AEM40940

Highly-efficient, regulated dual-output, ambient energy manager for high-frequency RF input with optional primary battery

Features

Ultra-low-power start-up:
- RF input power from -19.5 dBm up to 10 dBm (typical)
- Cold start from the RF input or from the storage device

Wide frequency range, low power, integrated rectifier:
- With 868 MHz, 915 MHz and 2.45 GHz matching networks available

Ultra-low-power boost regulator:
- Open-circuit voltage sensing for MPPT every 0.33 s
- Configurable MPPT with 2-pin programming
- Selectable Voc ratios of 60, 65 or 70 %
- Input voltage operation range from 50 mV to 2.5 V
- MPPT voltage operation range from 50 mV to 2.5 V
- Constant impedance matching (ZMPPT)

Integrated 1.2/1.8 V LDO regulator:
- Up to 20 mA load current
- Power gated dynamically by external control
- Selectable output voltage

Integrated 1.8/2.5/3.3 V LDO regulator:
- Up to 80 mA load current with 300 mV drop-out
- Power gated dynamically by external control
- Selectable output voltage

Flexible energy storage management:
- Selectable overcharge and overdischarge protection for any type of rechargeable battery or (super)capacitor
- Fast supercapacitor charging
- Warns the load when battery is running low
- Warns when output voltage regulators are available

Smallest footprint, smallest BOM:
- Only seven passive external components

Optional primary battery:
- Automatically switches to the primary battery when the secondary battery is exhausted

Integrated balun for dual-cell supercapacitor

Applications

- RF harvesting
- Industrial monitoring
- Indoor geolocation
- Home automation
- E-health monitoring
- Wireless sensor nodes

Description

The AEM40940 is an integrated energy management subsystem that extracts AC power from high-frequency RF inputs to simultaneously store energy in a rechargeable element and supply the system with two independent regulated voltages. The AEM40940 allows to extend battery lifetime and ultimately eliminates the primary energy storage element in a large range of wireless applications, such as industrial monitoring, indoor geolocation, home automation, e-health monitoring and wireless sensor nodes.

The AEM40940 harvests the available input power up to 10 dBm. It integrates an ultra-low power rectifier combined with a boost converter to charge a storage element, such as a Li-ion battery, a thin film battery, a supercapacitor or a conventional capacitor. With its unique cold-start circuit, it can start operating with empty storage elements at an input power as low as -19.5 dBm.
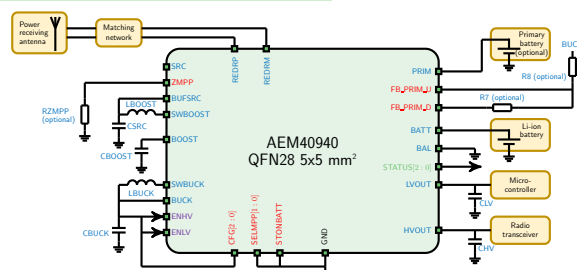
The low-voltage supply typically drives a microcontroller at 1.2 V or 1.8 V. The high-voltage supply typically drives a radio transceiver at 1.8 V, 2.5 V or 3.3 V. Both are driven by highly-efficient LDO (Low Drop-Out) regulators for low noise and high stability.

Configuration pins determine various operating modes by setting predefined conditions for the energy storage element (overcharge or overdischarge voltages), and by selecting the voltage of the high-voltage supply and the low-voltage supply.

The chip integrates all the active elements for powering a typical wireless sensor. Five capacitors and two inductors are required, available in the small 0402 and 0603 size, respectively. With only seven external components excluding the matching network, integration is maximum, footprint and BOM are minimum, optimizing the time-to-market and the costs of WSN designs.

Device information

Part number	Package	Body size
10AEM40940C0000	QFN 28-pin	5 mm x 5 mm

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Figure 1: Simplified schematic view

1   Introduction

The AEM40940 is a full-featured energy efficient power management circuit able to charge a storage element (battery or supercapacitor, connected to BATT) from an energy source (connected to the rectifier) as well as to supply loads at different operating voltages through two power supplying LDO regulators (LVOUT and HVOUT).

The heart of the AEM40940 is a cascade rectifier and two regulated switching converters, namely the boost converter and the buck converter with high-power conversion efficiencies (See Page 18).

At first start-up, as soon as a required cold-start input power (See Table 6) is available from the harvested energy source, the AEM coldstarts. Note that the STONBATT pin make it possible to bypass the cold-start procedure using the pre-charged storage element to start the AEM40940 (see Page 11).

Through three configuration pins (CFG[2:0]), the user can select a specific operating mode from a range of seven modes. Those operating modes define the LDO output voltages and the protection levels of the storage element.

The Maximum Power Point (MPP) ratio can be configured using two configuration pins (SELMPP[1:0]) (See Page 11).

Two logic control pins are provided (ENLV and ENHV) to dynamically activate or deactivate the LDO regulators that supply the low- and high-voltage load, respectively. The status pin STATUS[0] alerts the user that the LDOs are operational and can be enabled. This signal can also be used to enable an optional external regulator.

If the battery voltage gets depleted, the LDOs are power gated and the controller is no longer supplied by the storage element to protect it from further discharge. Around 600 ms before the shutdown of the AEM, the status pin STATUS[1] alerts the user for a clean shutdown of the system.

However, if the storage element gets depleted and an optional primary battery is connected on PRIM, the chip automatically uses it as a source to recharge the storage element before switching back to the ambient source. This guarantees continuous operation even under the most adverse conditions (See Page 10). STATUS[1] is asserted when the primary battery is providing power.

The status of the MPP controller is reported with one dedicated status pin (STATUS[2]). The status pin is asserted when a MPP calculation is being performed.

AEM40940

Figure 2: Pinout diagram QFN28

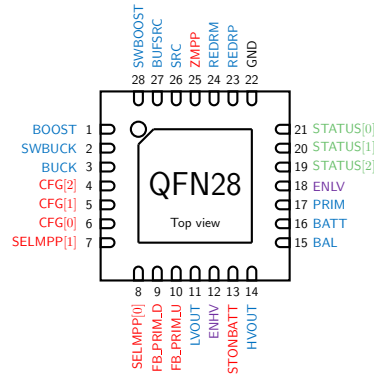| NAME	PIN NUMBER	FUNCTION	
Power pins			
BOOST	1	Output of the boost converter.	
SWBUCK	2	Switching node of the buck converter.	
BUCK	3	Output of the buck converter.	
LVOUT	11	Output of the low voltage LDO regulator.	
HVOUT	14	Output of the high voltage LDO regulator.	
BAL	15	Connection to mid-point of a dual-cell supercapacitor (optional). Must be connected to GND if not used.	
BATT	16	Connection to the energy storage element, battery or capacitor. Cannot be left floating.	
PRIM	17	Connection to the primary battery (optional). Must be connected to GND if not used.	
REDRP	23	RF positive input voltage of the rectifier.	
REDRM	24	RF negative input voltage of the rectifier.	
SRC	26	Output of the rectifier. Must be left floating.	
BUFSRC	27	Connection to an external capacitor buffering the boost converter input.	
SWBOOST	28	Switching node of the boost converter.	
Configuration pins			
CFG[2]	4	Used for the configuration of the threshold voltages for the energy storage element and the output voltage of the LDOs.	See Page 11
CFG[1]	5		
CFG[0]	6		
SELMPP[1]	7	Used for the configuration of the MPP ratio.	
SELMPP[0]	8		
FB_PRIM_D	9	Used for the configuration of the primary battery (optional). Must be connected to GND if not used.	
FB_PRIM_U	10		
STONBATT	13	Used for the configuration of the cold start (optional). Must be connected to GND if not used.	
ZMPPT	25	Used for the configuration of the ZMPPT (optional). Must be left floating if not used.	
Control pins			
ENHV	12	Enabling pin for the high-voltage LDO.	See Page 9
ENLV	18	Enabling pin for the low-voltage LDO.	
Status pins			
STATUS[2]	19	Logic output. Asserted when the AEM performs a MPP evaluation.	See Pages 8-10
STATUS[1]	20	Logic output. Asserted if the battery voltage falls below Vovdis or if the AEM is taking energy from the primary battery.	
STATUS[0]	21	Logic output. Asserted when the LDOs can be enabled.	
Other pins			
GND	22, Exposed Pad	Ground connection, should be solidly tied to the PCB ground plane.	

Table 1: Pins description

2 Absolute Maximum Ratings

Parameter	Rating
REDRP,REDRM	2.75 V
Operating junction temperature	-40 °C to +125 °C
Storage temperature	-65 °C to +150 °C
Input power	30 dBm

Table 2: Absolute maximum ratings

3 Thermal Resistance

Package	θ_{JA}	θ_{JC}	Unit
QFN28	38.3	2.183	°C/W

Table 3: Thermal data

ESD CAUTION
ESD (ELECTROSTATIC DISCHARGE) SENSITIVE DEVICE These devices have limited built-in ESD protection and damage may thus occur on devices subjected to high-energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

4 Typical Electrical Characteristics at 25 °C

Symbol	Parameter	Conditions	Min	Typ	Max	Unit
Power conversion						
Pin_{CS}	Source power required for cold start.	During cold start (at 915 MHz)	-19.5			dBm
Pin	Source power.	After cold start (at 915 MHz)	-19.5		10	dBm
Fin	Source frequency.		865		2450	MHz
Vsrc	Output of the rectifier.	During cold start	0.38		2.5	V
		After cold start	0.05		2.5	
Vboost	Output of the boost converter.	During normal operation	2.2		4.5	V
Vbuck	Output of the buck converter.	During normal operation	2	2.2	2.5	
Storage element						
Vbatt	Voltage on the storage element.	Rechargeable battery	2.2		4.5	V
		Capacitor	0		4.5	V
Tcrit	Time before shutdown after STA-TUS[1] has been asserted.		400	600	800	ms
Vprim	Voltage on the primary battery.		0.6		5	V
Vfb_prim_u	Feedback for the minimal voltage level on the primary battery.		0.15		1.1	V
Vovch	Maximum voltage accepted on the storage element before disabling the boost converter.	see Table 8	2.7		4.5	V
Vchrdy	Minimum voltage required on the storage element before enabling the LDOs after a cold start.	see Table 8	2.3		4.04	V
Vovdis	Minimum voltage accepted on the storage element before switching to primary battery or entering into a shutdown.	see Table 8	2.2		3.6	V
Low-voltage LDO regulator						
Vlv	Output voltage of the low-voltage LDO.	see Table 8	1.2		1.8	V
Ilv	Load current from the low-voltage LDO.		0		20	mA
High-voltage LDO regulator						
Vhv	Output voltage of the high-voltage LDO.	see Table 8	1.8		3.3	V
Ihv	Load current from the high-voltage LDO.		0		80	mA
Logic output pins						
STATUS[2:0]	Logic output levels on the status pins.	Logic high (VOH)	1.98	Vbatt		V
		Logic low (VOL)	-0.1		0.1	V

