

GS66508B-EVBDB1

GaN E-HEMT Daughter Board and GS665MB-EVB Evaluation Platform

Technical Manual

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DANGER!

This evaluation kit is designed for engineering evaluation in a controlled lab environment and **should be handled by qualified personnel ONLY**. High voltage will be exposed on the board during the test and even brief contact during operation may result in severe injury or death.

Never leave the board operating unattended. After it is de-energized, always wait until all capacitors are discharged before touching the board.



CAUTION

This product contains parts that are susceptible to damage by electrostatic discharge (ESD). Always follow ESD prevention procedures when handling the product.

Overview

The GS66508B-EVBDB1 daughter board style evaluation kit consists of two GaN Systems 650V GaN Enhancement-mode HEMTs (E-HEMTs) and all necessary circuits including half bridge gate drivers, isolated power supplies and optional heatsink to form a functional half bridge power stage. It allows users to easily evaluate the GaN E-HEMT performance in any half bridge-based topology, either with the universal mother board (P/N: GS665MB-EVB) or for quick prototyping of a users' own system design.

Features

- Serves as a reference design and evaluation tool as well as deployment-ready solution for easy in-system evaluation.
- Vertical mount style with height of 35mm, which fits in majority of 1U design and allows evaluation of GaN E-HEMT in traditional through-hole type power supply board.
- Current shunt position for switching characterization testing
- Universal form factor and footprint for all products

The daughter board and universal mother board ordering part numbers are below:

Table 1 Ordering part numbers

Part Number	GaN E-HEMT P/N:	Description
GS66508B-EVBDB1	GS66508B	GaN E-HEMT bottom side cooled 650V/30A, 50mΩ Analog Devices isolated driver ADUM4121ARZ
GS665MB-EVB		Universal 650V Mother Board

Control and Power I/Os

The daughter board GS66508B-EVBDB1 circuit diagram is shown in Figure 1. The control logic inputs on 2x3 pin header J1 are listed below:

Table 2 Control pins

Pin	Description
ENA	Enable input. It is internally pulled up to VCC, a low logic disables all the PWM gate drive outputs.
VCC	+5V auxillary power supply input for logic circuit and gate driver. On the daughter board there are 2 isolated 5V to 9V DC/DC power supplies for top and bottom switches.
VDRV	Optional 9V gate drive power input. This pin allows users to supply separate gate drive power supply. By default VDRV is connected to VCC on the daughter board via a 0 ohm jumper FB1. If bootstrap mode is used for high side gate drive, connect VDRV to 9V
PWMH	High side PWM logic input for top switch Q1. It is compatible wth 3.3V and 5V
PWML	Low side PWM logic input for bottom switch Q2. It is compatible wth 3.3V and 5V
0V	Logic inputs and gate drive power supply ground return.

Power pins

The 3 power pins are

- VDC+: Input DC Bus voltage
- VSW: Switching node output
- VDC-: Input DC bus voltage ground return. Note that control ground 0V is isolated from VDC-.

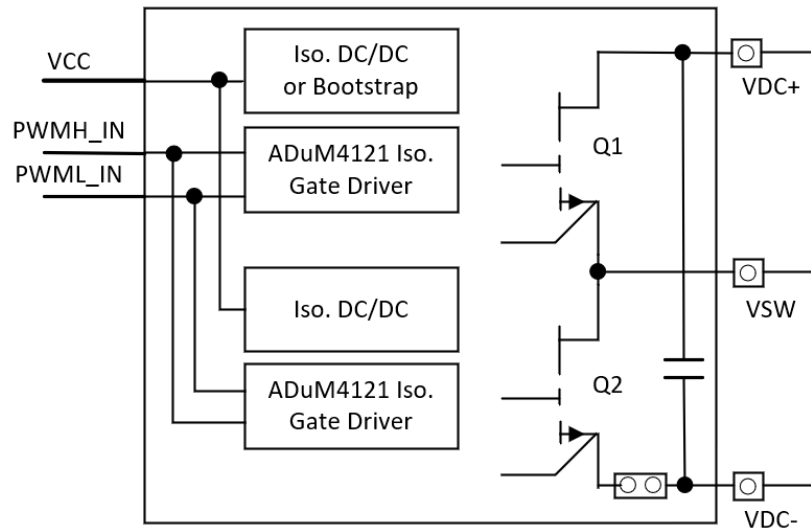


Figure 1 - GS66508B-EVBDB1 Evaluation Board Block Diagram

GS66508B-EVBDB1 half bridge daughter board

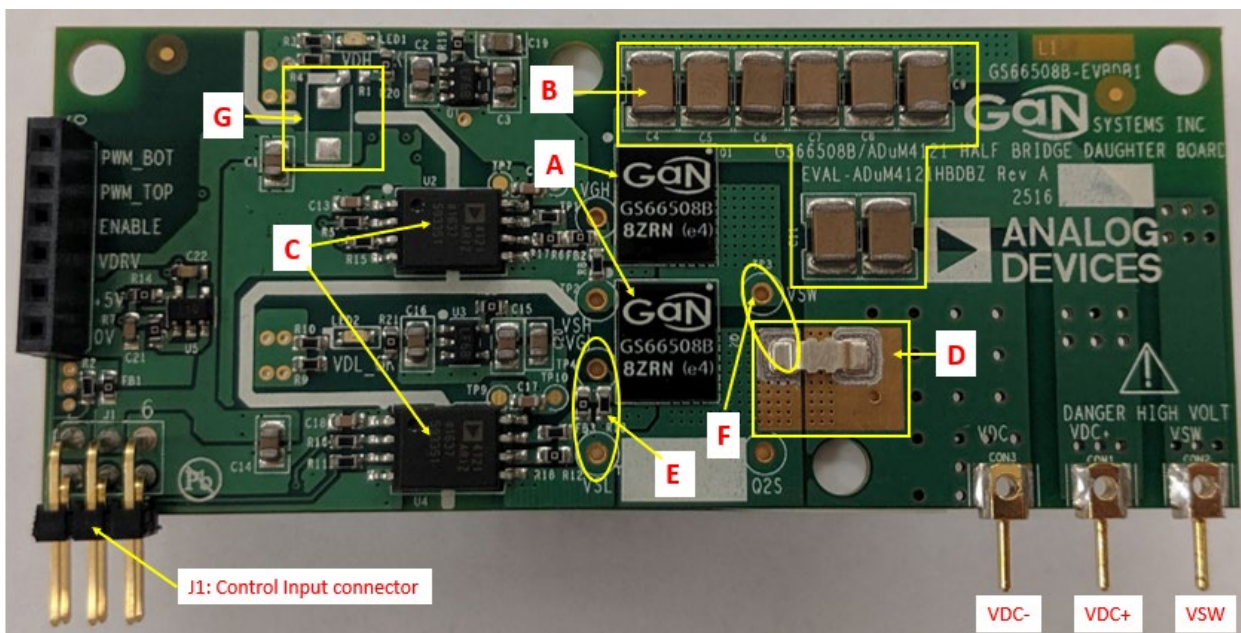


Figure 2 - GS66508B-EVBDB top side

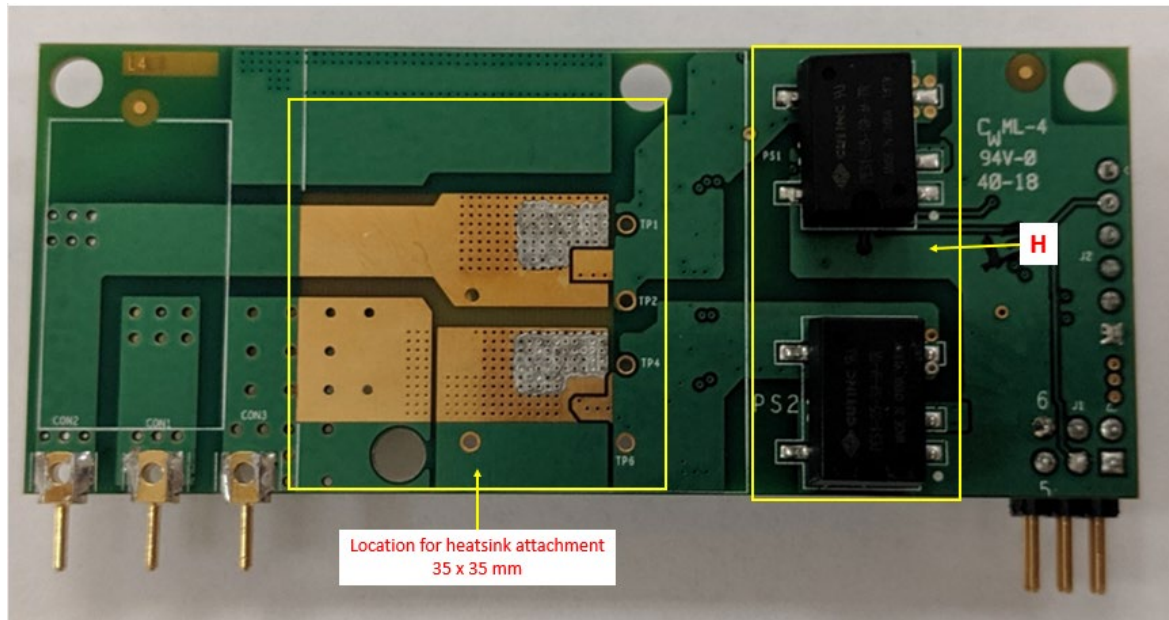


Figure 3 - GS66508B-EVBDB bottom side

- A. 2x GaN Systems 650V E-HEMT GS66508B, 30A/50mΩ
- B. Decoupling capacitors C4-C11
- C. 2 x Analog Devices ADuM4121ARZ Isolated gate driver
- D. Optional current shunt position JP1.
- E. Test points for bottom Q2 V_{GS} .
- F. Recommended probing positions for Q2 V_{DS} .
- G. Optional bootstrap circuit D1/R1 (unpopulated).
- H. 5V-9V isolated DC/DC gate drive power supply

GaN E-HEMTs

This daughter board includes two GaN Systems GS66508B (650V/30A, 50mΩ) E-HEMTs in a GaN_{PX}® bottom cooled package. The large S pad serves as the Source connection and thermal pad. Pin 4 is the Kelvin source connection for the gate drive return.

