INCH-POUND MIL-M-38510/113B 21 June 2005 SUPERSEDING MIL-M-38510/113A 10 February 2005

#### MILITARY SPECIFICATION

#### MICROCIRCUITS, LINEAR, 8 BIT, DIGITAL-TO-ANALOG CONVERTERS, MONOLITHIC SILICON

This specification is approved for use by all Departments and Agencies of the Department of Defense.

## Reactivated for new design as of 10 February 2005. May be used for either new or existing design acquisition.

The requirements for acquiring the product herein shall consist of this specification sheet and MIL-PRF-38535

1. SCOPE

1.1 <u>Scope.</u> This specification covers the detail requirements for monolithic silicon, 8 bit, digital-to-analog converters. Two product assurance classes and a choice of case outlines and lead finishes are provided for each type and are reflected in the complete part number. For this product, the requirements of MIL-M-38510 have been superseded by MIL-PRF-38535, (see 6.4)

1.2 Part or Identifying Number (PIN). The PIN is in accordance with MIL-PRF-38535, and as specified herein.

1.2.1 <u>Device types.</u> The device types are as follows:

| Device type | <u>Circuit</u>                        |  |  |  |  |  |  |  |
|-------------|---------------------------------------|--|--|--|--|--|--|--|
| 01          | D/A Converter, 8 bit, 0.19% linearity |  |  |  |  |  |  |  |
| 02          | D/A Converter, 8 bit, 0.10% linearity |  |  |  |  |  |  |  |

1.2.2 <u>Device class</u>. The device class is the product assurance level as defined in MIL-PRF-38535.

1.2.3 <u>Case outline</u>. The case outlines are as designated in MIL-STD-1835 and as follows:

| Outline letter | Descriptive designator | <u>Terminals</u> | Package style |
|----------------|------------------------|------------------|---------------|
| E              | GDIP1-T16 or CDIP2-T16 | 16               | Dual-in-line  |

1.3 Absolute maximum ratings.

| Supply voltage [+V <sub>cc</sub> – (-V <sub>cc</sub> )]                              | 36 Vdc                               |
|--------------------------------------------------------------------------------------|--------------------------------------|
| Voltage, digital input to negative supply [V <sub>logic</sub> – (-V <sub>cc</sub> )] | 0 to 36 Vdc                          |
| Voltage, logic control (V <sub>LC</sub> )                                            | -V <sub>cc</sub> to +V <sub>cc</sub> |
| Reference voltage input (V14, V15)                                                   | -Vcc to +Vcc                         |
| Reference input current (I <sub>14</sub> )                                           | 5.0 mA                               |
| Reference input differential voltage [(V14 – V15)]                                   | ±18 Vdc                              |
| Lead temperature (soldering, 60 sec)                                                 | +300°C.                              |
| Junction temperature (T <sub>J</sub> )                                               | +175°C                               |
| Storage temperature                                                                  | -65°C to +150°C                      |

Comments, suggestions, or questions on this document should be addressed to: Commander, Defense Supply Center Columbus, ATTN: DSCC-VAS, 3990 East Broad St., Columbus, OH 43218-3990, or emailed to <u>mailto:linear@dscc.dla.mil</u>. Since contact information can change, you may want to verify the currency of this address information using the ASSIST Online database at http://assist.daps.dla.mil.

#### 1.4 Recommended operating conditions.

| Supply voltage range      | ±5 Vdc to ±15 Vdc <u>1</u> / <u>2</u> / |
|---------------------------|-----------------------------------------|
| Ambient temperature range | -55°C to +125°C                         |

#### 1.5 Power and thermal characteristics.

| Case outline | <u>outline Package</u> Maximum allowa<br>power dissipatio |                                 | $\underline{\text{maximum}}\theta_{\text{JC}}$ | $\underline{\text{maximum}}  \theta_{\text{JA}}$ |
|--------------|-----------------------------------------------------------|---------------------------------|------------------------------------------------|--------------------------------------------------|
| E            | Dual-in-line                                              | 400 mW @ T <sub>A</sub> = 125°C | 35°C/W                                         | 120°C/W                                          |

#### 2. APPLICABLE DOCUMENTS

2.1 <u>General</u>. The documents listed in this section are specified in sections 3, 4, or 5 of this specification. This section does not include documents cited in other sections of this specification or recommended for additional information or as examples. While every effort has been made to ensure the completeness of this list, document users are cautioned that they must meet all specified requirements of documents cited in sections 3, 4, or 5 of this specification, whether or not they are listed.

#### 2.2 Government documents.

2.2.1 <u>Specifications, standards, and handbooks</u>. The following specifications and standards form a part of this specification to the extent specified herein. Unless otherwise specified, the issues of these documents are those listed in the solicitation or contract.

#### DEPARTMENT OF DEFENSE SPECIFICATIONS

MIL-PRF-38535 - Integrated Circuits, Manufacturing, General Specification for.

#### DEPARTMENT OF DEFENSE STANDARDS

MIL-STD-883 - Test Method Standard for Microelectronics.

MIL-STD-1835 - Interface Standard Electronic Component Case Outlines.

(Copies of these documents are available online at <u>http://assist.daps.dla.mil/quicksearch/</u> or <u>http://assist.daps.dla.mil</u> or from the Standardization Document Order Desk, 700 Robbins Avenue, Building 4D, Philadelphia, PA 19111-5094.)

2.2 <u>Order of precedence</u>. In the event of a conflict between the text of this specification and the references cited herein the text of this document shall takes precedence. Nothing in this document, however, supersedes applicable laws and regulations unless a specific exemption has been obtained.

#### 3. REQUIREMENTS

3.1 <u>Qualification</u>. Microcircuits furnished under this specification shall be products that are manufactured by a manufacturer authorized by the qualifying activity for listing on the applicable qualified manufacturers list before contract award (see 4.3 and 6.3).

3.2 <u>Item requirements</u>. The individual item requirements shall be in accordance with MIL-PRF-38535 and as specified herein or as modified in the device manufacturer's Quality Management (QM) plan. The modification in the QM plan shall not affect the form, fit, or function as described herein.

3.3 <u>Design, construction, and physical dimensions</u>. The design, construction, and physical dimensions shall be as specified in MIL-PRF-38535 and herein.

- $\underline{1}$  A slight degradation in linearity can occur when the supply is near the ±5 V end of the recommended operating range.
- $\underline{2}$ / Sequence of power supply turn-on must be -V<sub>cc</sub> prior to +V<sub>cc</sub> unless the positive supply has current limiting resistance of 100  $\Omega \pm 10\%$ . If a current limiting resistance is used, a slight degradation in linearity will occur.

3.3.1 <u>Terminal connections and functional block diagram.</u> The terminal connections and functional block diagram shall be as specified on figure 1.

3.3.2 <u>Schematic circuits</u>. The schematic circuits shall be maintained by the manufacturer and made available to the qualifying activity and the preparing activity upon request.

3.3.3 Case outlines. The case outlines shall be as specified in 1.2.3.

3.4 Lead material and finish. The lead material and finish shall be in accordance with MIL-PRF-38535 (see 6.6).

3.5 <u>Electrical performance characteristics</u>. The electrical performance characteristics are as specified in table I, and apply over the full recommended ambient operating temperature range, unless otherwise specified.

3.6 <u>Electrical test requirements</u>. Electrical test requirements for each device class shall be the subgroups specified in table II. The electrical tests for each subgroup are described in table III.

3.7 Marking. Marking shall be in accordance with MIL-PRF-38535.

3.8 <u>Microcircuit group assignment</u>. The devices covered by this specification shall be in microcircuit group number 56 (see MIL-PRF-38535, appendix A).

4. VERIFICATION.

4.1 <u>Sampling and inspection</u>. Sampling and inspection procedures shall be in accordance with MIL-PRF-38535 or as modified in the device manufacturer's Quality Management (QM) plan. The modification in the QM plan shall not effect the form, fit, or function as function as described herein.

4.2 <u>Screening</u>. Screening shall be in accordance with MIL-PRF-38535, and shall be conducted on all devices prior to qualification and quality conformance inspection. The following additional criteria shall apply:

a. The burn-in test duration, test condition, and test temperature, or approved alternatives shall be as specified in the device manufacturer's QM plan in accordance with MIL-PRF-38535. The burn-in test circuit shall be maintained under document control by the device manufacturer's Technology Review Board (TRB) in accordance with MIL-PRF-38535 and shall be made available to the acquiring or preparing activity upon request. The test circuit shall specify the inputs, outputs, biases, and power dissipation, as applicable, in accordance with the intent specified in test method 1015 of MIL-STD-883.

NOTE: If accelerated high-temperature test conditions are used, the device manufacturer shall ensure that at least 85 percent of the applied voltage is dropped across the device at temperature. The device is not considered functional under accelerated test conditions.

- b. Interim and final electrical test parameters shall be as specified in table II, except interim electrical parameters test prior to burn-in is optional at the discretion of the manufacturer.
- c. Additional screening for space level product shall be as specified in MIL-PRF-38535.

4.3 <u>Qualification inspection</u>. Qualification inspection shall be in accordance with MIL-PRF-38535.

4.4 <u>Technology Conformance inspection (TCI)</u>. Technology conformance inspection shall be in accordance with MIL-PRF-38535 and herein for groups A, B, C, and D inspections (see 4.4.1 through 4.4.4).

|                                      |                           |                                                                              |        | Lii   | mits  |       |
|--------------------------------------|---------------------------|------------------------------------------------------------------------------|--------|-------|-------|-------|
| Characteristics                      | Symbol                    | Conditions <u>1</u> /                                                        | Device | Min   | Max   | Units |
|                                      |                           | $-55^{\circ}C \leq T_A \leq +125^{\circ}C$                                   | type   |       |       |       |
|                                      |                           | (table III and figures 2, 3, and 4                                           |        |       |       |       |
|                                      |                           | unless otherwise indicated)                                                  |        |       |       |       |
| Supply current from +V <sub>cc</sub> | Icc+                      | All input bits high                                                          | All    | 0.4   | 3.8   | mA    |
| Supply current from<br>-Vcc          | Icc-                      | All input bits high                                                          | All    | -7.8  | -0.8  | mA    |
| Full scale current                   | IFS                       | All input bits high,                                                         | 01     | 1.94  | 2.04  | mA    |
|                                      |                           | Measure Io                                                                   | 02     | 1.984 | 2.000 |       |
|                                      | IFS                       | All input bits low,                                                          | 01     | 1.94  | 2.04  | mA    |
|                                      |                           | Measure lo                                                                   | 02     | 1.984 | 2.000 |       |
| Zero scale current                   | Izs                       | All input bits low, measure Io                                               | 01     | -2.0  | 2.0   | μΑ    |
|                                      |                           |                                                                              | 02     | -1.0  | 1.0   |       |
|                                      | Izs                       | All input bits high, measure lo                                              | 01     | -2.0  | 2.0   | μA    |
|                                      | 120                       |                                                                              | 02     | -1.0  | 1.0   |       |
| Power supply sensitivity             | Pssl <sub>FS</sub> +1     | All input bits high, measure Io                                              | All    | -4.0  | 4.0   | μΑ    |
| from +Vcc                            |                           | +V <sub>cc</sub> = 4.5 V to +5.5 V, -V <sub>cc</sub> = -18 V                 |        |       |       |       |
|                                      | Psslfs+1                  | All input bits low, measure $\overline{10}$                                  | All    | -4.0  | 4.0   | μA    |
|                                      |                           | +Vcc = 4.5 V to +5.5 VVcc = -18 V                                            |        |       |       |       |
| Power supply sensitivity             | Psslfs+2                  | All input bits high, measure $I_0$                                           | All    | -8.0  | 8.0   | uА    |
| from +V <sub>cc</sub>                |                           | +Vcc = 12 V to 18 V, -Vcc = -18 V                                            |        |       |       |       |
|                                      | $\overline{Pssles} \pm 2$ | All input hits low measure lo                                                | All    | -8.0  | 8.0   | μA    |
|                                      | 1 001 0 1 2               | $+V_{cc} = 12 \text{ V to } 18 \text{ V} -V_{cc} = -18 \text{ V}$            |        |       |       |       |
| Power supply sensitivity             | Peelre-1                  | All input bits high measure lo                                               | All    | -8.0  | 8.0   | ıιΔ   |
| from -V <sub>cc</sub>                | 1 33173 1                 | $+V_{cc} = 18 \text{ V}, -V_{cc} = -12 \text{ V} \text{ to } -18 \text{ V}$  | 7.01   | 0.0   | 0.0   | μΛ    |
|                                      |                           | All input hits low measure lo                                                | All    | -8.0  | 8.0   | μA    |
|                                      | 1 3311 3 - 1              | $\pm$ V = = 18 V = V = = -12 V to -18 V                                      |        |       |       |       |
| Power supply sensitivity             | Peoleo-2                  | All input bits high measure lo                                               | ۵۱     | -2.0  | 2.0   |       |
| from -V <sub>cc</sub>                | 1 22122                   | $+V_{cc} = 18 \text{ V} -V_{cc} = -4.5 \text{ V} \text{ to } -5.5 \text{ V}$ |        | -2.0  | 2.0   | μΛ    |
|                                      |                           | $I_{REF} = 1 \text{ mA}$                                                     |        |       |       |       |
|                                      | Pssles - 2                | All input hits low measure 10                                                | All    | -2.0  | 2.0   | μA    |
|                                      | 100110 2                  | $+V_{22} = 18 V_{-1}V_{22} = -4.5 V_{10} = 5.5 V_{-10}$                      |        |       |       |       |
| Output current range                 | IreR4                     | All input bits high measure lo                                               | All    | 21    |       | mA    |
| output ouriont range                 | 15111                     | $-V_{CC} = -10 \text{ V}$ . VRFF = 15 V                                      | 7.41   | 2.1   |       | 110 ( |
|                                      |                           |                                                                              | All    | 2.1   |       | mA    |
|                                      | IFSR1                     |                                                                              |        |       |       |       |
|                                      |                           | $-V_{CC} = -10$ V, $V_{REF} = 15$ V                                          | A 11   | 4.0   |       |       |
| Output current range                 | IFSK2                     | All input bits high, measure $I_0$                                           | All    | 4.2   |       | mA    |
|                                      |                           | $-v_{CC} = -12 v$ , $v_{REF} = 23 v$                                         | ΔII    | 10    |       | m۸    |
|                                      | IFSR2                     | All input bits low, measure lo                                               |        | 4.2   |       | IIIA  |
|                                      |                           | -V <sub>CC</sub> = -12 V, V <sub>REF</sub> = 25 V                            |        |       |       |       |

## TABLE I. Electrical performance characteristics.

|                                   |                          |                                                                   |                                                   |        | Limi  |      |       |
|-----------------------------------|--------------------------|-------------------------------------------------------------------|---------------------------------------------------|--------|-------|------|-------|
| Characteristics                   | Symbol                   | Conditi                                                           | ons <u>1</u> /                                    | Device | Min   | Max  | Units |
|                                   |                          | $-55^{\circ}C \le T_{A}$                                          | .≤+125°C                                          | type   |       |      |       |
|                                   |                          | (table III and fig                                                | ures 2, 3, and 4                                  |        |       |      |       |
|                                   |                          | unless otherw                                                     | vise indicated)                                   |        |       |      |       |
| Reference bias current            | I <sub>REF</sub> -       | All input bits low                                                |                                                   | All    | -3.0  | 0    | μΑ    |
| High level input current          | lін                      | All input bits V <sub>IN</sub> = 18<br>measured separatel         | 8 V, each input<br>y                              | All    | -0.05 | 10.0 | μΑ    |
| Low level input current           | lı∟                      | All input bits V <sub>IN</sub> = -1<br>measured separatel         | 0 V, each input<br>y                              | All    | -10.0 |      | μA    |
| Full scale current at             | I <sub>FS</sub> +        | All input bits high, m                                            | easure l <sub>o</sub> ,                           | 01     | 1.90  | 2.08 | mA    |
| +18 V compliance                  |                          | V <sub>IO</sub> = 18 V                                            |                                                   | 02     | 1.94  | 2.04 |       |
|                                   | IFS +                    | All input bits low, me                                            | easure lo,                                        | 01     | 1.90  | 2.08 | mA    |
|                                   |                          | VIO = 18 V                                                        |                                                   | 02     | 1.94  | 2.04 |       |
| Full scale current at             | I <sub>FS</sub> -        | All input bits high, m                                            | easure l <sub>o</sub> ,                           | 01     | 1.90  | 2.08 | mA    |
| -10 V compliance                  |                          | V <sub>IO</sub> = -10 V                                           |                                                   | 02     | 1.94  | 2.04 |       |
|                                   | IFS -                    | All input bits low, me                                            | easure lo,                                        | 01     | 1.90  | 2.08 | mA    |
|                                   |                          | VIO = -10 V                                                       |                                                   | 02     | 1.94  | 2.04 |       |
| Change in full scale              | $\Delta I_{FSC}$         | All input bits high,                                              | $25^\circ C \leq T_{\textbf{A}} \leq 125^\circ C$ | All    | -4.0  | 4.0  | μΑ    |
| current due to voltage compliance |                          | measure I <sub>o</sub> ,<br>V <sub>IO</sub> = 18 V to -10 V       | T <sub>A</sub> = -55°C                            |        | -8.0  | 8.0  |       |
|                                   | $\Delta \overline{IFSC}$ | All input bits low,                                               | $25^\circ C \leq T_{\textbf{A}} \leq 125^\circ C$ | All    | -4.0  | 4.0  | μΑ    |
|                                   |                          | measure lo,                                                       | T <sub>A</sub> = -55°C                            |        | -8.0  | 8.0  |       |
|                                   |                          | $\overline{\text{VIO}}$ = 18 V to -10 V                           |                                                   |        |       |      |       |
| Positive bit errors               | $\Sigma NL +$            | . ΣPos                                                            | itive bit errors                                  | 01     | 0     | 0.19 | %     |
|                                   |                          | Measure I <sub>o</sub> ,                                          | IFS                                               | 02     | 0     | 0.10 |       |
|                                   | $\overline{\Sigma NI} +$ | $-(\Sigma Pos$                                                    | sitive bit errors                                 | 01     | 0     | 0.19 | %     |
|                                   |                          | Measure Io, $\left(\frac{2100}{100000000000000000000000000000000$ | IFS                                               | 02     | 0     | 0.10 |       |
| Negative bit errors               | $\Sigma NL -$            | Manager (ΣNeg                                                     | ative bit errors )                                | 01     | -0.19 | 0    | %     |
|                                   |                          |                                                                   | IFS                                               | 02     | -0.10 | 0    |       |
|                                   | $\overline{\Sigma NL} =$ | $-(\Sigma Ne)$                                                    | gative bit errors                                 | 01     | -0.19 | 0    | %     |
|                                   | 2                        | Measure IO, $\left(\frac{2.10}{10}\right)$                        | IFS                                               | 02     | -0.10 | 0    |       |