Table 4: Electrical characteristics

5 Recommended Operation Conditions

Symbol	Parameter		Min	Typ	Max	Unit
External components						
CSRC	Capacitor decoupling the boost converter input.		8	10	22	μF
CBOOST	Capacitor of the boost converter.		10	22	25	μF
LBOOST	Inductor of the boost converter.		4	10	25	μH
CBUCK	Capacitor of the buck converter.		8	10	22	μF
LBUCK	Inductor of the buck converter.		4	10	25	μH
CLV	Capacitor decoupling the low-voltage LDO regulator.		8	10	14	μF
CHV	Capacitor decoupling the high-voltage LDO regulator.		8	10	14	μF
CBATT	**Optional** - Capacitor on BATT if no storage element is connected (see Page 11).		150			μF
RZMPP	**Optional** - Resistor for the ZMPPT configuration (see Page 11).		10		1M	Ω
RP	**Optional** - Resistor to be used with a primary battery. Equal to R7 + R8 (see Page 11).		100		500	kΩ
Logic input pins						
ENHV	Enabling pin for the high-voltage LDO[1].	Logic high (VOH)	1.75	Vbuck	Vbuck	V
		Logic low (VOL)	-0.01	0	0.01	
ENLV	Enabling pin for the low-voltage LDO[2].	Logic high (VOH)	1.75	Vbuck	Vboost	V
		Logic low (VOL)	-0.01	0	0.01	
SELMPP[1:0]	Configuration pins for the MPP evaluation (see Table 9).	Logic high (VOH)	Connect to BUCK			
		Logic low (VOL)	Connect to GND			
CFG[2:0]	Configuration pins for the storage element (see Table 8).	Logic high (VOH)	Connect to BUCK			
		Logic low (VOL)	Connect to GND			
STONBATT	Configuration pin to select the energy source during the cold start.	Logic high (VOH)	Connect to BATT			
		Logic low (VOL)	Connect to GND			

Table 5: Recommended operating conditions

Note 1: ENHV can be dynamically driven by a logic signal from the LV domain. For a static usage, connect to BUCK (High) or GND (Low).
Note 2: ENLV can be dynamically driven by a logic signal from the HV domain. For a static usage, connect to BUCK or BOOST (High) or GND (Low).
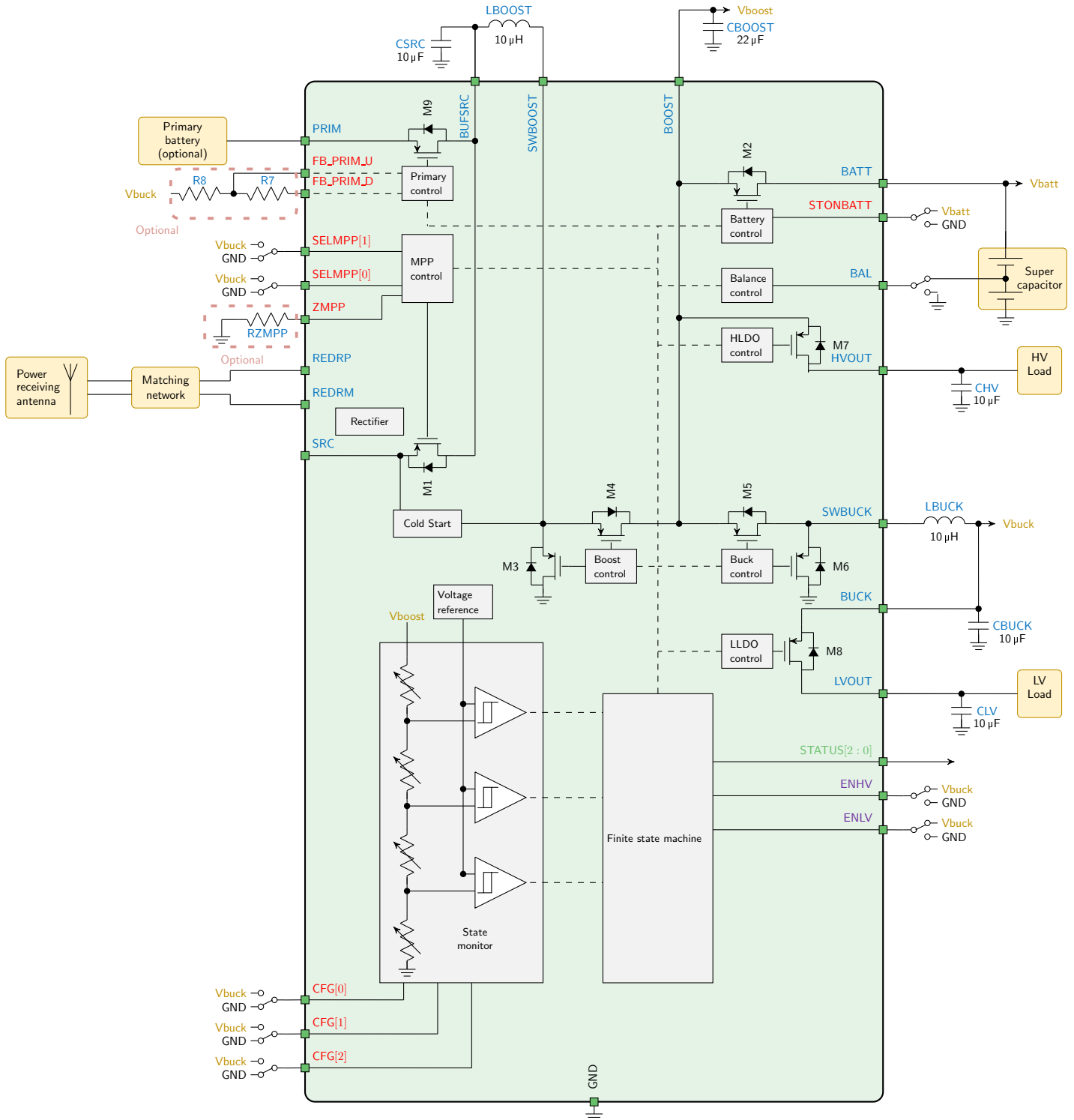
6 Functional Block Diagram
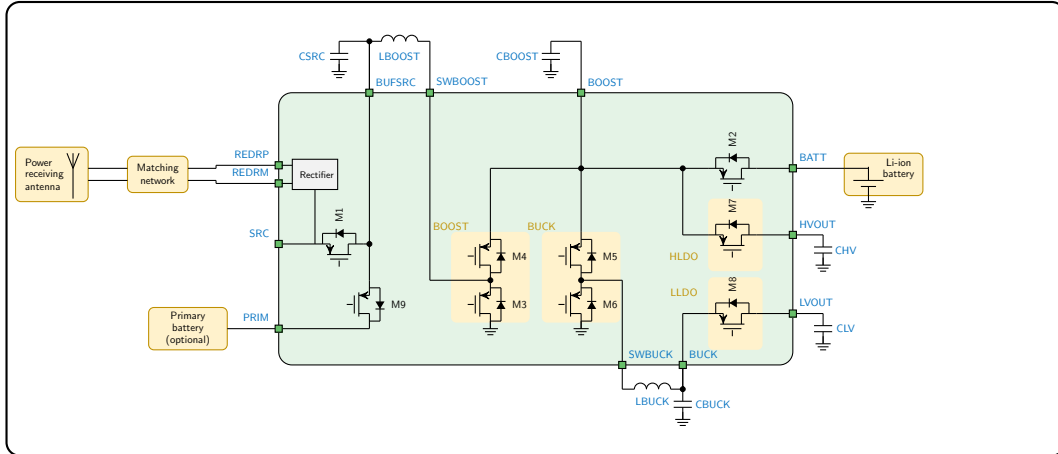

Figure 3: Functional block diagram

Figure 4: Simplified schematic view of the AEM40940

7 Theory of Operation

7.1 Deep sleep & Wake up modes

The DEEP SLEEP MODE is a state where all nodes are deeply discharged and there is no available energy to be harvested. As soon as the required cold-start input power (See Table 6) is available at the input of the matching network, (See Table 6 for the corresponding RF input power), the WAKE UP MODE is activated. Vboost and Vbuck rises up to a voltage of 2.2 V. Vboost then rises alone up to Vovch.

At that stage, both LDOs are internally deactivated. Therefore, STATUS[0] is equal to 0 as shown in Figure 8 and Figure 9.

When Vboost reaches Vovch, two scenarios are possible: in the first scenario, a super-capacitor or a capacitor having a voltage lower than Vchrdy is connected to the BATT node. In the second scenario, a charged battery is connected to the BATT node.

Frequency [MHz]	Pin [dBm]	Pin [µW]
868	-18.5	14.1
915	-19.5	11.2
2450	-12	63

Table 6: Minimum input power for the cold start (typical). Results obtained with the matching network designed by e-peas

Supercapacitor as a storage element
If the storage element is a supercapacitor, the storage element may need to be charged from 0 V. If combined with the boost converter, the rectifier charges BATT from the input source and by modulating the conductance of M2. During the charge of the BATT node, both LDOs are deactivated and STATUS[0]

is de-asserted. When Vbatt reaches Vchrdy, the circuit enters NORMAL MODE, STATUS[0] is asserted and the LDOs can be activated by the user using the ENLV and ENHV control pins as shown in Figure 8.

Battery as a storage element
If the storage element is a battery, but its voltage is lower than Vchrdy, then the storage element first needs to be charged until it reaches Vchrdy. Once Vbatt exceeds Vchrdy, or if the battery was initially charged above Vchrdy, the circuit enters NORMAL MODE. STATUS[0] is asserted and the LDOs can be activated by the user thanks to ENLV and ENHV as shown in Figure 9.
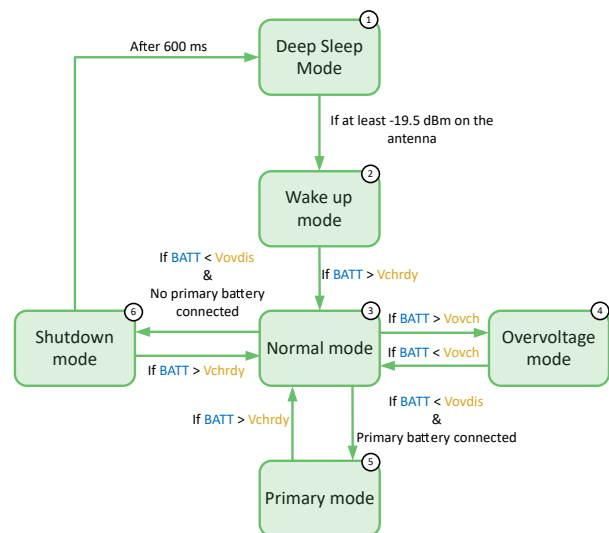

Figure 5: Diagram of the AEM40940 modes

7.2 Normal mode

Once the AEM enters NORMAL MODE, three scenarios are possible:

- There is enough power provided by the source to maintain Vbatt above Vovdis but Vbatt is below Vovch. In that case, the circuit remains NORMAL MODE.
- The source provides more power than the load consumes, and Vbatt increases above Vovch, the circuit enters into the OVERVOLTAGE MODE, as explained in the Overvoltage mode section.
- Due to a lack of power from the source, Vbatt falls below Vovdis. In this case, either the circuit enters SHUTDOWN MODE as explained in Shutdown mode section or, if a charged primary battery is connected on PRIM, the circuit enters PRIMARY MODE as explained in the Primary mode section.