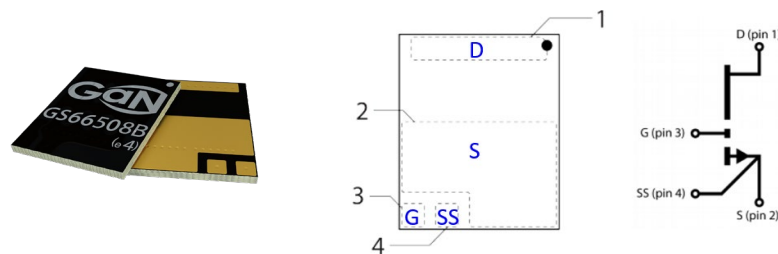


Figure 4 - Package outline of GS66508B

Gate driver circuit

- The half bridge evaluation boards use two Analog Devices high voltage, isolated gate drivers (ADuM4121ARZ) to drive the GaN transistors directly. The ADuM4121ARZ gate driver is used to isolate and drive the GaN transistor, operating at high DC bus voltage. It has a rail-to-rail output with maximum output current of 2A to turn the GaN device on and off efficiently and reliably. An external 20Ω gate resistor is used to limit the current for sourcing and sinking.
- The ADuM4121ARZ has a propagation delay of less than 53 ns and typical rise and fall times of approximately 18 ns. The very high Common-mode transient immunity (CMTI) of 150 kV/us (min) isolates high transient noise during the high frequency operation and prevents erroneous outputs.
- The GaN E-HEMT switching speed and slew rate can be directly controlled by the gate resistors. By default the turn-on/turn-off gate resistors, R6/R12, are 20Ω. The user can adjust the values of gate resistors to fine tune the turn-on and turn-off speed.
- FB2/FB3 are footprints for optional ferrite bead. By default they are populated with 0Ω jumpers. If gate oscillation is observed, it is recommended to replace them with ferrite bead with Z=10-20Ω@100MHz.

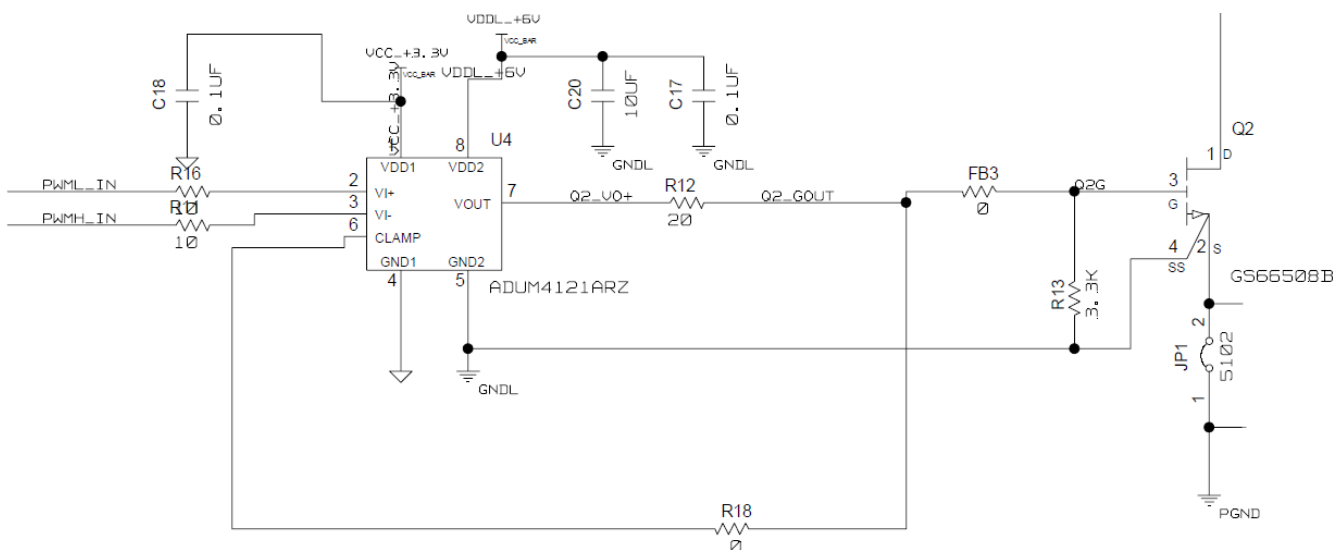


Figure 5 - Gate driver circuit

Gate drive power supply

- 5V-9V isolated DC/DC converters are used for the gate drive. The 9V output is regulated down to 6V for the gate driver.
- By default gate drive supply input VDRV is tied to VCC +5V via 0Ω jumper (FB1). Remove FB1 if separate gate drive input voltage is to be used.

Bootstrap mode

- The board has the option for users to experiment with non-isolated bootstrap circuit with following circuit changes:

- Remove PS2 and short circuit pin 2 to 5 and pin 1 to 4.
- Populate D1/ R1 (not supplied): D1 is the high voltage bootstrap diode (for example ES1J) and use 1-2Ω 0805 SMD resistor on R1. Depopulate PS1, LED1 and replace C2 with 1uF capacitor.
- Remove 0Ω jumper at FB1 and supply +9V at VDRV.

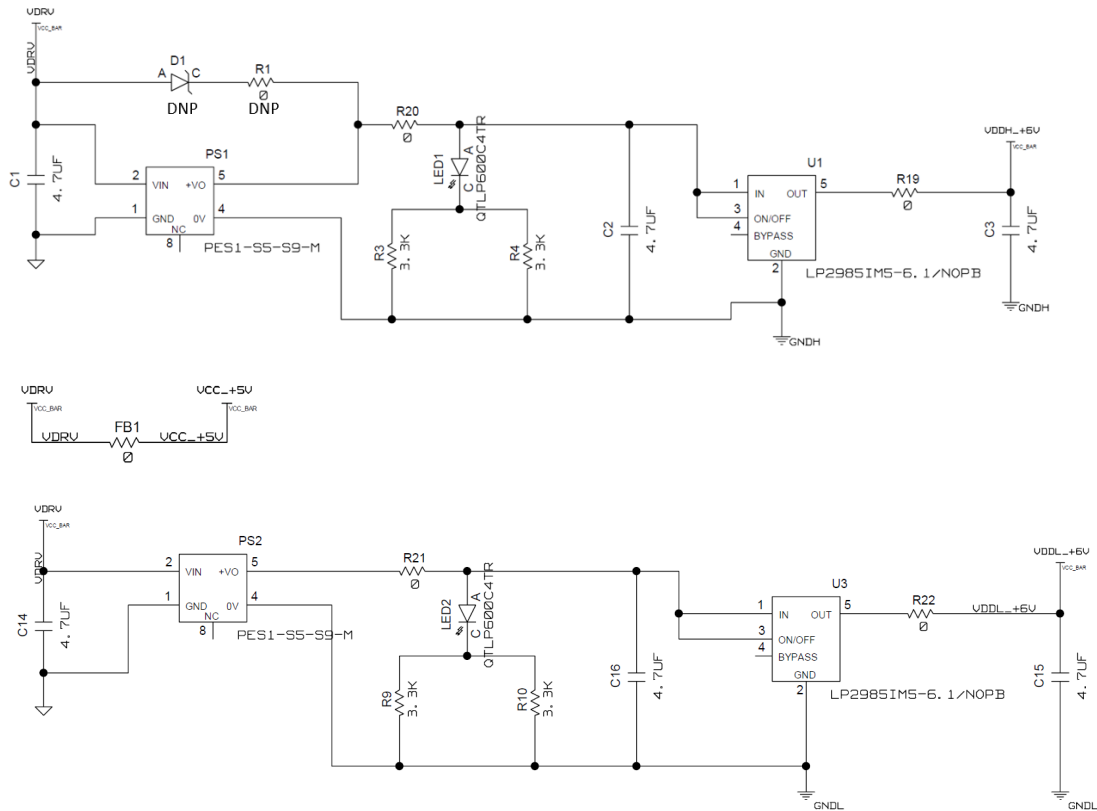


Figure 6 - Gate drive power supply with optional bootstrap mode

Current shunt JP1

- The board provides an optional current shunt position JP1 between the source of Q2 and power ground return. This allows drain current measurement for switching characterization test such as Eon/Eoff measurement.
- The JP1 footprint is compatible with T&M Research SDN series coaxial current shunt (recommended P/N: SDN-414-10, 2GHz B/W, 0.1Ω)
- If current shunt is not used JP1 must be shorted. JP1 affects the power loop inductance and its inductance should be kept as low as possible. Use a copper foil or jumper with low inductance.



CAUTION

Check the JP1 before the first time use. To complete the circuit JP1 needs to be either shorted or a current shunt must be inserted before powering up.

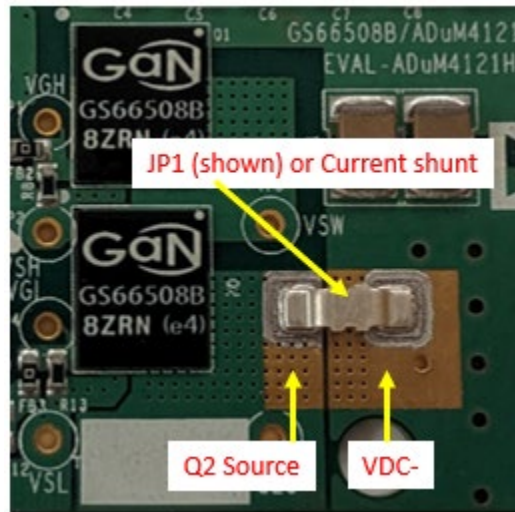


Figure 7 - Current shunt position JP1

Measurement with current shunt

1. When measuring VSW with current shunt, ensure all channel probe grounds and current shunt BNC output case are all referenced to the source end of Q2 before the current shunt. The recommended setup of probes is shown as below.
2. The output of coaxial current shunt can be connected to oscilloscope via 50Ω termination impedance to reduce the ringing.
3. The measured current is inverted and can be scaled by using: $I_d = V_{id} / R_{sense}$.

