## Description

The PAM2305D is a step-down current-mode, DC-DC converter. At heavy load, the constant frequency PWM control per forms excellent stability and transient response. To ensure the longest battery life in portable applications, the PAM2305D provides a power-saving PulseSkipping Modulation (PSM) mode to reduce quiescent current under light load operation to save power.

The PAM2305D supports a range of input voltages from 2.5 V to 5.5 V , allowing the use of a single $\mathrm{Li}+/ \mathrm{Li}$-polymer cell, multiple Alkaline/NiMH cell, USB, and other standard power sources. The output voltage is adjustable from 0.6 V to the input voltage. All versions employ internal power switch and synchronous rectifier to minimize external part count and realize high efficiency. During shutdown, the input is disconnected from the output and the shutdown current is less than $0.1 \mu \mathrm{~A}$. Other key features include under-voltage lockout to prevent deep battery discharge.

The PAM2305D is available in TSOT25, DFN2x2-6 pin and QFN3x316 pin packages.

## Features

- Efficiency up to $96 \%$
- Only $40 \mu \mathrm{~A}$ (Typ) Quiescent Current
- Output Current: Up to 1A
- Internal Synchronous Rectifier
- 1.5 MHz Switching Frequency
- Soft Start
- Under-Voltage Lockout
- Short Circuit Protection
- Thermal Shutdown
- 5-Pin Small TSOT25, DFN2x2-6 Pin and QFN3x3-16 Pin Packages
- Pb-Free Packages


## Pin Assignments



## Applications

- Cellular Phone
- Portable Electronics
- Wireless Devices
- Cordless Phone
- Computer Peripherals
- Battery Powered Widgets
- Electronic Scales
- Digital Frame

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## Typical Applications Circuit



$$
\mathrm{V}_{\mathrm{O}}=0.6 \times\left(1+\frac{\mathrm{K} 1}{\mathrm{R} 2}\right)
$$

## Pin Descriptions

| Pin <br> Name | Package Name |  |  |  |
| :---: | :---: | :---: | :---: | :--- |
|  | TSOT25 | DFN2x2-6L | QFN3x3-16L |  |
| VIN | 1 | 3 | $9,10,11,12$ | Chip main power supply pin. |
| GND | 2 | 5 | $1,2,3,5$ | Ground. |
| EN | 3 | 2 | 7 | Enable Control Input. Force this pin voltage above 1.5V, enables the chip, and <br> below 0.3V shuts down the device. |
| FB | 4 | 6 | 4 | Feedback voltage to internal error amplifier, the threshold voltage is 0.6V. |
| SW | 5 | 4 | $13,14,15$ | The drains of the internal main and synchronous power MOSFET. |
| NC | - | 1 | $6,8,16$ | No connection. |

## Functional Block Diagram



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## Absolute Maximum Ratings ( $@ \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified.)

These are stress ratings only and functional operation is not implied. Exposure to absolute maximum ratings for prolonged time periods may affect device reliability. All voltages are with respect to ground.

| Parameter | Rating | Unit |
| :--- | :---: | :---: |
| Input Voltage | -0.3 to +6.0 | V |
| EN, FB Pin Voltage | -0.3 to VIN | V |
| SW Pin Voltage | -0.3 to $\left(\mathrm{V}_{\mathrm{IN}}+0.3\right)$ | V |
| Junction Temperature | +150 | ${ }^{\circ} \mathrm{C}$ |
| Storage Temperature Range | -65 to +150 | $\left.{ }^{\circ} \mathrm{C}\right)$ |
| Soldering Temperature | $300,5 \mathrm{~s}$ | ${ }^{\circ} \mathrm{C}$ |

## Recommended Operating Conditions $\left(@ T_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$, unless otherwise ${ }^{\text {spechified. }}$ )

| Parameter | Rating |  |
| :--- | :---: | :---: |
| Supply Voltage | 2.5 to 5.5 | Unit |
| Operation Temperature Range | -40 to +85 | V |
| Junction Temperature Range | -40 to +125 |  |

## Thermal Information



Note: 1. The maximun output current for TSOT25 package is limited by internal power dissipation capacity as described in Application Information here inafter.

