## CONSONANCE

# PWM Step-down DC-DC Controller IC CN5208 

## General Descriptions:

The CN5208 is a switch-mode PWM step-down DC-DC controller using few external components. It achieves 5A continuous output current over a wide input supply range with excellent load and line regulation. The output voltage is internally set at 5 V .

The high switching frequency of 550 KHz allows tiny external components to be usable. The CN5208 is designed to be stable with ceramic output capacitor. Pulse skipping mode is adopted under light load for high efficiency. Furthermore, the low operating current and low dropout operation make the CN5208 is suitable for battery powered systems.
Fault protection includes cycle-by-cycle current limit, short output protection and output overvoltage protection. In shutdown mode, the CN5208 draws only $7.5 \mu \mathrm{~A}(\mathrm{VCC}=15 \mathrm{~V})$ of supply current. On-chip soft-start minimizes the inrush supply current and the output overshoot at initial startup.
The CN5208 is available in a space-saving 8-pin SOP package.

## Applications:

- Car Charger
- Set-Top Box, Modems
- Pre-regulator
- Distributed Power Systems
- Battery Chargers


## Features:

- Wide Input Voltage: 4.8 V to 32 V
- Operating with an External P-Channel MOSFET
- Output Current Up to 5A
- Fixed Switching Frequency: 550 KHz
- Fixed Output Voltage with $1 \%$ Accuracy
- Efficiency up to $95 \%$
- Low Drop-Out Mode
- Stable with Low-ESR Output Ceramic Capacitor
- On-Chip Power-On Delay to Debounce Input Supply
- Cycle-by-Cycle Current Limit
- Overvoltage protection
- Frequency Foldback for Output Short Circuit Protection
- Built-in Soft Start
- High Efficiency at Light Load with Pulse Skipping Mode
- Shutdown Curent: 7.5uA typical at 15 V
- Operating Ambient Temperature $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
- Available in 8-Pin SOP Package
- Pb-free, Rohs-Compliant, Halogen Free


## Pin Assignment:



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## Typical Application Circuit:



Figure 1 Typical Application Circuit
In Figure 1,

- C 2 is $100 \mathrm{nF}(0603)$
- C 3 is $10 \mathrm{nF}(0603)$
- R1 is 1 K ohm ( 0603 or 0402 )
- Please refer to section of Application Information for the selection of the other components


## Ordering Information:

| Part No. | Shipment | Output Voltage | Operating Ambient Temperature |
| :---: | :---: | :---: | :---: |
| CN5208 | Tape and Reel, $4000 /$ Reel | 5 V | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |

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## Pin Description:

| Pin No. | Name | Descriptions |
| :---: | :---: | :--- |
| 1 | VG | Internal Voltage Regulator Output. VG internally supplies power to gate <br> driver, connect a 100nF capacitor between VG pin and VCC pin. |
| 2 | GND | Ground. Negative terminal of input supply. <br> 3 |
| SHDN | Shutdown Input. Applying a voltage of above 2.2V at this pin puts the CN5208 <br> into low-current shutdown mode; The CN5208 will be back to normal operation <br> if this pin voltage is pulled below 0.5V after a typical delay of 13ms. <br> Do NOT apply a voltage between 0.5V to 2.2V to SHDN pin, otherwise the <br> CN5208 may be in uncertain state. |  |
| 4 | COM | Frequency Compensation Input. The closed-loop's frequency compensation <br> network is connected at this pin. |
| 5 | SWT | Output Voltage Sensing Input. It monitors the converter's output voltage, and <br> the the positive terminal of the output bypass capacitor is connected. |
| 6 | Switching Node. The inductor and the cathode of the freewheeling diode should <br> be connected to this pin. The voltage swing of SW pin is from a diode drop <br> below Ground to VCC. |  |
| 7 | VCC | Unregulated DC Power Supply. VCC is also the power supply for CN5208 <br> internal circuit. Bypass this pin with capacitors. |
| 8 | DRV | Gate Drive Pin. Drive the gate of external P-channel MOSFET, connect DRV <br> pin to the gate of the external P-channel MOSFET. |

Absolute Maximum Ratings
Voltage from VCC, VG, SW, DRV, to GND ..... -0.3 V to 36 V
Voltage from VG to VCC. ..... -8 V to +0.3 V
Voltage from OUT, SHDN and COM to GND ..... -0.3 V to 6.5 V
Storage Temperature $-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
Operating Ambient Temperature. ..... $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$
Lead Temperature(Soldering, 10 seconds) ..... $.260^{\circ} \mathrm{C}$

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## Electrical Characteristics:

$\left(\mathrm{VCC}=15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}\right.$ to $85^{\circ} \mathrm{C}$, unless otherwise noted)

| Parameters | Symbol | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input Voltage Range | VCC |  | 4.8 |  | 32 | V |
| Under voltage lockout Threshold | UVLO |  | 3.6 | 4.2 | 4.7 | V |
| Operating Current | $\mathrm{I}_{\mathrm{VCC}}$ | $\mathrm{V}_{\text {OuT }}=5.5 \mathrm{~V}$, No switching | 360 | 460 | 560 | uA |
| Regulated Output Voltage | $V_{\text {Out }}$ |  | 4.95 | 5 | 5.05 | V |
| OUT Pin Current | Iout | $\mathrm{V}_{\text {OuT }}=5 \mathrm{~V}$ | 6 | 9 | 12 | uA |
| Overvoltage Trip Level | Vov | Output voltage rises | 1.04 | 1.06 | 1.08 | $\% \mathrm{~V}_{\text {OUT }}$ |
| Overvoltage Clear Level | Vclr | Output voltage falls | 1.0 | 1.02 | 1.04 |  |
| Power-on Delay | $\mathrm{t}_{\text {delay }}$ |  | 10 | 13 | 16 | ms |
| Soft Start Time | tss |  | 44 | 52 | 60 | ms |
| Inductor Current Limit |  |  |  |  |  |  |
| Current Limit Threshold | $\mathrm{V}_{\text {ILIM }}$ | VCC - V ${ }_{\text {sw }}$, Temp $=25^{\circ} \mathrm{C}$ | 108 | 120 | 132 | mV |
| Temperature Coefficient | TC ${ }_{\text {ILIM }}$ |  |  | +0.35 |  | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |
| Propagation Delay | PD | 20mV Overdrive |  | 220 |  | ns |
| Oscillator |  |  |  |  |  |  |
| Switching Frequency | $\mathrm{f}_{\text {osc }}$ |  | 450 | 550 | 650 | kHZ |
| Maximum Duty Cycle | Dmax |  |  | 100 |  | \% |
| Foldback Frequency | $\mathrm{f}_{\text {fold }}$ | $\mathrm{V}_{\text {OuT }}=0 \mathrm{~V}$ | 90 | 110 | 130 | KHz |
| SHDN Pin |  |  |  |  |  |  |
| Input Voltage High | $\mathrm{V}_{\text {IH }}$ |  | 2.2 |  |  | V |
| Input Voltage Low | $\mathrm{V}_{\text {IL }}$ |  |  |  | 0.5 | V |
| SHDN Bias Current | ISHDN |  | $-100$ | 0 | +100 | nA |
| DRV Pin |  |  |  |  |  |  |
| $\mathrm{V}_{\text {DRV }}$ High (VCC - $\mathrm{V}_{\text {DRV }}$ ) | VH | $\mathrm{I}_{\mathrm{DRV}}=-10 \mathrm{~mA}$ |  | 60 |  | mV |
| $\mathrm{V}_{\text {DRV }}$ Low (VCC-V $\mathrm{V}_{\text {DRV }}$ ) | VL | $\mathrm{I}_{\mathrm{DRV}}=0 \mathrm{~mA}$ |  | 6.3 |  | V |
| Rise Time | $\mathrm{t}_{\mathrm{r}}$ | Cload $=2 \mathrm{nF}, 10 \%$ to $90 \%$ | 30 | 40 | 65 | ns |
| Fall Time | $\mathrm{t}_{\mathrm{f}}$ | Cload $=2 \mathrm{nF}, 90 \%$ to $10 \%$ | 30 | 40 | 65 | ns |

Note: Vout is the regulated output voltage.

## Detailed Description:

The CN5208 is an asynchronous step-down (buck) DC to DC controller that drives an external P-channel MOSFET with few external components. The CN5208 regulates the output voltage with fixed frequency PWM mode, the wide input voltage range is from 4.8 V to 32 V , the output voltage is internally fixed at 5 V , and the maximum output current can be up to 5 A . The pulse skipping mode is adopted under light load conditions for high efficiency. The switching frequency is fixed at 550 KHz , which makes the low-profile inductor usable in the application circuit.
The on-chip resistor divider, high precision bandgap voltage and error amplifier make the accuracy of the output voltage within $1 \%$. CN5208's current consumption is only 460uA (Typical), also low drop-out mode is adopted when input voltage is close to the output voltage, which make the device suitable for battery powered system.

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The frequency foldback reduces the switching frequency to 110 KHz by increasing off time during overcurrent conditions or short circuit condition to help control the inductor current.
The other fault protection includes overvoltage protection, cycle-by-cycle inductor current limit, etc.
The input high level of shutdown input (SHDN) puts the CN5208 into low-current shut down state
The on-chip soft start can limit the inrush current on power up, or SHDN being pulled low from high level, or release from short circuit.

## Application Information

## Under voltage Lockout (UVLO)

An under voltage lockout circuit monitors the input voltage and keeps CN5208 off if VCC falls below 4.7V
(Maximum). The CN5208 begins functioning only after VCC rises above 4.7 V and a 13 ms (Typical) delay expires. The delay can debounce the input supply.

## Shutdown Mode

The SHDN pin is active high shutdown input. Pulling this pin above 2.2 V causes the CN5208 to completely shut down and enters a low current state, in which the current consumption is only 7.5 uA typical when VCC is 15 V . Pulling SHDN pin below 0.5 V brings the CN5208 back to normal operation after a delay of 13 ms (Typical). Do NOT apply a voltage between 0.5 V to 2.2 V to SHDN pin, otherwise the CN5208 may be in uncertain state.

## Soft Start

The built-in soft start circuit can limit the inrush current, and can be activated by events of power up, or SHDN being pulled low from high level, or release from short circuit.

The typical duration time of soft start is 52 ms .