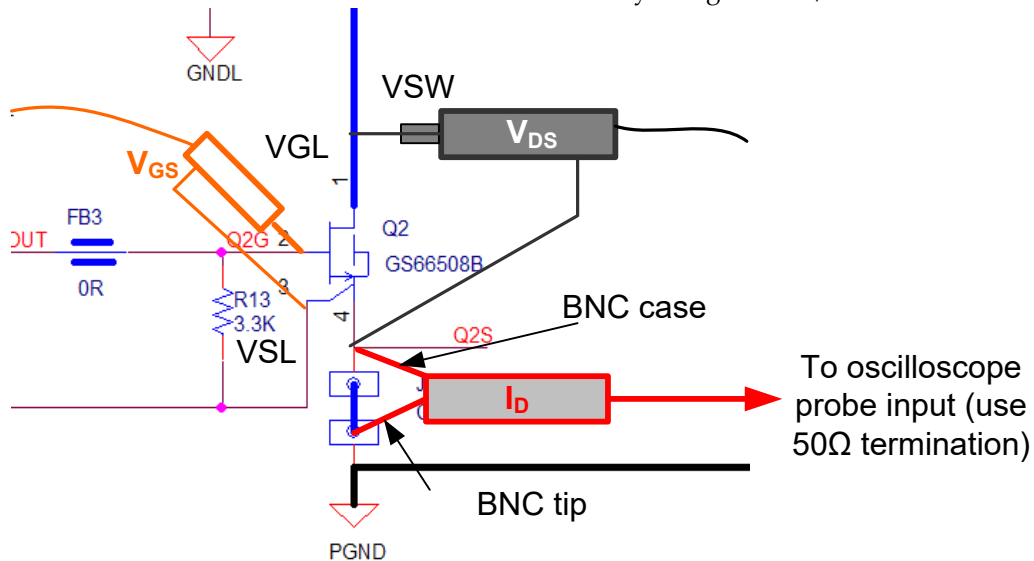


Figure 8 - Recommended probe connection with current shunt

Thermal design

1. GS66508B has a thermal pad at the bottom side for heat dissipation. The heat is transferred to the bottom side of PCB using thermal vias and copper plane.
2. A heatsink (35x35mm size) can be attached to the bottom side of board for optimum cooling. Thermal Interface Material (TIM) is needed to provide electrical insulation and conformance to the PCB surface. The daughter board evaluation kit includes a sample 35x35mm fin heatsink (not installed), although other heatsinks can also be used to fit users' system design.
3. A thermal tape type TIM (Bergquist® Bond-Ply 100) is chosen for its easy assembly. The supplied heatsink has the thermal tape pre-applied so simply peel off the protective film and attach the heatsink to the back of board as marked in Figure 3.
4. Two optional mounting holes as shown in Figure 9 are provided for mounting customized heatsink using screws.
5. Using the supplied heatsink and TIM, the overall junction to ambient thermal resistance R_{thJA} is $\sim 9^{\circ}\text{C}/\text{W}$ with 500LFM airflow.
6. Forced air cooling is recommended for power testing.

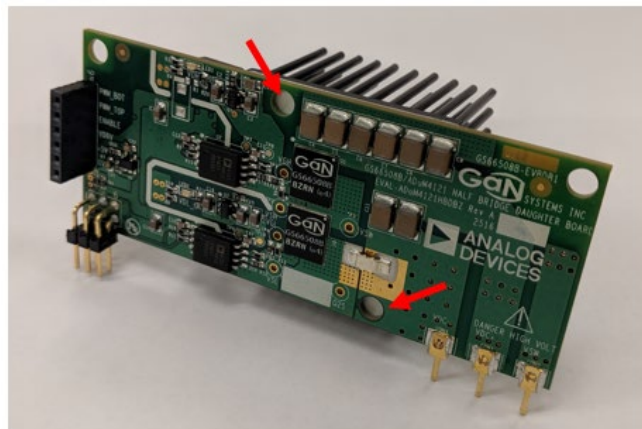


Figure 9 The daughter board with heatsink attached



CAUTION:

There is no on-board over-temperature protection. Device temperature must be closely monitored during the test. Never operate the board with device temperature exceeding T_{J_MAX} (150°C)

Using GS66508B-EVBDB1 with universal mother board GS665MB-EVB

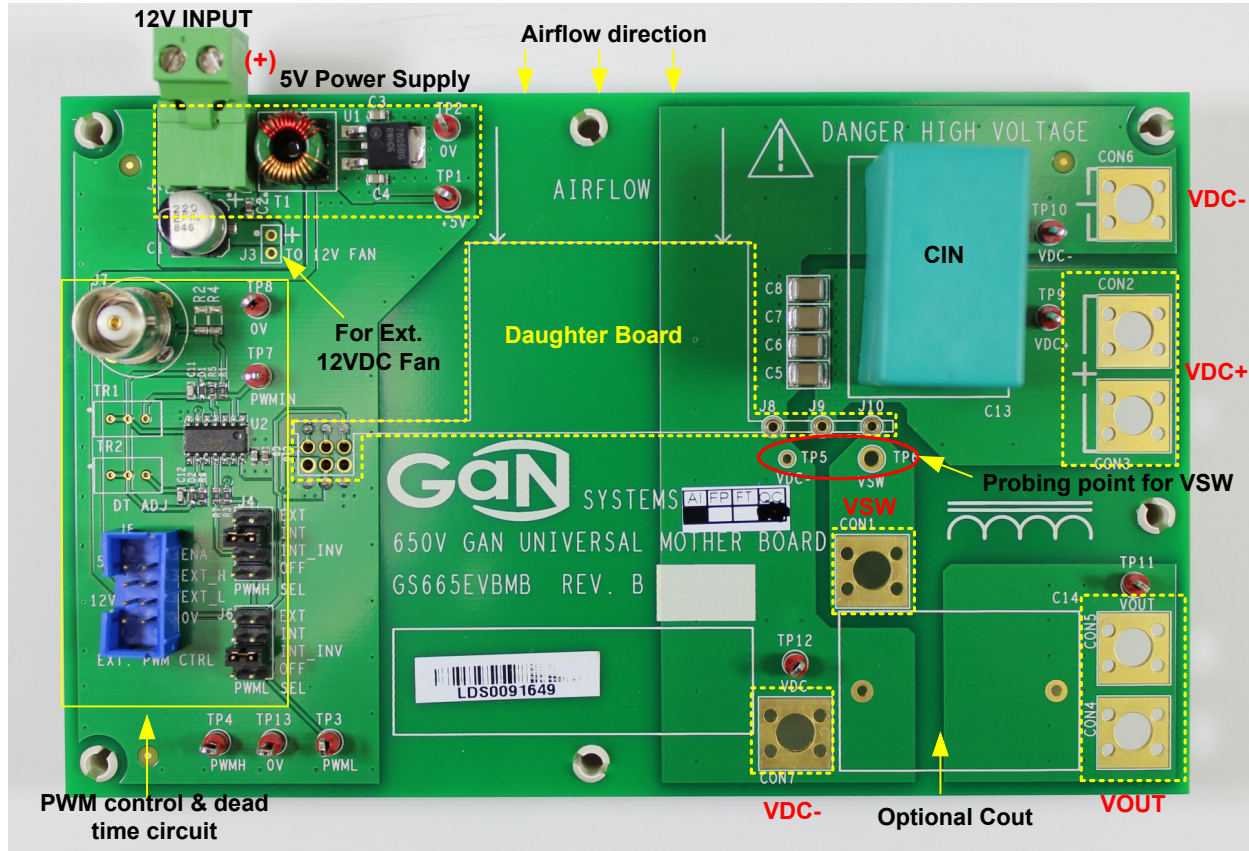


Figure 10 - 650V universal mother board GS665MB-EVB

GaN Systems offers a universal 650V mother board (ordering part number: GS665MB-EVB, sold separately) that can be used as the basic evaluation platform for all the daughter boards.

The universal 650V mother board evaluation kit includes following items:

1. Mother board GS665MB-EVB
2. 12VDC Fan

12V input

The board can be powered by 9-12V on J1. On-board voltage regulator creates to 5V for daughter board and control logic circuits. J3 is used for external 12VDC fan.