| TABLE I. Electr | ical performance | characteristics - | - Continued. |
|-----------------|------------------|-------------------|--------------|
|-----------------|------------------|-------------------|--------------|

|                                              |                                   |                                                                                                                                                                |                | Lim   |      |        |  |  |  |  |
|----------------------------------------------|-----------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------|-------|------|--------|--|--|--|--|
| Characteristics                              | Symbol                            | $\label{eq:conditions} \frac{1}{2} -55^\circ C \leq T_A \leq +125^\circ C \\ \mbox{(table III and figures 2, 3, and 4 } \\ \mbox{unless otherwise indicated)}$ | Device<br>type | Min   | Мах  | Units  |  |  |  |  |
| Positive and negative bit                    | $\Delta \Sigma NL$                | Measure I <sub>0</sub> , $ \Sigma NL +  -  \Sigma NL - $                                                                                                       | 01             | -0.05 | 0.05 | %      |  |  |  |  |
| error difference                             |                                   |                                                                                                                                                                | 02             | -0.03 | 0.03 |        |  |  |  |  |
|                                              | $\Lambda \overline{\Sigma NL}$    | Measure $\overline{IO}$ $\Sigma\overline{NI} + -\Sigma\overline{NI} -$                                                                                         | 01             | -0.05 | 0.05 | %      |  |  |  |  |
|                                              |                                   |                                                                                                                                                                | 02             | -0.03 | 0.03 |        |  |  |  |  |
| Positive relative accuracy                   | NL+                               | Measure I <sub>o</sub> , $ \Sigma NL +  +  \Delta \Sigma NL $                                                                                                  | 01             | 0     | 0.19 | %      |  |  |  |  |
|                                              |                                   |                                                                                                                                                                | 02             | 0     | 0.10 |        |  |  |  |  |
|                                              | $\overline{NL}$ +                 | Measure $\overline{IO}$ $\Sigma \overline{NI} + + \Delta \Sigma \overline{NI}$                                                                                 | 01             | 0     | 0.19 | %      |  |  |  |  |
|                                              |                                   |                                                                                                                                                                | 02             | 0     | 0.10 |        |  |  |  |  |
| Negative relative                            | NL-                               | Measure I <sub>0</sub> , $ \Sigma NL -   +  \Delta \Sigma NL $                                                                                                 | 01             | 0     | 0.19 | %      |  |  |  |  |
| accuracy                                     |                                   |                                                                                                                                                                | 02             | 0     | 0.10 |        |  |  |  |  |
|                                              | NL –                              | Measure $\overline{IO}$ $\Sigma \overline{NI} = \pm \Lambda \Sigma \overline{NI}$                                                                              | 01             | 0     | 0.19 | %      |  |  |  |  |
|                                              |                                   |                                                                                                                                                                | 02             | 0     | 0.10 |        |  |  |  |  |
| Monotonicity                                 | Δ(i)                              | Measure I <sub>0</sub> , $(I_{ON}-I_{ON-1}) \ge 0$ at each major carry point                                                                                   | All            | 0     | 16.0 | μΑ     |  |  |  |  |
|                                              | $\Delta(\overline{i})$            | Measure $\overline{IO}$ , $(\overline{ION} - \overline{ION - 1}) \ge 0$ at each major carry point                                                              | All            | 0     | 16.0 | μΑ     |  |  |  |  |
| Output symmetry                              | Δlfs                              | IFS – IFS                                                                                                                                                      | 01             | -8.0  | 8.0  | μΑ     |  |  |  |  |
|                                              |                                   |                                                                                                                                                                | 02             | -4.0  | 4.0  |        |  |  |  |  |
| Full scale current temperature coefficient   | T <sub>C</sub> (I <sub>FS</sub> ) | All input bits high, measure Io                                                                                                                                | All            | -50.0 | 50.0 | ppm/°C |  |  |  |  |
|                                              | Tc(IFS)                           | All input bits low, measure lo                                                                                                                                 | All            | -50.0 | 50.0 | ppm/°C |  |  |  |  |
| Propagation delay time,<br>high-to-low level | t <sub>PHL</sub>                  | Figure 3, measure Vo                                                                                                                                           | All            | 6.0   | 60.0 | ns     |  |  |  |  |
| Propagation delay time,<br>low-to-high level | t <sub>PLH</sub>                  | Figure 3, measure Vo                                                                                                                                           | All            | 6.0   | 60.0 | ns     |  |  |  |  |
| Reference amplifier input slew rate          | dl <sub>o</sub> /dt               | Figure 4, measure $V_0$ ,<br>T <sub>A</sub> = 25°C                                                                                                             | All            | 1.5   |      | mA/μs  |  |  |  |  |
| Settling time high-to-low                    | t <sub>sн∟</sub>                  | Figure 3, output within 1/2 LSB of final value of $I_0$ , $T_A = 25^{\circ}C$                                                                                  | All            | 10    | 135  | ns     |  |  |  |  |
| Settling time low-to-high                    | t <sub>sLH</sub>                  | Figure 3, output within 1/2 LSB of final value of $I_0$ , $T_A = 25^{\circ}C$                                                                                  | All            | 10    | 135  | ns     |  |  |  |  |

| TABLE I. | <b>Electrical</b> | performance | characteristics - | - Continued. |
|----------|-------------------|-------------|-------------------|--------------|
|          |                   |             |                   |              |

|                                         | Subgroups      | (see table III) |
|-----------------------------------------|----------------|-----------------|
| MIL-PRF-38535                           | Class S        | Class B         |
| test requirements                       | devices        | devices         |
|                                         |                |                 |
| Interim electrical parameters           | 1              | 1               |
|                                         |                |                 |
| Final electrical test parameters        | 1*, 2, 3       | 1*, 2, 3        |
|                                         |                |                 |
| Group A test requirements               | 1, 2, 3,       | 1, 2, 3,        |
|                                         | 9, 10, 11, 12  | 9, 10, 11, 12   |
| Group B electrical test parameters when | 1, 2, 3 and    | N/A             |
| using the method 5005 QCI option        | table IV delta |                 |
|                                         | limits         |                 |
| Group C end-point electrical            | 1, 2, 3 and    | 1 and table     |
| parameters                              | table IV delta | IV delta        |
|                                         | limits         | limits          |
| Group D end-point electrical            | 1, 2, 3        | 1               |
| parameters                              |                |                 |

## TABLE II. Electrical test requirements.

\*PDA applies to subgroup 1.



Terminal connections.



Functional block diagram.

Figure 1. Terminal connections and functional block diagram.



## NOTES:

- 1/ The reference D/A converter selected should have a resolution of 8 bits or more, and a linearity of 0.015% or better.
- $\underline{2}$ / The voltage reference should have an accuracy of  $\pm 0.02\%$  or better.
- $\underline{3}$ / All relays are shown in their unexcited state.

FIGURE 2. Test circuit for static tests.



NOTES:

- 1. For turn-ON,  $V_L = 2.7 \text{ V}$ ; for turn-OFF,  $V_L = 0.7 \text{ V}$ .
- 2. Minimize capacitance at this node, by using short runs and adequate spacing between runs.
- 3. Diodes must be Schottky type (MBD 501 or equivalent).
- 4. Bandwidth of oscilloscope used for waveform measurement should be 50 MHz minimum; saturation of preamp must be avoided.

FIGURE 3. Test circuit for propagation delay and settling time, device type 01 and 02.



FIGURE 3. <u>Test circuit for propagation delay and settling time, device type 01 and 02</u> – Continued.





FIGURE 4. Test circuit for slew rate, device types 01 and 02.

| Subaroup              | Symbol                             | MIL-STD- | Test          |                    | Adapter pin numbers |      |      |      |      |      |      | Energized            | Measured pin |     | pin             | -    |                                                                            |          |
|-----------------------|------------------------------------|----------|---------------|--------------------|---------------------|------|------|------|------|------|------|----------------------|--------------|-----|-----------------|------|----------------------------------------------------------------------------|----------|
| <u>-</u>              | -,                                 | method   | No.           | 1-8<br>logic state | 9 V                 | 10 V | 11 V | 12 V | 13 V | 14 V | 15 V | 16-23<br>logic state | relays       | No. | Value           | Unit |                                                                            | ľ        |
| 1                     | I <sub>cc</sub> +                  | 3005     | 1             | 11111111           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 11  | I <sub>1</sub>  | mΑ   | $I_{cc} + = I_1$                                                           | (        |
| T <sub>A</sub> = 25°C | I <sub>cc</sub> -                  |          | 2             | 11111111           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 12  | I <sub>2</sub>  | mΑ   | $ _{CC^{-}} =  _{2}$                                                       | -        |
|                       | I <sub>FS</sub>                    |          | 3 <u>1</u> /  | 11111111           | -                   |      | +15  | -15  | +15  | -15  | 0    | 11111111             |              | 24  | E <sub>1</sub>  | V    | $I_{FS} = 1.992 - 0.01E_1$                                                 | 1        |
|                       | IFS                                |          | 4             | 00000000           |                     |      | +15  | -15  | +15  | -15  | 0    | 11111111             | K2           | 24  | E <sub>2</sub>  | V    | <br>IFS = 1.992 - 0.01E <sub>2</sub>                                       | 1        |
|                       | Izs                                |          | 5             | 00000000           | 1                   |      | +15  | -15  | +15  | -15  | 0    |                      | K4           | 24  | E <sub>3</sub>  | V    | $I_{zs} = -10E_3$                                                          | ĺ        |
|                       | Izs                                |          | 6             | 11111111           | 1                   |      | +15  | -15  | +15  | -15  | 0    |                      | K2, K4       | 24  | E <sub>4</sub>  | V    | $\overline{\text{Izs}} = -10\text{E}_4$                                    |          |
|                       | P <sub>ss</sub> I <sub>Fs</sub> +1 |          | 7             | 11111111           |                     |      | 5.5  | -18  | +15  | -15  | 0    | 11111111             |              | 24  | E <sub>5</sub>  | V    | $P_{SS}I_{FS}+1 = -10(E_5-E_6)$                                            | 1        |
|                       |                                    |          | 8             | 11111111           |                     |      | 4.5  | -18  | +15  | -15  | 0    | 11111111             |              | 24  | E <sub>6</sub>  | V    |                                                                            |          |
|                       | $\overline{Pssl_{FS}+1}$           |          | 9             | 00000000           |                     |      | 5.5  | -18  | +15  | -15  | 0    | 11111111             | K2           | 24  | E <sub>7</sub>  | V    | $\overline{Psslfs+1} = -10(E_7-E_8)$                                       |          |
|                       |                                    |          | 10            | 0000000            |                     |      | 4.5  | -18  | +15  | -15  | 0    | 11111111             | K2           | 24  | E <sub>8</sub>  | V    |                                                                            | <u> </u> |
|                       | P <sub>ss</sub> I <sub>Fs</sub> +2 |          | 11            | 11111111           |                     |      | 18   | -18  | +15  | -15  | 0    | 11111111             |              | 24  | E <sub>9</sub>  | V    | $P_{SS}I_{FS}+2 = -10(E_9-E_{10})$                                         |          |
|                       |                                    |          | 12            | 11111111           |                     |      | 12   | -18  | +15  | -15  | 0    | 11111111             |              | 24  | E <sub>10</sub> | V    |                                                                            |          |
|                       | $\overline{\text{PssIFs}+2}$       |          | 13            | 00000000           |                     |      | 18   | -18  | +15  | -15  | 0    | 11111111             | K2           | 24  | E <sub>11</sub> | V    | $\overline{PssIFs + 2} = -10(E_{11}-E_{12})$                               | L        |
|                       |                                    |          | 14            | 00000000           |                     |      | 12   | -18  | +15  | -15  | 0    | 11111111             | K2           | 24  | E <sub>12</sub> | V    |                                                                            | L        |
|                       | P <sub>ss</sub> I <sub>Fs</sub> -1 |          | 15            | 11111111           |                     |      | 18   | -12  | +15  | -15  | 0    | 11111111             |              | 24  | E <sub>13</sub> | V    | $P_{SS}I_{FS}-1=-10(E_{13}-E_{9})$                                         | ⊢        |
|                       | PssIFs - 1                         |          | 16            | 00000000           |                     |      | 18   | -12  | +15  | -15  | 0    | 11111111             | K2           | 24  | E <sub>14</sub> | V    | $\overline{PssIFs - 1} = -10(E_{14}-E_{11})$                               |          |
|                       | P <sub>ss</sub> I <sub>Fs</sub> -2 |          | 17            | 11111111           |                     |      | 18   | -5.5 | +15  | -15  | 0    | 11111111             | K5           | 24  | E <sub>15</sub> | V    | P <sub>SS</sub> I <sub>FS</sub> -2= -10(E <sub>15</sub> -E <sub>16</sub> ) | L        |
|                       |                                    |          | 18            | 11111111           |                     |      | 18   | -4.5 | +15  | -15  | 0    | 11111111             | K5           | 24  | E <sub>16</sub> | V    |                                                                            | ⊢        |
|                       | Psslfs – 2                         |          | 19            | 00000000           |                     |      | 18   | -5.5 | +15  | -15  | 0    | 11111111             | K2, K5       | 24  | E <sub>17</sub> | V    | Psslfs - 2 = -10(E <sub>17</sub> -E <sub>18</sub> )                        | L        |
|                       |                                    |          | 20            | 00000000           |                     |      | 18   | -4.5 | +15  | -15  | 0    | 11111111             | K2, K5       | 24  | E <sub>18</sub> | V    |                                                                            | ⊢.       |
|                       | I <sub>FS</sub> R <sub>1</sub>     |          | 21            | 11111111           | 15                  |      | +15  | -10  | 30   | -5   | 0    |                      | K1, K4       | 26  | E <sub>19</sub> | V    | $I_{FS}R_1 = 0.2E_{19}$                                                    |          |
|                       | IFSR1                              |          | 22            | 00000000           | 15                  |      | +15  | -10  | 30   | -5   | 0    |                      | K1, K2, K4   | 26  | E <sub>20</sub> | V    | $I_{FSR1} = 0.2E_{20}$                                                     |          |
|                       | IFSR2                              |          | 23            | 11111111           | 25                  |      | +15  | -12  | 30   | -5   | 0    |                      | K1, K4       | 26  | E <sub>21</sub> | V    | $I_{FS}R_2 = 0.2E_{21}$                                                    | -        |
|                       | IFSR2                              |          | 24            | 00000000           | 25                  |      | +15  | -12  | 30   | -5   | 0    |                      | K1, K2, K4   | 26  | E <sub>22</sub> | V    | $I_{FSR2} = 0.2E_{22}$                                                     |          |
|                       | I <sub>REF</sub> -                 |          | 25            | 00000000           |                     | 0    | +15  | -15  | +15  | -15  | 0    |                      | K3           | 10  | l <sub>3</sub>  | A    | $I_{REF} = I_3 \times 10^\circ$                                            | ⊢_       |
|                       | I <sub>IH1</sub>                   |          | 26 <u>2</u> / | 10000000           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 1   | 4               | A    | $I_{IH1} = I_4 \times 10^{\circ}$                                          |          |
|                       | I <sub>IH2</sub>                   |          | 27 <u>2</u> / | 01000000           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 2   | I <sub>5</sub>  | A    | $I_{IH2} = I_5 \times 10^6$                                                | -(       |
|                       | I <sub>IH3</sub>                   |          | 28 <u>2</u> / | 00100000           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 3   | I <sub>6</sub>  | Α    | $I_{IH3} = I_6 \times 10^6$                                                | -(       |
|                       | I <sub>IH4</sub>                   |          | 29 <u>2</u> / | 00010000           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 4   | 1 <sub>7</sub>  | Α    | $I_{IH4} = I_7 \times 10^6$                                                | -(       |
|                       | I <sub>IH5</sub>                   |          | 30 <u>2</u> / | 00001000           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 5   | I <sub>8</sub>  | Α    | $I_{\rm IH5} = I_8 \times 10^6$                                            | -(       |
|                       | I <sub>IH6</sub>                   |          | 31 <u>2</u> / | 00000100           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 6   | l <sub>9</sub>  | Α    | $I_{IH6} = I_9 \times 10^6$                                                | -0       |
|                       | I <sub>IH7</sub>                   |          | 32 <u>2</u> / | 00000010           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 7   | I <sub>10</sub> | Α    | $I_{IH7} = I_{10} \times 10^{6}$                                           | -0       |
|                       | I <sub>IH8</sub>                   |          | 33 <u>2</u> / | 0000001            |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 8   | I <sub>11</sub> | Α    | $I_{IH8} = I_{11} \times 10^{6}$                                           | -0       |
|                       | I <sub>IL1</sub>                   |          | 34 <u>2</u> / | 01111111           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 1   | I <sub>12</sub> | Α    | $I_{IL1} = I_{12} \times 10^6$                                             | - 1      |
|                       | I <sub>IL2</sub>                   |          | 35 <u>2</u> / | 10111111           | 1                   |      | +15  | -15  | +15  | -15  | 0    |                      |              | 2   | I <sub>13</sub> | Α    | $I_{\rm IL2} = I_{13} \times 10^6$                                         | -        |
|                       | I <sub>IL3</sub>                   |          | 36 <u>2</u> / | 11011111           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 3   | I <sub>14</sub> | А    | $I_{IL3} = I_{14} \times 10^6$                                             |          |
|                       | I <sub>IL4</sub>                   |          | 37 <u>2</u> / | 11101111           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 4   | I <sub>15</sub> | Α    | $I_{IL4} = I_{15} X 10^6$                                                  | L        |
|                       | I <sub>IL5</sub>                   |          | 38 <u>2</u> / | 11110111           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 5   | I <sub>16</sub> | А    | $I_{1L5} = I_{16} \times 10^{6}$                                           | -        |
|                       | I <sub>IL6</sub>                   |          | 39 <u>2</u> / | 11111011           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 6   | I <sub>17</sub> | А    | $I_{IL6} = I_{17} \times 10^6$                                             | L -      |
|                       | I <sub>IL7</sub>                   |          | 40 <u>2</u> / | 11111101           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 7   | I <sub>18</sub> | Α    | $I_{1L7} = I_{18} \times 10^6$                                             | <u> </u> |
|                       | I <sub>IL8</sub>                   |          | 41 <u>2</u> / | 11111110           |                     |      | +15  | -15  | +15  | -15  | 0    |                      |              | 8   | I <sub>19</sub> | Α    | $I_{\rm IL8} = I_{19} \times 10^6$                                         | - L      |