Matching network

The AEM40940 uses an RF antenna as input power supply. The matching network modifies the impedance relationship between the RF source and the AEM40940 in order to optimize the low power transfer over a frequency band and an input power range. A matching network, optimized for low input power, is available (See Page 23). It is connected to the internal rectifier via the pins REDRP and REDRM.

Rectifier

The rectifier takes the RF AC signal as an input and converts it into a DC signal. The output of the low power rectifier is connected on SRC, which is connected to the input of the boost converter (BUFSRC) through M1.

Boost

The boost (or step-up) converter raises the voltage available at BUFSRC to a level suitable for charging the storage element, in the range of 2.2 V to 4.5 V, according to the system configuration. This voltage (Vboost) is available at the BOOST pin. The switching transistors of the boost converter are M3 and M4, with the switching node available externally at SWBOOST. The reactive power components of this converter are the external inductor and capacitor LBOOST and CBOOST. Periodically, the MPP control circuit disconnects the rectifier from the BUFSRC pin with the transistor M1 in order to measure the open-circuit voltage of the rectifier on SRC and define the optimal level of voltage. BUFSRC is decoupled by the capacitor CSRC, which smooths the voltage against the current pulses induced by the boost converter.

The storage element is connected to the BATT pin, at a voltage Vbatt. This node is linked to BOOST through the transistor M2. In NORMAL MODE, this transistor effectively shorts the battery to the BOOST node (Vbatt = Vboost). When energy harvesting is occurring, the boost converter delivers a current that is shared between the battery and the loads. M2 is

opened to disconnect the storage element when Vbatt reaches Vovdis. However, in such a scenario, the AEM40940 offers the possibility of connecting a primary battery to recharge Vbatt up to the Vchrdy. The transistor M9 connects PRIM to BUFSRC and the transistor M1 is opened to disconnect the rectifier as explained in the Primary mode section and shown in Figure 12.

Buck

The buck (or step-down) converter lowers the voltage from Vboost to a constant Vbuck value of 2.2 V. This voltage is available at the BUCK pin. The switching transistors of the buck converter are M5 and M6, with the switching node available externally at SWBUCK. The reactive power components of the buck converter are the external inductor LBUCK and the capacitor CBUCK.

LDO outputs

Two LDOs are available to supply loads at different operating voltages:

Through M7, Vboost supplies the high-voltage LDO that powers its load through HVOUT. This regulator delivers a clean voltage (Vhv) with a maximum current of 80 mA on HVOUT. An output voltage of 1.8 V, 2.5 V or 3.3 V can be selected. The high-voltage output can be dynamically enabled or disabled with the logic control pin ENHV. The output is decoupled by the external capacitor CHV.

Through M8, Vbuck supplies the low-voltage LDO that powers its load through LVOUT. This regulator delivers a clean voltage (Vlv) of 1.8 V or 1.2 V with a maximum current of 20 mA on LVOUT. The low-voltage output can be dynamically enabled or disabled with the logic control pin ENLV. The output is decoupled by the external capacitor CLV.

Status pin STATUS[0] alerts the user when the LDOs can be enabled as explained in the Deep sleep & Wake up modes section and in the Shutdown mode section. The table below shows the four possible configurations:

ENLV	ENHV	LV output	HV output
1	1	Enabled	Enabled
1	0	Enabled	Disabled
0	1	Disabled	Enabled
0	0	Disabled	Disabled

Table 7: LDOs configurations

7.3 Overvoltage mode

When Vbatt reaches Vovch, the charge is complete and the internal logic maintains Vbatt around Vovch with a hysteresis of a few mV as shown in Figure 10 to prevent damage to the storage element and to the internal circuitry. In this configuration, the boost converter is periodically activated to maintain Vbatt and the LDOs are still available.

7.4   Primary mode

When Vbatt drops below Vovdis, the circuit compares the voltage on PRIM with the voltage on FB_PRIM_U to determine whether a charged primary battery is connected on PRIM. The voltage on FB_PRIM_U is set thanks to two optional resistances as explained in the Primary battery configuration section. If the voltage on PRIM divided by 4 is higher than the voltage on FB_PRIM_U, the circuit considers the primary battery as available and the circuit enters PRIMARY MODE as shown in Figure 12.

In that mode, transistor M1 is opened and the primary battery is connected to BUFSRC through transistor M9 to become the source of energy for the AEM40940. The chip remains in this mode until Vbatt reaches Vchrdy. When Vbatt reaches Vchrdy, the circuit enters NORMAL MODE. As long as the chip is in PRIMARY MODE, STATUS[1] is asserted.

If no primary battery is used in the application, PRIM, FB_PRIM_U and FB_PRIM_D must be tied to GND.

7.5   Shutdown mode

When Vbatt drops below Vovdis and no power is available from a primary battery, the circuit enters SHUTDOWN MODE as shown in Figure 11 to prevent deep discharge potentially leading to damage to the storage element and instability of the LDOs. The circuit asserts STATUS[1] to warn the system that a shutdown will occur. Both LDO regulators remain enabled. If no primary battery is used, this allows the load, whether it is powered on LVOUT or HVOUT, to be interrupted by the low-to-high transition of STATUS[1], and to take all appropriate actions before power shutdown.

If energy at the input source is available and Vbatt recovers to Vchrdy within Tcrit (∼ 600 ms), the AEM returns in NORMAL MODE. But if, after Tcrit, Vbatt does not reach Vchrdy, the circuit enters DEEP SLEEP MODE. The LDOs are deactivated and BATT is disconnected from BOOST to avoid damaging the battery due to the overdischarge. From now, the AEM will have to go through the wake-up procedure described in the Deep sleep & Wake up modes section.

7.6   Maximum power point tracking

During NORMAL MODE, SHUTDOWN MODE and a part of WAKE UP MODE, the boost converter is regulated thanks to an internal MPPT (Maximum Power Point Tracking) module. Vmpp is the voltage level of the MPP, and depends on the input power available at the source. The MPPT module evaluates Vmpp as a given fraction of Voc, the open-circuit voltage of the rectifier. By temporarily disconnecting the rectifier from CSRC as shown in Figure 4 for 5.12 ms, the MPPT module receives from and maintains knowledge of Vmpp. This sampling occurs approximatively every 0.33 s .

With the exception of this sampling process, the voltage of the rectifier output, Vsrc, is continuously compared to Vmpp. When Vsrc exceeds Vmpp by a small hysteresis, the boost converter is switched on, extracting electrical charges from the source and lowering its voltage. When Vsrc falls below Vmpp by a small hysteresis, the boost converter is switched off, allowing the harvester to accumulate new electrical charges into CSRC, which restores its voltage. In this manner, the boost converter regulates its input voltage so that the electrical current (or flow of electrical charges) that enters the boost converter yields the best power transfer from the harvester under any ambient conditions. The AEM40940 supports any Vmpp level in the range from 0.05 V to 2.5 V. It offers a choice of three values for the Vmpp/Voc fraction or to match the input impedance of the BOOST converter with an impedance connected to the ZMPP terminal through configuration pins SELMPP[1:0] as shown in Table 9. The status of the MPPT controller is reported through one dedicated status pins (STATUS[2]). The status pin is asserted when a MPP calculation is being performed.

7.7   Balun for dual-cell supercapacitor

The balun circuit allows users to balance the internal voltage in a dual-cell supercapacitor in order to avoid damaging the super-capacitor because of excessive voltage on one cell. If BAL is connected to GND, the balun circuit is disabled. This configuration must be used if a battery, a capacitor or a single-cell supercapacitor is connected on BATT. If BAL is connected to the node between the cells of a supercapacitor, the balun circuit compensates for any mismatch of the two cells that could lead to over-charge of one of both cells. The balun circuit ensures that BAL remains close to Vbatt/2. This configuration must be used if a dual-cell supercapacitor is connected on BATT.

8   System Configuration

Configuration pins			Storage element threshold voltages			LDOs output voltages		Typical use
CFG[2]	CFG[1]	CFG[0]	Vovch	Vchrdy	Vovdis	Vhv	Vlv	
1	1	1	4.12 V	3.67 V	3.60 V	3.3 V	1.8 V	Li-ion battery
1	1	0	4.12 V	4.04 V	3.60 V	3.3 V	1.8 V	Solid state battery
1	0	1	4.12 V	3.67 V	3.01 V	2.5 V	1.8 V	Li-ion/NiMH battery
1	0	0	2.70 V	2.30 V	2.20 V	1.8 V	1.2 V	Single-cell supercapacitor
0	1	1	4.50 V	3.67 V	2.80 V	2.5 V	1.8 V	Dual-cell supercapacitor
0	1	0	4.50 V	3.92 V	3.60 V	3.3 V	1.8 V	Dual-cell supercapacitor
0	0	1	3.63 V	3.10 V	2.80 V	2.5 V	1.8 V	LiFePO4 battery
0	0	0	Reserved for future use					

Table 8: Usage of CFG[2:0]

8.1   Battery and LDOs configuration

Through three configuration pins (CFG[2:0]), the user can set a particular operating mode without any dedicated external component as shown in Table 8. The three threshold levels are defined as:

- Vovch : Maximum voltage accepted on the storage element before disabling the boost converter,

- Vchrdy : Minimum voltage required on the storage element after a cold start before enabling the LDOs,

- Vovdis : Minimum voltage accepted on the storage element before considering the storage element as depleted.

See Theory of Operation section for more information about the purposes of these thresholds.

The two LDOs output voltages are called Vhv and Vlv for the high- and low-output voltages, respectively. Seven combinations of these voltage levels are hardwired and selectable through the CFG[2:0] configuration pins.

8.2   MPPT configuration

Two dedicated configuration pins, SELMPP[1:0], allow selecting the MPP tracking ratio based on the characteristic of the input power source.

SELMPP[1]	SELMPP[0]	Vmpp/Voc
0	0	60 %
0	1	65 %
1	0	70 %
1	1	ZMPP

Table 9: Usage of SELMPP[1:0]

8.3   Primary battery configuration

To use the primary battery, it is mandatory to determine Vprim_min, the voltage of the primary battery at which it has to be considered as empty. During the evaluation of Vprim_min, the circuit connects FB_PRIM_D to GND. The circuit uses a resistive divider between BUCK and FB_PRIM_D to define the voltage on FB_PRIM_U as Vprim_min divided by 4. When Vprim_min is not evaluated, FB_PRIM_D is left floating to avoid quiescent current on the resistive divider. If we define the total resistor (R7 + R8) as RP, R7 and R8 are calculated as:

- $100 \text{ k}\Omega \leq \text{RP} \leq 500 \text{ k}\Omega$

- $\text{R7} = (\frac{\text{Vprim\_min}}{4} * \text{RP})/2.2 \text{ V}$

- R8=RP-R7

Note that FB_PRIM_U and FB_PRIM_D must be tied to GND if no primary battery is used.