PWM control circuit

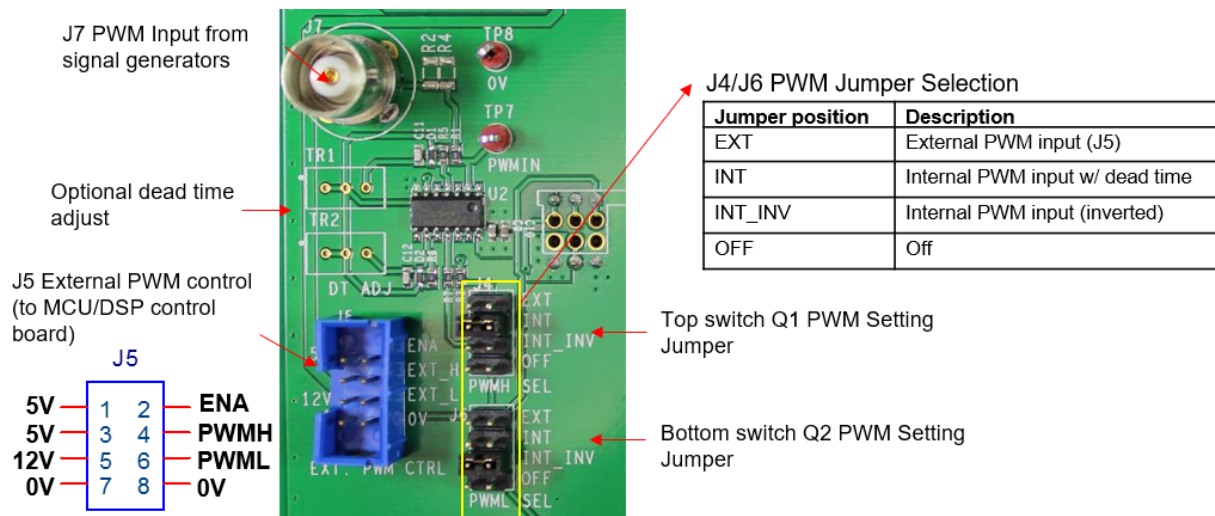


Figure 11 - PWM control input and dead time circuit

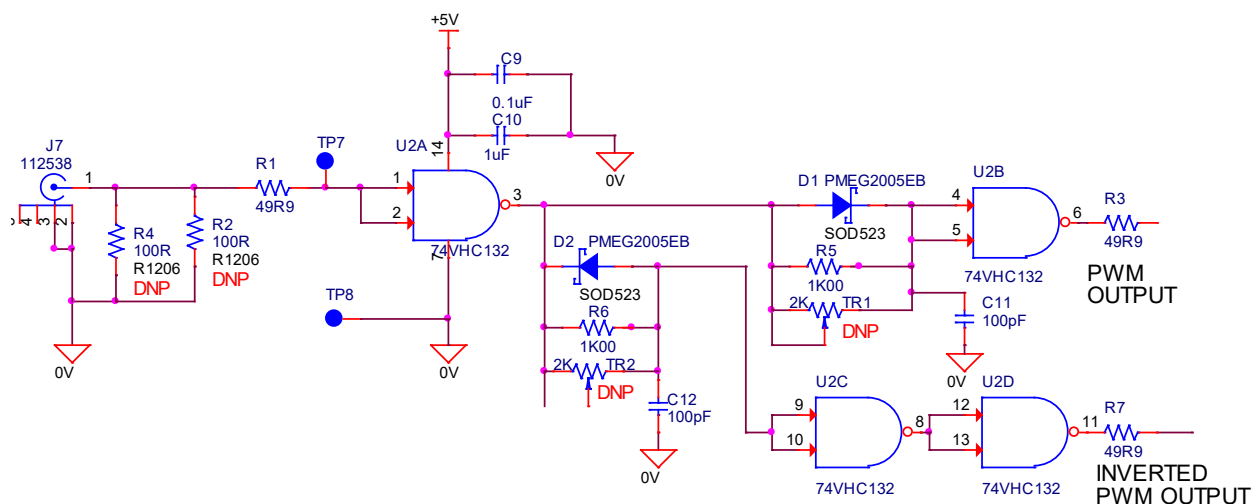


Figure 12 - On board dead time generation circuit

The top and bottom switches PWM inputs can be individually controlled by two jumpers J4 and J6. Users can choose between a pair of complementary on-board internal PWM signals (non-inverted and inverted, controlled by J7 input) with dead time or external high/low side drive signals from J5 (users' own control board).

An on-board dead time generation circuit is included on the mother board. Dead time is controlled by two RC delay circuits, R6/C12 and R5/C11. The default dead time is set to about 100ns. Additionally two potentiometers locations are provided (TR1/TR2, not included) to allow fine adjustment of the dead time if needed.


WARNING

ALWAYS double check the jumper setting and PWM gate drive signals before applying power. Incorrect PWM inputs or jumper settings may cause device failures

Test points

Test points are designed in groups/pairs to facilitate probing:

Test points	Name	Description
TP1/TP2	+5V/0V	5V bias power
TP7/TP8	PWMIN/0V	PWM input signal from J7
TP4/TP3/TP13	PWMH/PWML/0V	High/low side gate signals to daughter board
TP9/TP10	VDC+/VDC-	DC bus voltage
TP11/TP12	VOUT/VDC-	Output voltage
TP6/TP5	VSW/VDC-	Switching node output voltage (for HV oscilloscope probe)

Power connections

CON1-CON7 mounting pads are designed to be compatible with following mounting terminals:

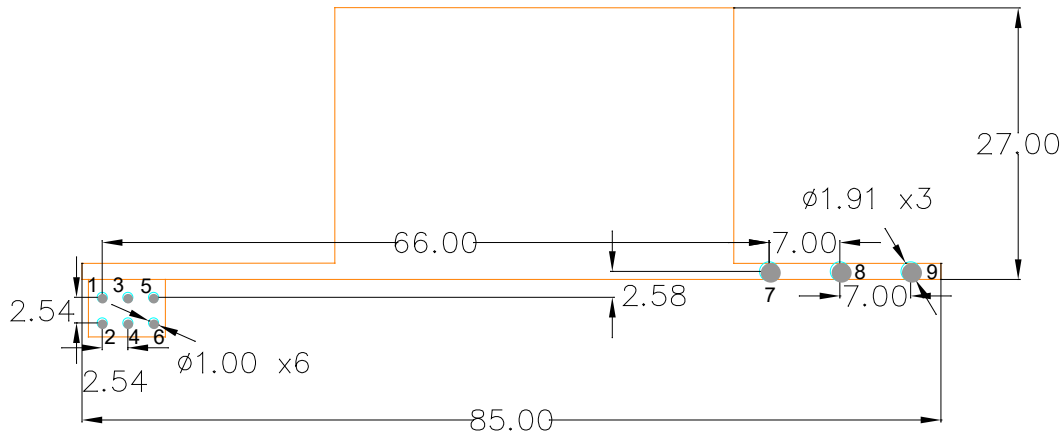
- #10-32 Screw mount,
- Banana Jack PCB mount (Keystone P/N: **575-4**), or
- PC Mount Screw Terminal (Keystone P/N: **8191**)

Output passives (L and C14)

An external power inductor (not included) can be connected between VSW (CON1) and VOUT (CON4/5) or VDC+ (CON2/3) for double pulse test. Users can choose their inductor size to meet the test requirement. Generally it is recommended to use power inductor with low inter-winding capacitance to obtain best switching performance. For the double pulse testing we use 2x 60uH/40Amp inductor (CWS, P/N: HF467-600M-40AV) in series. C14 is designed to accommodate a film capacitor as output filter.

Using GS66508B-EVBDB1 in system

The daughter board allows users to easily evaluate the GaN performance in their own systems. Refer to the footprint drawing of GS66508B-EVBDB1 shown in figure 14.



1. All units are in mm.
2. Pin 1-6: Dia. 1mm
3. Pin 7-9: 1.91mm (75mil) mounting hole for Mill-max Receptacle P/N: 0312-0-15-15-34-27-10-0.

Figure 13 - Recommended footprint drawing of daughter board GS66508B-EVBDB1

Double pulse test mode

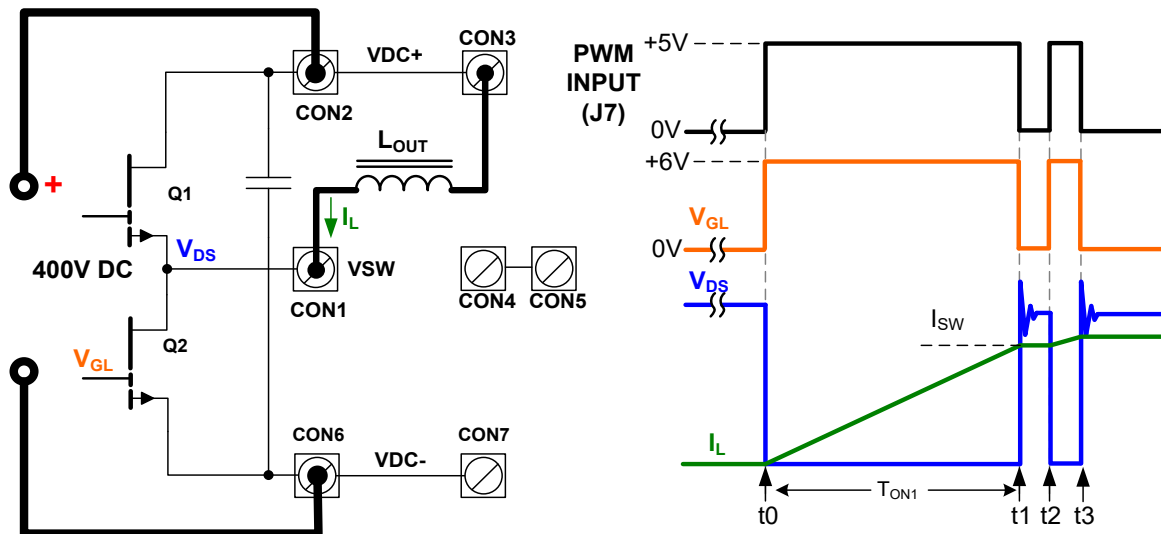


Figure 14 - Double pulse test setup

Double pulse test allows easy evaluation of device switching performance at high voltage/current without the need of actually running at high power. It can also be used for switching loss (Eon/Eoff) measurement and other switching characterization parameter test.

The circuit configuration and operating principle can be found in Figure 13:

1. The output inductor is connected to the VDC+.
2. At t_0 when Q2 is switched on, the inductor current starts to ramp up until t_1 . The period of first pulse T_{ON1} defines the switching current $I_{SW} = (V_{DS} * T_{ON1}) / L$.
3. t_1 - t_2 is the free wheeling period when the inductor current I_L forces Q1 to conduct in reverse.
4. t_1 (turn-off) and t_2 (turn-on) are of interest for this test as they are the hard switching transients for the half bridge circuit when Q2 is under high switching stress.
5. The second pulse t_2 - t_3 is kept short to limit the peak inductor current at t_3 .

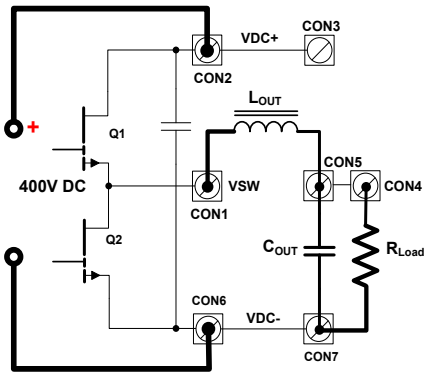
The double pulse signal can be generated using programmable signal generator or microcontroller/DSP board. As this test involves high switching stress and high current, it is recommended to set the double pulse test gate signal as single trigger mode or use long repetition period (for example >50-100ms) to void excess stress to the switches. Q1 can be kept off during the test or driven synchronously (J4 set to OFF or INT_INV) and Q2 is set to INT (or EXT position if PWM signal is from J5).



WARNING

Limit the maximum switching test current to 30A and ensure maximum drain voltage, including ringing, is kept below 650V for pulse testing. Exceeding this limit may cause damage to the devices.