# TABLE III. Group A inspection for device types 01 and 02.

|                     | 1                        | 1               | 1    |                    |     |      |        |        |      |      |      |                      |           |     |                 |      |                                                                                                                    |   |
|---------------------|--------------------------|-----------------|------|--------------------|-----|------|--------|--------|------|------|------|----------------------|-----------|-----|-----------------|------|--------------------------------------------------------------------------------------------------------------------|---|
| Subgroup            | Symbol                   | MIL-STD-<br>883 | Test |                    |     | /    | Adapte | er pin | numb | ers  |      |                      | Energized | Me  | asured          | pin  | Equation                                                                                                           | 1 |
|                     |                          | method          | No.  | 1-8<br>logic state | 9 V | 10 V | 11 V   | 12 V   | 13 V | 14 V | 15 V | 16-23<br>logic state | relays    | No. | Value           | Unit |                                                                                                                    |   |
| 1                   | V <sub>CAL1</sub>        |                 | 42   |                    |     |      | +15    | -15    | 30   | 0    | 18   | 00000000             | K3        | 24  | E <sub>23</sub> | V    | $V_{CAL1} = E_{23}$                                                                                                |   |
| $T_A = 25^{\circ}C$ | I <sub>FS</sub> +        |                 | 43   | 11111111           |     |      | +15    | -15    | 30   | 0    | 18   | 11111111             |           | 24  | E <sub>24</sub> | V    | $I_{FS}$ + = 1.992 - 0.01( $E_{24}$ - $E_{23}$ )                                                                   |   |
|                     | IFS +                    |                 | 44   | 00000000           |     |      | +15    | -15    | 30   | 0    | 18   | 11111111             | K2        | 24  | E <sub>25</sub> | V    | $\overline{I_{FS} +} = 1.992 - 0.01(E_{25} - E_{23})$                                                              |   |
|                     | V <sub>CAL2</sub>        |                 | 45   |                    |     |      | +15    | -15    | +15  | -15  | -10  | 00000000             | K3        | 24  | E <sub>26</sub> | V    | $V_{CAL2} = E_{26}$                                                                                                |   |
|                     | I <sub>FS</sub> -        |                 | 46   | 11111111           |     |      | +15    | -15    | +15  | -15  | -10  | 11111111             |           | 24  | E <sub>27</sub> | V    | $I_{FS} = 1.992 - 0.01(E_{27} - E_{26})$                                                                           |   |
|                     | IFS -                    |                 | 47   | 00000000           |     |      | +15    | -15    | +15  | -15  | -10  | 11111111             | K2        | 24  | E <sub>28</sub> | V    | IFS-= 1.992-0.01(E <sub>28</sub> -E <sub>26</sub> )                                                                |   |
|                     | ∆l <sub>FSC</sub>        |                 | 48   |                    |     |      |        |        |      |      |      |                      |           |     |                 |      | $\Delta I_{FSC} = 1000(I_{FS} + -I_{FS} -)$                                                                        |   |
|                     | $\Delta \overline{IFSC}$ |                 | 49   |                    |     |      |        |        |      |      |      |                      |           |     |                 |      | $\Delta \overline{\text{IFSC}} = 1000 \left(\overline{\text{IFS} + - \text{IFS} -}\right)$                         |   |
|                     | V <sub>CAL3</sub>        |                 | 50   | 00000000           |     |      | +15    | -15    | +15  | -15  | 0    | 00000000             |           | 24  | E <sub>29</sub> | V    | $V_{CAL3} = E_{29}$                                                                                                |   |
|                     | V <sub>CAL4</sub>        |                 | 51   | 11111111           |     |      | +15    | -15    | +15  | -15  | 0    | 11111111             |           | 24  | E <sub>30</sub> | V    | $V_{CAL4} = E_{30}$                                                                                                |   |
|                     | V <sub>CAL5</sub>        |                 | 52   | 00000000           |     |      | +15    | -15    | +15  | -15  | 0    | 11111111             | K2        | 24  | E <sub>31</sub> | V    | $V_{CAL5} = E_{31}$                                                                                                |   |
|                     | V <sub>CAL6</sub>        |                 | 53   | 11111111           |     |      | +15    | -15    | +15  | -15  | 0    | 00000000             | K2        | 24  | E <sub>32</sub> | V    | $V_{CAL6} = E_{32}$                                                                                                | _ |
|                     | NL <sub>1</sub>          |                 | 54   | 1000000            |     |      | +15    | -15    | +15  | -15  | 0    | 10000000             |           | 24  | E <sub>33</sub> | V    | $NL_{1} = \left(\begin{array}{c} (E_{33} - V_{CAL3}) \\ I_{FS} \times 10^{3} \end{array}\right) -$                 |   |
|                     |                          |                 |      |                    |     |      |        |        |      |      |      |                      |           |     |                 |      | $\frac{(128)}{(255)} \ \frac{(V_{CAL4} - V_{CAL3})}{I_{FS} \times 10^3}$                                           |   |
|                     | NL <sub>2</sub>          |                 | 55   | 01000000           |     |      | +15    | -15    | +15  | -15  | 0    | 01000000             |           | 24  | E <sub>34</sub> | V    | $NL_{2} = \left(\begin{array}{c} \frac{\left(E_{34} - V_{CAL3}\right)}{I_{FS} \times 10^{3}} \end{array}\right) -$ |   |
|                     |                          |                 |      |                    |     |      |        |        |      |      |      |                      |           |     |                 |      | $\frac{(64)}{(255)} \ \frac{(VCAL4-VCAL3)}{IFS\times 10^3}$                                                        |   |
|                     | NL <sub>3</sub>          |                 | 56   | 00100000           |     |      | +15    | -15    | +15  | -15  | 0    | 00100000             |           | 24  | E <sub>35</sub> | V    | $NL_{3} = \left(\begin{array}{c} \frac{\left(E_{35} - V_{CAL3}\right)}{I_{FS} \times 10^{3}} \end{array}\right) -$ |   |
|                     |                          |                 |      |                    |     |      |        |        |      |      |      |                      |           |     |                 |      | $\frac{(32)}{(255)} \frac{(VCAL4 - VCAL3)}{IFS \times 10^3}$                                                       |   |
|                     | NL₄                      |                 | 57   | 00010000           |     |      | +15    | -15    | +15  | -15  | 0    | 00010000             |           | 24  | E <sub>36</sub> | V    | $NL_{4} = \left(\begin{array}{c} \frac{\left(E_{36} - V_{CAL3}\right)}{I_{FS} \times 10^{3}} \end{array}\right) -$ |   |
|                     |                          |                 |      |                    |     |      |        |        |      |      |      |                      |           |     |                 |      | $\frac{(16)}{(255)} \ \frac{(VCAL4 - VCAL3)}{I_{FS} \times 10^3}$                                                  |   |
|                     | NL <sub>5</sub>          |                 | 58   | 00001000           |     |      | +15    | -15    | +15  | -15  | 0    | 00001000             |           | 24  | E <sub>37</sub> | V    | $NL_{5} = \left(\begin{array}{c} \frac{\left(E_{37} - VCAL3\right)}{IFS \times 10^3} \end{array}\right)^{-1}$      |   |
|                     |                          |                 |      |                    |     |      |        |        |      |      |      |                      |           |     |                 |      | $\frac{(8)}{(255)} \frac{(VCAL4 - VCAL3)}{IFS \times 10^3}$                                                        |   |

| -                          |                 |                 |      |                    |     |      |        |        |       |      |      |                      |           |     |                 |      |                                                                                                                                                                                                                                                                                                                                                                                    | _ |
|----------------------------|-----------------|-----------------|------|--------------------|-----|------|--------|--------|-------|------|------|----------------------|-----------|-----|-----------------|------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---|
| Subaroup                   | Symbol          | MIL-STD-<br>883 | Test |                    |     | /    | Adapte | er pin | numbe | ers  |      |                      | Eneraized | Me  | easured         | pin  | Equation                                                                                                                                                                                                                                                                                                                                                                           |   |
| 0 1                        | ,               | method          | No.  | 1-8<br>logic state | 9 V | 10 V | 11 V   | 12 V   | 13 V  | 14 V | 15 V | 16-23<br>logic state | relays    | No. | Value           | Unit |                                                                                                                                                                                                                                                                                                                                                                                    |   |
| 1<br>T <sub>A</sub> = 25°C | NL <sub>6</sub> |                 | 59   | 00000100           |     |      | +15    | -15    | +15   | -15  | 0    | 00000100             |           | 24  | E <sub>38</sub> | V    | $\begin{array}{l} NL_6 = \left( \begin{array}{c} \left( \underline{E}_{38} - VCAL3 \right) \\ \mathbf{IFS} \times 10^3 \end{array} \right) \\ \hline \left( \begin{array}{c} (4) \\ (255) \end{array} \\ \end{array} \\ \begin{array}{c} \left( \frac{VCAL4 - VCAL3}{IFS \times 10^3} \right) \end{array} \end{array}$                                                             |   |
|                            | NL7             |                 | 60   | 00000010           |     |      | +15    | -15    | +15   | -15  | 0    | 00000010             |           | 24  | E <sub>39</sub> | V    | $ \begin{array}{c} NL_{7} = \left( \begin{array}{c} \displaystyle \frac{\left(E_{39} - VCAL3\right)}{IFS \times 10^{3}} \end{array} \right) \\ \\ \displaystyle \frac{(2)}{(255)} \begin{array}{c} \displaystyle \frac{(VCAL4 - VCAL3)}{IFS \times 10^{3}} \end{array} \end{array} $                                                                                               |   |
|                            | NL8             |                 | 61   | 00000001           |     |      | +15    | -15    | +15   | -15  | 0    | 00000001             |           | 24  | E <sub>40</sub> | V    | $ \begin{array}{c} NL_8 = \left( \begin{array}{c} \displaystyle \frac{\left(E_{40} - VCAL3\right)}{IFS \times 10^3} \end{array} \right) \text{-} \\ \displaystyle \frac{(1)}{(255)} \begin{array}{c} \displaystyle \frac{(VCAL4 - VCAL3)}{IFS \times 10^3} \end{array} \end{array} $                                                                                               |   |
|                            | NL1             |                 | 62   | 01111111           |     |      | +15    | -15    | +15   | -15  | 0    | 1000000              |           | 24  | E <sub>41</sub> | V    | $\frac{\overline{NL}_1}{(128)} = \left( \begin{array}{c} \frac{(E_{41} - VCAL5)}{IFS \times 10^3} \end{array} \right) - \frac{(128)}{(255)} \frac{(VCAL6 - VCAL5)}{IFS \times 10^3}$                                                                                                                                                                                               |   |
|                            | NL2             |                 | 63   | 10111111           |     |      | +15    | -15    | +15   | -15  | 0    | 01000000             |           | 24  | E <sub>42</sub> | V    | $\overline{\text{NL}_2} = \left(\begin{array}{c} \left(\underline{\text{E}_{42} - \text{V}_{\text{CAL5}}}\right)\\ \overline{\text{I}_{\text{FS}} \times 10^3} \end{array}\right) - \\ \hline \left(\frac{64)}{(255)} \frac{(\text{V}_{\text{CAL6}} - \text{V}_{\text{CAL5}})}{\overline{\text{I}_{\text{FS}} \times 10^3}} \\ \end{array}$                                        |   |
|                            | NL3             |                 | 64   | 11011111           |     |      | +15    | -15    | +15   | -15  | 0    | 00100000             |           | 24  | E <sub>43</sub> | V    | $\label{eq:NL3} \begin{array}{ c c c }\hline \hline NL3 = \left( \begin{array}{c} \left( E_{43} - V_{CAL5} \right) \\ \hline I_{FS} \times 10^3 \end{array} \right) \\ \hline \left( \begin{array}{c} (32) \\ \hline (255) \end{array} \begin{array}{c} \left( \begin{array}{c} VCAL6 - V_{CAL5} \right) \\ \hline I_{FS} \times 10^3 \end{array} \end{array} \right) \end{array}$ |   |
|                            | NL4             |                 | 65   | 11101111           |     |      | +15    | -15    | +15   | -15  | 0    | 00010000             |           | 24  | E <sub>44</sub> | V    | $\label{eq:NL4} \overline{\text{NL4}} = \left( \begin{array}{c} \left( \underline{\text{E44} - \text{VCAL5}} \right) \\ \overline{\text{IFS} \times 10^3} \end{array} \right) \text{-} \\ \hline \left( \begin{array}{c} 16 \\ 1255 \end{array} \right) \frac{(\text{VCAL6} - \text{VCAL5})}{\text{IFS} \times 10^3} \end{array}$                                                  |   |
|                            | NL5             |                 | 66   | 11110111           |     |      | +15    | -15    | +15   | -15  | 0    | 00001000             |           | 24  | E <sub>45</sub> | V    | $\overline{\text{NL5}} = \left( \begin{array}{c} \frac{\left(\text{E45} - \text{VCAL5}\right)}{\text{IFS} \times 10^3} \end{array} \right) \text{-} \\ \frac{(8)}{(255)} \frac{(\text{VCAL6} - \text{VCAL5})}{\text{IFS} \times 10^3} \end{array}$                                                                                                                                 |   |
|                            | NL6             |                 | 67   | 11111011           |     |      | +15    | -15    | +15   | -15  | 0    | 00000100             |           | 24  | E <sub>46</sub> | V    | $ \frac{\overline{NL6} = \left( \begin{array}{c} \left( \underline{E46} - VCAL5 \right) \\ \overline{IFS \times 10^3} \end{array} \right) - \\ \frac{(4)}{(255)} \begin{array}{c} \left( \underbrace{VCAL6} - \operatorname{VCAL5} \right) \\ \overline{IFS \times 10^3} \end{array} $                                                                                             | _ |

| Subgroup            | Symbol                          | MIL-STD-<br>883<br>method | Test<br>No. |                    |     | ŀ    | Adapte | er pin i | numbe | ers  |      |                      | Energized<br>relays | Me  | asured          | pin  | Equation                                                                                                                                        |
|---------------------|---------------------------------|---------------------------|-------------|--------------------|-----|------|--------|----------|-------|------|------|----------------------|---------------------|-----|-----------------|------|-------------------------------------------------------------------------------------------------------------------------------------------------|
|                     |                                 |                           |             | 1-8<br>logic state | 9 V | 10 V | 11 V   | 12 V     | 13 V  | 14 V | 15 V | 16-23<br>logic state |                     | No. | Value           | Unit | -                                                                                                                                               |
| $T_A = 25^{\circ}C$ | NL7                             |                           | 68          | 11111101           |     |      | +15    | -15      | +15   | -15  | 0    | 00000010             |                     | 24  | E <sub>47</sub> | V    | $\overline{NL7} = \left(\begin{array}{c} (\underline{E47 - VCAL5}) \\ \overline{IFS \times 10^3} \end{array}\right)$                            |
|                     |                                 |                           |             |                    |     |      |        |          |       |      |      |                      |                     |     |                 |      | $\frac{(2)}{(255)} \ \frac{(V_{CAL6} - V_{CAL5})}{I_{FS} \times 10^3}$                                                                          |
|                     | NL8                             |                           | 69          | 11111110           |     |      | +15    | -15      | +15   | -15  | 0    | 00000001             |                     | 24  | E <sub>48</sub> | V    | $\overline{NL_8} = \left( \begin{array}{c} \left( \underline{E_{48} - V_{CAL5}} \right) \\ \overline{I_{FS} \times 10^3} \end{array} \right)^-$ |
|                     |                                 |                           |             |                    |     |      |        |          |       |      |      |                      |                     |     |                 |      | $\frac{(1)}{(255)} \frac{(V_{CAL6} - V_{CAL5})}{I_{FS} \times 10^3}$                                                                            |
|                     | ΣNL <sup>+</sup>                |                           | 70          |                    |     |      |        |          |       |      |      |                      |                     |     |                 |      | $\Sigma NL^{+} = NL_{i} + NL_{K} +$<br>(i, k, bits having positive errors)                                                                      |
|                     | $\overline{\Sigma NL^+}$        |                           | 71          |                    |     |      |        |          |       |      |      |                      |                     |     |                 |      | $\overline{\Sigma NL^{+}} = \overline{NLi^{1}} + \overline{NLk^{1}} + \dots$ (i, k, bits having positive errors)                                |
|                     | ΣNL                             |                           | 72          |                    |     |      |        |          |       |      |      |                      |                     |     |                 |      | $\Sigma NL = NL_m + NL_n +$<br>(m, n, bits having negative errors)                                                                              |
|                     | $\overline{\Sigma NL}^{-}$      |                           | 73          |                    |     |      |        |          |       |      |      |                      |                     |     |                 |      | $\overline{\Sigma NL^{-}} = \overline{NLm^{1}} + \overline{NLn^{1}} + \dots$ (m, n, bits having negative errors)                                |
|                     | ΔΣΝL                            |                           | 74          |                    |     |      |        |          |       |      |      |                      |                     |     |                 |      | $\Delta \Sigma NL = \left  \Sigma NL^+ \right  - \left  \Sigma NL^- \right $                                                                    |
|                     | $\Delta \Sigma \overline{NL}$   |                           | 75          |                    |     |      |        |          |       |      |      |                      |                     |     |                 |      | $\Delta \Sigma \overline{NL} = \left  \Sigma \overline{NL}^+ \right  - \left  \Sigma \overline{NL}^- \right $                                   |
|                     | NL⁺                             |                           | 76          |                    |     |      |        |          |       |      |      |                      |                     |     |                 |      | $NL^{+} = \left  \Sigma NL^{+} \right  + \left  \Delta \Sigma NL \right $                                                                       |
|                     | $\overline{NL^+}$               |                           | 77          |                    |     |      |        |          |       |      |      |                      |                     |     |                 |      | $\overline{NL^+} = \left  \Sigma \overline{NL}^+ \right  + \left  \Delta \Sigma \overline{NL} \right $                                          |
|                     | NL                              |                           | 78          |                    |     |      |        |          |       |      |      |                      |                     |     |                 |      | $NL^{-} = \left  \Sigma NL^{-} \right  + \left  \Delta \Sigma NL \right $                                                                       |
|                     | NL <sup>-</sup>                 |                           | 79          |                    |     |      |        |          |       |      |      |                      |                     |     |                 |      | $\overline{\mathrm{NL}^{-}} = \left  \Sigma \overline{\mathrm{NL}}^{-} \right  + \left  \Delta \Sigma \overline{\mathrm{NL}} \right $           |
|                     | (I <sub>01</sub> ) <sub>a</sub> |                           | 80          | 10000000           |     |      | +15    | -15      | +15   | -15  | 0    | 10000000             |                     | 24  | E <sub>49</sub> | V    | $(I_{01})_a = I_{FS} \times \frac{128}{255} - 0.01(E_{49})$                                                                                     |
|                     | (I <sub>01</sub> )ь             |                           | 81          | 01111111           |     |      | +15    | -15      | +15   | -15  | 0    | 01111111             |                     | 24  | E <sub>50</sub> | V    | $(I_{01})_{b} = I_{FS} \times \frac{127}{255} - 0.01(E_{50})$                                                                                   |
|                     | $\Delta(I_{01})$                |                           | 82          |                    |     |      |        |          |       |      |      |                      |                     |     |                 |      | $\Delta(I_{01}) = [(I_{01})_{a} - (I_{01})_{b}] \times 10^{3}$                                                                                  |