8.4   ZMPPT configuration

Instead of working at a ratio of the open-circuit voltage, the AEM40940 can regulate the input impedance of the BOOST converter so that it matches a constant impedance connected to the ZMPP pin (RZMPP). In this case, the AEM40940 regulates Vsrc at a voltage equals to the product of the ZMPP impedance and the current available at the rectifier output.

- $10 \ \Omega \leq \text{RZMPP} \leq 1 \text{ M}\Omega$

8.5   Start-on-battery configuration

Alternatively to the cold-start procedure described in Deep sleep & Wake up modes section, by connecting STONBATT to BATT, the circuit can also start with the energy provided by the storage element connected on BATT if its voltage is higher than Vchrdy. Note the AEM40940 will not start if the voltage on BATT is lower than Vchrdy.

8.6   No-battery configuration

If the harvested energy source is permanently available and covers the application purposes or if the application does not need to store energy when the harvested energy source is not available, the storage element may be replaced by an external capacitor CBATT of minimum 150 μF.

8.7   Storage element information

The energy storage element of the AEM40940 can be a rechargeable battery, a supercapacitor or a large capacitor (minimum 150 μF). It should be chosen so that its voltage does not fall below Vovdis even during occasional peaks of the load current. If the internal resistance of the storage element cannot sustain this voltage limit, it is advisable to buffer the battery with a capacitor.

The BATT pin that connects the storage element must never be left floating. If the application expects a disconnection of the battery (e.g. because of a user removable connector), the

PCB should include a capacitor of at least 150 μF. The leakage current of the storage element should be small as leakage currents directly impact the quiescent current of the subsystem.

External inductors information

The AEM40940 operates with two standard miniature inductors of 10 μH. LBOOST and LBUCK must respectively sustain a peak current of at least 250 mA and 50 mA and a switching frequency of at least 10 MHz. Low equivalent series resistance (ESR) favors the power conversion efficiency of the boost and buck converters.

External capacitors information

The AEM40940 operates with four identical standard miniature ceramic capacitors of 10 μF and one miniature ceramic capacitor of 22 μF. The leakage current of the capacitors should be small as leakage currents directly impact the quiescent current of the subsystem.

CSRC

This capacitor acts as an energy buffer at the input of the boost converter. It prevents large voltage fluctuations when the boost converter is switching. The recommended value is 10 μF +/- 20 %.

CBUCK

This capacitor acts as an energy buffer for the buck converter. It also reduces the voltage ripple induced by the current pulses inherent to the switched mode of the converter. The recommended value is 10 μF +/- 20 %.

CBOOST

This capacitor acts as an energy buffer for the boost converter. It also reduces the voltage ripple induced by the current pulses inherent to the switched mode of the converter. The recommended value is 22 μF +/- 20 %.

CHV and CLV

These capacitors ensure a high-efficiency load regulation of the high-voltage and low-voltage LDO regulators. Closed-loop stability requires the value to be in the range of 8 μF to 14 μF.

9 Typical Application Circuits
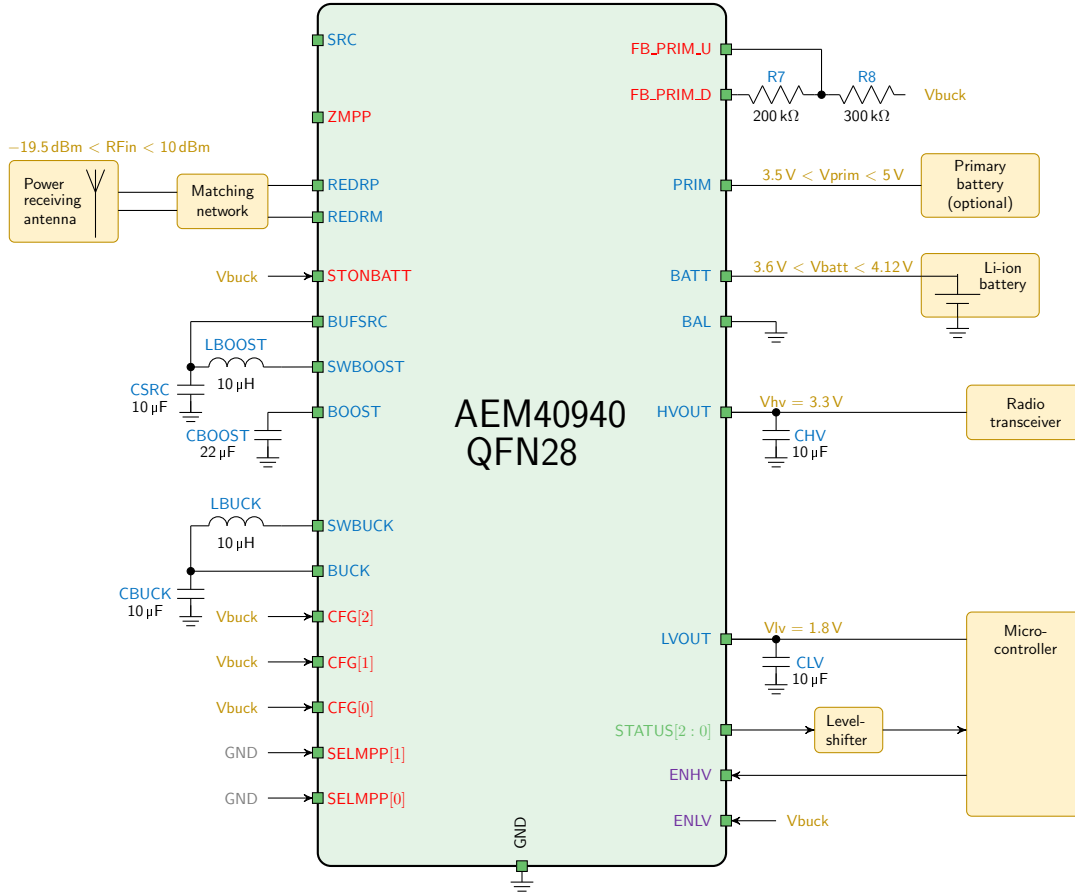
9.1 Example circuit 1

Figure 6: Typical application circuit 1

The energy source is a RF source, and the storage element is a standard Li-ion battery cell. The radio communication makes use of a transceiver that operates from a 3.3 V supply. A micro-controller supplied by a 1.8 V supply controls the application.

STONBATT is tied to BATT, bypassing the cold-start procedure to start thanks to the energy stored in the pre-charged Li-ion battery cell.

This circuit uses an operating mode, typical of systems that use standard components for radio and energy storage.

The operating mode pins are connected to:

- CFG[2:0] = 111

Referring to Table 8, in this mode, the threshold voltages are:

- Vovch = 4.12 V

- Vchrdy = 3.67 V

- Vovdis = 3.60 V

Moreover, the LDOs output voltages are:

- Vhv = 3.3 V

- Vlv = 1.8 V

A primary battery is also connected as a back-up solution. The minimal level allowed on this battery is set at 3.5 V. Following equations on Page 11:

- RP = 0.5 MΩ

- R7 = ($\frac{3.5\ \text{V}}{4}$*0.5 MΩ)/2.2 V = 200 kΩ

- R8 = 0.5 MΩ-200 kΩ = 300 kΩ

The MPP configuration pins SELMPP[1:0] are tied to GND (logic low), selecting an MPP ratio of 60 %.

The ENLV enable pin for the low-voltage LDO is tied to BUCK. The microcontroller will be enabled after system wake-up.

The application software can enable or disable the radio transceiver with a GPIO connected to ENHV.
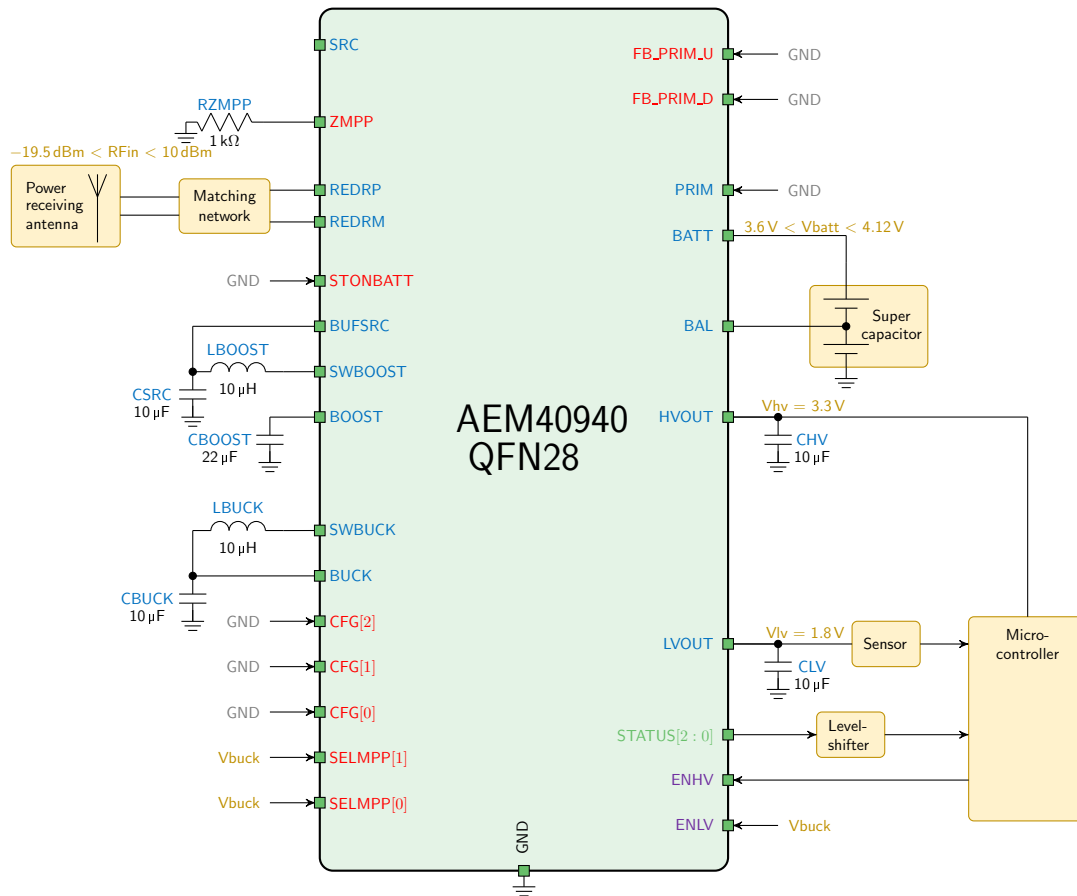
9.2 Example circuit 2

AEM40940
QFN28

Figure 7: Typical application circuit 2

The energy source is an RF source, and the storage element is a dual-cell supercapacitor. The supercapacitor can be completely depleted during the cold start. Consequently, STONBATT is tied to GND to use the input energy source.

Moreover, BAL is connected to the dual-cell supercapacitor to compensate for any mismatch between the two cells and in that way protect the supercapacitor.