Buck/Standard half bridge mode



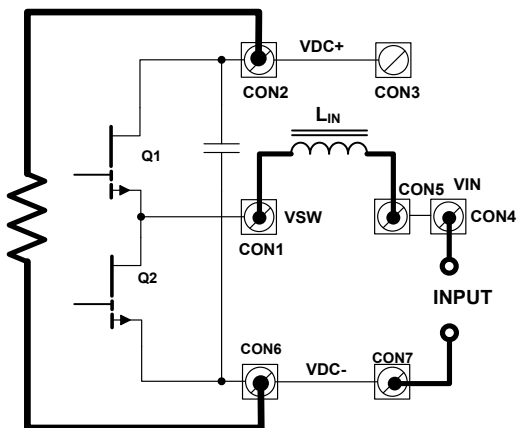
This is standard half bridge configuration that can be used in following circuits :

- Synchronous Buck DC/DC
- Single phase half bridge inverter
- ZVS half bridge LLC
- Phase leg for full bridge DC/DC or
- Phase leg for a 3-phase motor drive

Jumper setting:

- J4 (Q1): INT
- J6 (Q2): INT_INV

Boost mode



When the output becomes the input and the load is attached between VDC+ and VDC-, the board is converted into a boost mode circuit and can be used for:

- Synchronous Boost DC/DC
- Totem pole bridgeless PFC

Jumper setting:

- J4 (Q1): INT_INV
- J6 (Q2): INT

Quick Start procedure – Double pulse test

Follow the instructions below to quickly get started with your evaluation of GaN E-HEMT. Equipment and components you will need:

- Four-channel oscilloscope with 500MHz bandwidth or higher
 - high bandwidth (500MHz or higher) passive probe
 - high bandwidth (500MHz) high voltage probe (>600V)
 - AC/DC current probe for inductor current measurement
 - 12V DC power supply
 - Signal generator capable of creating testing pulses
 - High voltage power supply (0-400VDC) with current limit.
 - External power inductor (recommend toroid inductor 50-200uH)
1. Check the JP1 on daughter board GS66508B-EVBDB1. Use a copper foil and solder to short JP1.
 2. Install GS66508B-EVBDB1 on the mother board. Press all the way down until you feel a click. Connect probe between VGL and VSL for gate voltage measurement.
 3. Set up the mother board:
 - a. Connect 12VDC bias supply to J1.
 - b. Connect PWM input gate signal (0-5V) to J7. If it is generated from a signal generator ensure the output mode is high-Z mode.
 - c. Set J4 to OFF position and J7 to INT.
 - d. Set High voltage (HV) DC supply voltage to 0V and ensure the output is OFF. Connect HV supply to **CON2** and **CON6**.
 - e. Use HV probe between TP6 and TP5 for Vds measurement.
 - f. Connect external inductor between **CON1** and **CON3**. Use current probe to measure inductor current IL.
 4. Set up and check PWM gate signal:
 - a. Turn-on 12VDC power.
 - b. Check the 2 LEDs on the daughter board. They should be turned on indicating the isolated 9V is present.
 - c. Set up signal generator to create the waveforms as shown in Figure 13. Use equation $I_{sw} = (V_{DS} * T_{ON1}) / L$ to calculate the pulse width of the first pulse and ensure the I_{sw_max} is $\leq 30A$ at 400VDC.
 - d. Set the operation mode to either single trigger or Burst mode with repetition period of 100ms.
 - e. Turn on the PWM output and check on the oscilloscope to make sure the VGL waveform is present and matches the PWM input.
 5. Power-on:
 - a. Turn on the output of the HV supply. Start with low voltage and slowly ramp the voltage up until it reaches 400VDC. During the ramping period closely observe the the voltage and current waveforms on the oscilloscope.
 6. Power-off:
 - a. After the test is complete, slowly ramp down the HV supply voltage to 0V and turn off the output. Then turn off the 12V bias supply and signal generator output.

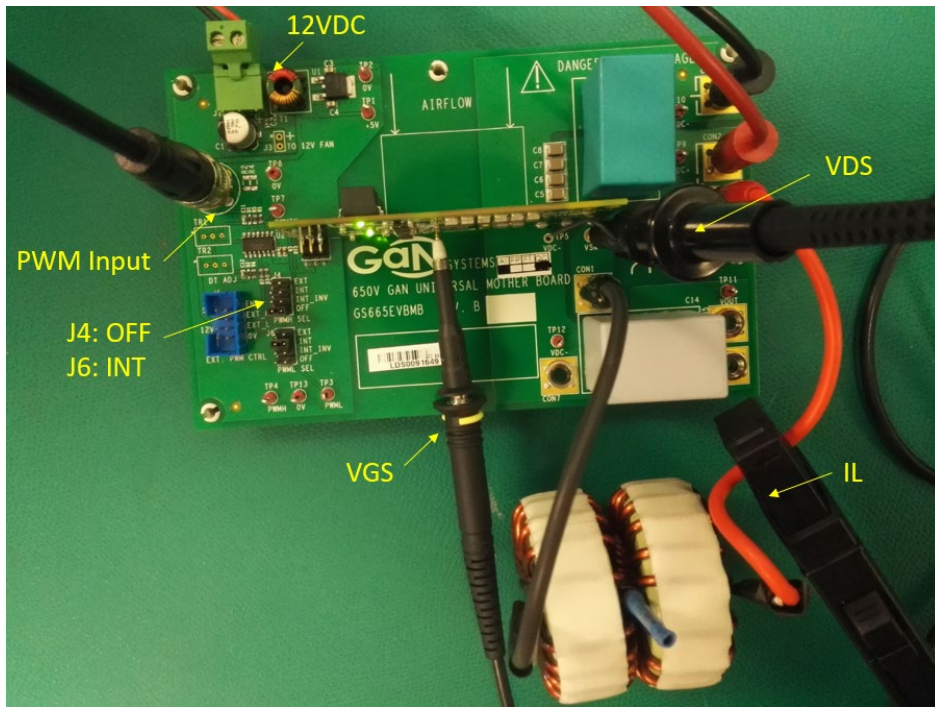


Figure 15 Double pulse test setup example (GS66508B-EVBDB1)

Test results – GS66508B-EVBDB1

Double Pulse test (VDS=400V, I_{MAX} = 30A, L=120uH, R_{G(ON)}=20Ω, R_{G(OFF)}=20Ω)

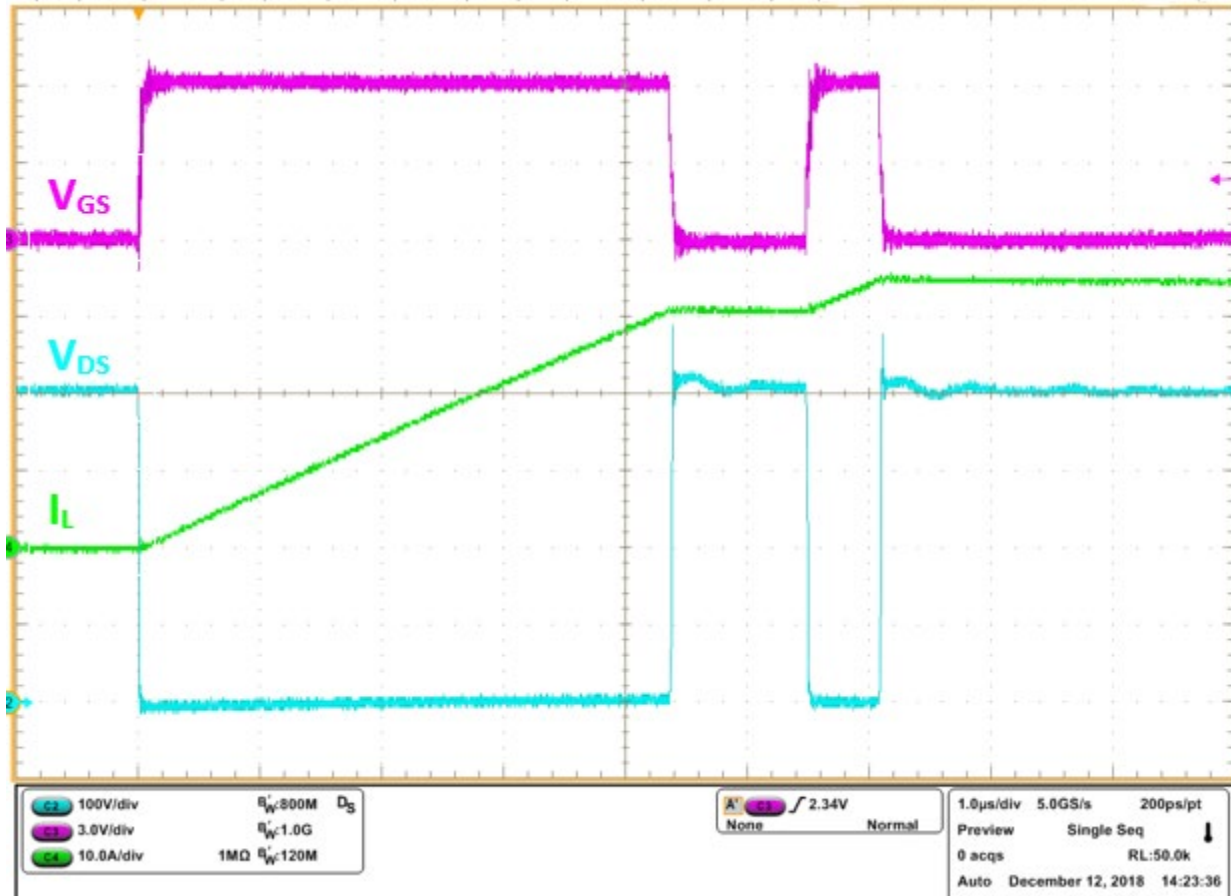


Figure 16 - 400V/30A double pulse test waveform

Figure 16 shows the hard switching on waveforms at 400V/30A. A V_{ds} dip can be seen due to the rising drain current (di/dt in the power loop $\Delta V=L_p \times di/dt$, where L_p is the total power loop inductance). After the drain current reaches the inductor current, the V_{ds} starts to fall. The V_{gs} undershoot spike is caused by the miller feedback via C_{gd} under negative dv/dt .