| Subgroup                   | Symbol                          | MIL-STD-<br>883<br>method | Test<br>No |                    |     | ļ    | Adapte | er pin i | numbe | ers  |      |                      | Energized | Me  | asured          | pin  | Equation                                                       |
|----------------------------|---------------------------------|---------------------------|------------|--------------------|-----|------|--------|----------|-------|------|------|----------------------|-----------|-----|-----------------|------|----------------------------------------------------------------|
|                            |                                 | mounou                    | 110.       | 1-8<br>logic state | 9 V | 10 V | 11 V   | 12 V     | 13 V  | 14 V | 15 V | 16-23<br>logic state | ·         | No. | Value           | Unit |                                                                |
| 1<br>T <sub>A</sub> = 25°C | (I <sub>02</sub> ) <sub>a</sub> |                           | 83         | 01000000           |     |      | +15    | -15      | +15   | -15  | 0    | 01000000             |           | 24  | E <sub>51</sub> | V    | $(I_{02})_a = I_{FS} \times \frac{64}{255} - 0.01(E_{51})$     |
|                            | (I <sub>02</sub> ) <sub>b</sub> |                           | 84         | 00111111           |     |      | +15    | -15      | +15   | -15  | 0    | 00111111             |           | 24  | E <sub>52</sub> | V    | $(I_{02})_{b} = I_{FS} X \frac{63}{255} - 0.01(E_{52})$        |
|                            | $\Delta(I_{02})$                |                           | 85         |                    |     |      |        |          |       |      |      |                      |           |     |                 |      | $\Delta(I_{02}) = [(I_{02})_{a} - (I_{02})_{b}] \times 10^{3}$ |
|                            | (I <sub>03</sub> ) <sub>a</sub> |                           | 86         | 00100000           |     |      | +15    | -15      | +15   | -15  | 0    | 00100000             |           | 24  | E <sub>53</sub> | V    | $(I_{03})_a = I_{FS} X \frac{32}{255} - 0.01(E_{53})$          |
|                            | (I <sub>03</sub> ) <sub>b</sub> |                           | 87         | 00011111           |     |      | +15    | -15      | +15   | -15  | 0    | 00011111             |           | 24  | E <sub>54</sub> | V    | $(I_{03})_b = I_{FS} \times \frac{31}{255} - 0.01(E_{54})$     |
|                            | $\Delta(I_{03})$                |                           | 88         |                    |     |      |        |          |       |      |      |                      |           |     |                 |      | $\Delta(I_{03}) = [(I_{03})_{a} - (I_{03})_{b}] \times 10^{3}$ |
|                            | (I <sub>04</sub> ) <sub>a</sub> |                           | 89         | 00010000           |     |      | +15    | -15      | +15   | -15  | 0    | 00010000             |           | 24  | E <sub>55</sub> | V    | $(I_{04})_a = I_{FS} \times \frac{16}{255} - 0.01(E_{55})$     |
|                            | (I <sub>04</sub> ) <sub>b</sub> |                           | 90         | 00001111           |     |      | +15    | -15      | +15   | -15  | 0    | 00001111             |           | 24  | E <sub>56</sub> | V    | $(I_{04})_{b} = I_{FS} \times \frac{15}{255} - 0.01(E_{56})$   |
|                            | $\Delta(I_{04})$                |                           | 91         |                    |     |      |        |          |       |      |      |                      |           |     |                 |      | $\Delta(I_{04}) = [(I_{04})_{a} - (I_{04})_{b}] \times 10^{3}$ |
|                            | (I <sub>05</sub> ) <sub>a</sub> |                           | 92         | 00001000           |     |      | +15    | -15      | +15   | -15  | 0    | 00001000             |           | 24  | E <sub>57</sub> | V    | $(I_{05})_a = I_{FS} \times \frac{8}{255} - 0.01(E_{57})$      |
|                            | (I <sub>05</sub> ) <sub>b</sub> |                           | 93         | 00000111           |     |      | +15    | -15      | +15   | -15  | 0    | 00000111             |           | 24  | E <sub>58</sub> | V    | $(I_{05})_{b} = I_{FS} \times \frac{7}{255} - 0.01(E_{58})$    |
|                            | $\Delta(I_{05})$                |                           | 94         |                    |     |      |        |          |       |      |      |                      |           |     |                 |      | $\Delta(I_{05}) = [(I_{05})_{a} - (I_{05})_{b}] \times 10^{3}$ |
|                            | (I <sub>06</sub> ) <sub>a</sub> |                           | 95         | 00000100           |     |      | +15    | -15      | +15   | -15  | 0    | 00000100             |           | 24  | E <sub>59</sub> | V    | $(I_{06})_a = I_{FS} \times \frac{4}{255} - 0.01(E_{59})$      |
|                            | (I <sub>06</sub> ) <sub>b</sub> |                           | 96         | 00000011           |     |      | +15    | -15      | +15   | -15  | 0    | 00000011             |           | 24  | E <sub>60</sub> | V    | $(I_{06})_{b} = I_{FS} X \frac{3}{255} - 0.01(E_{60})$         |
|                            | $\Delta(I_{06})$                |                           | 97         |                    |     |      |        |          |       |      |      |                      |           |     |                 |      | $\Delta(I_{06}) = [(I_{06})_{a} - (I_{06})_{b}] \times 10^{3}$ |
|                            | (I <sub>07</sub> )a             |                           | 98         | 00000010           |     |      | +15    | -15      | +15   | -15  | 0    | 00000010             |           | 24  | E <sub>61</sub> | V    | $(I_{07})_a = I_{FS} X \frac{2}{255} - 0.01(E_{61})$           |
|                            | (I <sub>07</sub> ) <sub>b</sub> |                           | 99         | 00000001           |     |      | +15    | -15      | +15   | -15  | 0    | 00000001             |           | 24  | E <sub>62</sub> | V    | $(I_{07})_{b} = I_{FS} \times \frac{1}{255} - 0.01(E_{62})$    |
|                            | $\Delta(I_{07})$                |                           | 100        |                    |     |      |        |          |       |      |      |                      |           |     |                 |      | $\Delta(I_{07}) = [(I_{07})_{a} - (I_{07})_{b}] \times 10^{3}$ |
|                            | (l <sub>08</sub> ) <sub>b</sub> |                           | 101        | 00000000           |     |      | +15    | -15      | +15   | -15  | 0    | 00000000             |           | 24  | E <sub>63</sub> | V    | $(I_{08})_{b} = -0.01(E_{63})$                                 |
|                            | (I <sub>08</sub> )              |                           | 102        |                    |     |      |        |          |       |      |      |                      |           |     |                 |      | $\Delta(I_{08}) = [(I_{07})_{b} - (I_{08})_{b}] \times 10^{3}$ |
|                            | ∆l <sub>FS</sub>                |                           | 103        |                    |     |      |        |          |       |      |      |                      |           |     |                 |      | $I_{FS} - \overline{I_{FS}} = \Delta I_{FS}$                   |

| Subaroup               | Symbol                                 | MIL-STD- | Test           |                    |     | ŀ    | Adapte | er pin | numbe | ers  |      |                      | Eperaized  | Me  | asured          | pin  | Equation                                                                   | D  |
|------------------------|----------------------------------------|----------|----------------|--------------------|-----|------|--------|--------|-------|------|------|----------------------|------------|-----|-----------------|------|----------------------------------------------------------------------------|----|
| Cubgroup               | Cynibol                                | method   | No.            | 1-8<br>logic state | 9 V | 10 V | 11 V   | 12 V   | 13 V  | 14 V | 15 V | 16-23<br>logic state | relays     | No. | Value           | Unit |                                                                            | ľ  |
| 2                      | I <sub>cc</sub> +                      | 3005     | 104            | 11111111           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 11  | I <sub>20</sub> | mΑ   | $ _{CC} + =  _{20}$                                                        | (  |
| T <sub>A</sub> = 125°C | Icc-                                   |          | 105            | 11111111           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 12  | I <sub>21</sub> | mA   | $I_{CC^{-}} = I_{21}$                                                      | -  |
|                        | I <sub>FS</sub>                        |          | 106 <u>1</u> / | 11111111           |     |      | +15    | -15    | +15   | -15  | 0    | 11111111             |            | 24  | E <sub>64</sub> | V    | $I_{FS} = 1.992 - 0.01E_{64}$                                              | 1  |
|                        | IFS                                    |          | 107            | 00000000           |     |      | +15    | -15    | +15   | -15  | 0    | 11111111             | K2         | 24  | E <sub>65</sub> | V    | IFS = 1.992 - 0.01E <sub>65</sub>                                          | 1  |
|                        | Izs                                    |          | 108            | 00000000           |     |      | +15    | -15    | +15   | -15  | 0    |                      | K4         | 24  | E <sub>66</sub> | V    | I <sub>zs</sub> = -10E <sub>66</sub>                                       |    |
|                        | Izs                                    |          | 109            | 11111111           |     |      | +15    | -15    | +15   | -15  | 0    |                      | K2, K4     | 24  | E <sub>67</sub> | V    | $\overline{\text{Izs}} = -10E_{67}$                                        |    |
|                        | P <sub>ss</sub> I <sub>Fs</sub> +1     |          | 110            | 11111111           |     |      | 5.5    | -18    | +15   | -15  | 0    | 11111111             |            | 24  | E <sub>68</sub> | V    | $P_{SS}I_{FS}+1 = -10(E_{68}-E_{69})$                                      | 1  |
|                        |                                        |          | 111            | 11111111           |     |      | 4.5    | -18    | +15   | -15  | 0    | 11111111             |            | 24  | E <sub>69</sub> | V    | ]                                                                          |    |
|                        | $\overline{\text{Pssl}_{\text{Fs}}+1}$ |          | 112            | 00000000           |     |      | 5.5    | -18    | +15   | -15  | 0    | 11111111             | K2         | 24  | E <sub>70</sub> | V    | $\overline{\text{PssIFs}+1} = -10(\text{E}_{70}-\text{E}_{71})$            |    |
|                        |                                        |          | 113            | 00000000           |     |      | 4.5    | -18    | +15   | -15  | 0    | 11111111             | K2         | 24  | E <sub>71</sub> | V    |                                                                            |    |
|                        | P <sub>ss</sub> I <sub>Fs</sub> +2     |          | 114            | 11111111           |     |      | 18     | -18    | +15   | -15  | 0    | 11111111             |            | 24  | E <sub>72</sub> | V    | $P_{SS}I_{FS}+2 = -10(E_{72}-E_{73})$                                      |    |
|                        |                                        |          | 115            | 11111111           |     |      | 12     | -18    | +15   | -15  | 0    | 11111111             |            | 24  | E <sub>73</sub> | V    |                                                                            |    |
|                        | $\overline{\text{PssIFs}+2}$           |          | 116            | 00000000           |     |      | 18     | -18    | +15   | -15  | 0    | 11111111             | K2         | 24  | E <sub>74</sub> | V    | $\overline{\text{PssIFs}+2}$ = -10(E <sub>74</sub> -E <sub>75</sub> )      |    |
|                        |                                        |          | 117            | 00000000           |     |      | 12     | -18    | +15   | -15  | 0    | 11111111             | K2         | 24  | E <sub>75</sub> | V    |                                                                            |    |
|                        | P <sub>ss</sub> I <sub>Fs</sub> -1     |          | 118            | 11111111           |     |      | 18     | -12    | +15   | -15  | 0    | 11111111             |            | 24  | E <sub>76</sub> | V    | $P_{ss}I_{Fs}-1 = -10(E_{76}-E_{72})$                                      |    |
|                        | PssIFs -1                              |          | 119            | 00000000           |     |      | 18     | -12    | +15   | -15  | 0    | 11111111             | K2         | 24  | E <sub>77</sub> | V    | $\overline{PssIFs - 1} = -10(E_{77}-E_{74})$                               |    |
|                        | P <sub>ss</sub> I <sub>Fs</sub> -2     |          | 120            | 11111111           |     |      | 18     | -5.5   | +15   | -15  | 0    | 11111111             | K5         | 24  | E <sub>78</sub> | V    | P <sub>SS</sub> I <sub>FS</sub> -2= -10(E <sub>78</sub> -E <sub>79</sub> ) |    |
|                        |                                        |          | 121            | 11111111           |     |      | 18     | -4.5   | +15   | -15  | 0    | 11111111             | K5         | 24  | E <sub>79</sub> | V    |                                                                            |    |
|                        | $\overline{\text{Psslfs}-2}$           |          | 122            | 00000000           |     |      | 18     | -5.5   | +15   | -15  | 0    | 11111111             | K2, K5     | 24  | E <sub>80</sub> | V    | $\overline{PssIrs - 2} = -10(E_{80}-E_{81})$                               |    |
|                        |                                        |          | 123            | 0000000            |     |      | 18     | -4.5   | +15   | -15  | 0    | 11111111             | K2, K5     | 24  | E <sub>81</sub> | V    |                                                                            |    |
|                        | I <sub>FS</sub> R <sub>1</sub>         |          | 124            | 11111111           | 15  |      | +15    | -10    | 30    | -5   | 0    |                      | K1, K4     | 26  | E <sub>82</sub> | V    | $I_{FS}R_1 = 0.2E_{82}$                                                    |    |
|                        | IFSR1                                  |          | 125            | 00000000           | 15  |      | +15    | -10    | 30    | -5   | 0    |                      | K1, K2, K4 | 26  | E <sub>83</sub> | V    | IFSR1 = 0.2E <sub>83</sub>                                                 | 2  |
|                        | I <sub>FS</sub> R <sub>2</sub>         |          | 126            | 11111111           | 25  |      | +15    | -12    | 30    | -5   | 0    |                      | K1, K4     | 26  | E <sub>84</sub> | V    | $I_{FS}R_2 = 0.2E_{84}$                                                    | 4  |
|                        | IFSR2                                  |          | 127            | 00000000           | 25  |      | +15    | -12    | 30    | -5   | 0    |                      | K1, K2, K4 | 26  | E <sub>85</sub> | V    | IFSR2 = 0.2E <sub>85</sub>                                                 | 4  |
|                        | I <sub>REF</sub> -                     |          | 128            | 00000000           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      | K3         | 10  | <sub>22</sub>   | Α    | $I_{REF} = I_{22} \times 10^6$                                             |    |
|                        | I <sub>IH1</sub>                       |          | 129 <u>2</u> / | 10000000           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      |            | 1   | I <sub>23</sub> | Α    | $I_{\rm IH1} = I_{23} \times 10^{\circ}$                                   | -( |
|                        | I <sub>IH2</sub>                       |          | 130 <u>2</u> / | 01000000           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      |            | 2   | I <sub>24</sub> | Α    | $I_{1H2} = I_{24} \times 10^6$                                             | -( |
|                        | I <sub>IH3</sub>                       |          | 131 <u>2</u> / | 00100000           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      |            | 3   | I <sub>25</sub> | Α    | $I_{IH3} = I_{25} \times 10^{6}$                                           | -( |
|                        | I <sub>IH4</sub>                       |          | 132 <u>2</u> / | 00010000           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      |            | 4   | I <sub>26</sub> | Α    | $I_{1H4} = I_{26} \times 10^{6}$                                           | -( |
|                        | I <sub>IH5</sub>                       |          | 133 <u>2</u> / | 00001000           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      |            | 5   | I <sub>27</sub> | Α    | $I_{1H5} = I_{27} \times 10^{6}$                                           | -( |
|                        | I <sub>IH6</sub>                       |          | 134 <u>2</u> / | 00000100           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      |            | 6   | I <sub>28</sub> | Α    | $I_{1H6} = I_{28} \times 10^{\circ}$                                       | -( |
|                        | I <sub>IH7</sub>                       |          | 135 <u>2</u> / | 00000010           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      |            | 7   | I <sub>29</sub> | Α    | $I_{1H7} = I_{29} \times 10^{6}$                                           | -( |
|                        | I <sub>IH8</sub>                       |          | 136 <u>2</u> / | 00000001           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      |            | 8   | I <sub>30</sub> | Α    | $I_{\rm IH8} = I_{30} \times 10^{6}$                                       | -( |
|                        | I <sub>IL1</sub>                       |          | 137 <u>2</u> / | 01111111           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      |            | 1   | I <sub>31</sub> | Α    | $I_{IL1} = I_{31} \times 10^{\circ}$                                       | -  |
|                        | I <sub>IL2</sub>                       |          | 138 <u>2</u> / | 10111111           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      |            | 2   | I <sub>32</sub> | Α    | $I_{IL2} = I_{32} \times 10^{\circ}$                                       | -  |
|                        | I <sub>IL3</sub>                       |          | 139 <u>2</u> / | 11011111           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      |            | 3   | I <sub>33</sub> | Α    | $I_{IL3} = I_{33} \times 10^6$                                             | -  |
|                        | I <sub>IL4</sub>                       |          | 140 <u>2</u> / | 11101111           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      |            | 4   | I <sub>34</sub> | Α    | $I_{IL4} = I_{34} \times 10^6$                                             | -  |
|                        | I <sub>IL5</sub>                       |          | 141 <u>2</u> / | 11110111           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      |            | 5   | I <sub>35</sub> | Α    | $I_{IL5} = I_{35} \times 10^6$                                             | -  |
|                        | I <sub>IL6</sub>                       |          | 142 <u>2</u> / | 11111011           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 6   | I <sub>36</sub> | Α    | $I_{IL6} = I_{36} X 10^6$                                                  | -  |
|                        | I <sub>IL7</sub>                       |          | 143 <u>2</u> / | 11111101           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 7   | I <sub>37</sub> | Α    | $I_{1L7} = I_{37} \times 10^{6}$                                           | -  |
|                        | I <sub>IL8</sub>                       |          | 144 <u>2</u> / | 11111110           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 8   | I <sub>38</sub> | А    | $I_{IL8} = I_{38} \times 10^{\circ}$                                       | -  |