A micro-controller pilots and collects information from a sensor. The operating mode pins are connected to:

- CFG[2:0]= 010

Referring to Table 8, in this operation mode, the threshold voltages are:

- Vovch = 4.5 V

- Vchrdy = 3.92 V

- Vovdis = 3.60 V

Moreover, the LDOs output voltages are:

- Vhv = 3.3 V

- Vlv = 1.8 V

The ENHV enable pin for the high-voltage LDO is tied to BUCK. The microcontroller is enabled when Vbatt and Vboost exceeds Vchrdy as the high-voltage regulator supplies it.

The MPP configuration pins SELMPP[1:0] are tied to BUCK (logic high), selecting the ZMPPT configuration to match a 1 KΩ impedance.

No primary battery is connected and the PRIM, FB_PRIM_U and FB_PRIM_D pins are tied to GND.

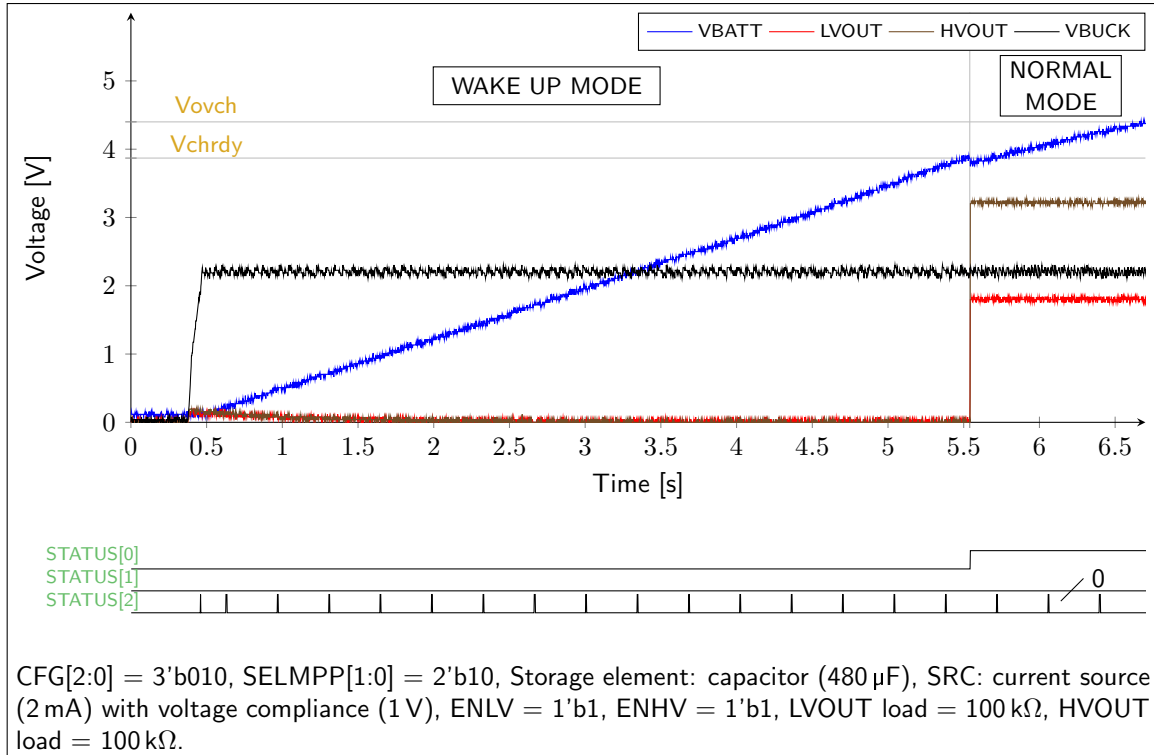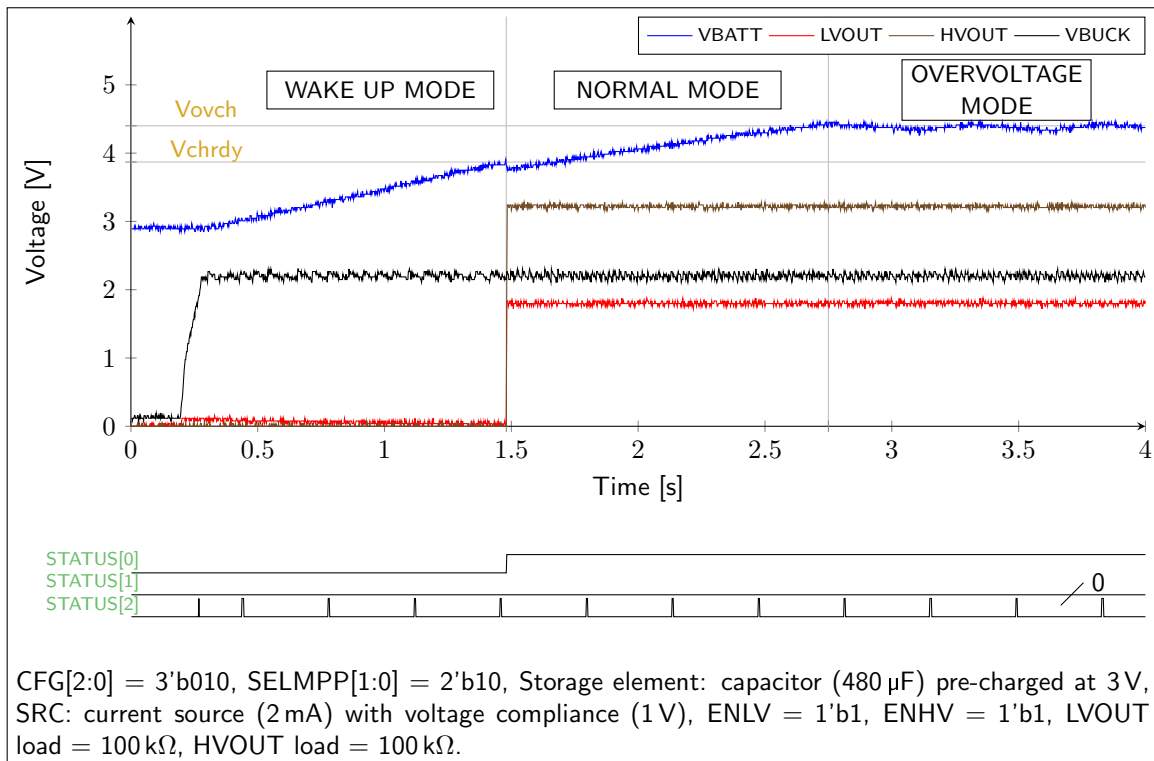*Figure 8: Cold start with a capacitor connected to BATT*

CFG[2:0] = 3'b010, SELMPP[1:0] = 2'b10, Storage element: capacitor (480 μF), SRC: current source (2 mA) with voltage compliance (1 V), ENLV = 1'b1, ENHV = 1'b1, LVOUT load = 100 kΩ, HVOUT load = 100 kΩ.

Figure 9: Cold start with a battery connected to BATT

CFG[2:0] = 3'b010, SELMPP[1:0] = 2'b10, Storage element: capacitor (480 μF) pre-charged at 3 V, SRC: current source (2 mA) with voltage compliance (1 V), ENLV = 1'b1, ENHV = 1'b1, LVOUT load = 100 kΩ, HVOUT load = 100 kΩ.

CFG[2:0] = 3'b111, SELMPP[1:0] = 2'b00, Storage element: capacitor (4.85 mF), SRC: current source (1 mA) with voltage compliance (3 V), ENLV = 1'b1, ENHV = 1'b1, LVOUT load = 22 kΩ, HVOUT load = 22 kΩ.

Figure 10: Overvoltage mode

CFG[2:0] = 3'b010, SELMPP[1:0] = 2'b10, Storage element: capacitor (4.85 mF), SRC: current source (2 mA) with voltage compliance (1 V), ENLV = 1'b1, ENHV = 1'b1, LVOUT load = 10 kΩ, HVOUT load = 10 kΩ.

Figure 11: Shutdown mode (without primary battery)
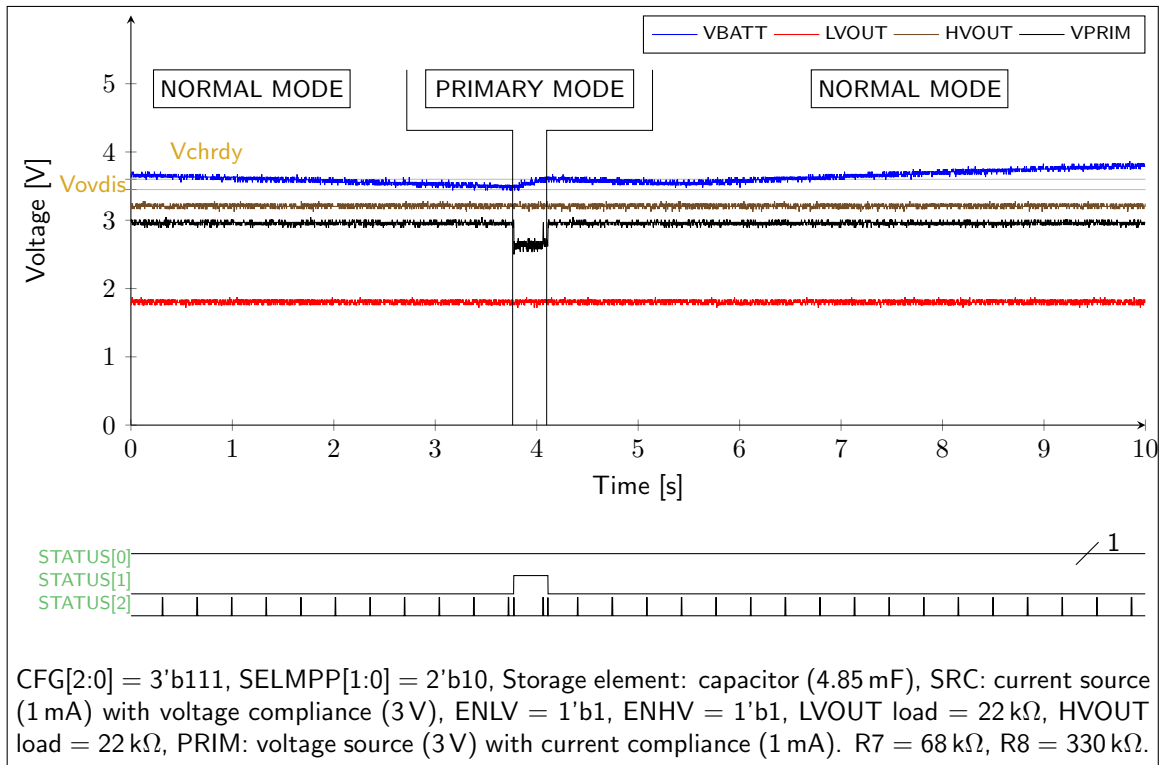
Figure 12: Switch to primary battery if the battery is overdischarged