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Electrical Characteristics $\left(@ T_{A}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}, \mathrm{~V}_{\mathrm{O}}=1.8 \mathrm{~V}, \mathrm{C}_{\mathrm{IN}}=10 \mu \mathrm{~F}, \mathrm{C}_{\mathrm{OUT}}=10 \mu \mathrm{~F}, \mathrm{~L}=4.7 \mu \mathrm{H}\right.$, unless otherwise specified.)

| Parameter | Symbol | Test Conditions |  | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input Voltage Range | $\mathrm{V}_{\text {IN }}$ | - |  | 2.5 | - | 5.5 | V |
| Regulated Feedback Voltage | $V_{F B}$ | $1 \mathrm{lo}=100 \mathrm{~mA}$ |  | 0.588 | 0.6 | 0.612 | V |
| Reference Voltage Line Regulation | $\Delta \mathrm{V}_{\mathrm{FB}}$ | - |  | - | 0.3 | - | \%/V |
| Regulated Output Voltage Accuracy | $\mathrm{V}_{0}$ | $\mathrm{IO}_{0}=100 \mathrm{~mA}$ |  | -3 | - | +3 | \% |
| Peak Inductor Current | lPK | $\mathrm{V}_{\mathrm{IN}}=3 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}}=0.5 \mathrm{~V}$ or $\mathrm{V}_{\mathrm{O}}=90 \%$ |  | - | 1.5 | - | A |
| Output Voltage Line Regulation | LNR | $\mathrm{V}_{\mathrm{IN}}=2.5 \mathrm{~V}$ to $5 \mathrm{~V}, \mathrm{I}_{\mathrm{O}}=10 \mathrm{~mA}$ |  | - | 0.2 | 0.5 | \%/V |
| Output Voltage Load Regulation | LDR | $\mathrm{I}_{0}=1 \mathrm{~mA}$ to 800 mA |  | - | 1.5 | - | \% |
| Quiescent Current | IQ | No load |  | - | 40 | 70 | $\mu \mathrm{A}$ |
| Shutdown Current | ISD | $\mathrm{V}_{\text {EN }}=0 \mathrm{~V}$ |  |  | 0.1 | 1 | $\mu \mathrm{A}$ |
| Oscillator Frequency | fosc | $\mathrm{V}_{\mathrm{O}}=100 \%$ |  | 1.2 | 1.5 | 1.8 | MHz |
|  |  | $\mathrm{V}_{\mathrm{FB}}=0 \mathrm{~V}$ or $\mathrm{V}_{\mathrm{O}}=0 \mathrm{~V}$ |  | - | 500 | - | kHz |
| Drain-Source On-State Resistance | RDS(ON) | $\mathrm{IDS}=100 \mathrm{~mA}$ | P MOSFET | - | 0.3 | 0.45 | $\Omega$ |
|  |  |  | N MOSFET | - | 0.35 | 0.5 | $\Omega$ |
| SW Leakage Current | ILsw | - |  | - | $\pm 0.01$ | 1 | $\mu \mathrm{A}$ |
| EN Threshold High | $\mathrm{V}_{\mathrm{EH}}$ | - |  | 1.5 | - | - | V |
| EN Threshold Low | $\mathrm{V}_{\mathrm{EL}}$ | - |  |  | - | 0.3 | V |
| EN Leakage Current | $\mathrm{I}_{\mathrm{EN}}$ | - |  | - | $\pm 0.01$ | - | $\mu \mathrm{A}$ |
| Over Temperature Protection | OTP | - |  | - | +150 | - | ${ }^{\circ} \mathrm{C}$ |
| OTP Hysteresis | OTH | - |  | - | +30 | - | ${ }^{\circ} \mathrm{C}$ |

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Typical Performance Characteristics $\left(@ T_{A}=+25^{\circ} \mathrm{C}, \mathrm{C}_{1 \mathrm{~N}}=10 \mu \mathrm{~F}, \mathrm{C}_{\mathrm{O}}=10 \mu \mathrm{~F}, \mathrm{~L}=4.7 \mu \mathrm{H}\right.$, unless otherwise specified.)