Due to the low gate charge and small R_{G(OFF)}, GaN E-HEMT gate has limited control on the turn-off dv/dt . Instead the V_{ds} rise time is determined by how fast the turn-off current charges switching node capacitance (C_{oss}).

The low C_{oss} of GaN E-HEMT and low parasitic inductance of GaNP® package together with optimized PCB layout, enables a fast and clean turn-off V_{ds} waveform with only 50V the turn-off V_{ds} overshoot at $dv/dt > 100V/ns$. The measured rise time is 3.9ns at 400V and 30A hard turn-off.

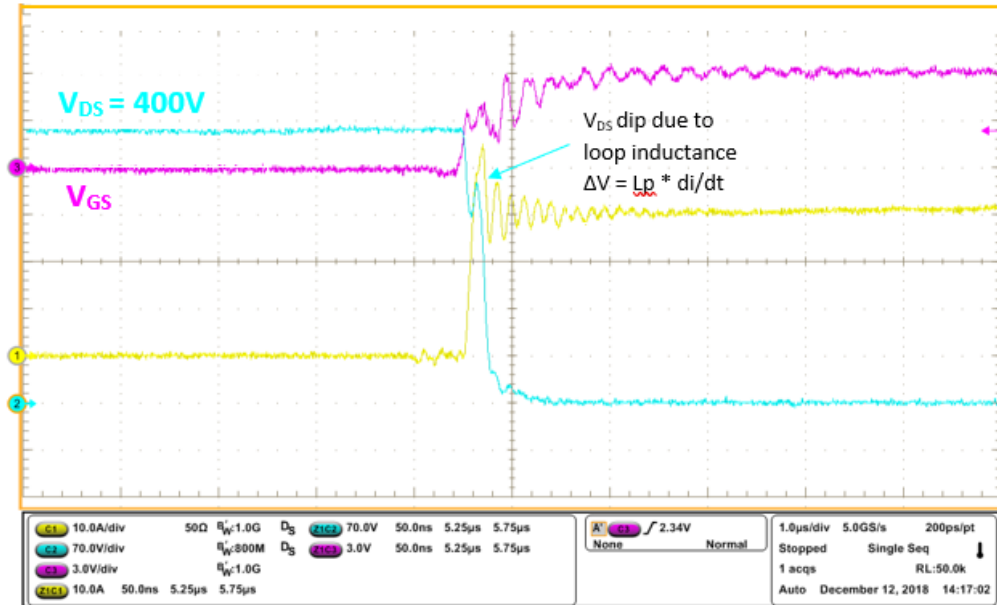


Figure 17 - Double pulse test switching transient - hard switching turn-on 400V/30A

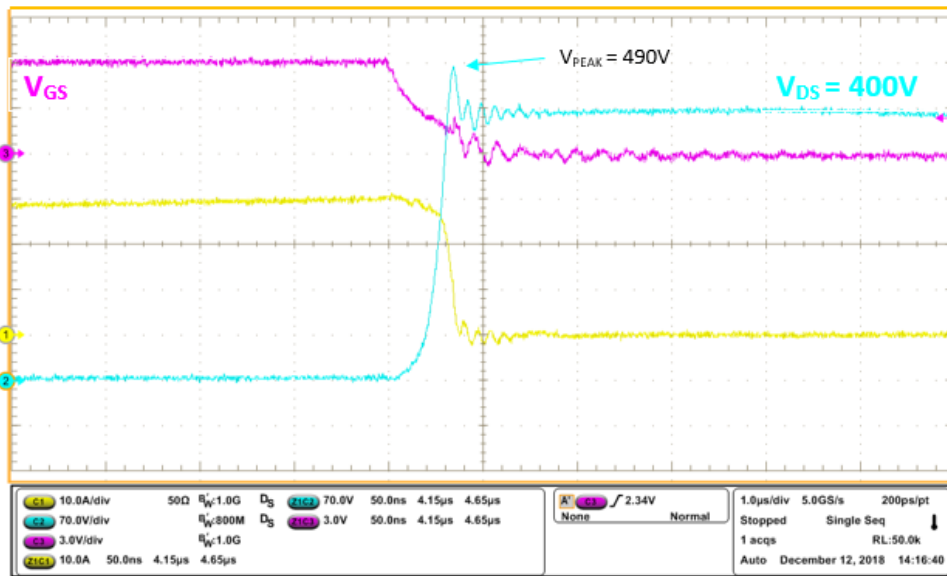


Figure 18 - Double pulse test switching transient - hard switching turn-off 400V/30A

Switching Loss energy (Eon/Eoff) measurement

A T&M search coaxial current shunt (SDN-414-10, 0.1Ω) is installed for switching loss measurement as shown below.

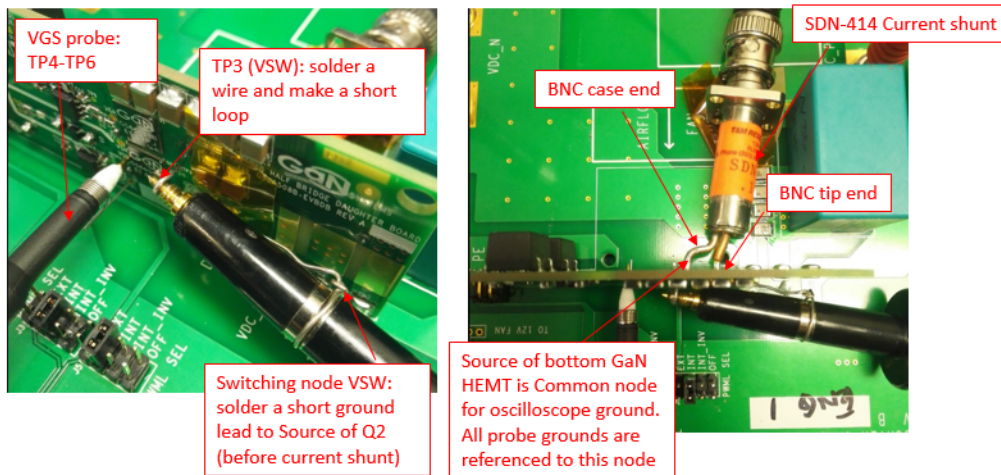


Figure 1917 - Eon/Eoff measurement probe connection with current shunt

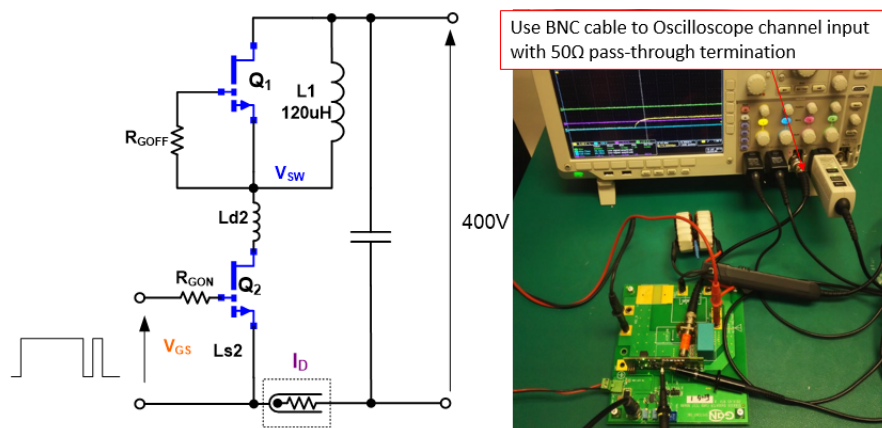


Figure 2018 - Eon/Eoff measurement and test bench setup

The switching energy can be calculated from the measured switching waveform $P_{sw} = V_{ds} \cdot I_d$. The integral of the P_{sw} during switching period is the measured switching loss. The channel deskewing is critical for measurement accuracy. It is recommended to manually deskew I_d against V_{ds} as shown in Figure 20. The drain current spike is caused by charging the high side switch C_{oss} (Q_{oss} loss).

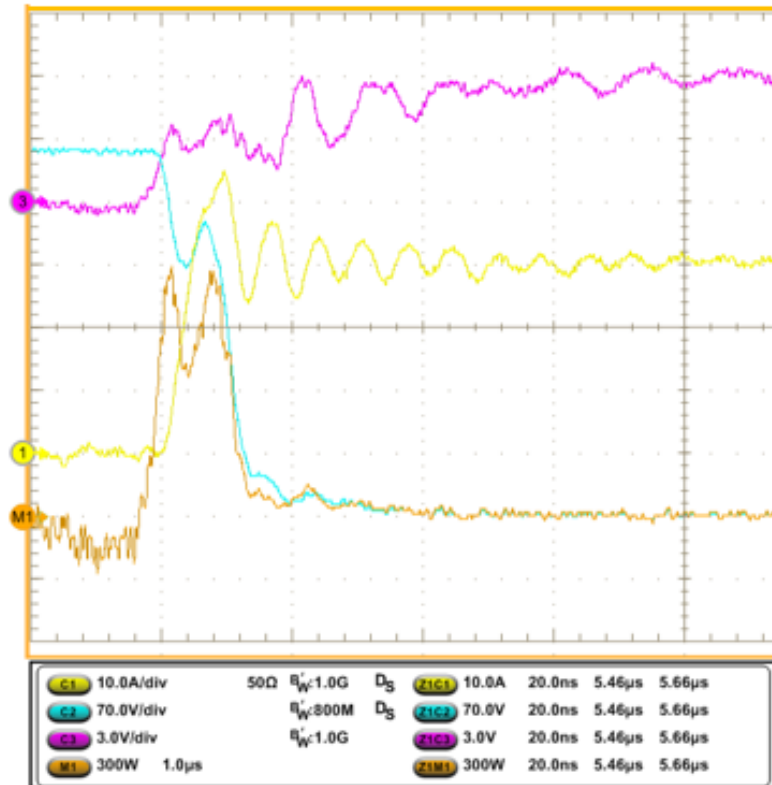


Figure 21 - Turn-on switching loss measurement (Eon=106uJ, 400V/30A)