10 Performance Data

10.1 BOOST conversion efficiency
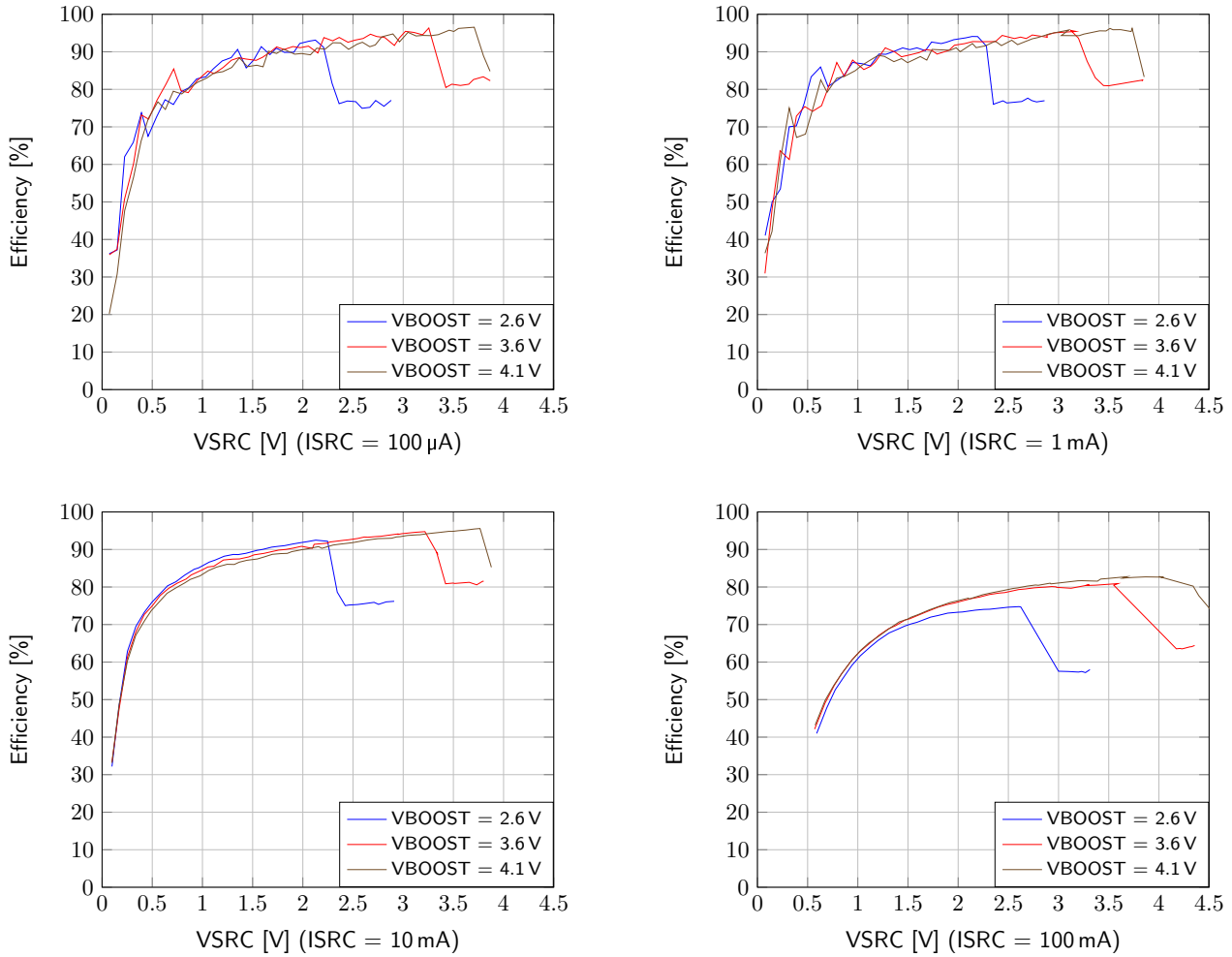
Figure 13: Boost efficiency for current delivered by the rectifier at 100 µA, 1 mA, 10 mA and 100 mA

10.2 Quiescent current
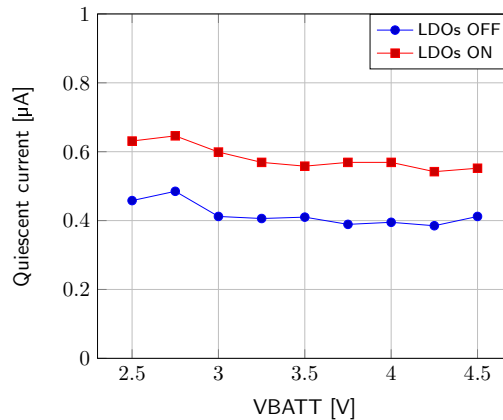
Figure 14: Quiescent current with LDOs on and off
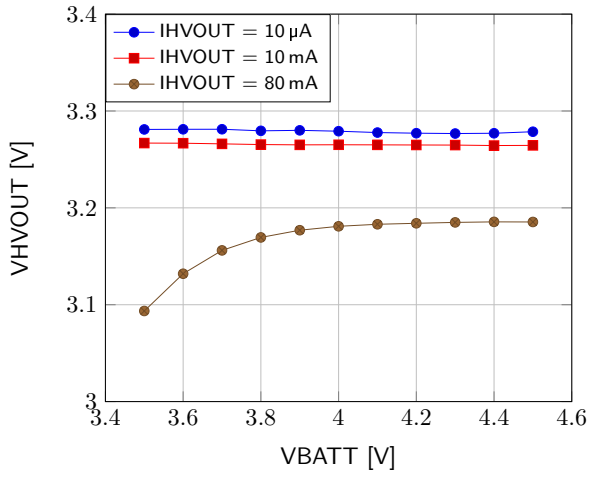
10.3 High-voltage LDO regulation
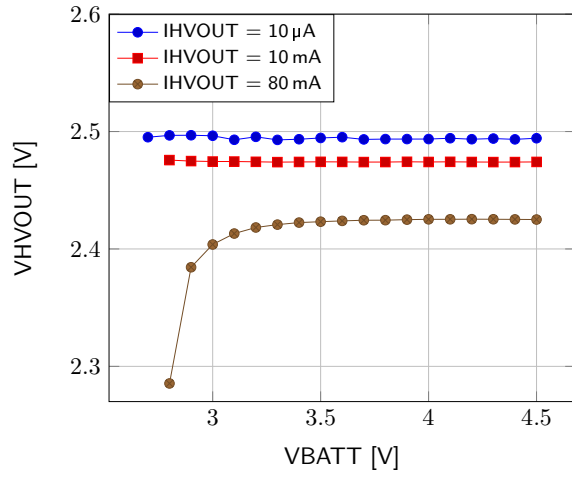
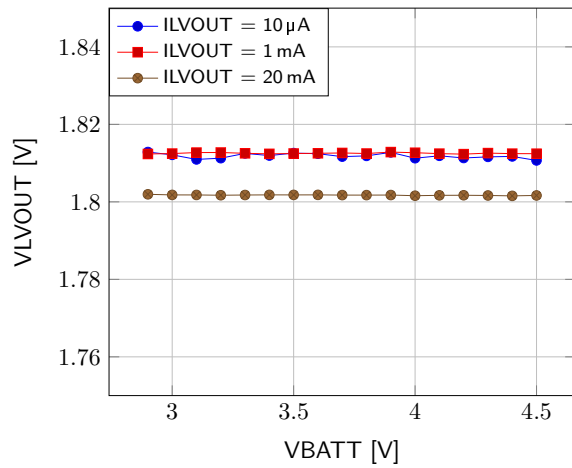*Figure 15: HVOUT at 3.3 V and 2.5 V*
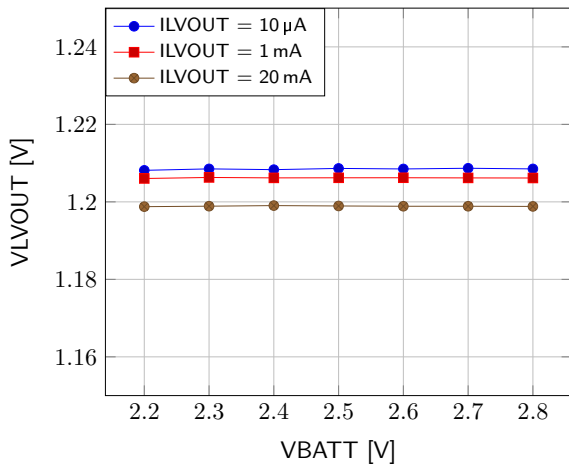
10.4 Low-voltage LDO regulation