Efficiency vs Output Current ( $\mathrm{Vo}=1.5 \mathrm{~V}$ )


Efficiency vs Input Voltage (Vo=1.2V)


Efficiency vs Input Voltage ( $V o=1.5 \mathrm{~V}$ )


Eifficiency vs Input Voltage ( $\mathrm{Vo}=1.8 \mathrm{~V}$ )


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Typical Performance Characteristics (continued) ( $@ T_{A}=+25^{\circ} \mathrm{C}, \mathrm{C}_{\mathrm{N}}=10 \mu \mathrm{~F}, \mathrm{C}_{\mathrm{O}}=10 \mu \mathrm{~F}, \mathrm{~L}=4.7 \mathrm{HH}$, unless otherwise specified.)


Efficiency vs Output Current ( $\mathrm{Vo}=3.3 \mathrm{~V}$ )


Output Oument(mA)
Quiescent Current vs Input Voltage


Efficiency vs Input Voltage ( $\mathrm{Vo}=2.5 \mathrm{~V}$ )


Efficiency vs Input Voltage $(\mathrm{Vo}=3.3 \mathrm{~V})$


Rdson vs Input Voltage


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Typical Performance Characteristics (continued) (@TA $=+25^{\circ} \mathrm{C}, \mathrm{C}_{\mathbb{N}}=10 \mu \mathrm{~F}, \mathrm{C}_{\mathrm{O}}=10 \mu \mathrm{~F}, \mathrm{~L}=4.7 \mathrm{HH}$, unless otherwise specified.)


Oscillator Frequency vs Supply Voltage


Supply Volage(V)

Load Transient
$10=0-1 \mathrm{~A}, \mathrm{~V}_{\mathrm{O}}=3.3 \mathrm{~V}, \mathrm{Vin}=5 \mathrm{~V}$



Oscillator Frequency vs Temperature


Load Transient
$\mathrm{Io}=0-1 \mathrm{~A}, \mathrm{Vo}=1.2 \mathrm{~V}$, Vin= $=5 \mathrm{~V}$


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## Application Information

The basic PAM2305D application circuit is shown in Page 2. External component selection is determined by the load requirement, selecting L first and then $\mathrm{C}_{\mathrm{IN}}$ and Cout.

## Inductor Selection

For most applications, the value of the inductor will fall in the range of $1 \mu \mathrm{H}$ to $4.7 \mu \mathrm{H}$. Its value is chosen based on the desired ripple current. Large value inductors lower ripple current and small value inductors result in higher ripple currents. Higher $\mathrm{V}_{\mathbb{N}}$ or $\mathrm{V}_{\text {OUt }}$ also increases the ripple current as shown in Equation 1. A reasonable starting point for setting ripple current is $\Delta I_{L}=400 \mathrm{~mA}(40 \%$ of 1 A$)$.

$$
\Delta \mathrm{I}_{\mathrm{L}}=\frac{1}{(\mathrm{f})(\mathrm{L})} \mathrm{V}_{\text {OUT }}\left(1-\frac{\mathrm{V}_{\text {OUT }}}{\mathrm{V}_{\mathrm{IN}}}\right)
$$

Equation (1)

The DC current rating of the inductor should be at least equal to the maximum load current plus half the ripple current to prevent core saturation. Thus, a 1.4 A rated inductor should be enough for most applications $(1 \mathrm{~A}+400 \mathrm{~mA})$. For better efficiency, choose a low DC-resistance inductor.