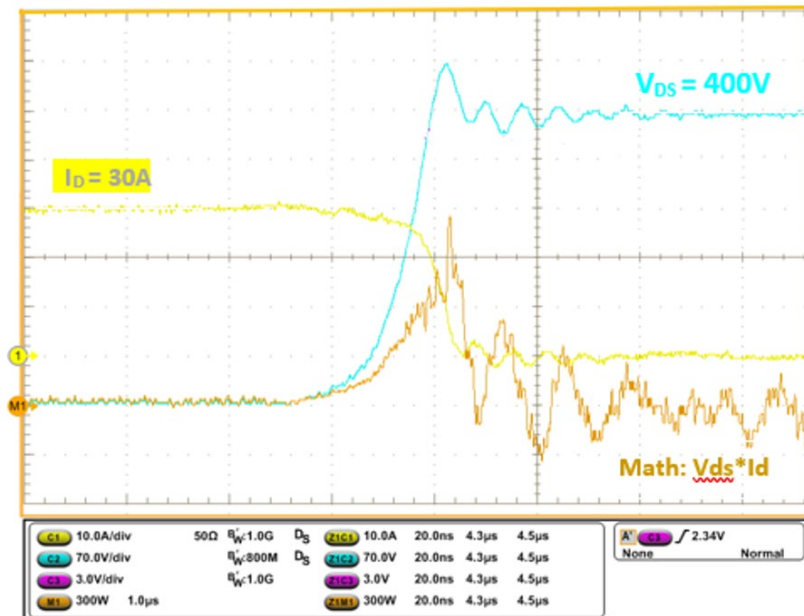


Figure 19 - Turn-off switching loss measurement (Eoff=76 uJ, 400V/30A)

The switching loss measurements with drain current from 0 to 30A can be found in Figure 22. The turn-on loss dominates the overall hard switching loss. Eon at 0A is the Qoss loss caused by the Coss at high side switch.

The turn-off loss remain almost constant from 0A up to 20A about 8uJ. the measured Eoff matches well with the Eoss @400V, which indicates that turn-off energy is dominated by Eoss, the energy required to charge Coss from 0V to bus voltage. This energy is not part of loss at turn-off, but actually part of turn-on loss at next hard switching turn-on period. This means that with the fast turn-off speed the GaN E-HEMT can achieve near zero turn-off switching loss.

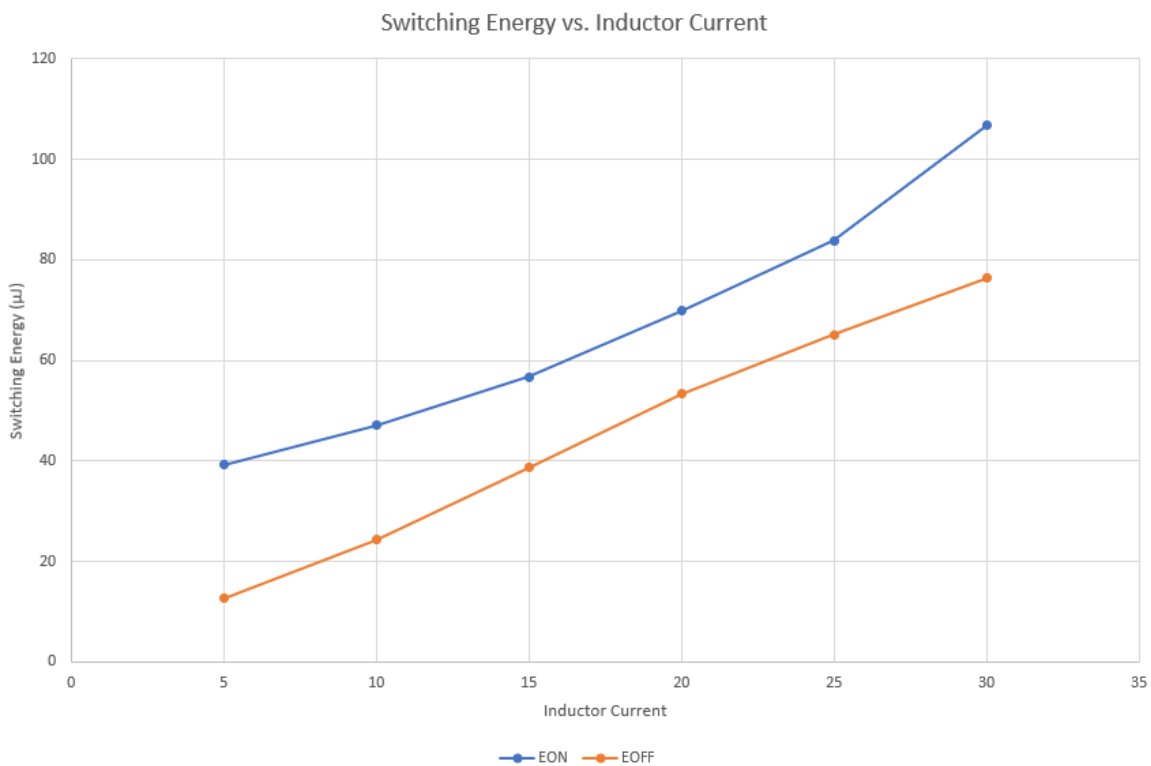
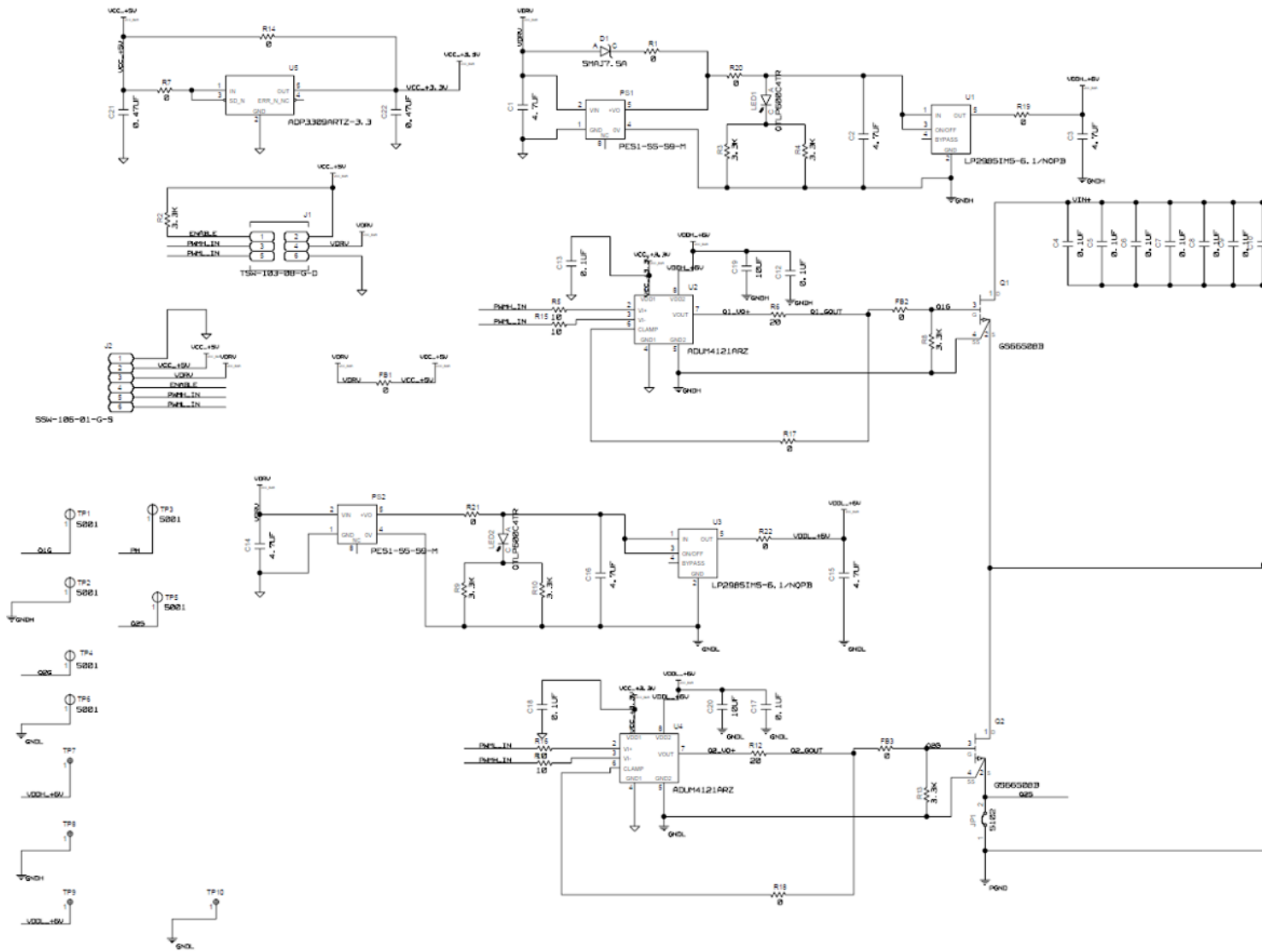


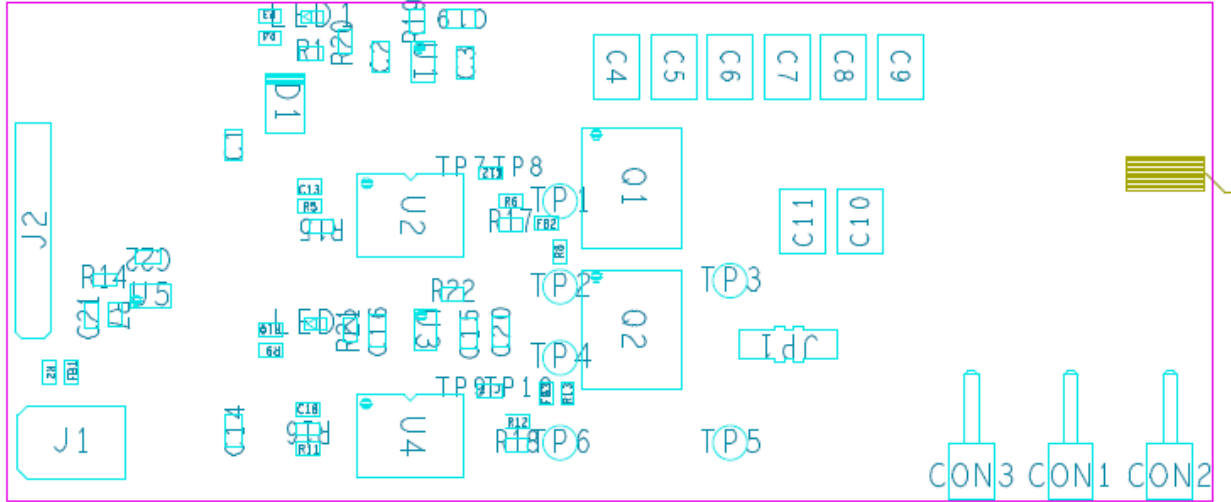
Figure 20 - GS66508B Switching Loss Measurement (VDS = 400V, TJ=25°C)