Figure 16: LVOUT at 1.2 V and 1.8 V

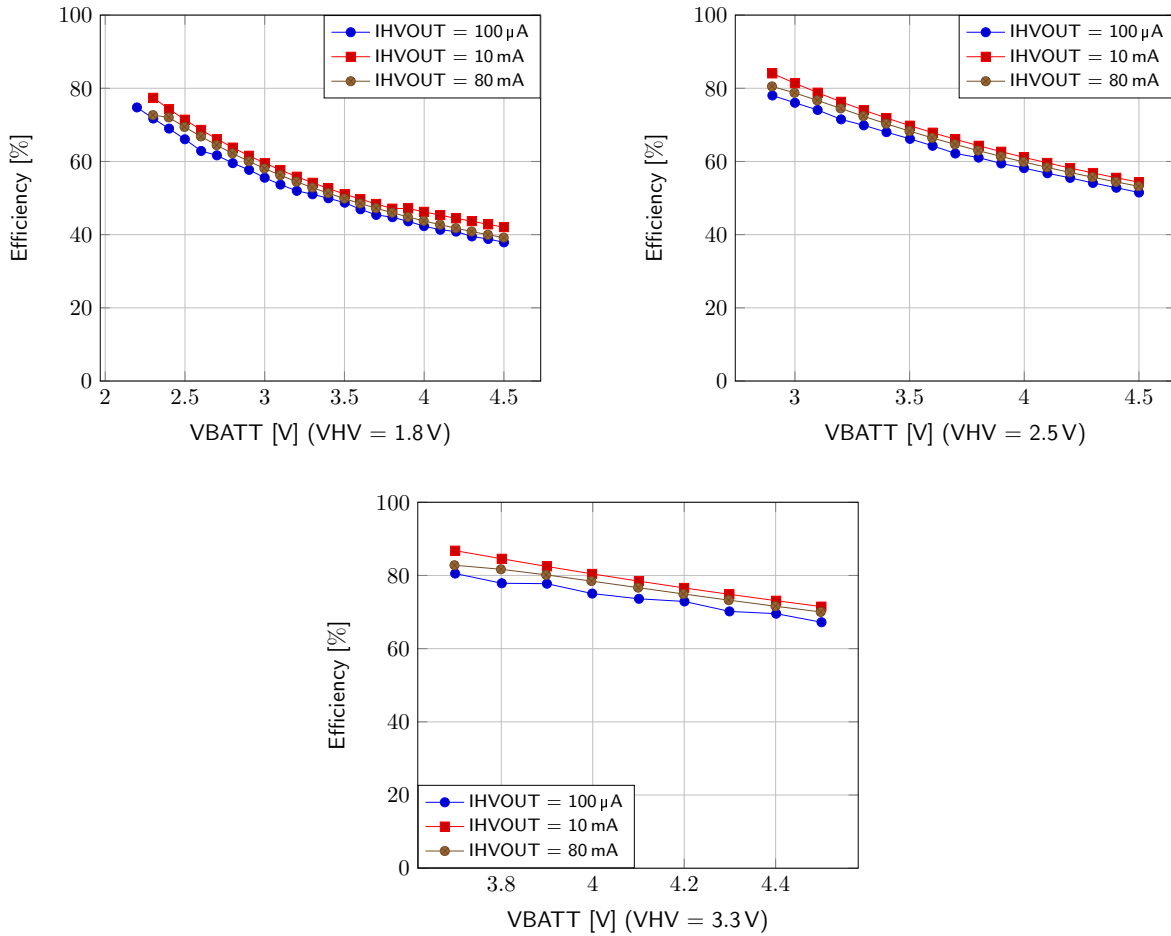## 10.5   High-voltage LDO efficiency

Figure 17: HVOUT efficiency at 1.8 V, 2.5 V and 3.3 V

The theoretical efficiency of a LDO can be simply calculated as $\frac{V_{out}}{V_{in}}$ if quiescent current can be neglected with regards to the output current. In the case of the high-voltage LDO, the theoretical efficiency is equal to $\frac{V_{hv}}{V_{batt}}$.
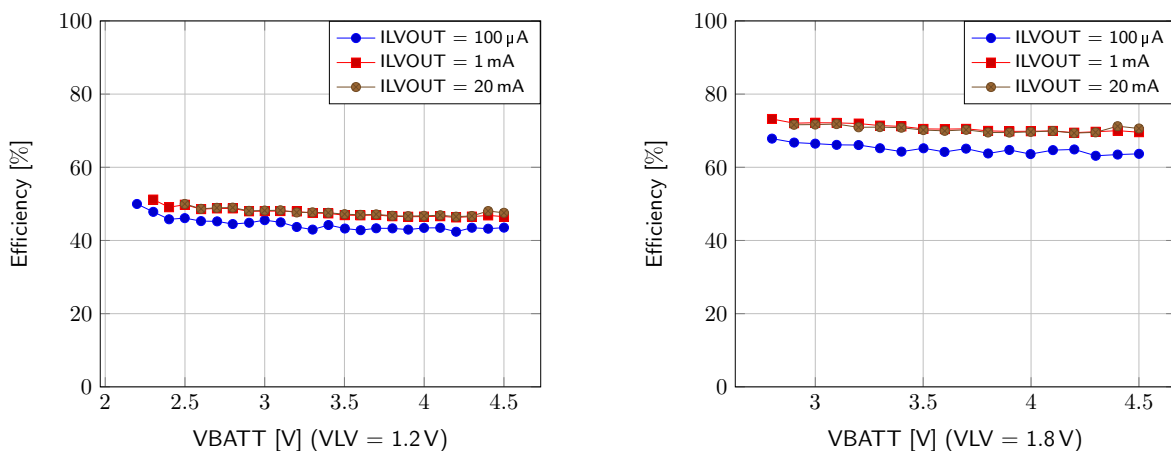
10.6   Low-voltage LDO efficiency

Figure 18: Efficiency of BUCK cascaded with LVOUT at 1.2 V and 1.8 V

The theoretical efficiency of the low-voltage LDO is equal to $\frac{V_{lv}}{V_{buck}}$. Starting from the battery, the efficiency of the buck converter has to be taken into account (see Figure 4). The efficiency between Vbatt and Vlv is therefore equal to $\eta_{buck}\frac{V_{lv}}{V_{buck}}$.

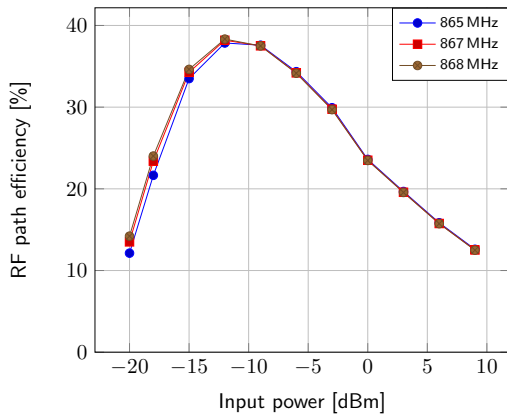## 10.7   RF path efficiency

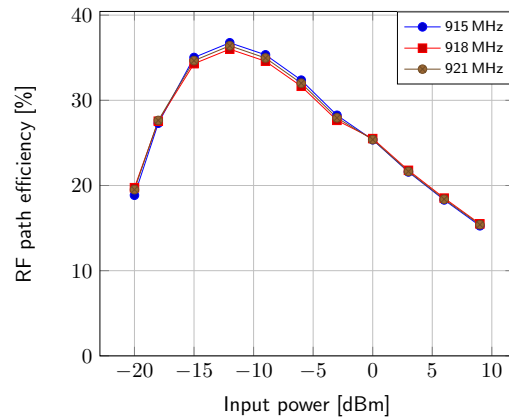

Figure 19: Efficiency for 868 MHz band

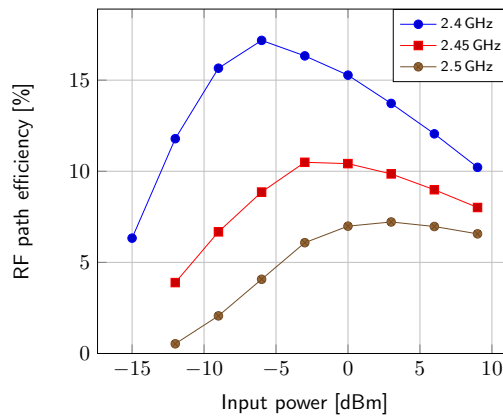Figure 20: Efficiency for 915 MHz band

Figure 21: Efficiency for 2.4 GHz band

The RF path efficiency is defined as the ratio between the power available at the output of the rectifier (SRC) and the power at the input of the matching network (50 Ω single input SMA).
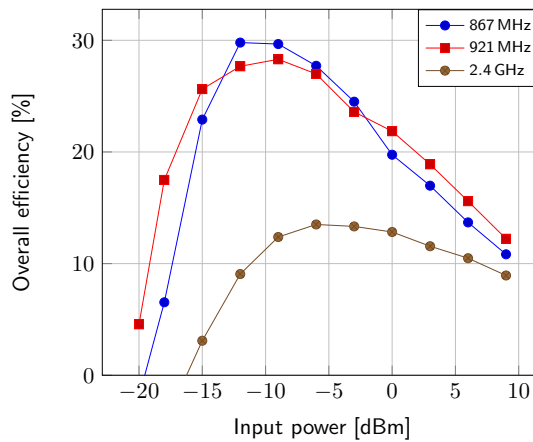
10.8   Overall efficiency

Figure 22: Overall efficiency (RF path and boost converter) with VBOOST = 4.5 V

The overall efficiency is defined as the ratio between the power available at the output of the boost converter and the power at the input of the matching network (50 Ω single input SMA).
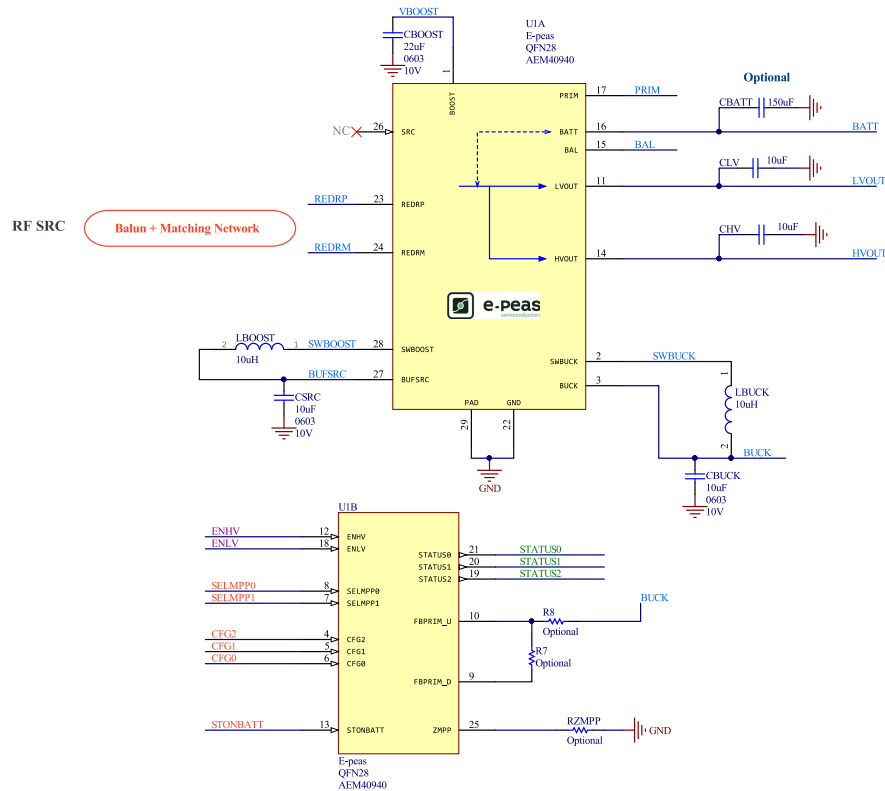
11 Schematic

11.1 AEM schematic

Figure 23: Schematic example

Designator	Description	Quantity	Supplier	Link
CBOOST	Ceramic Cap 22 μF, 10 V, 20 %, X5R 0603	1	Farnell	http://be.farnell.com/2426957
CBUCK	Ceramic Cap 10 μF, 10 V, 20 %, X5R	1	Farnell	http://be.farnell.com/2309028
CHV	Ceramic Cap 10 μF, 10 V, 20 %, X5R	1	Farnell	http://be.farnell.com/2309028
CLV	Ceramic Cap 10 μF, 10 V, 20 %, X5R	1	Farnell	http://be.farnell.com/2309028
CSRC	Ceramic Cap 10 μF, 10 V, 20 %, X5R	1	Farnell	http://be.farnell.com/2309028
LBOOST	Power Inductor 10 μH - 0,55 A - LPS4012	1	Farnell	http://be.farnell.com/2408076
LBUCK	Power Inductor 10 μH - 0,25 A	1	Farnell	http://be.farnell.com/2215635
U1	AEM40940 - Symbol QFN28	1		order at sales@e-peas.com
	Matching network	1		more details at support@e-peas.com

Table 10: BOM example for AEM40940 and its required passive components
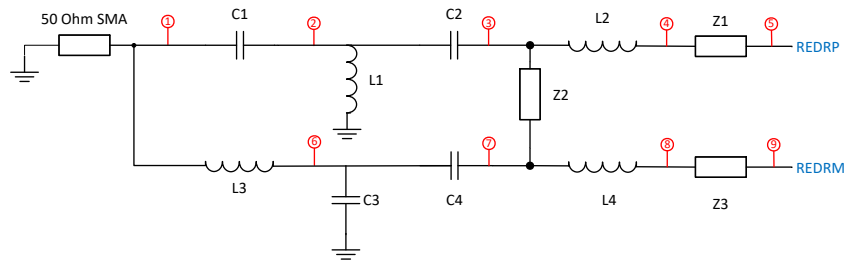
11.2 Matching network schematic

