0$  > 15.0 V).
- 15. Common mode transient immunity in a low state is the maximum tolerable dV<sub>CM</sub>/dt of the common mode pulse, V<sub>CM</sub>, to assure that the output will remain in a low state (i.e.,  $V_0$  < 1.0 V).
- 16. In accordance with UL1577, each optocoupler is proof tested by applying an insulation test voltage  $\geq 4500$  V<sub>RMS</sub> for 1 second (leakage detection current limit,  $I_{10} \leq 5 \mu A$ ).
- 17. Device considered a two-terminal device: pins 1, 2, 3 and 4 shorted together and pins 5, 6, 7 and 8 shorted together.
- 18. The device was mounted on a high conductivity test board as per JEDEC 51-7.





Figure 1. High output rail voltage vs. temperature.

Figure 2. V<sub>or VS</sub>. temperature.





Figure 3. V<sub>ol.</sub> vs. Temperature.

Figure 4. I<sub>cc</sub> vs. temperature.





Figure 5. I<sub>cc</sub> vs. V<sub>cc</sub>.

Figure 6. I<sub>FLH</sub> hysteresis.



Figure 7. I<sub>FLH</sub> vs. temperature.





Figure 9. Propagation delay vs. I.

Figure 10. Propagation delay vs. temperature.







Figure 11. Propagation delay vs. Rg.

Figure 12. Propagation delay vs. Cg.



Figure 13. Input Current vs. forward voltage.



Figure 14. I<sub>OH</sub> test circuit.



Figure 15. I<sub>OL</sub> test circuit.



**Figure 16. V<sub>OH</sub> test circuit.** 



Figure 17. V<sub>OL</sub> test circuit.



**Figure 18. IFLH test circuit.**



**Figure 19. UVLO test circuit.**





**Figure 20. tPLH, tPHL, t<sup>r</sup> and t<sup>f</sup> test circuit and waveforms.**



**Figure 21. CMR test circuit and waveforms.**

#### **Application Information**

#### **Recommended Application Circuit**

The recommended application circuit shown in Figure 22 illustrates a typical gate drive implementation using the QCPL-341H. The following describes about driving IGBT. However, it is also applicable to MOSFET. Designers will need to adjust the Vcc supply voltage, depending on the MOSFET or IGBT gate threshold requirements (Recommended V<sub>CC</sub> = 15 V for IGBT and 12 V for MOSFET).

The supply bypass capacitors (1 µF) provide the large transient currents necessary during a switching transition. Because of the transient nature of the charging currents, a low current (5.0 mA) power supply will be enough to power the device. The gate resistor R<sub>G</sub> serves to limit gate charge current and controls the IGBT collector voltage rise and fall times.

In PC board design, care should be taken to avoid routing the IGBT collector or emitter traces close to the QCPL-341H's inputs as this can result in unwanted coupling of transient signals into QCPL-341H and degrade performance.



Figure 22. Recommended application circuit with split resistors LED drive.

#### **Selecting the Gate Resistor (Rg)**

Step 1: Calculate Rg minimum from the  $I_{OL}$  peak specification. The IGBT and Rg in Figure 22 can be analyzed as a simple RC circuit with a voltage supplied by QCPL-341H.

$$
Rg \ge \frac{V_{CC} - V_{EE}}{I_{OLPEAK}}
$$

$$
= \frac{15V + 5V}{2.5A}
$$

$$
= 8\Omega
$$

Step 1: Check the QCPL-341H power dissipation and increase Rg if necessary. The QCPL-341H total power dissipation ( $Pr$ ) is equal to the sum of the emitter power  $(P_E)$  and the output power  $(P_0)$ .

 $P_T = P_E + P_O$  $P_E = I_F \cdot V_F \cdot Duty$  Cycle  $P_O = P_{O(BIAS)} + P_{O(SWITCHING)}$  $= I_{CC} \cdot (V_{CC} \cdot V_{EE}) + E_{SW}(Rg;Cg) \cdot f$ 

Using I<sub>F</sub>(worst case) = 16 mA, Rq = 8  $\Omega$ , Max Duty Cycle = 80%, Cq = 25 nF, f = 25 kHz and T<sub>A</sub> max = 70 °C:

 $P_E = 16$  mA  $\cdot$  1.95 V  $\cdot$  0.8 = 25 mW

 $P_0 = 5$  mA • 20 V + 4  $\mu$ J • 25 kHz  $= 100$  mW  $+ 100$  mW  $= 200$  mW < 250 mW (P<sub>O(MAX)</sub> @ 70 °C)

The value of 5 mA for  $\text{I}_{\text{CC}}$  in the previous equation is the maximum  $\text{I}_{\text{CC}}$  over the entire operating temperature range.