| Subgroup               | Symbol                   | MIL-STD- | Tost |                    |     | /    | Adapte | er pin | numbe | ers  |      |                      | Enorgized | Me  | asured           | pin  | Equation                                                                                                                                |
|------------------------|--------------------------|----------|------|--------------------|-----|------|--------|--------|-------|------|------|----------------------|-----------|-----|------------------|------|-----------------------------------------------------------------------------------------------------------------------------------------|
| Subgroup               | Symbol                   | method   | No.  | 1-8<br>logic state | 9 V | 10 V | 11 V   | 12 V   | 13 V  | 14 V | 15 V | 16-23<br>logic state | relays    | No. | Value            | Unit |                                                                                                                                         |
| 2                      | V <sub>CAL1</sub>        |          | 145  |                    |     |      | +15    | -15    | 30    | 0    | 18   | 00000000             | K3        | 24  | E <sub>86</sub>  | V    | $V_{CAL1} = E_{86}$                                                                                                                     |
| T <sub>A</sub> = 125°C | l <sub>FS</sub> +        |          | 146  | 11111111           |     |      | +15    | -15    | 30    | 0    | 18   | 11111111             |           | 24  | E <sub>87</sub>  | V    | $I_{FS}$ + = 1.992-0.01( $E_{87}$ - $E_{86}$ )                                                                                          |
|                        | IFS +                    |          | 147  | 00000000           |     |      | +15    | -15    | 30    | 0    | 18   | 11111111             | K2        | 24  | E <sub>88</sub>  | V    | $\overline{I_{FS} +} = 1.992 - 0.01(E_{88} - E_{86})$                                                                                   |
|                        | V <sub>CAL2</sub>        |          | 148  |                    |     |      | +15    | -15    | +15   | -15  | -10  | 00000000             | K3        | 24  | E <sub>89</sub>  | V    | $V_{CAL2} = E_{89}$                                                                                                                     |
|                        | I <sub>FS</sub> -        |          | 149  | 11111111           |     |      | +15    | -15    | +15   | -15  | -10  | 11111111             |           | 24  | E <sub>90</sub>  | V    | $I_{FS} = 1.992 - 0.01(E_{90} - E_{89})$                                                                                                |
|                        | IFS -                    |          | 150  | 00000000           |     |      | +15    | -15    | +15   | -15  | -10  | 11111111             | K2        | 24  | E <sub>91</sub>  | V    | IFS = 1.992-0.01(E <sub>91</sub> - E <sub>89</sub> )                                                                                    |
|                        | $\Delta I_{FSC}$         |          | 151  |                    |     |      |        |        |       |      |      |                      |           | -   |                  |      | $\Delta I_{FSC} = 1000(I_{FS} + I_{FS} -)$                                                                                              |
|                        | $\Delta \overline{IFSC}$ |          | 152  |                    |     |      |        |        |       |      |      |                      |           |     |                  |      | $\Delta \overline{\text{IFSC}} = 1000 \left(\overline{\text{IFS} + - \text{IFS} -}\right)$                                              |
|                        | V <sub>CAL3</sub>        |          | 153  | 00000000           |     |      | +15    | -15    | +15   | -15  | 0    | 00000000             |           | 24  | E <sub>92</sub>  | V    | $V_{CAL3} = E_{92}$                                                                                                                     |
|                        | V <sub>CAL4</sub>        |          | 154  | 11111111           |     |      | +15    | -15    | +15   | -15  | 0    | 11111111             |           | 24  | E <sub>93</sub>  | V    | $V_{CAL4} = E_{93}$                                                                                                                     |
|                        | V <sub>CAL5</sub>        |          | 155  | 00000000           |     |      | +15    | -15    | +15   | -15  | 0    | 11111111             | K2        | 24  | E <sub>94</sub>  | V    | $V_{CAL5} = E_{94}$                                                                                                                     |
|                        | V <sub>CAL6</sub>        |          | 156  | 11111111           |     |      | +15    | -15    | +15   | -15  | 0    | 00000000             | K2        | 24  | E <sub>95</sub>  | V    | $V_{CAL6} = E_{95}$                                                                                                                     |
|                        | NL <sub>1</sub>          |          | 157  | 10000000           |     |      | +15    | -15    | +15   | -15  | 0    | 10000000             |           | 24  | E <sub>96</sub>  | V    | $NL_{1} = \left(\begin{array}{c} \frac{\left(E_{96} - V_{CAL3}\right)}{I_{FS} \times 10^{3}} \end{array}\right) -$                      |
|                        |                          |          |      |                    |     |      |        |        |       |      |      |                      |           |     |                  |      | $\frac{(128)}{(255)} \frac{(V_{CAL4} - V_{CAL3})}{I_{FS} \times 10^3}$                                                                  |
|                        | NL₂                      |          | 158  | 01000000           |     |      | +15    | -15    | +15   | -15  | 0    | 01000000             |           | 24  | E <sub>97</sub>  | V    | $NL_{2} = \left(\begin{array}{c} \frac{\left(E_{97} - V_{CAL3}\right)}{I_{FS} \times 10^{3}} \end{array}\right) -$                      |
|                        |                          |          |      |                    |     |      |        |        |       |      |      |                      |           |     |                  |      | $\frac{(64)}{(255)} \; \frac{(V_{CAL4} - V_{CAL3})}{I_{FS} \times 10^3}$                                                                |
|                        | NL <sub>3</sub>          |          | 159  | 00100000           |     |      | +15    | -15    | +15   | -15  | 0    | 00100000             |           | 24  | E <sub>98</sub>  | V    | $NL_{3} = \left(\begin{array}{c} \left(\underline{E_{98} - V_{CAL3}}\right) \\ \overline{I_{FS} \times 10^{3}} \end{array}\right)^{-1}$ |
|                        |                          |          |      |                    |     |      |        |        |       |      |      |                      |           |     |                  |      | $\frac{(32)}{(255)} \frac{(V_{CAL4} - V_{CAL3})}{I_{FS} \times 10^3}$                                                                   |
|                        | NL₄                      |          | 160  | 00010000           |     |      | +15    | -15    | +15   | -15  | 0    | 00010000             |           | 24  | E <sub>99</sub>  | V    | $NL_{4} = \left(\begin{array}{c} \frac{\left(E_{99} - V_{CAL3}\right)}{I_{FS} \times 10^{3}} \end{array}\right) -$                      |
|                        |                          |          |      |                    |     |      |        |        |       |      |      |                      |           |     |                  |      | $\frac{(16)}{(255)} \frac{(V_{CAL4} - V_{CAL3})}{I_{FS} \times 10^3}$                                                                   |
|                        | NL <sub>5</sub>          |          | 161  | 00001000           |     |      | +15    | -15    | +15   | -15  | 0    | 00001000             |           | 24  | E <sub>100</sub> | V    | $NL_{5} = \left(\begin{array}{c} \frac{\left(E_{100} - V_{CAL3}\right)}{I_{FS} \times 10^{3}} \end{array}\right) - $                    |
|                        |                          |          |      |                    |     |      |        |        |       |      |      |                      |           |     |                  |      | $\frac{(8)}{(255)} \frac{(V_{CAL4} - V_{CAL3})}{I_{FS} \times 10^3}$                                                                    |

| Subgroup                    | Symbol          | MIL-STD-<br>883 | Test |                    |     | ,    | Adapte | ər pin | numb | ers  |      |                      | Energized | Me  | easured          | pin  |                                                                                                                                                                     |
|-----------------------------|-----------------|-----------------|------|--------------------|-----|------|--------|--------|------|------|------|----------------------|-----------|-----|------------------|------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| 5 1                         | -               | method          | No.  | 1-8<br>logic state | 9 V | 10 V | 11 V   | 12 V   | 13 V | 14 V | 15 V | 16-23<br>logic state | relays    | No. | Value            | Unit |                                                                                                                                                                     |
| 2<br>T <sub>A</sub> = 125°C | NL <sub>6</sub> |                 | 162  | 00000100           |     |      | +15    | -15    | +15  | -15  | 0    | 00000100             |           | 24  | E <sub>101</sub> | V    | $NL_{6} = \left(\begin{array}{c} \frac{\left(E_{101} - V_{CAL3}\right)}{I_{FS} \times 10^{3}} \end{array}\right) - $ $(4)  (V_{CAL4} - V_{CAL3})$                   |
|                             |                 |                 |      |                    |     |      |        |        |      | 1-   |      |                      |           |     | _                |      | (255) IFS×10 <sup>3</sup>                                                                                                                                           |
|                             | NL <sub>7</sub> |                 | 163  | 00000010           |     |      | +15    | -15    | +15  | -15  | 0    | 00000010             |           | 24  | E <sub>102</sub> | V    | $NL_{7} = \left(\begin{array}{c} \frac{(E_{102} - V_{CAL3})}{I_{FS} \times 10^{3}} \end{array}\right) - $ $(2)  (V_{CAL4} - V_{CAL3})$                              |
|                             |                 |                 |      |                    |     |      |        |        |      |      |      |                      |           |     |                  |      | $\frac{(2)}{(255)} (1000000000000000000000000000000000000$                                                                                                          |
|                             | NL <sub>8</sub> |                 | 164  | 00000001           |     |      | +15    | -15    | +15  | -15  | 0    | 00000001             |           | 24  | E <sub>103</sub> | V    | $NL_8 = \left( \begin{array}{c} \frac{\left(E_{103} - V_{CAL3}\right)}{I_{FS} \times 10^3} \end{array} \right) -$                                                   |
|                             |                 |                 |      |                    |     |      |        |        |      |      |      |                      |           |     |                  |      | $\frac{(1)}{(255)} \frac{(VCAL4 - VCAL3)}{IES \times 10^3}$                                                                                                         |
|                             | NL1             |                 | 165  | 01111111           |     |      | +15    | -15    | +15  | -15  | 0    | 10000000             |           | 24  | E <sub>104</sub> | V    | $\overline{\text{NL}_{1}} = \left(\begin{array}{c} \frac{(\text{E}_{104} - \text{V}_{\text{CAL5}})}{\text{I}_{\text{FS}} \times 10^{3}} \end{array}\right) - $      |
|                             |                 |                 |      |                    |     |      |        |        |      |      |      |                      |           |     |                  |      | $\frac{(128)}{(255)} \frac{(VCAL6 - VCAL5)}{IFE \times 10^3}$                                                                                                       |
|                             | NL2             |                 | 166  | 10111111           |     |      | +15    | -15    | +15  | -15  | 0    | 01000000             |           | 24  | E <sub>105</sub> | V    | $\overline{NL_2} = \left( \begin{array}{c} (\underline{E_{105} - V_{CAL5})} \\ \overline{IFS \times 10^3} \end{array} \right) - $                                   |
|                             |                 |                 |      |                    |     |      |        |        |      |      |      |                      |           |     |                  |      | $\frac{(64)}{(255)} \frac{(V_{CAL6} - V_{CAL5})}{I_{FS} \times 10^3}$                                                                                               |
|                             | NL3             |                 | 167  | 11011111           |     |      | +15    | -15    | +15  | -15  | 0    | 00100000             |           | 24  | E <sub>106</sub> | V    | $\overline{\text{NL}_3} = \left( \begin{array}{c} \frac{\left(\text{E}_{106} - \text{V}_{\text{CAL5}}\right)}{\text{IFS} \times 10^3} \end{array} \right) \text{-}$ |
|                             |                 |                 |      |                    |     |      |        |        |      |      |      |                      |           |     |                  |      | $\frac{(32)}{(255)} \frac{(V_{CAL6} - V_{CAL5})}{I_{FS} \times 10^3}$                                                                                               |
|                             | NL4             |                 | 168  | 11101111           |     |      | +15    | -15    | +15  | -15  | 0    | 00010000             |           | 24  | E <sub>107</sub> | V    | $\overline{NL4} = \left( \begin{array}{c} \frac{\left(E_{107} - V_{CAL5}\right)}{I_{FS} \times 10^3} \end{array} \right) \text{-}$                                  |
|                             |                 |                 |      |                    |     |      |        |        |      |      |      |                      |           |     |                  |      | $\frac{(16)}{(255)} \frac{(VCAL6 - VCAL5)}{IFS \times 10^3}$                                                                                                        |
|                             | NL5             |                 | 169  | 11110111           |     |      | +15    | -15    | +15  | -15  | 0    | 00001000             |           | 24  | E <sub>108</sub> | V    | $\overline{NL_5} = \left( \begin{array}{c} \underline{\left( E_{108} - V_{CAL5} \right)} \\ \overline{I_{FS} \times 10^3} \end{array} \right) \text{-}$             |
|                             |                 |                 |      |                    |     |      |        |        |      |      |      |                      |           |     |                  |      | $\frac{(8)}{(255)} \frac{(V_{CAL6} - V_{CAL5})}{I_{FS} \times 10^3}$                                                                                                |
|                             | NL6             |                 | 170  | 11111011           |     |      | +15    | -15    | +15  | -15  | 0    | 00000100             |           | 24  | E <sub>109</sub> | V    | $\overline{\text{NL}_6} = \left( \begin{array}{c} \frac{\left(\text{E}_{109} - \text{V}_{\text{CAL5}}\right)}{\text{IFS} \times 10^3} \end{array} \right) \text{-}$ |
|                             |                 |                 |      |                    |     |      |        |        |      |      |      |                      |           |     |                  |      | $\frac{(4)}{(255)} \frac{(V_{CAL6} - V_{CAL5})}{I_{FS} \times 10^3}$                                                                                                |

| Subgroup                    | Symbol                          | MIL-STD-<br>883 | Test |             |     | ļ    | Adapte | er pin | numbe | ers  |      |             | Energized | Me | asured           | pin   | Equation                                                                                                                                                   |
|-----------------------------|---------------------------------|-----------------|------|-------------|-----|------|--------|--------|-------|------|------|-------------|-----------|----|------------------|-------|------------------------------------------------------------------------------------------------------------------------------------------------------------|
|                             |                                 | method          | NO.  | 1-8         |     |      |        |        |       |      |      | 16-23       | relays    | No | Value            | Unit  |                                                                                                                                                            |
|                             |                                 |                 |      | logic state | 9 V | 10 V | 11 V   | 12 V   | 13 V  | 14 V | 15 V | logic state |           |    | value            | Unit. |                                                                                                                                                            |
| 2<br>T <sub>A</sub> = 125°C | NL7                             |                 | 171  | 11111101    |     |      | +15    | -15    | +15   | -15  | 0    | 00000010    |           | 24 | E <sub>110</sub> | V     | $\overline{\text{NL7}} = \left( \begin{array}{c} \frac{(\text{E}_{110} - \text{V}_{\text{CAL5}})}{\text{I}_{\text{ES}} \times 10^3} \end{array} \right) -$ |
|                             |                                 |                 |      |             |     |      |        |        |       |      |      |             |           |    |                  |       | $\frac{(2)}{(255)} \frac{(VCAL6 - VCAL5)}{1 - 2 - 2 - 2 - 2}$                                                                                              |
|                             | NI a                            |                 | 172  | 11111110    |     |      | +15    | -15    | +15   | -15  | 0    | 00000001    |           | 24 | E <sub>111</sub> | V     | $(=10)  \text{IFS} \times 10  (=111 - \text{VCAL5})$                                                                                                       |
|                             | IVES                            |                 |      |             |     |      |        |        |       |      |      |             |           |    |                  |       | $NL_8 = \left( \frac{(L_1 + V_0) L_0}{1 FS \times 10^3} \right)^{-1}$                                                                                      |
|                             |                                 |                 |      |             |     |      |        |        |       |      |      |             |           |    |                  |       | $\frac{(1)}{(255)} \frac{(V_{CAL6} - V_{CAL5})}{I_{FS} \times 10^3}$                                                                                       |
|                             | $\Sigma NL^+$                   |                 | 173  |             |     |      |        |        |       |      |      |             |           |    |                  |       | $\Sigma NL^+ = NL_i + NL_K +$<br>(i, k, bits having positive errors)                                                                                       |
|                             | $\overline{\Sigma NL^+}$        |                 | 174  |             |     |      |        |        |       |      |      |             |           |    |                  |       | $\overline{\Sigma NL^{+}} = \overline{NLi^{1}} + \overline{NLk^{1}} + \dots$ (i, k, bits having positive errors)                                           |
|                             | ΣNL                             |                 | 175  |             |     |      |        |        |       |      |      |             |           |    |                  |       | $\Sigma NL^{-} = NL_m + NL_n +$<br>(m, n, bits having negative errors)                                                                                     |
|                             | $\Sigma NL^{-}$                 |                 | 176  |             |     |      |        |        |       |      |      |             |           |    |                  |       | $\overline{\Sigma NL^{-}} = \overline{NLm^{1}} + \overline{NLn^{1}} + \dots$ (m, n, bits having negative errors)                                           |
|                             | ΔΣNL                            |                 | 177  |             |     |      |        |        |       |      |      |             |           |    |                  |       | $\Delta \Sigma NL = \left  \Sigma NL^+ \right  - \left  \Sigma NL^- \right $                                                                               |
|                             | $\Delta \Sigma \overline{NL}$   |                 | 178  |             |     |      |        |        |       |      |      |             |           |    |                  |       | $\Delta \Sigma \overline{NL} = \left  \Sigma \overline{NL}^+ \right  - \left  \Sigma \overline{NL}^- \right $                                              |
|                             | NL⁺                             |                 | 179  |             |     |      |        |        |       |      |      |             |           |    |                  |       | $NL^{+} = \left  \Sigma NL^{+} \right  + \left  \Delta \Sigma NL \right $                                                                                  |
|                             | NL <sup>+</sup>                 |                 | 180  |             |     |      |        |        |       |      |      |             |           |    |                  |       | $\overline{NL^+} = \left  \Sigma \overline{NL}^+ \right  + \left  \Delta \Sigma \overline{NL} \right $                                                     |
|                             | NL                              |                 | 181  |             |     |      |        |        |       |      |      |             |           |    |                  |       | $NL^{-} = \left  \Sigma NL^{-} \right  + \left  \Delta \Sigma NL \right $                                                                                  |
|                             | <br>NL <sup></sup>              |                 | 182  |             |     |      |        |        |       |      |      |             |           |    |                  |       | $\overline{NL^{-}} = \left  \Sigma \overline{NL}^{-} \right  + \left  \Delta \Sigma \overline{NL} \right $                                                 |
|                             | (l <sub>01</sub> )a             |                 | 183  | 1000000     |     |      | +15    | -15    | +15   | -15  | 0    | 10000000    |           | 24 | E <sub>112</sub> | V     | $(I_{01})_a = I_{FS} X \frac{128}{255} - 0.01(E_{112})$                                                                                                    |
|                             | (l <sub>01</sub> ) <sub>b</sub> |                 | 184  | 01111111    |     |      | +15    | -15    | +15   | -15  | 0    | 01111111    |           | 24 | E <sub>113</sub> | V     | $(I_{01})_{b} = I_{FS} X \frac{127}{255} - 0.01(E_{113})$                                                                                                  |
|                             | $\Delta(I_{01})$                |                 | 185  |             |     |      |        |        |       |      |      |             |           |    |                  |       | $\Delta(I_{01}) = [(I_{01})_{a} - (I_{01})_{b}] \times 10^{3}$                                                                                             |