Figure 24: Proposed matching network for a 50 Ω antenna (track impedance in red)

	Designator	Description	Manufacturer PN
868 MHz	C1	Ceramic Cap 2.7 pF KEMET HiQ	CBR02C279B5GAC
	C2	Ceramic Cap 100 pF 0402 HiQ	CBR04C101F3GAC
	C3	Ceramic Cap 2.7 pF KEMET HiQ	CBR02C279B5GAC
	C4	Ceramic Cap 100 pF 0402 HiQ	CBR04C101F3GAC
	L1	Power Inductor 12 nH - 0402 - LQW15A serie	LQW15AN12NG00D
	L2	Power Inductor 2.4 nH - 0402 - LQW15A serie	LQW15AN2N4B00D
	L3	Power Inductor 12 nH - 0402 - LQW15A serie	LQW15AN12NG00D
	L4	Power Inductor 2.4 nH - 0402 - LQW15A serie	LQW15AN2N4B00D
	Z1	Power Inductor 22 nH - 0402 - LQW15A serie	LQW15AN22NG00D
	Z2	Power Inductor 9.5 nH - 0402 - LQW15A serie	LQW15AN9N5G00D
	Z3	Power Inductor 22 nH - 0402 - LQW15A serie	LQW15AN22NG00D
915 MHz	C1	Ceramic Cap 2.2 pF KEMET HiQ	CBR02C229B5GAC
	C2	Ceramic Cap 100 pF 0402 HiQ	CBR04C101F3GAC
	C3	Ceramic Cap 2.2 pF KEMET HiQ	CBR02C229B5GAC
	C4	Ceramic Cap 100 pF 0402 HiQ	CBR04C101F3GAC
	L1	Power Inductor 12 nH - 0402 - LQW15A serie	LQW15AN12NG00D
	L2	Power Inductor 6.2 nH - 0402 - LQW15A serie	LQW15AN6N2D00D
	L3	Power Inductor 12 nH - 0402 - LQW15A serie	LQW15AN12NG00D
	L4	Power Inductor 6.2 nH - 0402 - LQW15A serie	LQW15AN6N2D00D
	Z1	Power Inductor 15 nH - 0402 - LQW15A serie	LQW15AN15NG00D
	Z2	Power Inductor 9.1 nH - 0402 - LQW15A serie	LQW15AN9N1G00D
	Z3	Power Inductor 15 nH - 0402 - LQW15A serie	LQW15AN15NG00D
2.45 GHz	C1	Ceramic Cap 0.7 pF KEMET HiQ	CBR04C708B5GAC
	C2	Ceramic Cap 100 pF 0402 HiQ	CBR04C101F3GAC
	C3	Ceramic Cap 0.7 pF KEMET HiQ	CBR04C708B5GAC
	C4	Ceramic Cap 100 pF 0402 HiQ	CBR04C101F3GAC
	L1	Power Inductor 4 nH - 0402 - LQW15A serie	LQW15AN4N0D8ZD
	L2	Power Inductor 3.3 nH - 0402 - LQW15A serie	LQW15AN3N3D10D
	L3	Power Inductor 4 nH - 0402 - LQW15A serie	LQW15AN4N0D8ZD
	L4	Power Inductor 3.3 nH - 0402 - LQW15A serie	LQW15AN3N3D10D
	Z1	none	
	Z2	Ceramic Cap 1.5 pF KEMET HiQ	CBR02C159B5GAC
	Z3	none	

Table 11: BOM example for AEM40940 matching networks and their required passive components

	1	2	3	4	5	6	7	8	9
868 MHz	50 Ω	50 Ω	50 Ω	50 Ω	W^3	50 Ω	50 Ω	50 Ω	W^3
915 MHz	50 Ω	50 Ω	50 Ω	50 Ω	W^3	50 Ω	50 Ω	50 Ω	W^3
2.45 GHz	50 Ω	50 Ω	50 Ω	W^3	W^3	50 Ω	50 Ω	W^3	W^3

Table 12: Recommended track impedance for AEM40940 matching network

Note 3: 'W' refers to the impedance of the track linking the AEM40940 and the closest components of the matching network (See subsection 12.1).
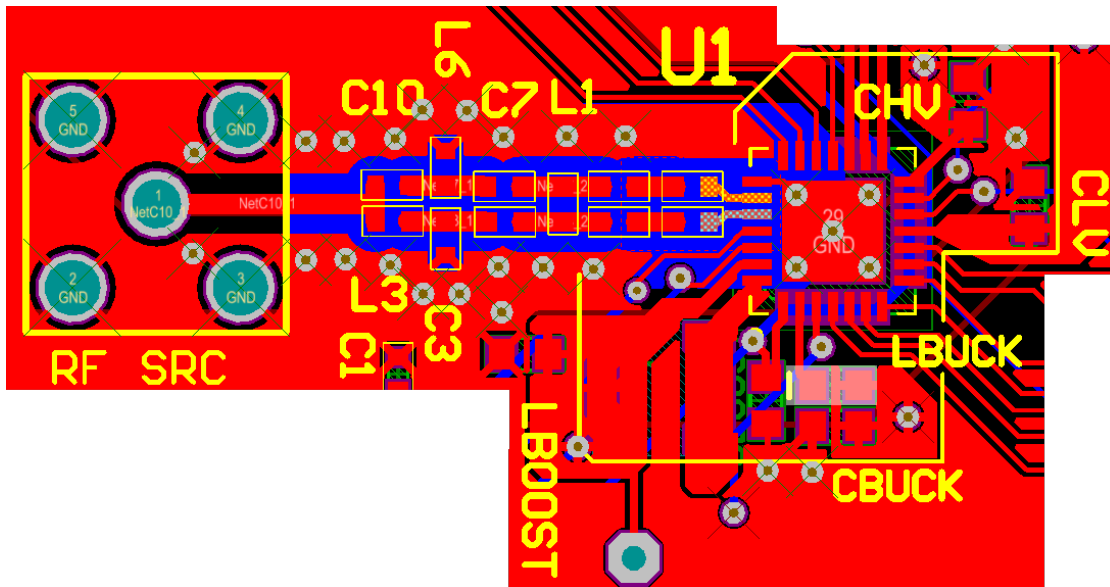
12   Layout

Figure 25: Layout example for the AEM40940 and its passive components

Note 4: Schematic, symbol and footprint for the e-peas component can be ordered by contacting the e-peas support: support@e-peas.com

12.1   RF layout consideration

The implementation of a printed circuit board (PCB) with RF layout must be made carefully and should adhere to the following recommended instructions:

- Referring to Figure 24 and Table 12, use a width of 0.6 mm for 50 Ω tracks and 0.3 mm for W tracks. These widths are valid for the recommended PCB stackup (See Figure 26).

- A GND plane must be placed below the RF path on the bottom layer.

- A GND plane on the top layer must be placed all around the RF path and with a clearance of 0.6 mm from the tracks.

- Vias must be placed all around the RF path and be directly connected to the top GND plane.

- Inductors connected to the AEM (Z1 and Z3 for 868 MHz and 915 MHz or L2 and L4 for 2.45 GHz on

Figure 24) must be placed as close as possible of the AEM40940 input pins and must have planes cropped below them.

- The recommended PCB stackup is a 4 layers with standard stack:

Figure 26: Recommended PCB stackup

13   Package Information

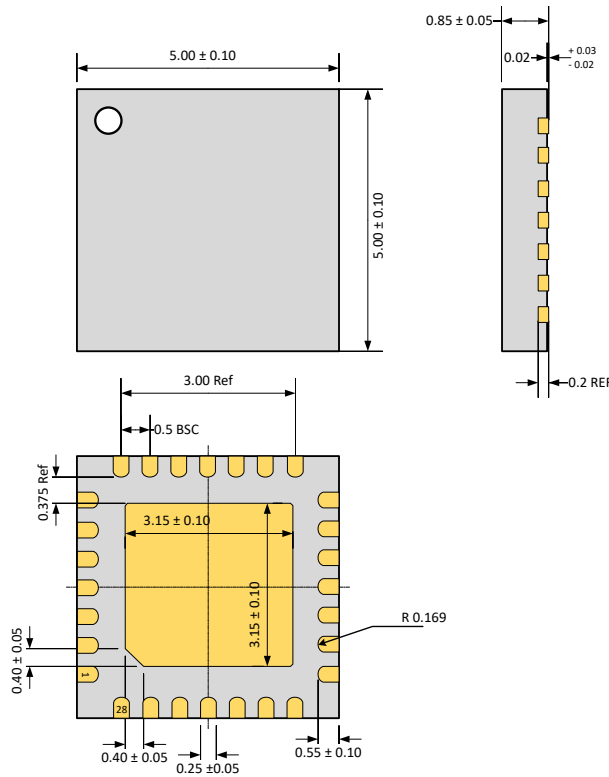## 13.1   Plastic quad flatpack no-lead (QFN28 5x5mm)

Figure 27: QFN28 5x5mm
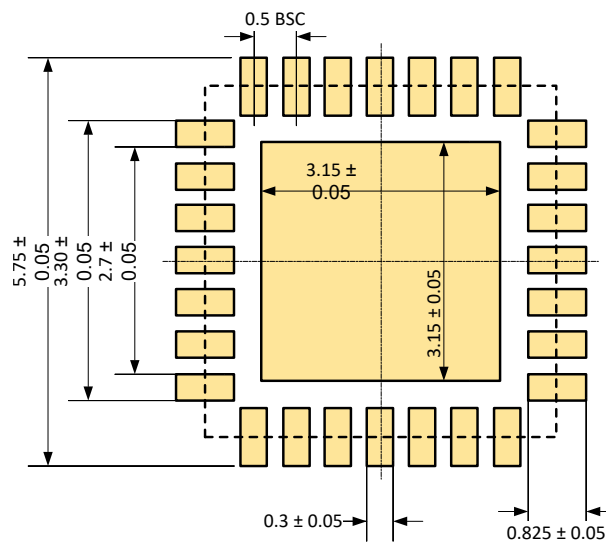
13.2   Board layout

Figure 28: Board layout

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PI3VST01ZEEX XRP7724ILB-1015-F PI5USB1458AZAEX PI5USB1468AZAEX TCKE712BNL,RF ISL91211AIKZT7AR5874
ISL91211BIKZT7AR5878 ISL91212AIIZ-TR5770 ISL91212BIIZ-TR5775 CPX200D AX-3005D-3 TP-1303 TP-1305 TP-1603 TP-2305
TP-30102 TP-4503N MIC5167YML-TR LR745N8-G STLUX383A TP-60052 LM26480SQ-AA/NOPB LM81BIMTX-3/NOPB
LM81CIMT-3/NOPB MIC5166YML-TR GPS-2303 GPS-3303 GPS-4303 TPS65920A2ZCHR MB39C811QN-G-EFE2 MAX881REUB+
NCV7680PWR2G UAA2016PG LTC2926CUFD#PBF L6718 MAX4069AUB+