Since Po is less than P<sub>O(MAX)</sub>, Rg = 8  $\Omega$  is alright for the power dissipation.





#### **Dead Time and Propagation Delay Specifications**

The QCPL-341H includes a Propagation Delay Difference (PDD) specification intended to help designers minimize "dead time" in their power inverter designs. Dead time is the time period during which both the high and low side power transistors (Q1 and Q2 in Figure 22) are off. Any overlap in Q1 and Q2 conduction will result in large currents flowing through the power devices between the high and low voltage motor rails.

To minimize dead time in a given design, the turn on of LED2 should be delayed (relative to the turn off of LED1) so that under worstcase conditions, transistor Q1 has just turned off when transistor Q2 turns on, as shown in Figure 23. The amount of delay necessary to achieve this condition is equal to the maximum value of the propagation delay difference specification, PDD<sub>MAX</sub>, which is specified to be 100 ns over the operating temperature range of -40 °C to 105 °C.

Delaying the LED signal by the maximum propagation delay difference ensures that the minimum dead time is zero, but it does not tell a designer what the maximum dead time will be. The maximum dead time is equivalent to the difference between the maximum and minimum propagation delay difference specifications as shown in Figure 24. The maximum dead time for the QCPL-341H is 400 ns (= 200 ns - (-200 ns)) over an operating temperature range of -40 °C to 105 °C.

Note that the propagation delays used to calculate PDD and dead time are taken at equal temperatures and test conditions since the optocouplers under consideration are typically mounted in close proximity to each other and are switching identical IGBTs.



\*PDD = PROPAGATION DELAY DIFFERENCE NOTE: FOR PDD CALCULATIONS THE PROPAGATION DELAYS<br>ARE TAKEN AT THE SAME TEMPERATURE AND TEST CONDITIONS.

Figure 23. Minimum LED skew for zero dead time.



Figure 24. Waveforms for dead time.

#### **LED Current Input with Hysteresis**

The detector has optical receiver input stage with built in Schmitt trigger to provide logic compatible waveforms, eliminating the need for additional wave shaping. The hysteresis (Figure 6) provides differential mode noise immunity and minimizes the potential for output signal chatter.

#### **Under Voltage Lockout**

The QCPL-341HUnder Voltage Lockout (UVLO) feature is designed to prevent the application of insufficient gate voltage to the IGBT by forcing the QCPL-341H output low during power-up. IGBTs typically require gate voltages of 15 V to achieve their rated V $_{CE(ON)}$  voltage. At gate voltages below 13 V typically, the  $V_{CE(ON)}$  voltage increases dramatically, especially at higher currents. At very low gate voltages (below 10 V), the IGBT may operate in the linear region and quickly overheat. The UVLO function causes the output to be clamped whenever insufficient operating supply (Vcc) is applied. Once Vcc exceeds V<sub>UVLO</sub>+ (the positive-going UVLO threshold), the UVLO clamp is released to allow the device output to turn on in response to input signals.

#### **Thermal Model for QCPL-341H**

Definitions: TJE: LED junction temperature TJD: Detector IC junction temperature TC: Case temperature measured at the center of the package bottom θLC : LED-to-case thermal resistance θLD: LED-to-detector thermal resistance θ<sub>DC</sub>: Detector-to-case thermal resistance θCA: Case-to-ambient thermal resistance \*θCA will depend on the board design and the placement of the part TA: Ambient temperature.

$$
\theta_{\text{LO}} = 467 \text{ °C/W} \text{ T}_{\text{JD}} \text{ T}_{\text{JD}}
$$
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$$
\theta_{\text{LO}} = 467 \text{ °C/W} \text{ T}_{\text{C}} \text{ T}_{\text{D}} \text{ T}_{\text{JD}}
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\theta_{\text{L}} = 467 \text{ °C/W} \text{ T}_{\text{C}} \text{ T}_{\text{C}} \text{ T}_{\text{D}} \text{ T}_{\text{D}}
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\theta_{\text{C}} = 126 \text{ °C/W}
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\theta_{\text{C}} = 126 \text{ °C/W}
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\theta_{\text{C}} = 126 \text{ °C/W}
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Figure 25. Thermal model.

#### **Related Application Noted**

AN5336 – Gate Drive Optocoupler Basic Design for IGBT / MOSFET

AN1043 – Common-Mode Noise: Sources and Solutions

AV02-0310EN –Plastics Optocouplers Product ESD and Moisture Sensitivity

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