## Overvoltage Protection

An overvoltage comparator guards against transient overshoots and other conditions that may overvoltage the output. Once the over voltage is asserted, the P-channel MOSFET is turned off until the overvoltage condition is cleared. Typically the over voltage is asserted when output voltage is $5.8 \%$ higher than the nominal value, and is cleared when the output voltage falls below $102.2 \%$ of nominal value.

## Cycle-by-Cycle Current Limit

The CN5208 has cycle-by-cycle current limit control, the inductor current is monitored during the on-state of the external P-channel MOSFET by sensing the voltage drop across the on-resistance of the P-channel MOSFET. If the voltage across the on-resistance exceeds the preset threshold, the power MOSFET is turned off to prevent the inductor current from further increasing. The CN5208 supports temperature-compensated current limit threshold.
The propagation delay with the current limit circuit block is 220 ns ( 20 mV Overdrive). So the actual maximum inductor current is decided by the following equation after taking the propagation delay into consideration:

$$
\text { ILMAX }=\frac{\text { VILIM }}{\text { Rdson }}+220 \times 10^{-9} \times \frac{\text { VIN-Vout }}{L}
$$

Where:
$\mathrm{I}_{\text {LMAX }}$ is the maximum inductor current
$\mathrm{V}_{\text {ILIM }}$ is the current limit threshold
Rdson is the on resistance of the external P-channel MOSFET

## Short-Circuit Protection and Frequency Foldback

In addition to the cycle-by-cycle current limit, the CN5208 also includes the frequency foldback circuit to further limit the inductor current from runaway or short circuit at the output. In these cases, the switching frequency is reduced to 110 KHz from 550 KHz by increasing the off time, the duty cycle is kept very low, hence the inductor current is further limited.

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## Gate Drive

The CN5208's gate driver can provide high transient current to drive the external pass transistor. The rise and fall times are typically 35 ns when driving a 2000 pF load, which is typical for a P-channel MOSFET with Rds(on) in the range of $20 \mathrm{~m} \Omega$.
A voltage clamp is added to limit the gate drive to 8 V max. below VCC. For example, if VCC is 20 V , then the DRV pin output will be pulled down to 12 V min. This allows low voltage P -channel MOSFETs with superior Rds(on) to be used as the pass transistor, which increases efficiency.

## Input Capacitor

The input voltage source impedance and cable length determine the size of the input capacitor, which is typically in the range of $10 \mu \mathrm{~F}$ to $50 \mu \mathrm{~F}$. The input bypass capacitor should have low impedance at the frequency of 550 KHz . A low ESR capacitor or two type of capacitors in parallel is recommended. For the low ESR capacitors, high-quality ceramic type X 5 R or X 7 R is recommended. The voltage rating should be greater than the maximum input voltage.
The input ripple voltage can be approximated by the following equation:

$$
V_{\text {INrip }}=\frac{0.25 \times \text { lomax }}{\mathrm{fsw}_{\mathrm{w}} \times \mathrm{C} 1}+\text { ESR } \times \text { lomax }
$$

Where,
$\mathrm{V}_{\text {INrip }}$ is the ripple voltage at input supply
Iomax is the maximum output current in Ampere
$\mathrm{f}_{\text {SW }}$ is the switching frequency $(550 \mathrm{KHz})$
C 1 is the intput bypass capacitor in Farad
ESR is the equivalent series resistance of C1
Please note that the input capacitor can see a very high surge current during loading transient and solid tantalum capacitors can fail catastrophically under these conditions.

## Output Capacitor

The output capacitor keeps the output voltage ripple small and ensures feedback loop stability. The CN5208 is designed to be stable with low-ESR ceramic capacitor at output. The output capacitor impedance should be low at the switching frequency. Ceramic capacitors with X5R or X7R dielectrics are highly recommended for their low ESR characteristics. When choosing the output capacitor, special consideration should be given to the voltage coefficient of the capacitor, since the capacitance may be reduced by the applied DC bias voltage.
The output voltage ripple can be estimated by the following equation:

$$
\text { Vripple }=0.31 \mathrm{omax} X\left[E S R+\frac{1}{8 \mathrm{fsw} \times \mathrm{Co}}\right]
$$

Where,
$\mathrm{V}_{\text {ripple }}$ is the output voltage ripple in Volt
Iomax is the maximum output current in Ampere
$\mathrm{f}_{\text {SW }}$ is the switching frequency $(550 \mathrm{KHz})$
$\mathrm{C}_{0}$ is the output bypass capacitor in Farad
ESR is the equivalent series resistance of $\mathrm{C}_{0}$
If an electrolytic capacitor is used, it is highly recommended to put a low-ESR ceramic capacitor in parallel with the electrolytic capacitor.

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## MOSFET Selection

The CN5208 uses a P-channel power MOSFET to regulate the output voltage. The MOSFET must be selected to meet the maximum output current and the efficiency or power dissipation requirements of the application circuit as well as the maximum temperature of the MOSFET. The important parameters for the power MOSFET are the breakdown voltage $B V_{D S S}$, the turn-on voltage, the on resistance $R_{\text {dson }}$, the total gate charge $Q_{g}$, the reverse transfer capacitance $\mathrm{C}_{\text {RSS }}$ and the maximum drain current $\mathrm{I}_{\mathrm{D}}$.