| $\mathrm{V}_{\mathrm{O}}$ | 1.2 V | 1.5 V | 1.8 V | 2.5 V | 3.3 V |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L | $2.2 \mu \mathrm{H}$ | $2.2 \mu \mathrm{H}$ | $2.2 \mu \mathrm{H}$ | $4.7 \mu \mathrm{H}$ | $4.7 \mu \mathrm{H}$ |

## $\mathrm{C}_{\text {IN }}$ and $\mathrm{C}_{\text {оut }}$ Selection

In continuous mode, the source current of the top MOSFET is a square wave of duty cycle $V_{\text {OUT }} / V_{\text {IN }}$. To prevent large voltage transients, a low ESR input capacitor sized for the maximum RMS current must be used. The maximum RMS capacitor current is given by:

$$
\mathrm{C}_{\text {IN }} \text { required } \mathrm{I}_{\mathrm{RMS}} \cong \operatorname{lOMAX} \frac{\left[\mathrm{~V}_{\text {OUT }}\left(\mathrm{V}_{\text {IN }}-\mathrm{V}_{\text {OUT }}\right)\right]^{1 / 2}}{\mathrm{~V}_{\text {IN }}}
$$

This formula has a maximum at $\mathrm{V}_{\mathbb{I N}}=2 \mathrm{~V}_{\text {OUT }}$, where $\mathrm{I}_{\mathrm{RMS}}=\mathrm{I}_{\text {Out }} / 2$. This simple worst-case condition is commonly used for design because even significant deviations do not offer much relief. Note that the capacitor manufacturer's ripple current ratings are often based on 2000 hours of life. This makes it advisable to further derate the capacitor, or choose a capacitor rated at a higher temperature than required. Consult the manufacturer if there is any question.

The selection of Cout is driven by the required effective series resistance (ESR).
Typically, once the ESR requirement for Cout has been met, the RMS current rating generally far exceeds the IRIPPLE (P-P) requirement. The output ripple $\Delta \mathrm{V}_{\text {OUT }}$ is determined by:

$$
\Delta \mathrm{V}_{\mathrm{OUT}} \cong \Delta \mathrm{iL}\left(\mathrm{ESR}+\frac{1}{8 \mathrm{f} \mathrm{COUT}}\right)
$$

Where $\mathrm{f}=$ operating frequency, Cout $=$ output capacitance and $\Delta L_{L}=$ ripple current in the inductor. For a fixed output voltage, the output ripple is highest at maximum input voltage since $\Delta L L$ increases with input voltage.

## Using Ceramic Input and Output Capacitors

Higher values, lower cost ceramic capacitors are now becoming available in smaller case sizes. Their high ripple current, high voltage rating and low ESR make them ideal for switching regulator applications. Using ceramic capacitors can achieve very low output ripple and small circuit size.

When choosing the input and output ceramic capacitors, choose the X5R or X7R dielectric formulations. These dielectrics have the best temperature and voltage characteristics of all the ceramics for a given value and size.

## Thermal Consideration

Thermal protection limits power dissipation in the PAM2305D. When the junction temperature exceeds $150^{\circ} \mathrm{C}$, the OTP (Over Temperature Protection) starts the thermal shutdown and turns the pass transistor off. The pass transistor resumes operation after the junction temperature drops below $+120^{\circ} \mathrm{C}$.

For continuous operation, the junction temperature should be maintained below $+125^{\circ} \mathrm{C}$.
The power dissipation is defined as:
$\mathrm{P}_{\mathrm{D}}=\mathrm{I}^{2} \frac{\mathrm{~V}_{\mathrm{O}} \mathrm{R}_{\mathrm{DS}(\mathrm{ON}) \mathrm{H}^{+}\left(\mathrm{V}_{\mathrm{IN}}-\mathrm{V}_{\mathrm{O}}\right) R_{\mathrm{DS}(\mathrm{ON}) \mathrm{L}}}^{\mathrm{V}_{\mathrm{IN}}}+\left(\mathrm{t}_{\mathrm{SW}} \mathrm{Fslo}_{\mathrm{S}}+\mathrm{l}_{\mathrm{Q}}\right) \mathrm{V}_{\mathrm{IN}}}{}$
$I_{Q}$ is the step-down converter quiescent current. The term tsw is used to estimate the full load step-down converter switching losses.