| Subgroup                    | Symbol                          | MIL-STD-<br>883 | Test |                    |     | ŀ    | Adapte | er pin i | numbe | ers  |      |                      | Energized | Me  | asured           | pin  | Equation                                                       |
|-----------------------------|---------------------------------|-----------------|------|--------------------|-----|------|--------|----------|-------|------|------|----------------------|-----------|-----|------------------|------|----------------------------------------------------------------|
|                             |                                 | method          | No.  |                    |     |      |        |          |       |      |      |                      | relays    |     |                  |      |                                                                |
|                             |                                 |                 |      | 1-8<br>logic state | 9 V | 10 V | 11 V   | 12 V     | 13 V  | 14 V | 15 V | 16-23<br>logic state |           | No. | Value            | Unit |                                                                |
| 2<br>T <sub>A</sub> = 125°C | (I <sub>02</sub> ) <sub>a</sub> |                 | 186  | 01000000           |     |      | +15    | -15      | +15   | -15  | 0    | 01000000             |           | 24  | E <sub>114</sub> | V    | $(I_{02})_a = I_{FS} \times \frac{64}{255} - 0.01(E_{114})$    |
|                             | (I <sub>02</sub> ) <sub>b</sub> |                 | 187  | 00111111           |     |      | +15    | -15      | +15   | -15  | 0    | 00111111             |           | 24  | E <sub>115</sub> | V    | $(I_{02})_{b} = I_{FS} X \frac{63}{255} - 0.01(E_{115})$       |
|                             | $\Delta(I_{02})$                |                 | 188  |                    |     |      |        | -        |       |      |      |                      |           |     |                  |      | $\Delta(I_{02}) = [(I_{02})_a - (I_{02})_b] \times 10^3$       |
|                             | (I <sub>03</sub> ) <sub>a</sub> |                 | 189  | 00100000           |     |      | +15    | -15      | +15   | -15  | 0    | 00100000             |           | 24  | E <sub>116</sub> | V    | $(I_{03})_a = I_{FS} X \frac{32}{255} - 0.01(E_{116})$         |
|                             | (I <sub>03</sub> ) <sub>b</sub> |                 | 190  | 00011111           |     |      | +15    | -15      | +15   | -15  | 0    | 00011111             |           | 24  | E <sub>117</sub> | V    | $(I_{03})_{b} = I_{FS} X \frac{31}{255} - 0.01(E_{117})$       |
|                             | $\Delta(I_{03})$                |                 | 191  |                    |     |      |        |          |       |      |      |                      |           |     |                  |      | $\Delta(I_{03}) = [(I_{03})_{a} - (I_{03})_{b}] \times 10^{3}$ |
|                             | (I <sub>04</sub> ) <sub>a</sub> |                 | 192  | 00010000           |     |      | +15    | -15      | +15   | -15  | 0    | 00010000             |           | 24  | E <sub>118</sub> | V    | $(I_{04})_a = I_{FS} X \frac{16}{255} - 0.01(E_{118})$         |
|                             | (I <sub>04</sub> ) <sub>b</sub> |                 | 193  | 00001111           |     |      | +15    | -15      | +15   | -15  | 0    | 00001111             |           | 24  | E <sub>119</sub> | V    | $(I_{04})_{b} = I_{FS} X \frac{15}{255} - 0.01(E_{119})$       |
|                             | $\Delta(I_{04})$                |                 | 194  |                    |     |      |        | -        |       |      |      |                      |           |     |                  |      | $\Delta(I_{04}) = [(I_{04})_{a} - (I_{04})_{b}] \times 10^{3}$ |
|                             | (I <sub>05</sub> ) <sub>a</sub> |                 | 195  | 00001000           |     |      | +15    | -15      | +15   | -15  | 0    | 00001000             |           | 24  | E <sub>120</sub> | V    | $(I_{05})_a = I_{FS} X \frac{8}{255} - 0.01(E_{120})$          |
|                             | (I <sub>05</sub> )ь             |                 | 196  | 00000111           |     |      | +15    | -15      | +15   | -15  | 0    | 00000111             |           | 24  | E <sub>121</sub> | V    | $(I_{05})_{b} = I_{FS} X \frac{7}{255} - 0.01(E_{121})$        |
|                             | $\Delta(I_{05})$                |                 | 197  |                    |     |      |        | -        |       |      |      |                      |           |     |                  |      | $\Delta(I_{05}) = [(I_{05})_{a} - (I_{05})_{b}] \times 10^{3}$ |
|                             | (I <sub>06</sub> ) <sub>a</sub> |                 | 198  | 00000100           |     |      | +15    | -15      | +15   | -15  | 0    | 00000100             |           | 24  | E <sub>122</sub> | V    | $(I_{06})_a = I_{FS} X \frac{4}{255} - 0.01(E_{122})$          |
|                             | (I <sub>06</sub> )ь             |                 | 199  | 00000011           |     |      | +15    | -15      | +15   | -15  | 0    | 00000011             |           | 24  | E <sub>123</sub> | V    | $(I_{06})_{b} = I_{FS} X \frac{3}{255} - 0.01(E_{123})$        |
|                             | $\Delta(I_{06})$                |                 | 200  |                    |     |      |        | -        |       |      |      |                      |           |     |                  |      | $\Delta(I_{06}) = [(I_{06})_{a} - (I_{06})_{b}] \times 10^{3}$ |
|                             | (I <sub>07</sub> ) <sub>a</sub> |                 | 201  | 00000010           |     |      | +15    | -15      | +15   | -15  | 0    | 00000010             |           | 24  | E <sub>124</sub> | V    | $(I_{07})_a = I_{FS} X \frac{2}{255} - 0.01(E_{124})$          |
|                             | (I <sub>07</sub> ) <sub>b</sub> |                 | 202  | 00000001           |     |      | +15    | -15      | +15   | -15  | 0    | 00000001             |           | 24  | E <sub>125</sub> | V    | $(I_{07})_{b} = I_{FS} X \frac{1}{255} - 0.01(E_{125})$        |
|                             | $\Delta(I_{07})$                |                 | 203  |                    |     |      |        |          |       |      |      |                      |           |     |                  |      | $\Delta(I_{07}) = [(I_{07})_{a} - (I_{07})_{b}] \times 10^{3}$ |
|                             | (I <sub>08</sub> )ь             |                 | 204  | 00000000           |     |      | +15    | -15      | +15   | -15  | 0    | 00000000             |           | 24  | E <sub>126</sub> | V    | $(I_{08})_{b} = I_{FS} X \frac{1}{255} - 0.01(E_{126})$        |
|                             | (l <sub>08</sub> )              |                 | 205  |                    |     |      |        |          |       |      |      |                      |           |     |                  |      | $\Delta(I_{08}) = [(I_{07})_{b} - (I_{08})_{b}] \times 10^3$   |
|                             | $\Delta I_{FS}$                 |                 | 206  |                    |     |      |        |          |       |      |      |                      |           |     |                  |      | $I_{FS} - \overline{I_{FS}} = \Delta I_{FS}$                   |

|                        |                                    |                 |                |                    |     |      |        |        |       |      |      |                      |            |     |                  |      |                                                                              | _        |
|------------------------|------------------------------------|-----------------|----------------|--------------------|-----|------|--------|--------|-------|------|------|----------------------|------------|-----|------------------|------|------------------------------------------------------------------------------|----------|
| Subgroup               | Symbol                             | MIL-STD-<br>883 | Test           |                    |     | ļ    | Adapte | er pin | numbe | ers  |      |                      | Energized  | Me  | asured           | pin  | Equation                                                                     |          |
| 0 1                    |                                    | method          | No.            | 1-8<br>logic state | 9 V | 10 V | 11 V   | 12 V   | 13 V  | 14 V | 15 V | 16-23<br>logic state | relays     | No. | Value            | Unit |                                                                              |          |
| 3                      | I <sub>cc</sub> +                  | 3005            | 207            | 11111111           | -   |      | +15    | -15    | +15   | -15  | 0    |                      |            | 11  | I <sub>39</sub>  | mΑ   | $I_{cc} + = I_{39}$                                                          |          |
| T <sub>A</sub> = -55°C | I <sub>cc</sub> -                  |                 | 208            | 11111111           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 12  | I <sub>40</sub>  | mΑ   | $I_{CC} = I_{40}$                                                            |          |
|                        | I <sub>FS</sub>                    |                 | 209 <u>1</u> / | 11111111           |     |      | +15    | -15    | +15   | -15  | 0    | 11111111             |            | 24  | E <sub>127</sub> | V    | I <sub>FS</sub> = 1.992-0.01E <sub>127</sub>                                 |          |
|                        | IFS                                |                 | 210            | 00000000           | -   |      | +15    | -15    | +15   | -15  | 0    | 11111111             | K2         | 24  | E <sub>128</sub> | V    | <br>IFS = 1.992-0.01E <sub>128</sub>                                         |          |
|                        | lzs                                |                 | 211            | 00000000           | -   |      | +15    | -15    | +15   | -15  | 0    |                      | K4         | 24  | E <sub>129</sub> | V    | $I_{ZS} = -10E_{129}$                                                        |          |
|                        | Izs                                |                 | 212            | 11111111           | -   |      | +15    | -15    | +15   | -15  | 0    |                      | K2, K4     | 24  | E <sub>130</sub> | V    | Izs = -10E <sub>130</sub>                                                    |          |
|                        | P <sub>ss</sub> I <sub>Fs</sub> +1 |                 | 213            | 11111111           |     |      | 5.5    | -18    | +15   | -15  | 0    | 11111111             |            | 24  | E <sub>131</sub> | V    | $P_{SS}I_{FS}+1 = -10(E_{131}-E_{132})$                                      |          |
|                        |                                    |                 | 214            | 11111111           | -   |      | 4.5    | -18    | +15   | -15  | 0    | 11111111             |            | 24  | E <sub>132</sub> | V    |                                                                              |          |
|                        | PssIFs + 1                         |                 | 215            | 00000000           |     |      | 5.5    | -18    | +15   | -15  | 0    | 11111111             | K2         | 24  | E <sub>133</sub> | V    | PssIFs + 1 = -10(E <sub>133</sub> -E <sub>134</sub> )                        |          |
|                        |                                    |                 | 216            | 00000000           |     |      | 4.5    | -18    | +15   | -15  | 0    | 11111111             | K2         | 24  | E <sub>134</sub> | V    |                                                                              |          |
|                        | P <sub>ss</sub> I <sub>Fs</sub> +2 |                 | 217            | 11111111           |     |      | 18     | -18    | +15   | -15  | 0    | 11111111             |            | 24  | E <sub>135</sub> | V    | $P_{ss}I_{Fs}+2 = -10(E_{135}-E_{136})$                                      | L        |
|                        |                                    |                 | 218            | 11111111           |     |      | 12     | -18    | +15   | -15  | 0    | 11111111             |            | 24  | E <sub>136</sub> | V    |                                                                              | L        |
|                        | $\overline{\text{PssIFs}+2}$       |                 | 219            | 00000000           |     |      | 18     | -18    | +15   | -15  | 0    | 11111111             | K2         | 24  | E <sub>137</sub> | V    | $\overline{\text{Psslfs}+2}$ = -10(E <sub>137</sub> -E <sub>138</sub> )      |          |
|                        |                                    |                 | 220            | 00000000           |     |      | 12     | -18    | +15   | -15  | 0    | 11111111             | K2         | 24  | E <sub>138</sub> | V    |                                                                              | _        |
|                        | P <sub>SS</sub> I <sub>FS</sub> -1 |                 | 221            | 11111111           |     |      | 18     | -12    | +15   | -15  | 0    | 11111111             |            | 24  | E <sub>139</sub> | V    | $P_{SS}I_{FS}-1=-10(E_{139}-E_{135})$                                        | L        |
|                        | PssIFs – 1                         |                 | 222            | 00000000           |     |      | 18     | -12    | +15   | -15  | 0    | 11111111             | K2         | 24  | E <sub>140</sub> | V    | Psslfs - 1 = -10(E <sub>140</sub> -E <sub>137</sub> )                        |          |
|                        | P <sub>ss</sub> I <sub>Fs</sub> -2 |                 | 223            | 11111111           |     |      | 18     | -5.5   | +15   | -15  | 0    | 11111111             | K5         | 24  | E <sub>141</sub> | V    | P <sub>SS</sub> I <sub>FS</sub> -2= -10(E <sub>141</sub> -E <sub>142</sub> ) |          |
|                        |                                    |                 | 224            | 11111111           |     |      | 18     | -4.5   | +15   | -15  | 0    | 11111111             | K5         | 24  | E <sub>142</sub> | V    |                                                                              | <u> </u> |
|                        | PsslFs – 2                         |                 | 225            | 00000000           |     |      | 18     | -5.5   | +15   | -15  | 0    | 11111111             | K2, K5     | 24  | E <sub>143</sub> | V    | Psslfs - 2 = -10(E <sub>143</sub> -E <sub>144</sub> )                        |          |
|                        | - 6                                |                 | 226            | 00000000           |     |      | 18     | -4.5   | +15   | -15  | 0    | 11111111             | K2, K5     | 24  | E <sub>144</sub> | V    |                                                                              | _        |
|                        |                                    |                 | 227            | 00000000           | 15  |      | +15    | -10    | 30    | -5   | 0    |                      | K1, K4     | 26  | E <sub>145</sub> | V    | $I_{FS}R_1 = 0.2E_{145}$                                                     | +        |
|                        | IFSR1                              |                 | 228            | 11111111           | 15  |      | +15    | -10    | 30    | -5   | 0    |                      | K1, K2, K4 | 26  | E146             | V    | $IFSR1 = 0.2E_{146}$                                                         | L        |
|                        | IFSR2                              |                 | 229            | 00000000           | 20  |      | +15    | -12    | 30    | -5   | 0    |                      | K1, K4     | 20  | ⊑147<br>⊑        | V    | $I_{FSR_2} = 0.2E_{147}$                                                     | +        |
|                        | IFSR2                              |                 | 230            | 00000000           | 25  |      | +15    | -12    | 30    | -0   | 0    |                      | K1, K2, K4 | 20  | ⊏148             | V    | $IFSR_2 = 0.2E_{148}$                                                        |          |
|                        | IREF-                              |                 | 231            | 00000000           |     | 0    | +15    | -15    | +15   | -15  | 0    |                      | K3         | 10  | I <sub>41</sub>  | A    | $I_{REF} = I_{41} \times 10$                                                 | -        |
|                        | liH1                               |                 | <u>232</u>     | 1000000            |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 1   | 42               | A    | $I_{\text{IH}1} = I_{42}X \ 10$                                              | -        |
|                        | I <sub>IH2</sub>                   |                 | <u>233 Z/</u>  | 01000000           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 2   | 43               | A    | $I_{1H2} = I_{43} \land 10$                                                  |          |
|                        | IIH3                               |                 | 234 <u>2/</u>  | 00100000           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 3   | I <sub>44</sub>  | A    | $I_{1H3} = I_{44} \land I \cup$                                              | -        |
|                        | IIH4                               |                 | 235 <u>2/</u>  | 00010000           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 4   | 45               | A    | $I_{1H4} = I_{45} \land IU$                                                  | -        |
|                        | I <sub>IH5</sub>                   |                 | 236 <u>2</u> / | 00001000           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 5   | 46               | A    | $I_{1H5} = I_{46}X \ 10$                                                     |          |
|                        | IIH6                               |                 | <u>237 </u> 2/ | 00000100           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 0   | 47               | A    | $I_{1H6} = I_{47} \land IO$                                                  |          |
|                        |                                    |                 | 238 <u>2</u> / | 00000010           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | /   | 1 <sub>48</sub>  | A    | $I_{1H7} = I_{48} \times 10^{-10}$                                           | -        |
|                        | I <sub>IH8</sub>                   |                 | 239 <u>2</u> / | 0000001            |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 8   | I <sub>49</sub>  | A    | $I_{1H8} = I_{49} \times 10^{-10}$                                           |          |
|                        | I <sub>IL1</sub>                   |                 | 240 <u>2</u> / | 01111111           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 1   | 1 <sub>50</sub>  | A    | $I_{1L1} = I_{50} \times 10^{5}$                                             | <u> </u> |
|                        | I <sub>IL2</sub>                   |                 | 241 <u>2</u> / | 10111111           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 2   | 1 <sub>51</sub>  | A    | $I_{1L2} = I_{51} X 10^{\circ}$                                              | <u> </u> |
|                        | I <sub>IL3</sub>                   |                 | 242 <u>2</u> / | 11011111           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 3   | 1 <sub>52</sub>  | A    | $I_{1L3} = I_{52} \times 10^{\circ}$                                         | ┡        |
|                        | I <sub>IL4</sub>                   |                 | 243 <u>2</u> / | 11101111           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 4   | I <sub>53</sub>  | A    | $I_{IL4} = I_{53} X 10^{\circ}$                                              | Ļ        |
|                        | I <sub>IL5</sub>                   |                 | <u>244 2</u> / | 11110111           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 5   | 1 <sub>54</sub>  | A    | $I_{IL5} = I_{54} \times 10^{\circ}$                                         | ┡        |
|                        | I <sub>IL6</sub>                   |                 | 245 <u>2</u> / | 11111011           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 6   | 1 <sub>55</sub>  | A    | $I_{IL6} = I_{55} \times 10^{\circ}$                                         | L        |
|                        | I <sub>IL7</sub>                   |                 | 246 <u>2</u> / | 11111101           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 7   | 1 <sub>56</sub>  | Α    | $I_{IL7} = I_{56} \times 10^{\circ}$                                         | L        |
|                        | I <sub>IL8</sub>                   |                 | 247 <u>2</u> / | 11111110           |     |      | +15    | -15    | +15   | -15  | 0    |                      |            | 8   | I <sub>57</sub>  | Α    | I <sub>IL8</sub> = I <sub>57</sub> X 10°                                     | 1        |