The peak-to-peak gate drive voltage is set internally, this voltage is typically 6 V . Consequently, logic-level threshold MOSFETs must be used. The maximum turn-on voltage should be less than 3 V .
The MOSFET power dissipation at maximum output current is approximated by the equation:

$$
\text { Pd }=\frac{\text { Vout }}{\text { VCC }} \times \operatorname{Rds}(\text { on }) \times \text { lout }^{2} \times(1+0.005 \mathrm{dT})
$$

Where:
Pd is the power dissipation of the power MOSFET
Vout is the maximum battery voltage
VCC is the minimum input voltage
Rds(on) is the power MOSFET's on resistance at room temperature
Iout is the output current
dT is the temperature difference between actual ambient temperature and room temperature $\left(25^{\circ} \mathrm{C}\right)$
In addition to the $I^{2} \mathrm{Rds}(\mathrm{on})$ loss, the power MOSFET still has transition loss, which are highest at the highest input voltage. Generally speaking, for VIN $<20 \mathrm{~V}$, the $\mathrm{I}^{2} \mathrm{Rds}$ (on) loss may be dominant, so the MOSFET with lower Rds(on) should be selected for better efficiency; for VIN $>20 \mathrm{~V}$, the transition loss may be dominant, so the MOSFET with lower C $_{\text {RSS }}$ can provide better efficiency. $\mathrm{C}_{\text {RSS }}$ is usually specified in the MOSFET characteristics; if not, then $C_{\text {RSS }}$ can be calculated using $C_{R S S}=\mathrm{Q}_{\mathrm{GD}} / \Delta \mathrm{V}_{\mathrm{DS}}$.
The CN5208 performs cycle-by-cycle inductor current sensing by monitoring the voltage across the on-resistance of the power MOSFET, so the MOSFET's on-resistance should be chosen based on the required output current. The current limit threshold voltage is temperature compensated to comply with the MOSFET's on-resistance variation with temperature. The following equation is a good guide for determining the required $\mathrm{R}_{\mathrm{dson}(\mathrm{MAX})}$ at $\mathrm{V}_{\mathrm{GS}}=4.5 \mathrm{~V}, 25^{\circ} \mathrm{C}$ (manufacturer's specification), allowing some margin for ripple current, current limit and variations in the CN5208 and external component values:

$$
\operatorname{Rdson}(\text { MAX }) \cong \frac{90 \mathrm{mV}}{\mathrm{lo}(\mathrm{MAX})}
$$

## Diode Selection

The diode D1 in Figure 1 is Schottky diode that has the current rating larger than the output current limit, and the reverse breakdown voltage exceeding the maximum expected input voltage.

However, if the Schottky diode The diode that is much larger than that is sufficient can result in larger transition losses due to their larger junction capacitance.

## Inductor Selection

The inductor current ramps up/down when the P-channel MOSFET is turned on/off, its ripple increases with lower inductance or higher input voltage. Higher inductor ripple current results in higher ripple voltage and greater core losses. So the inductor's ripple current should be limited within a reasonable range.
An inductor should be chosen that can carry the maximum output current, also the ripple current is limited to $30 \%$ of maximum output current. The inductor's saturation current should be at least 1.5 times of the maximum output current.

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The following equation is used to calculate the minimum value of the inductor:

$$
\mathrm{L}_{\mathrm{MIN}}=\frac{\mathrm{V}_{\mathrm{OUT}(\mathrm{MAX})} \times\left(\mathrm{V}_{\mathrm{IN}(\text { MAX })}-\mathrm{V}_{\mathrm{OUT}}\right)}{\mathrm{V}_{\mathrm{IN}(\text { MAX })} \times 0.3 \times \mathrm{I}_{\mathrm{OUT}} \times f_{\mathrm{SW}}}
$$

Where, $\mathrm{f}_{\text {SW }}$ is the switching frequency, here is 550 KHz .
For most applications, a $4.7 \mu \mathrm{H}$ to $27 \mu \mathrm{H}$ inductor with a DC current rating of at least $30 \%$ higher than the maximum output current is recommended.

## Frequency Compensation Network Design

Figure 2 shows the AC response-related circuit of a step-down DC-DC Converter using the CN5208.


Figure 2 AC Response-Related Circuit
The inductor, output bypass capacitor and the load resistance Rout form 2 poles and 1 zero, they are:

- The double pole formed by inductor and output capacitor:

$$
\omega_{\mathrm{p} 1, \mathrm{P} 2}=\frac{1}{\sqrt{\mathrm{LC} \mathrm{C}_{\mathrm{O}}}}
$$

- The zero formed by the output capacitor and its equivalent series resistance(ESR)

$$
\omega_{z 1}=\frac{1}{r_{\text {esr }} C_{0}}
$$

This zero $\omega_{z 1}$ can be neglected if low ESR ceramic capacitor is used.
In the above 2 equations, $\mathrm{C}_{0}$ is the output bypass capacitance, $\mathrm{r}_{\text {esr }}$ is the ESR of output bypass capacitor, and L is the inductance.
In Fig. 2, C3, C4 and R3 form the compensation network. The design procedure of the compensation network is:
Step 1: Calculate $\omega_{\mathrm{P} 1}, \omega_{\mathrm{p} 2}$ and $\omega_{\mathrm{z} 1}$ based on the above 2 equations
Step 2: Make the zero $\omega_{z}$ formed by R3 and C3 around $0.7 * \omega_{\mathrm{P} 1}$, and make C 3 equal to 10 nF , then R 3 value can be calculated by the following equation:

$$
\mathrm{R} 3=\frac{1}{\omega_{\mathrm{z}} \mathrm{C} 3}-1800
$$

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Where, $\omega_{\mathrm{z}}$ equals to $0.7 \omega_{\mathrm{P} 1}$
R3's unit is ohm.
Step 3: Determine C4's value in Farad (F)
R3 and C4 form a pole to cancel the effect of $\omega_{z 1}$. If low ESR capacitor is used for output capacitor Co, $\omega_{z 1}$ can be neglected. To be exact, C4 is not needed if $\omega_{z 1}$ is greater than 250 KHz . If needed, C4 can be calculated by the following equation:

$$
\mathrm{C} 4=\frac{0.8}{\mathrm{R} 3 \cdot \omega_{\mathrm{z} 1}}
$$

## Application Circuit for Input Voltage Beyond 20V

When the input supply is applied to the input bypass low-ESR ceramic capacitors of the DC-DC converter, voltage spikes may be created in case of long cable, and these voltage spikes can easily be twice the amplitude of input voltage, which may damage the CN5208 or P-channel MOSFET shown in Figure 1 if the input voltage is high..
To prevent the CN5208 and P-channel MOSFET from being damaged by the voltage spike, the voltage rating of the P-channel MOSFET should be higher than the voltage spike. A low-pass RC filter should be added to protect CN5208 as shown in Figure 3 if the input voltage is higher than 20V. Resistor R5 and capacitor C5 are used to filter out the input voltage spike. R5's value can be 5.1ohm (0805), C5's capacitance can be 10 uF ( 0805 ).


Figure 3 Protect CN5208 from Input Voltage Spike

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## Design Procedure

The following 6 steps of design procedure should be followed to determine the converter's circuit parameters.

## Step 1: Select Input Capacitor

The input bypass capacitor is decided by the requirement of the ripple voltage at input supply.
Generally speaking, the ripple voltage of input supply should be kept below 0.2 V . The ripple voltage is approximately decided by the following equation:

$$
\mathrm{V}_{\text {INrip }}=\frac{0.25 \times \text { lomax }}{\mathrm{fsw}_{\mathrm{w}} \times 1}+\text { ESR } \times \text { ІомAX }
$$

## Step 2: Select Output Capacitor

The output bypass capacitor is also decided by the requirement of output ripple voltage. Ceramic capacitors with X5R or X7R dielectrics are highly recommended for their low ESR characteristics. The output ripple voltage is estimated by the following equation:


## Step 3: Select P-channel MOSFET

The important parameters for the P-channel MOSFET are the breakdown voltage $\mathrm{BV}_{\mathrm{DSs}}$, the turn-on voltage, the on resistance $\mathrm{R}_{\text {dson }}$, the total gate charge $\mathrm{Q}_{\mathrm{g}}$, the reverse transfer capacitance and the maximum drain current $\mathrm{I}_{\mathrm{D}}$. The maximum turn-on voltage should be less than 3 V .

The maximum on-resistance at $\mathrm{V}_{\mathrm{GS}}=4.5 \mathrm{~V}, 25^{\circ} \mathrm{C}$ (manufacturer's specification) should meet the requirement of the following equation:

$$
\operatorname{Rdson}(\text { MAX }) \cong \frac{90 \mathrm{mV}}{\mathrm{lo}(\text { MAX })}
$$

## Step 4: Select Diode

The diode D1 in Figure 1 is Schottky diode that has the current rating larger than the output current limit, and the reverse breakdown voltage exceeding the maximum expected input voltage.

## Step 5: Select Inductor

An inductor should be chosen that can carry the maximum output current, also the ripple current is limited to $30 \%$ of maximum output current.
The inductor's saturation current should be at least 1.5 times of the maximum output current.
The inductance is estimated by the following equation:

$$
L_{\text {MIN }}=\frac{V_{\text {OUT(MAX) }} \times\left(\mathrm{V}_{\text {INMAX }}-\mathrm{V}_{\text {OUT }}\right)}{\mathrm{V}_{\text {IN(MAX) }} \times 0.3 \times \mathrm{I}_{\text {OUT }} \times f_{\text {SW }}}
$$

## Step 6: Design Compensation Network

Design the parameters of R3, C3 and C4 in Figure 1 according to the converter's poles and zero decided by the inductor, output capacitor and its ESR, etc.

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## Design Example

For this design example, use the following as the input parameters:

| Design Parameter | Example Value |
| :---: | :---: |
| Input Voltage | 20 V |
| Output Voltage | 5.0 V |
| Maximum Output Current | 5 A |
| Input Ripple Voltage | 0.2 V |
| Output Ripple Voltage | 50 mV |

(1) Choose the input capacitor C 1

The ceramic capacitor is chosen for input bypass capacitor, it is supposed that its ESR is 20 mohm . The required input capacitance can be calculated by solving the following equation with the input parameters of $\mathrm{V}_{\text {INrip }}=0.2 \mathrm{~V}, \mathrm{I}_{\text {OMAX }}=5 \mathrm{~A}, \mathrm{f}_{\text {SW }}=550 \mathrm{KHz}, \mathrm{ESR}=20 \mathrm{mohm}$ :

$$
V_{\text {INrip }}=\frac{0.25 \times \text { lomax }}{f_{\text {SW }} \times C 1}+\text { ESR } \times \text { lomax }
$$