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## Application Information (continued)

For the condition where the step-down converter is in dropout at $100 \%$ duty cycle, the total device dissipation reduces to:

$$
P_{D}=I_{O}^{2} R_{D S}(O N) H+I_{Q} V_{I N}
$$

Since $R_{\mathrm{Ds}(\mathrm{ON})}$, quiescent current, and switching losses all vary with input voltage, the total losses should be investigated over the complete input voltage range. The maximum power dissipation depends on the thermal resistance of IC package, PCB layout, the rate of surrounding airflow and temperature difference between junction and ambient. The maximum power dissipation can be calculated by the following formula:

$$
P_{D}=\frac{T_{J(M A X)}-T_{A}}{\theta_{J A}}
$$

Where $T_{J(M A X)}$ is the maximum allowable junction temperature $+125^{\circ} \mathrm{C} . \mathrm{T}_{\mathrm{A}}$ is the ambient temperature and $\theta_{\mathrm{JA}}$ is the thermal resistance from the junction to the ambient. Based on the standard JEDEC for a two layers thermal test board, the thermal resistance OJA of TSOT25 package is $250^{\circ} \mathrm{C} / \mathrm{W}$, DFN2X2 $102^{\circ} \mathrm{C} / \mathrm{W}$ and QFN3X3 $68^{\circ} \mathrm{C} / \mathrm{W}$, respectively. The maximum power dissipation at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ can be calculated by following formula:

SOT-25 package:

$$
\mathrm{P}=\left(125^{\circ} \mathrm{C}-25^{\circ} \mathrm{C}\right) / 250^{\circ} \mathrm{C} / \mathrm{W}=0.4 \mathrm{~W}
$$

DFN2*2 package:

$$
\mathrm{P}=\left(125^{\circ} \mathrm{C}-25^{\circ} \mathrm{C}\right) / 102^{\circ} \mathrm{C} / \mathrm{W}=0.984 \mathrm{~W}
$$

QFN3*3 package:

$$
\mathrm{P}=\left(125^{\circ} \mathrm{C}-25^{\circ} \mathrm{C}\right) / 68^{\circ} \mathrm{C} / \mathrm{W}=1.47 \mathrm{~W}
$$

## Setting the Output Voltage

The internal reference is 0.6 V (Typical). The output voltage is calculated as below:

$$
V_{O}=0.6 \times\left(1+\frac{\mathrm{R} 1}{\mathrm{R} 2}\right)
$$

The output voltage is given by Table 1.
Table 1: Resistor selection for output voltage setting.

| $\mathbf{V}_{\mathbf{o}}$ | $\mathbf{R 1}$ | $\mathbf{R 2}$ |
| :---: | :---: | :---: |
| 1.2 V | 100 k | 100 k |
| 1.5 V | 150 k | 100 k |
| 1.8 V | 200 k | 100 k |
| 2.5 V | 380 k | 120 k |
| 3.3 V | 540 k | 120 k |

## 100\% Duty Cycle Operation

As the input voltage approaches the output voltage, the converter turns the P-Channel transistor continuously on. In this mode the output voltage is equal to the input voltage minus the voltage drop across the P -Channel transistor:

$$
V_{\text {OUT }}=V_{\text {IN }}-\operatorname{ILCOAD}\left(R_{D S(O N)}+R_{L}\right)
$$

where $\mathrm{R}_{\mathrm{DS}(\mathrm{ON})}=\mathrm{P}$-Channel switch ON resistance, $\mathrm{I}_{\mathrm{LOAD}}=$ Output current, $\mathrm{R}_{\mathrm{L}}=$ Inductor DC resistance.