| Subaroup               | Symbol            | MIL-STD- | Test |                    |     | A    | Adapte | er pin | numbe | ers  |      |                      | Eneraized | Me  | asured           | pin  | Equation                                                                                                            |
|------------------------|-------------------|----------|------|--------------------|-----|------|--------|--------|-------|------|------|----------------------|-----------|-----|------------------|------|---------------------------------------------------------------------------------------------------------------------|
|                        | -,                | method   | No.  | 1-8<br>logic state | 9 V | 10 V | 11 V   | 12 V   | 13 V  | 14 V | 15 V | 16-23<br>logic state | relays    | No. | Value            | Unit |                                                                                                                     |
| 3                      | V <sub>CAL1</sub> |          | 248  |                    |     |      | +15    | -15    | 30    | 0    | 18   | 00000000             | K3        | 24  | E <sub>149</sub> | V    | $V_{CAL1} = E_{149}$                                                                                                |
| T <sub>A</sub> = -55°C | I <sub>FS</sub> + |          | 249  | 11111111           |     |      | +15    | -15    | 30    | 0    | 18   | 11111111             |           | 24  | E <sub>150</sub> | V    | I <sub>FS</sub> + =1.992-0.01(E <sub>150</sub> -E <sub>149</sub> )                                                  |
|                        | IFS +             |          | 250  | 00000000           |     |      | +15    | -15    | 30    | 0    | 18   | 11111111             | K2        | 24  | E <sub>151</sub> | V    | $\overline{I_{FS}}$ = 1.992-0.01(E <sub>151</sub> - E <sub>149</sub> )                                              |
|                        | V <sub>CAL2</sub> |          | 251  |                    |     |      | +15    | -15    | +15   | -15  | -10  | 00000000             | K3        | 24  | E <sub>152</sub> | V    | $V_{CAL2} = E_{152}$                                                                                                |
|                        | I <sub>FS</sub> - |          | 252  | 11111111           |     |      | +15    | -15    | +15   | -15  | -10  | 11111111             |           | 24  | E <sub>153</sub> | V    | $I_{FS}$ = 1.992-0.01( $E_{153}$ - $E_{152}$ )                                                                      |
|                        | IFS -             |          | 253  | 00000000           |     |      | +15    | -15    | +15   | -15  | -10  | 11111111             | K2        | 24  | E <sub>154</sub> | V    | IFS - = 1.992-0.01(E <sub>154</sub> -E <sub>152</sub> )                                                             |
|                        | ∆l <sub>FSC</sub> |          | 254  |                    |     |      |        |        |       |      |      |                      |           |     |                  |      | $\Delta I_{FSC} = 1000(I_{FS} + -I_{FS} -)$                                                                         |
|                        |                   |          | 255  |                    |     |      |        |        |       |      |      |                      |           |     |                  |      | $\Delta \overline{\text{IFSC}} = 1000 (\overline{\text{IFS} + - \text{IFS} -})$                                     |
|                        | V <sub>CAL3</sub> |          | 256  | 00000000           |     |      | +15    | -15    | +15   | -15  | 0    | 00000000             |           | 24  | E <sub>155</sub> | V    | $V_{CAL3} = E_{155}$                                                                                                |
|                        | V <sub>CAL4</sub> |          | 257  | 11111111           |     |      | +15    | -15    | +15   | -15  | 0    | 11111111             |           | 24  | E <sub>156</sub> | V    | $V_{CAL4} = E_{156}$                                                                                                |
|                        | V <sub>CAL5</sub> |          | 258  | 00000000           |     |      | +15    | -15    | +15   | -15  | 0    | 11111111             | K2        | 24  | E <sub>157</sub> | V    | $V_{CAL5} = E_{157}$                                                                                                |
|                        | V <sub>CAL6</sub> |          | 259  | 11111111           | -   |      | +15    | -15    | +15   | -15  | 0    | 00000000             | K2        | 24  | E <sub>158</sub> | V    | $V_{CAL6} = E_{158}$                                                                                                |
|                        | NL <sub>1</sub>   |          | 260  | 10000000           |     |      | +15    | -15    | +15   | -15  | 0    | 10000000             |           | 24  | E <sub>159</sub> | V    | $NL_{1} = \left(\begin{array}{c} (E_{159} - V_{CAL3}) \\ I_{FS} \times 10^{3} \end{array}\right) -$                 |
|                        |                   |          |      |                    |     |      |        |        |       |      |      |                      |           |     |                  |      | $\frac{(128)}{(255)} \frac{(V_{CAL4} - V_{CAL3})}{I_{FS} \times 10^3}$                                              |
|                        | NL <sub>2</sub>   |          | 261  | 01000000           |     |      | +15    | -15    | +15   | -15  | 0    | 01000000             |           | 24  | E <sub>160</sub> | V    | $NL_{2} = \left(\begin{array}{c} \frac{\left(E_{160} - V_{CAL3}\right)}{I_{FS} \times 10^{3}} \end{array}\right) -$ |
|                        |                   |          |      |                    |     |      |        |        |       |      |      |                      |           |     |                  |      | $\frac{(64)}{(255)} \frac{(V_{CAL4} - V_{CAL3})}{I_{FS} \times 10^3}$                                               |
|                        | NL <sub>3</sub>   |          | 262  | 00100000           |     |      | +15    | -15    | +15   | -15  | 0    | 00100000             |           | 24  | E <sub>161</sub> | V    | $NL_{3} = \left(\begin{array}{c} \frac{\left(E_{161} - V_{CAL3}\right)}{I_{FS} \times 10^{3}} \end{array}\right) -$ |
|                        |                   |          |      |                    |     |      |        |        |       |      |      |                      |           |     |                  |      | $\frac{(32)}{(255)} \frac{(V_{CAL4} - V_{CAL3})}{I_{FS} \times 10^3}$                                               |
|                        | NL₄               |          | 263  | 00010000           |     |      | +15    | -15    | +15   | -15  | 0    | 00010000             |           | 24  | E <sub>162</sub> | V    | $NL_{4} = \left(\begin{array}{c} \left(E_{162} - V_{CAL3}\right) \\ I_{FS} \times 10^{3} \end{array}\right) -$      |
|                        |                   |          |      |                    |     |      |        |        |       |      |      |                      |           |     |                  |      | $\frac{(16)}{(255)} \frac{(V_{CAL4} - V_{CAL3})}{I_{FS} \times 10^3}$                                               |
|                        | NL5               |          | 264  | 00001000           |     |      | +15    | -15    | +15   | -15  | 0    | 00001000             |           | 24  | E <sub>163</sub> | V    | $NL_{5} = \left( \begin{array}{c} \underline{(E_{163} - V_{CAL3})} \\ I_{FS} \times 10^{3} \end{array} \right) -$   |
|                        |                   |          |      |                    |     |      |        |        |       |      |      |                      |           |     |                  |      | $\frac{(8)}{(255)} \frac{(V_{CAL4} - V_{CAL3})}{I_{FS} \times 10^3}$                                                |

| Subaroup                    | Symbol          | MIL-STD-<br>883 | Test |                    |     | ,    | Adapte | er pin | numbe | ers  |      |                      | Eneraized | Me  | asured           | pin  | Equation                                                                                                                                                                                                                                                                                                                                                          |
|-----------------------------|-----------------|-----------------|------|--------------------|-----|------|--------|--------|-------|------|------|----------------------|-----------|-----|------------------|------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
|                             | -,              | method          | No.  | 1-8<br>logic state | 9 V | 10 V | 11 V   | 12 V   | 13 V  | 14 V | 15 V | 16-23<br>logic state | relays    | No. | Value            | Unit |                                                                                                                                                                                                                                                                                                                                                                   |
| 3<br>T <sub>A</sub> = -55°C | NL <sub>6</sub> |                 | 265  | 00000100           |     |      | +15    | -15    | +15   | -15  | 0    | 00000100             |           | 24  | E <sub>164</sub> | V    | $\begin{split} NL_6 &= \left( \begin{array}{c} \frac{\left(E_{164} - V_{CAL3}\right)}{I_{FS} \times 10^3} \end{array} \right) \text{-} \\ \frac{(4)}{(255)} & \frac{\left(V_{CAL4} - V_{CAL3}\right)}{I_{FS} \times 10^3} \end{split}$                                                                                                                            |
|                             | NL7             |                 | 266  | 00000010           |     |      | +15    | -15    | +15   | -15  | 0    | 00000010             |           | 24  | E <sub>165</sub> | V    | $NL_{7} = \left( \begin{array}{c} \frac{(E_{165} - V_{CAL3})}{I_{FS} \times 10^{3}} \end{array} \right) - \frac{(2)}{(255)} \frac{(V_{CAL4} - V_{CAL3})}{I_{FS} \times 10^{3}}$                                                                                                                                                                                   |
|                             | NL <sub>8</sub> |                 | 267  | 00000001           |     |      | +15    | -15    | +15   | -15  | 0    | 00000001             |           | 24  | E <sub>166</sub> | V    | $\begin{split} NL_8 = \left( \begin{array}{c} \frac{\left(E_{166} - V_{CAL3}\right)}{I_{FS} \times 10^3} \end{array} \right) - \\ \frac{(1)}{(255)} \begin{array}{c} \frac{\left(V_{CAL4} - V_{CAL3}\right)}{I_{FS} \times 10^3} \end{array} \end{split}$                                                                                                         |
|                             | NL1             |                 | 268  | 01111111           |     |      | +15    | -15    | +15   | -15  | 0    | 1000000              |           | 24  | E <sub>167</sub> | V    | $\overline{\text{NL}_{1}} = \left( \begin{array}{c} \frac{(\text{E}_{167} - \text{V}_{\text{CAL5}})}{\text{I}_{\text{FS}} \times 10^{3}} \end{array} \right) - \frac{(128)}{(255)} \frac{(\text{V}_{\text{CAL6}} - \text{V}_{\text{CAL5}})}{\text{I}_{\text{FS}} \times 10^{3}}$                                                                                  |
|                             | NL2             |                 | 269  | 10111111           |     |      | +15    | -15    | +15   | -15  | 0    | 0100000              |           | 24  | E <sub>168</sub> | V    | $\overline{\text{NL}_2} = \left(\begin{array}{c} \frac{\left(\text{E}_{168} - \text{V}_{\text{CAL5}}\right)}{\text{I}_{\text{FS}} \times 10^3} \end{array}\right) - \frac{(64)}{(255)} \frac{(\text{V}_{\text{CAL6}} - \text{V}_{\text{CAL5}})}{\text{I}_{\text{FS}} \times 10^3}$                                                                                |
|                             | NL3             |                 | 270  | 11011111           |     |      | +15    | -15    | +15   | -15  | 0    | 00100000             |           | 24  | E <sub>169</sub> | V    | $\label{eq:NL3} \begin{array}{ c c c }\hline \hline NL_3 = \left( \begin{array}{c} \left( \underline{E_{169} - V_{CAL5}} \right) \\ \hline I_{FS} \times 10^3 \end{array} \right) \\ \hline \left( \begin{array}{c} (32) \\ (255) \end{array} \\ \hline \left( \begin{array}{c} V_{CAL6} - V_{CAL5} \right) \\ \hline I_{FS} \times 10^3 \end{array} \end{array}$ |
|                             | NL4             |                 | 271  | 11101111           |     |      | +15    | -15    | +15   | -15  | 0    | 00010000             |           | 24  | E <sub>170</sub> | V    | $\overline{\text{NL4}} = \left( \begin{array}{c} \left( \underline{\text{E}_{170} - \text{V}_{\text{CAL5}}} \right) \\ \overline{\text{IFS} \times 10^3} \end{array} \right) \text{-}$ $\frac{(16)}{(255)} \frac{(\text{V}_{\text{CAL6}} - \text{V}_{\text{CAL5}})}{\overline{\text{IFS} \times 10^3}}$                                                           |
|                             | NL5             |                 | 272  | 11110111           |     |      | +15    | -15    | +15   | -15  | 0    | 00001000             |           | 24  | E <sub>171</sub> | V    | $\label{eq:NL5} \begin{split} \overline{NL5} &= \left( \begin{array}{c} \frac{\left(E_{171} - VCAL5\right)}{IFS \times 10^3} \end{array} \right) \text{-} \\ \frac{(8)}{(255)} & \frac{(VCAL6 - VCAL5)}{IFS \times 10^3} \end{split}$                                                                                                                             |
|                             | NL6             |                 | 273  | 11111011           |     |      | +15    | -15    | +15   | -15  | 0    | 00000100             |           | 24  | E <sub>172</sub> | V    | $\overline{\text{NL6}} = \left( \begin{array}{c} \frac{(\text{E}_{172} - \text{V}_{\text{CAL5}})}{\text{I}_{\text{FS}} \times 10^3} \end{array} \right) - \frac{(4)}{(255)} \frac{(\text{V}_{\text{CAL6}} - \text{V}_{\text{CAL5}})}{\text{I}_{\text{FS}} \times 10^3}$                                                                                           |

| Subgroup        | Symbol                          | MIL-STD-<br>883 | Test | Adapter pin numbers |     |      |      |      |      |      |      | Energized   | Measured pin |      |                  | Equation |                                                                                                                            |
|-----------------|---------------------------------|-----------------|------|---------------------|-----|------|------|------|------|------|------|-------------|--------------|------|------------------|----------|----------------------------------------------------------------------------------------------------------------------------|
|                 |                                 | method          | No.  | 1.0                 |     |      | 1    |      |      |      |      | 16.02       | relays       | No   | Volue            | Lloit    |                                                                                                                            |
|                 |                                 |                 |      | logic state         | 9 V | 10 V | 11 V | 12 V | 13 V | 14 V | 15 V | logic state |              | INO. | value            | Unit     |                                                                                                                            |
| 3<br>T₄ = -55°C | NL7                             |                 | 274  | 11111101            |     |      | +15  | -15  | +15  | -15  | 0    | 00000010    |              | 24   | E <sub>173</sub> | V        | $\overline{NL7} = \left(\begin{array}{c} \underline{(E173 - VCAL5)} \\ \end{array}\right) - $                              |
| ~               |                                 |                 |      |                     |     |      |      |      |      |      |      |             |              |      |                  |          | $(I_{FS} \times 10^3)$                                                                                                     |
|                 |                                 |                 |      |                     |     |      |      |      |      |      |      |             |              |      |                  |          | $\frac{(2)}{(255)} \frac{(VCAL6 - VCAL5)}{IFS \times 10^3}$                                                                |
|                 | NL8                             |                 | 275  | 11111110            |     |      | +15  | -15  | +15  | -15  | 0    | 00000001    |              | 24   | E <sub>174</sub> | V        | $\overline{NL_8} = \left(\begin{array}{c} \frac{\left(E_{174} - V_{CAL5}\right)}{I_{FS} \times 10^3} \end{array}\right) -$ |
|                 |                                 |                 |      |                     |     |      |      |      |      |      |      |             |              |      |                  |          | $\frac{(1)}{(255)} \frac{(V_{CAL6} - V_{CAL5})}{I_{FS} \times 10^3}$                                                       |
|                 | $\Sigma NL^+$                   |                 | 276  |                     |     |      |      |      |      |      |      |             |              |      |                  |          | $\Sigma NL^+ = NL_i + NL_K +$<br>(i, k, bits having positive errors)                                                       |
|                 | $\overline{\Sigma NL^+}$        |                 | 277  |                     |     |      |      |      |      |      |      |             |              |      |                  |          | $\overline{\Sigma NL^{+}} = \overline{NL^{1}} + \overline{NLk^{1}} + \dots$ (i, k, bits having positive errors)            |
|                 | ΣNL                             |                 | 278  |                     |     |      |      |      |      |      |      |             |              |      |                  |          | $\Sigma NL^{2} = NL_{m} + NL_{n} +$<br>(m, n, bits having negative errors)                                                 |
|                 | $\Sigma NL^{-}$                 |                 | 279  |                     |     |      |      |      |      |      |      |             |              |      |                  |          | $\overline{\Sigma NL^{-}} = \overline{NLm^{1}} + \overline{NLn^{1}} + \dots$ (m, n, bits having negative errors)           |
|                 | ΔΣNL                            |                 | 280  |                     |     |      |      |      |      |      |      |             |              |      |                  |          | $\Delta \Sigma NL = \left  \Sigma NL^+ \right  - \left  \Sigma NL^- \right $                                               |
|                 | $\Delta \Sigma \overline{NL}$   |                 | 281  |                     |     |      |      |      |      |      |      |             |              |      |                  |          | $\Delta \Sigma \overline{NL} = \left  \Sigma \overline{NL}^+ \right  - \left  \Sigma \overline{NL}^- \right $              |
|                 | NL⁺                             |                 | 282  |                     |     |      |      |      |      |      |      |             |              |      |                  |          | $NL^{+} = \left  \Sigma NL^{+} \right  + \left  \Delta \Sigma NL \right $                                                  |
|                 | $\overline{\rm NL^+}$           |                 | 283  |                     |     |      |      |      |      |      |      |             |              |      |                  |          | $\overline{NL^+} = \left  \Sigma \overline{NL}^+ \right  + \left  \Delta \Sigma \overline{NL} \right $                     |
|                 | NL                              |                 | 284  |                     |     |      |      |      |      |      |      |             |              |      |                  |          | $NL^{-} = \left  \Sigma NL^{-} \right  + \left  \Delta \Sigma NL \right $                                                  |
|                 | NL <sup>-</sup>                 |                 | 285  |                     |     |      |      |      |      |      |      |             |              |      |                  |          | $\overline{NL^{-}} = \left  \Sigma \overline{NL}^{-} \right  + \left  \Delta \Sigma \overline{NL} \right $                 |
|                 | (l <sub>01</sub> ) <sub>a</sub> |                 | 286  | 10000000            |     |      | +15  | -15  | +15  | -15  | 0    | 10000000    |              | 24   | E <sub>175</sub> | V        | $(I_{01})_a = I_{FS} \times \frac{128}{255} - 0.01(E_{175})$                                                               |
|                 | (l <sub>01</sub> ) <sub>b</sub> |                 | 287  | 01111111            |     |      | +15  | -15  | +15  | -15  | 0    | 01111111    |              | 24   | E <sub>176</sub> | V        | $(I_{01})_{b} = I_{FS} X \frac{127}{255} - 0.01(E_{176})$                                                                  |
|                 | $\Delta(I_{01})$                |                 | 288  |                     |     |      |      |      |      |      |      |             |              |      |                  |          | $\Delta(I_{01}) = [(I_{01})_a - (I_{01})_b] \times 10^3$                                                                   |