The input bypass capacitor should be 22.7 uF at least, so two $22 \mathrm{uF}(1206)$ ceramic capacitors in parallel can be used as the input bypass capacitor in light of the capacitor's voltage coefficient.
(2) Choose the output capacitor $\mathrm{C}_{o}$

The ceramic capacitor is chosen for output bypass capacitor, it is supposed that the ESR is 20 mohm . The required output capacitance can be calculated by solving the following equation with the input parameters of $\mathrm{V}_{\text {ripple }}=50 \mathrm{mV}, \mathrm{I}_{\text {OMAX }}=5 \mathrm{~A}, \mathrm{f}_{\mathrm{SW}}=550 \mathrm{KHz}, \mathrm{ESR}=20 \mathrm{mohm}:$

$$
\text { Vripple }=0.31 \mathrm{I} \max X\left[E S R+\frac{1}{8 \mathrm{fsw} \times \mathrm{Co}}\right]
$$

The output bypass capacitor should be 17 uF at least, so two $22 \mathrm{uF}(1206)$ ceramic capacitors in parallel are used as the output bypass capacitor, or at least three $10 \mathrm{uF}(0805)$ ceramic capacitors in parallel are used as the output bypass capacitor in light of the capacitor's voltage coefficient.
(3) Select the P-channel MOSFET

The P-channel MOSFET's on resistance should meet the following requirement:

$$
\operatorname{Rdson}(\text { MAX }) \cong \frac{90 \mathrm{mV}}{\mathrm{IO}(\mathrm{MAX})}
$$

The Rdson(max) is 20 mohm , so AOD4185 with 20 mohm on-resistance at 4.5 V is selected.
(4) Select the Schottky diode D1

The schottky diode 1N5824 is selected.
(5) Select the inductor

The inductor should have a saturation current of at least 7.5 A , and inductance should meet the requirement of the following equation:

$$
\mathrm{L}_{\mathrm{MIN}}=\frac{\mathrm{V}_{\mathrm{OUT}(\mathrm{MAX})} \times\left(\mathrm{V}_{\text {IN(MAX }}-\mathrm{V}_{\mathrm{OUT}}\right)}{\mathrm{V}_{\mathrm{IN}(\text { MAX })} \times 0.3 \times \mathrm{I}_{\mathrm{OUT}} \times f_{\mathrm{SW}}}
$$

The inductance should be 4.5 uH at least, so we choose a 4.7 uH inductor.

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(6) Calculate the compensation network

With inductor of 4.7 uH and $\mathrm{Co}_{0}$ of 44 uF , the poles $\omega_{\mathrm{P} 1}$ and $\omega_{\mathrm{p} 2}$ are calculated by the following equation:

$$
\omega_{\mathrm{p} 1, \mathrm{P} 2}=\frac{1}{\sqrt{\mathrm{LC}} \mathrm{C}_{\mathrm{o}}}
$$

So $\omega_{\mathrm{P} 1}$ and $\omega_{\mathrm{p} 2}$ are at 69.5 KHz , then the zero formed by R 3 and C 3 should be at $0.7 \omega_{\mathrm{P} 1}$, namely $\omega_{\mathrm{z}}$ is at 48.7 KHz . According to the equation:

$$
\mathrm{R} 3=\frac{1}{\omega_{\mathrm{z}} \mathrm{C} 3}-1800
$$

With C3 at 10 nF and $\omega_{\mathrm{z}}$ at $48.7 \mathrm{KHz}, \mathrm{R} 3$ is calculated at 253 ohm , round up to the nearest standard value, the 270 ohm resistor can be chosen for R3.

Since low-ESR ceramic capacitor is used for output capacitor $\mathrm{C}_{0}, \mathrm{C} 4$ is not needed.

## Circuit Parameters for some Typical Cases

Table 1 to Table 4 list the circuit parameters under some typical application conditions, the circuit parameters in the tables are corresponding to the application circuit shown in Figure 1.

## Disclaimer:

The circuit parameters listed in the following 4 tables are for reference only, it is not a suggestion, and may or may not be followed. The actual application circuit and its parameters should be strictly designed based on each application's operating conditions and environment.

Table 1 Input Voltage $\mathrm{VCC}=8 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=5 \mathrm{~V}$ with $\mathrm{I}_{\mathrm{omax}}=1 \mathrm{~A}, 2 \mathrm{~A}, 3.5 \mathrm{~A}$ and 5 A