## UVLO and Soft-Start

The reference and the circuit remain reset until the $\mathrm{V}_{\mathrm{IN}}$ crosses its UVLO threshold.

The PAM2305D has an internal soft-start circuit that limits the in-rush current during start-up. This prevents possible voltage drops of the input voltage and eliminates the output voltage overshoot. The soft-start acts as a digital circuit to increase the switch current in several steps to the P-Channel current limit ( 1500 mA ).

## Short Circuit Protection

The switch peak current is limited cycle-by-cycle to a typical value of 1500 mA . In the event of an output voltage short circuit, the device operates with a frequency of 400 kHz and minimum duty cycle, therefore the average input current is typically 200 mA .

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## Application Information (continued)

## Thermal Shutdown

When the die temperature exceeds $+150^{\circ} \mathrm{C}$, a reset occurs and the reset remains until the temperature decrease to $+120^{\circ} \mathrm{C}$, at which time the circuit can be restarted.

## PCB Layout Check List

When laying out the printed circuit board, the following checklist should be used to ensure proper operation of the PAM2305D. These items are also illustrated graphically in Figure 1. Check the following in your layout:

1. The power traces, consisting of the GND trace, the SW trace and the $\mathrm{V}_{\mathrm{IN}}$ trace should be kept short, direct and wide.
2. Does the $V_{\text {FB }}$ pin connect directly to the feedback resistors? The resistive divider R1/R2 must be connected between the ( + ) plate of Cout and ground.
3. Does the $(+)$ plate of $\mathrm{C}_{\mathbb{I N}}$ connect to $\mathrm{V}_{\mathbb{I N}}$ as closely as possible? This capacitor provides the AC current to the internal power MOSFETs.
4. Keep the switching node, SW, away from the sensitive $\mathrm{V}_{\mathrm{FB}}$ node.
5. Keep the (-) plates of $\mathrm{C}_{\mathrm{IN}}$ and Cout as close as possible.


Figure 1. PAM2305D Suggested Layout

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| Part Number | Output Voltage | Part Marking | Package Type | Standard Package |
| :---: | :---: | :---: | :---: | :---: |
| PAM2305DABADJ | ADJ | BKAYW | TSOT25 | 3000 Units/Tape\&Reel |
| PAM2305DJEADJ | ADJ | P2305D | QFN3x3 | 3000 Units/Tape\&Reel |
| PAM2305DGFADJ | ADJ | BKAYW | DFN2x2-6 | 3000 Units/Tape\&Reel |




| REF. | Millimeter |  |  |
| :---: | :---: | :---: | :---: |
|  | Min |  |  |
| A | Max |  |  |
| A1 | 0 | 0.10 MAX |  |
| A2 | 0.70 | 1 |  |
| c | 0.12 REF. |  |  |
| D | 2.70 | 3.10 |  |
| E | 2.60 | 3.00 |  |
| E1 | 1.40 | 1.80 |  |
| L | 0.45 REF. |  |  |
| L1 | 0.60 REF. |  |  |
| $\theta$ | $0^{\circ}$ | $10^{\circ}$ |  |
| $b$ | 0.30 | 0.50 |  |
| e | 0.95 REF. |  |  |
| e1 | 1.90 REF. |  |  |

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Package Outline Dimensions (continued) (All dimensions in mm.)

## DFN 2x2



PIN 1 DOT BY MARKING

TOP VIEW


PIN HI IDENTIFICATION CHAMFER

BOTTOM VIEW


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## Package Outline Dimensions (continued) (All dimensions in mm.)

## $3 \times 3$ mm QFN 16



Notes: $\quad$ 2. Controlling dimensions are in millimeters (angles in degress). 3. Coplanarity applies to the exposed pad as well as the terminals. 4. DAP is $1.90 \times 1.90 \mathrm{~mm}$.

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