| Subgroup                    | Symbol                          | MIL-STD-<br>883 | Test | Adapter pin numbers |     |      |      |      |      |      |      |                      |        | Measured pin |                  | pin  | Equation                                                       |
|-----------------------------|---------------------------------|-----------------|------|---------------------|-----|------|------|------|------|------|------|----------------------|--------|--------------|------------------|------|----------------------------------------------------------------|
|                             |                                 | method          | NO.  | 1.0                 | 1   |      |      |      | 1    |      |      | 10.00                | relays | NL           | 1.1.1            | 11.2 | -                                                              |
|                             |                                 |                 |      | 1-8<br>logic state  | 9 V | 10 V | 11 V | 12 V | 13 V | 14 V | 15 V | 16-23<br>logic state |        | NO.          | value            | Unit |                                                                |
| 3<br>T <sub>A</sub> = -55°C | (I <sub>02</sub> ) <sub>a</sub> |                 | 289  | 01000000            |     |      | +15  | -15  | +15  | -15  | 0    | 01000000             |        | 24           | E <sub>177</sub> | V    | $(I_{02})_a = I_{FS} X \frac{64}{255} - 0.01(E_{177})$         |
|                             | (I <sub>02</sub> ) <sub>b</sub> |                 | 290  | 00111111            |     |      | +15  | -15  | +15  | -15  | 0    | 00111111             |        | 24           | E <sub>178</sub> | V    | $(I_{02})_{b} = I_{FS} \times \frac{63}{255} - 0.01(E_{178})$  |
|                             | $\Delta(I_{02})$                |                 | 291  |                     |     |      |      |      |      |      |      |                      |        |              |                  |      | $\Delta(I_{02}) = [(I_{02})_{a} - (I_{02})_{b}] \times 10^{3}$ |
|                             | (I <sub>03</sub> ) <sub>a</sub> |                 | 292  | 00100000            |     |      | +15  | -15  | +15  | -15  | 0    | 00100000             |        | 24           | E <sub>179</sub> | V    | $(I_{03})_a = I_{FS} X \frac{32}{255} - 0.01(E_{179})$         |
|                             | (I <sub>03</sub> ) <sub>b</sub> |                 | 293  | 00011111            |     |      | +15  | -15  | +15  | -15  | 0    | 00011111             |        | 24           | E <sub>180</sub> | V    | $(I_{03})_{b} = I_{FS} X \frac{31}{255} - 0.01(E_{180})$       |
|                             | $\Delta(I_{03})$                |                 | 294  |                     |     |      |      |      |      |      |      |                      |        |              |                  |      | $\Delta(I_{03}) = [(I_{03})_{a} - (I_{03})_{b}] \times 10^{3}$ |
|                             | (I <sub>04</sub> ) <sub>a</sub> |                 | 295  | 00010000            |     |      | +15  | -15  | +15  | -15  | 0    | 00010000             |        | 24           | E <sub>181</sub> | V    | $(I_{04})_a = I_{FS} X \frac{16}{255} - 0.01(E_{181})$         |
|                             | (I <sub>04</sub> ) <sub>b</sub> |                 | 296  | 00001111            |     |      | +15  | -15  | +15  | -15  | 0    | 00001111             |        | 24           | E <sub>182</sub> | V    | $(I_{04})_{b} = I_{FS} X \frac{15}{255} - 0.01(E_{182})$       |
|                             | $\Delta(I_{04})$                |                 | 297  |                     |     |      |      |      |      |      |      |                      |        |              |                  |      | $\Delta(I_{04}) = [(I_{04})_{a} - (I_{04})_{b}] \times 10^{3}$ |
|                             | (I <sub>05</sub> ) <sub>a</sub> |                 | 298  | 00001000            |     |      | +15  | -15  | +15  | -15  | 0    | 00001000             |        | 24           | E <sub>183</sub> | V    | $(I_{05})_a = I_{FS} X \frac{8}{255} - 0.01(E_{183})$          |
|                             | (I <sub>05</sub> ) <sub>b</sub> |                 | 299  | 00000111            |     |      | +15  | -15  | +15  | -15  | 0    | 00000111             |        | 24           | E <sub>184</sub> | V    | $(I_{05})_{b} = I_{FS} X \frac{7}{255} - 0.01(E_{184})$        |
|                             | $\Delta(I_{05})$                |                 | 300  |                     |     |      |      |      |      |      |      |                      |        |              |                  |      | $\Delta(I_{05}) = [(I_{05})_a - (I_{05})_b] \times 10^3$       |
|                             | (I <sub>06</sub> ) <sub>a</sub> |                 | 301  | 00000100            |     |      | +15  | -15  | +15  | -15  | 0    | 00000100             |        | 24           | E <sub>185</sub> | V    | $(I_{06})_{a} = I_{FS} X \frac{4}{255} - 0.01(E_{185})$        |
|                             | (I <sub>06</sub> )ь             |                 | 302  | 00000011            |     |      | +15  | -15  | +15  | -15  | 0    | 00000011             |        | 24           | E <sub>186</sub> | V    | $(I_{06})_{b} = I_{FS} \times \frac{3}{255} - 0.01(E_{186})$   |
|                             | $\Delta(I_{06})$                |                 | 303  |                     |     |      |      |      |      |      |      |                      |        |              |                  |      | $\Delta(I_{06}) = [(I_{06})_{a} - (I_{06})_{b}] \times 10^{3}$ |
|                             | (I <sub>07</sub> )a             |                 | 304  | 00000010            |     |      | +15  | -15  | +15  | -15  | 0    | 00000010             |        | 24           | E <sub>187</sub> | V    | $(I_{07})_a = I_{FS} X \frac{2}{255} - 0.01(E_{187})$          |
|                             | (I <sub>07</sub> ) <sub>b</sub> |                 | 305  | 00000001            |     |      | +15  | -15  | +15  | -15  | 0    | 00000001             |        | 24           | E <sub>188</sub> | V    | $(I_{07})_{b} = I_{FS} \times \frac{1}{255} - 0.01(E_{188})$   |
|                             | $\Delta(I_{07})$                |                 | 306  |                     |     |      |      |      |      |      |      |                      |        |              |                  |      | $\Delta(I_{07}) = [(I_{07})_{a} - (I_{07})_{b}] \times 10^{3}$ |
|                             | (I <sub>08</sub> ) <sub>b</sub> |                 | 307  | 00000000            |     |      | +15  | -15  | +15  | -15  | 0    | 00000000             |        | 24           | E <sub>189</sub> | V    | $(I_{08})_{b} = I_{FS} X \frac{1}{255} - 0.01(E_{189})$        |
|                             | (l <sub>08</sub> )              |                 | 308  |                     |     |      |      |      |      |      |      |                      |        |              |                  |      | $\Delta(I_{08}) = [(I_{07})_{b} - (I_{08})_{b}] \times 10^3$   |
|                             | $\Delta I_{FS}$                 |                 | 309  |                     |     |      |      |      |      |      |      |                      |        |              |                  |      | $I_{FS} - \overline{I_{FS}} = \Delta I_{FS}$                   |

| Subgroup                     | Symbol               | MIL-STD-<br>883 | Test |                    | Adapter pin numbers Measured pin Energized relays                                               |                    |                                        |                   |                |           |      | Energized            | Measured pin |     |       | Equation |                                                                                               |
|------------------------------|----------------------|-----------------|------|--------------------|-------------------------------------------------------------------------------------------------|--------------------|----------------------------------------|-------------------|----------------|-----------|------|----------------------|--------------|-----|-------|----------|-----------------------------------------------------------------------------------------------|
|                              |                      | method          | INO. |                    |                                                                                                 |                    |                                        |                   |                |           |      |                      |              |     |       |          |                                                                                               |
|                              |                      |                 |      | 1-8<br>logic state | 9 V                                                                                             | 10 V               | 11 V                                   | 12 V              | 13 V           | 14 V      | 15 V | 16-23<br>logic state |              | No. | Value | Unit     |                                                                                               |
| 9<br>T <sub>A</sub> = 25°C   | TC(I <sub>FS</sub> ) |                 | 310  |                    |                                                                                                 |                    |                                        |                   |                |           |      |                      |              |     |       |          | $TC(I_{FS}) = \frac{(E_1 - E_{64})}{E_1} \times 10^4$                                         |
|                              | TC(I <sub>FS</sub> ) |                 | 311  |                    |                                                                                                 |                    |                                        |                   |                |           |      |                      |              |     |       |          | $TC(I_{FS}) = \frac{(E_1 - E_{127})}{0.8E_1} \times 10^4$                                     |
|                              | TC(IFS)              |                 | 312  |                    |                                                                                                 |                    |                                        |                   |                |           |      |                      |              |     |       |          | $\overline{\text{TC(IFS)}} = \frac{(\text{E}_2 - \text{E}_{65})}{\text{E}_2} \times 10^4$     |
|                              | TC(IFS)              |                 | 313  |                    |                                                                                                 |                    |                                        |                   |                |           |      |                      |              |     |       |          | $\overline{\text{TC(IFS)}} = \frac{(\text{E}_2 - \text{E}_{128})}{0.8\text{E}_2} \times 10^4$ |
|                              | t <sub>PHL</sub>     |                 | 314  | See figure 3.      | ee figure 3. $V_L = 2.7 V$ , $V_{OUT}$ high-to-low transition,<br>S1-OFF ( $V_M$ low-to-high)   |                    |                                        |                   |                |           |      |                      |              |     |       |          |                                                                                               |
|                              | t <sub>PLH</sub>     |                 | 315  | See figure 3.      | . V∟=<br>S1-0                                                                                   | 0.7 V,<br>OFF      | V <sub>OUT</sub><br>(VIN I             | low-to<br>nigh-to | -high<br>-low) | transitio | on,  |                      |              |     |       |          |                                                                                               |
| 10<br>T <sub>A</sub> = 125°C | t <sub>PHL</sub>     |                 | 316  | See figure 3.      | . V∟=<br>S1-0                                                                                   | 2.7 V,<br>OFF      | V <sub>OUT</sub><br>(V <sub>IN</sub> I | high-t<br>ow-to-  | o-low<br>high) | transitio | on,  |                      |              |     |       |          |                                                                                               |
|                              | t <sub>PLH</sub>     |                 | 317  | See figure 3.      | . V⊾=<br>S1-0                                                                                   | 0.7 V,<br>OFF      | V <sub>OUT</sub><br>(V <sub>IN</sub> ł | low-to<br>nigh-to | -high<br>-low) | transitio | on,  |                      |              |     |       |          |                                                                                               |
| 11<br>T <sub>A</sub> = -55°C | t <sub>PHL</sub>     |                 | 318  | See figure 3.      | . V⊾=<br>S1-0                                                                                   | 2.7 V,<br>OFF      | V <sub>OUT</sub><br>(V <sub>IN</sub> I | high-t<br>ow-to-  | o-low<br>high) | transitio | on,  |                      |              |     |       |          |                                                                                               |
|                              | t <sub>PLH</sub>     |                 | 319  | See figure 3.      | . V∟=<br>S1-0                                                                                   | 0.7 V,<br>OFF      | V <sub>OUT</sub><br>(V <sub>IN</sub> ł | low-to<br>nigh-to | -high<br>-low) | transitio | on,  |                      |              |     |       |          |                                                                                               |
| 12<br>T <sub>A</sub> = 25°C  | dlo<br>dt            |                 | 320  | See figure 4.      | . V <sub>IN</sub>  <br>V <sub>L</sub> =                                                         | ow-to-h<br>= 5 Vdc | nigh tra                               | ansitio           | n,             |           |      |                      |              |     |       |          | $\frac{dlo}{dt} = \frac{1}{\Delta t}$                                                         |
|                              | t <sub>sн∟</sub>     |                 | 321  | See figure 3.      | . V∟=<br>S1-0                                                                                   | 2.7 V,<br>DFF      | Vout<br>(VIN IC                        | high-t<br>w-to-l  | o-low<br>nigh) | transitio | on,  |                      |              |     |       |          |                                                                                               |
|                              | t <sub>slH</sub>     |                 | 322  | See figure 3.      | e figure 3. $V_L = 0.7 V$ , $V_{OUT}$ low-to-high transition,<br>S1-OFF ( $V_{IN}$ high-to-low) |                    |                                        |                   |                |           |      |                      |              |     |       |          |                                                                                               |

### NOTES:

<u>1</u>/ The measurement of  $I_{FS}$  and  $\overline{I_{FS}}$  can be made directly as a voltage measurement at pin 26 ( $I_{FS} = \begin{bmatrix} \frac{E_{pin26}}{5000} \end{bmatrix}$  mA)

provided that measurement accuracy is  $\pm 0.1\%$  or better. If the measurement is made in accordance with table III, the reference D/A converter must be calibrated for a full scale current of 2.0 mA  $\pm 0.1\%$ .

2/ For tests 26-33, 129-136, and 232-239, the logic input voltage shall be +18 V. For tests 34-41, 137-144, and 240-247, the logic input voltage shall be -10.0 V.

| Test | Symbol          |      | Device | e type 01 |       | Device type 02 |       |       |       |  |  |
|------|-----------------|------|--------|-----------|-------|----------------|-------|-------|-------|--|--|
| no.  |                 |      |        |           |       |                |       |       |       |  |  |
|      |                 | Lin  | nits   |           |       | Lin            | nits  |       |       |  |  |
|      |                 | Min  | Max    | Delta     | Units | Min            | Max   | Delta | Units |  |  |
| 3    | I <sub>FS</sub> | 1.94 | 2.04   | 0.01      | mA    | 1.984          | 2.000 | 0.005 | mA    |  |  |
| 4    | IFS             | 1.94 | 2.04   | 0.01      | mA    | 1.984          | 2.000 | 0.005 | mA    |  |  |
| 5    | Izs             | -2.0 | +2.0   | 0.5       | μΑ    | -1.0           | +1.0  | 0.3   | μΑ    |  |  |
| 6    | Izs             | -2.0 | +2.0   | 0.5       | μA    | -1.0           | +1.0  | 0.3   | μA    |  |  |

#### TABLE IV. Group C end point electrical parameters. $T_A = +25^{\circ}C; \pm V_{CC} = \pm 15 V$

- 4.4.1 Group A inspection. Group A inspection shall be in accordance with table III of MIL-PRF-38535 and as follows:
  - a. Tests shall be as specified in table II herein.
  - b. Subgroups 4, 5, 6, 7, and 8 shall be omitted.
  - c. Subgroup 12 shall be added to group A inspection for all classes and it shall consist of the conditions and limits as specified in table III. The sample size series number shall be 5 for all classes (accept on 0).
- 4.4.2 Group B inspection. Group B inspection shall be in accordance with table II of MIL-PRF-38535.
- 4.4.3 Group C inspection. Group C inspection shall be in accordance with table IV of MIL-PRF-38535 and as follows:
  - a. End point electrical parameters shall be as specified in table II herein.
  - b. The steady-state life test duration, test condition, and test temperature, or approved alternatives shall be as specified in the device manufacturer's QM plan in accordance with MIL-PRF-38535. The burn-in test circuit shall be maintained under document control by the device manufacturer's Technology Review Board (TRB) in accordance with MIL-PRF-38535 and shall be made available to the acquiring or preparing activity upon request. The test circuit shall specify the inputs, outputs, biases, and power dissipation, as applicable, in accordance with the intent specified in test method 1005 of MIL-STD-883.

4.4.4 <u>Group D inspection</u>. Group D inspection shall be in accordance with table V of MIL-PRF-38535. End point electrical parameters shall be as specified in table II herein.

4.5 <u>Methods of inspection</u>. Methods of inspection shall be specified and as follows.

4.5.1 <u>Voltage and current</u>. All voltage values given except the input offset voltage (or differential voltage) are referenced to the external zero reference level of the supply voltage. Currents given are conventional current and positive when flowing into the referenced terminal.

## 5. PACKAGING

5.1 <u>Packaging requirements</u>. For acquisition purposes, the packaging requirements shall be as specified in the contract or order (see 6.2). When packaging of materiel is to be performed by DoD or in-house contractor personnel, these personnel need to contact the responsible packaging activity to ascertain packaging requirements. Packaging requirements are maintained by the Inventory Control Point's packaging activity within the Military Service or Defense Agency, or within the military service's system command. Packaging data retrieval is available from the managing Military Department's or Defense Agency's automated packaging files, CD-ROM products, or by contacting the responsible packaging activity.

#### 6. NOTES

(This section contains information of a general or explanatory nature that may be helpful, but is not mandatory.)

6.1 <u>Intended use.</u> Microcircuits conforming to this specification are intended for original equipment design applications and logistic support of existing equipment.

- 6.2 <u>Acquisition requirements</u>. Acquisition documents should specify the following:
  - a. Title, number, and date of the specification.
  - b. PIN and compliance identifier, if applicable (see 1.2).
  - c. Requirements for delivery of one copy of the conformance inspection data pertinent to the device inspection lot to be supplied with each shipment by the device manufacturer, if applicable.
  - d. Requirements for certificate of compliance, if applicable.
  - e. Requirements for notification of change of product or process to acquiring activity in addition to notification of the qualifying activity, if applicable.
  - f. Requirements for failure analysis (including required test condition of MIL-STD-883, method 5003), corrective action and reporting of results, if applicable.
  - g. Requirements for product assurance options.
  - h. Requirements for special carriers, lead lengths, or lead forming, if applicable. These requirements should not affect the part number. Unless otherwise specified, these requirements will not apply to direct purchase by or direct shipment to the Government.
  - i. Requirements for "JAN" marking.
  - j. Packaging requirements (see 5.1).

6.3 <u>Qualification</u>. With respect to products requiring qualification, awards will be made only for products which are, at the time of award of contract, qualified for inclusion in Qualified Manufacturers List QML-38535 whether or not such products have actually been so listed by that date. The attention of the contractors is called to these requirements, and manufacturers are urged to arrange to have the products that they propose to offer to the Federal Government tested for qualification in order that they may be eligible to be awarded contracts or purchase orders for the products covered by this specification. Information pertaining to qualification of products may be obtained from DSCC-VQ, 3990 E. Broad Street, Columbus, Ohio 43123-1199.

6.4 <u>Superseding information</u>. The requirements of MIL-M-38510 have been superseded to take advantage of the available Qualified Manufacturer Listing (QML) system provided by MIL-PRF-38535. Previous references to MIL-M-38510 in this document have been replaced by appropriate references to MIL-PRF-38535. All technical requirements now consist of this specification and MIL-PRF-38535. The MIL-M-38510 specification sheet number and PIN have been retained to avoid adversely impacting existing government logistics systems and contractor's parts lists.

6.5 <u>Abbreviations, symbols, and definitions</u>. The abbreviations, symbols, and definitions used herein are defined in MIL-PRF-38535 and MIL-STD-1331.

6.6 Logistic support. Lead materials and finishes (see 3.3) are interchangeable. Unless otherwise specified, microcircuits acquired for Government logistic support will be acquired to device class B (see 1.2.2), lead material and finish A (see 3.4). Longer length leads and lead forming should not affect the part number.

6.7 <u>Substitutability</u>. The cross-reference information below is presented for the convenience of users. Microcircuits covered by this specification will functionally replace the listed generic-industry type. Generic-industry microcircuit types may not have equivalent operational performance characteristics across military temperature ranges or reliability factors equivalent to MIL-M-38510 device types and may have slight physical variations in relation to case size. The presence of this information should not be deemed as permitting substitution of generic-industry types for MIL-M-38510 types or as a waiver of any of the provisions of MIL-PRF-38535.

| Military device type | Generic-industry type |
|----------------------|-----------------------|
| 01                   | DAC-08                |
| 02                   | DAC-08A               |

6.8 <u>Changes from previous issue</u>. Marginal notations are not used in this revision to identify changes with respect to the previous issue, due to the extensiveness of the changes.

Custodians: Army – CR Navy - EC Air Force - 11 NASA - NA DLA – CC Review activities: Army - MI, SM

Navy - AS, CG, MC, SH, TD Air Force – 03, 19, 99 Preparing activity: DLA - CC

Project 5962-2127

NOTE: The activities listed above were interested in this document as of the date of this document. Since organizations and responsibilities can change, you should verify the currency of the information above using the ASSIST Online database at <a href="http://assist.daps.dla.mil">http://assist.daps.dla.mil</a>.

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