| Parameters | $\mathrm{I}_{\text {OMAX }}=1 \mathrm{~A}$ | $\mathrm{I}_{\text {OMAX }}=2 \mathrm{~A}$ | $\mathrm{I}_{\text {OMAX }}=3.5 \mathrm{~A}$ | $\mathrm{I}_{\text {OMAX }}=5 \mathrm{~A}$ |
| :---: | :---: | :---: | :---: | :---: |
| C1 | Ceramic capacitor, 10uF,0805 | Ceramic capacitor, $22 \mathrm{uF}, 1206$ | Ceramic capacitor, <br> Two (22uF, 1206) in parallel | Ceramic capacitor, <br> Two (22uF, 1206) in parallel |
| C2 | 100nF, 0603 | 100nF, 0603 | 100nF, 0603 | 100nF, 0603 |
| Co | Ceramic capacitor, <br> (10uF,0805) or (22uF, 1206) | Ceramic capacitor, (22uF, 1206) | Ceramic capacitor, <br> Two (22uF, 1206) <br> in parallel | Ceramic capacitor, <br> Two (22uF, 1206) in parallel |
| C3 | 10nF, 0603 | 10nF, 0603 | 10nF, 0603 | 10nF, 0603 |
| C4 | No need | No need | No need | No need |
| R1 | 1Kohm, 0603/0402 | 1Kohm, 0603/0402 | 1Kohm, 0603/0402 | 1Kohm, 0603/0402 |
| R3 | 510 ohm, 0603/0402 | 150 ohm, 0603/0402 | 300 ohm, 0603/0402 | 390 ohm, 0603/0402 |
| M1(P-MOS) | $\begin{gathered} \text { AO3401A,AO3407A } \\ \text { SI2305 } \end{gathered}$ | SI4435 | AO4407A,AON7403 | AO4407A, SI4425 |
| D1 | SS24 or SS34 | SS34 | SS54,1N5824 | 1N5824 |
| L | 12 uH or 15 uH | 6.8 uH or 10 uH | 4.7 uH or 6.8 uH | 4.7 uH |

## CONSONANCE

Table 2 Input Voltage VCC $=15 \mathrm{~V}$, Vout $=5 \mathrm{~V}$ with $I_{\text {omax }}=1 \mathrm{~A}, 2 \mathrm{~A}, 3.5 \mathrm{~A}$ and 5 A

| Parameters | $\mathrm{I}_{\text {OMAX }}=1 \mathrm{~A}$ | $\mathbf{I O M A X}=\mathbf{2 A}$ | $\mathrm{I}_{\text {OMAX }}=3.5 \mathrm{~A}$ | $\mathrm{I}_{\text {OMAX }}=5 \mathrm{~A}$ |
| :---: | :---: | :---: | :---: | :---: |
| C1 | Ceramic capacitor, 22uF, 1206 | Ceramic capacitor, 22uF, 1206 | Ceramic capacitor, <br> Two (22uF, 1206) in parallel | Ceramic capacitor, <br> Two (22uF, 1206) in parallel |
| C2 | 100nF, 0603 | 100nF, 0603 | 100nF, 0603 | 100nF, 0603 |
| Co | Ceramic capacitor, <br> (10uF,0805) or (22uF, 1206) | Ceramic capacitor, $(22 \mathrm{uF}, 1206)$ | Ceramic capacitor, <br> Two (22uF, 1206) in parallel | Ceramic capacitor, <br> Two (22uF, 1206) in parallel |
| C3 | 10nF, 0603 | 10nF, 0603 | 10nF, 0603 | 10nF, 0603 |
| C4 | No need | No need | No need | No need |
| R1 | 1Kohm, 0603/0402 | 1Kohm, 0603/0402 | 1Kohm, 0603/0402 | 1Kohm, 0603/0402 |
| R3 | 820 ohm, 0603/0402 | 390 ohm, 0603/0402 | 560 ohm, 0603/0402 | 560 ohm, 0603/0402 |
| M1(P-MOS) | AO3401A,SI3407A | AO4435, SI4435 | AO4407A,AON7403 | AO4407A, SI4425 |
| D1 | SS24 or SS34 | SS34 | SS54,1N5824 | 1N5824 |
| L | 22uH | 12uH | 6.8 uH | 4.7 uH |

Table 3 Input Voltage VCC $=24 \mathrm{~V}$, Vout $=5 \mathrm{~V}$ with $I_{\text {OMAX }}=1 \mathrm{~A}, 2 \mathrm{~A}, 3.5 \mathrm{~A}$ and 5 A

| Parameters | $\mathrm{I}_{\text {OMAX }}=1 \mathrm{~A}$ | $\mathrm{I}_{\text {OMAX }}=\mathbf{2 A}$ | $\mathrm{IOMAx}=3.5 \mathrm{~A}$ | $\mathrm{I}_{\text {OMAX }}=5 \mathrm{~A}$ |
| :---: | :---: | :---: | :---: | :---: |
| C1 | Ceramic capacitor, 22uF, 1206 | Ceramic capacitor, $2(22 u F, 1206)$ <br> in parallel | Ceramic capacitor, Two (22uF, 1206) in parallel | Ceramic capacitor, Three (22uF,1206) in parallel |
| C2 | 100nF, 0603 | 100nF, 0603 | 100nF, 0603 | 100nF, 0603 |
| Co | Ceramic capacitor, (10uF,0805) or (22uF, 1206) | Ceramic capacitor, (22uF, 1206) | Ceramic capacitor, <br> Two (22uF, 1206) <br> in parallel | Ceramic capacitor, <br> Two (22uF, 1206) <br> in parallel |
| C3 | 10nF, 0603 | 10nF, 0603 | 10nF, 0603 | 10nF, 0603 |
| C4 | No need | No need | No need | No need |
| R1 | 1Kohm, 0603/0402 | 1Kohm, 0603/0402 | 1Kohm, 0603/0402 | 1Kohm, 0603/0402 |
| R3 | 1.2Kohm, 0603/0402 | 390 ohm, 0603/0402 | 560 ohm, 0603/0402 | 5600 ohm, 0603/0402 |
| M1(P-MOS) | SI2319,AO3407A | SI4909,SI7611 | AON7403 | AOD4185 |
| D1 | SS24 or SS34 | SS34 | SS54,1N5824 | 1N5824 |
| L | 27uH | 12uH | 6.8 uH | 4.7 uH |

## CONSONANCE

Table 4 Input Voltage $V C C=32 \mathrm{~V}$, Vout $=5 \mathrm{~V}$ with $I_{\text {omax }}=1 \mathrm{~A}, 2 \mathrm{~A}, 3.5 \mathrm{~A}$ and 5 A

| Parameters | $\mathrm{I}_{\text {OMAX }}=1 \mathrm{~A}$ | $\mathbf{I O M A X}^{=2 \mathrm{~A}}$ | $\mathrm{I}_{\text {OMAX }}=3.5 \mathrm{~A}$ | $\mathrm{I}_{\text {OMAX }}=5 \mathrm{~A}$ |
| :---: | :---: | :---: | :---: | :---: |
| C1 | Ceramic capacitor, 22uF, 1206 | Ceramic capacitor, <br> Two (22uF, 1206) in parallel | Ceramic capacitor, Two (22uF, 1206) in parallel | Ceramic capacitor, Three (22uF, 1206) in parallel |
| C2 | 100nF, 0603 | 100nF, 0603 | 100nF, 0603 | 100nF, 0603 |
| Co | Ceramic capacitor, (10uF,0805) or (22uF,1206) | Ceramic capacitor, (22uF, 1206) | Ceramic capacitor, Two (22uF, 1206) in parallel | Ceramic capacitor, Two (22uF, 1206) in parallel |
| C3 | 10nF, 0603 | 10nF, 0603 | 10nF, 0603 | 10nF, 0603 |
| C4 | No need | No need | No need | No need |
| R1 | 1Kohm, 0603/0402 | 1Kohm, 0603/0402 | 1Kohm, 0603/0402 | 1Kohm, 0603/0402 |
| R3 | 1.2Kohm, 0603/0402 | 1.8Kohm, 0603/0402 | 1Kohm, 0603/0402 | 1Kohm, 0603/0402 |
| M1(P-MOS) | SI2319 | SI4909, AO4421 | AOD4185 | AOD4185 |
| D1 | SS24 or SS34 | SS34 | SS54,1N5824 | 1N5824 |
| L | 27uH | 15uH | 10uH | 6.8 uH |

## PCB Layout Considerations

When laying out the printed circuit board, the following considerations should be taken to ensure proper operation of the CN5208.
(1) Input bypass capacitor, P-channel MOSFET, diode, inductor and output bypass capacitor are the power components, and must be placed on one side of PCB (Solder side). The traces of these power components should have sufficient width to handle the required output current.
(2) To minimize radiation, the diode, P-channel MOSFET, inductor, the input bypass capacitor and the output bypass capacitor traces should be kept as short as possible. The positive side of the input capacitor should be close to the source of the P-channel MOSFET; it provides the AC current to the pass transistor. The connection between the diode and P-channel MOSFET should also be kept as short as possible.
(3) The compensation capacitor connected at the COM pin should return to the ground pin of the IC. This will prevent ground noise from disrupting the loop stability.
(4) Output bypass capacitor ground and freewheeling diode (D1 in Figure 1) ground connections need to feed into same copper that connects to the input capacitor ground before flying back into system ground.
(5) Analog ground and power ground (or switching ground) should return to system ground separately.
(6) The ground pins also works as a heat sink, therefore use a generous amount of copper around the ground pins. This is especially important for high VCC and/or high gate capacitance applications.
(7) Place the sensitive small signal nodes such as CN5208's pin 4 (COM) and pin 5 (OUT) away from the switching nodes such as SW pin (Freewheeling diode and inductor are connected) and DRV pin.
(8) For applications with multiple switching power converters connected to the same input supply, ensure that the input bypass capacitance for the CN5208 is not shared with the other converters. AC input current from another converter will cause substantial input voltage ripple that may interfere with proper operation of the CN5208.

## CONSONANCE

## Package Information

## SOP8 PACKAGE OUTLINE DIMENSIONS



| Symbol | Dimensions In Millimeters |  | Dimensions In Inches |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Min | Max | Min | Max |
| A | 1.350 | 1.750 | 0.053 | 0.069 |
| A1 | 0.100 | 0.250 | 0.004 | 0.010 |
| A2 | 1.350 | 1.550 | 0.053 | 0.061 |
| b | 0.330 | 0.510 | 0.013 | 0.020 |
| c | 0.170 | 0.250 | 0.006 | 0.010 |
| D | 4.700 | 5.100 | 0.185 | 0.200 |
| E | 3.800 | 4.000 | 0.150 | 0.157 |
| E1 | 5.800 | 6.200 | 0.228 | 0.244 |
| e | $1.270($ BSC $)$ |  | $0.050($ BSC $)$ |  |
| L | 0.400 | 1.270 | 0.016 | 0.050 |
| $\theta$ | $0^{\circ}$ | $8^{\circ}$ | $0^{\circ}$ | $8^{\circ}$ |

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[^0]:    Stresses beyond those listed under 'Absolute Maximum Ratings' may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied. Exposure to Absolute Maximum Rating Conditions for extended periods may affect device reliability.