Appendix A - GS66508B-EVBDB1 Circuit schematic

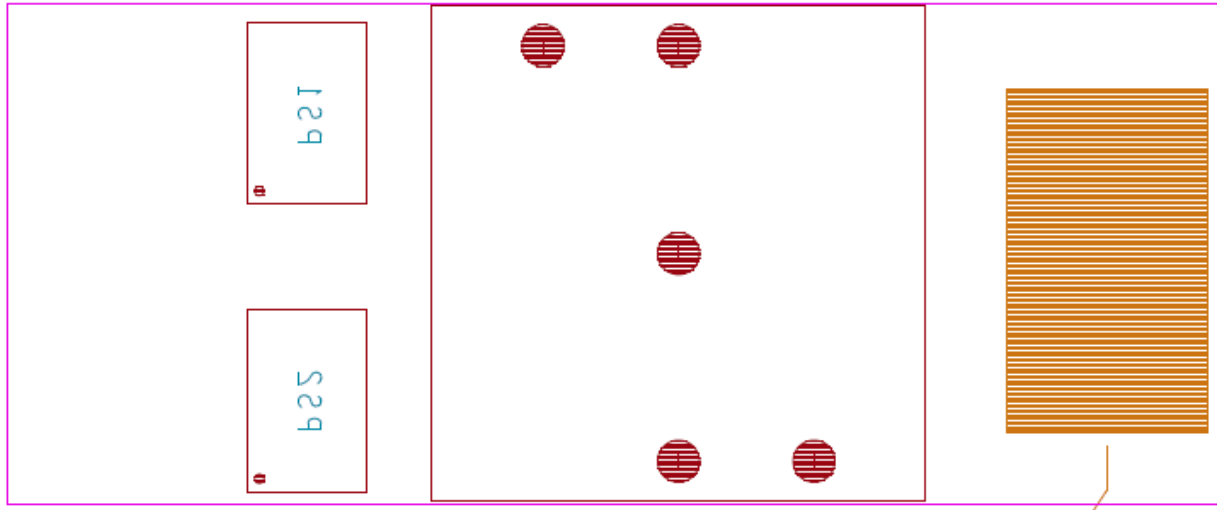


Assembly Drawing

TOP SIDE COMPONENTS

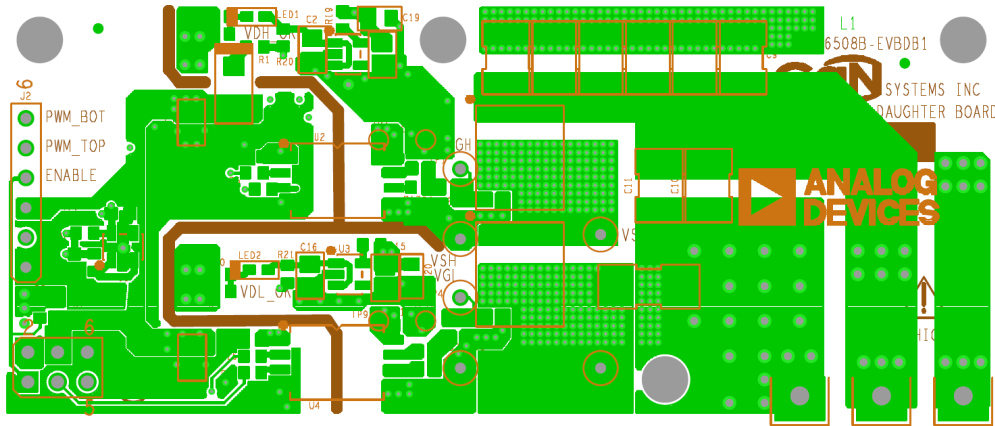


BOTTOM SIDE COMPONENTS

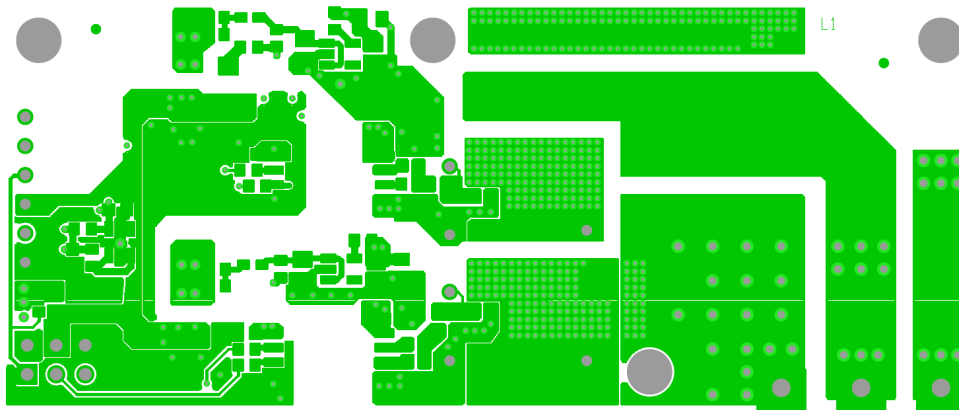


PCB layout

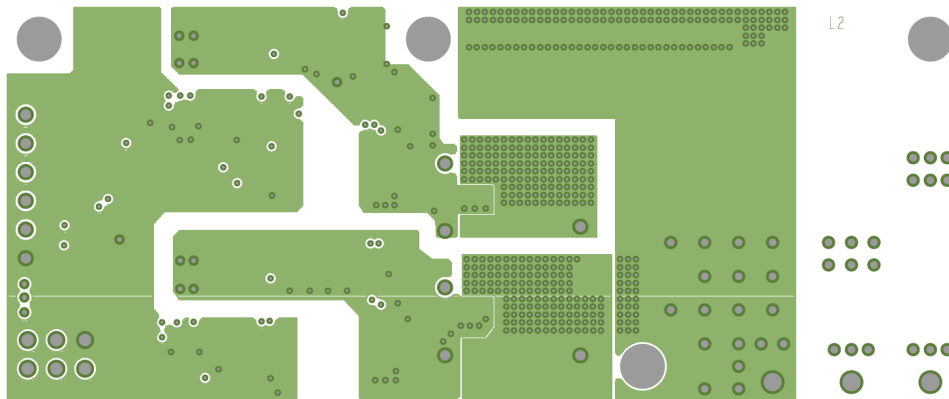
Top and Silk Layer



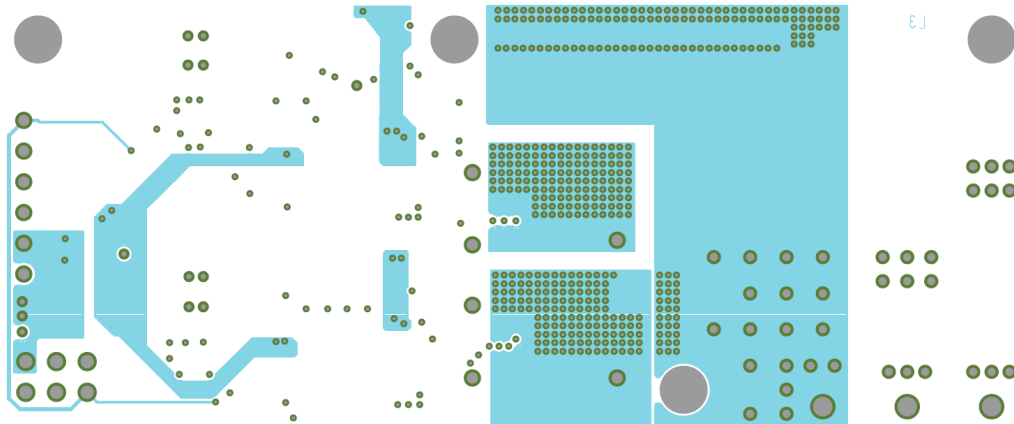
Top



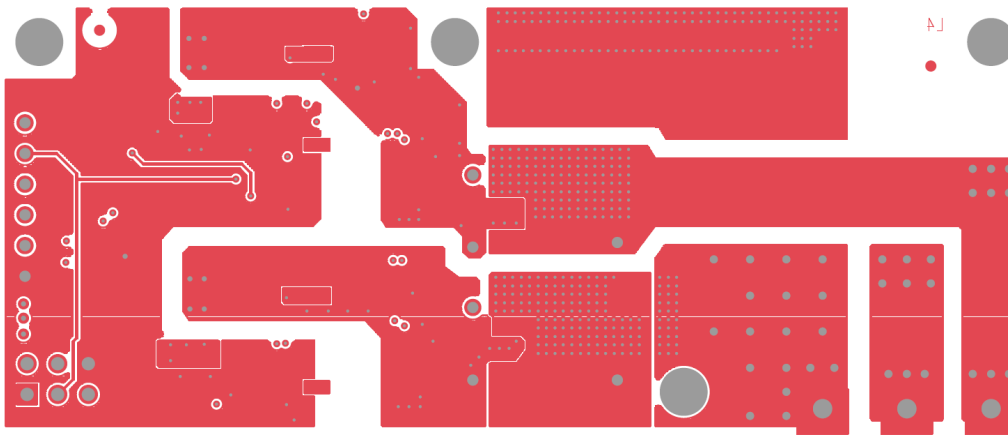
Layer 2



Layer 3



Bottom



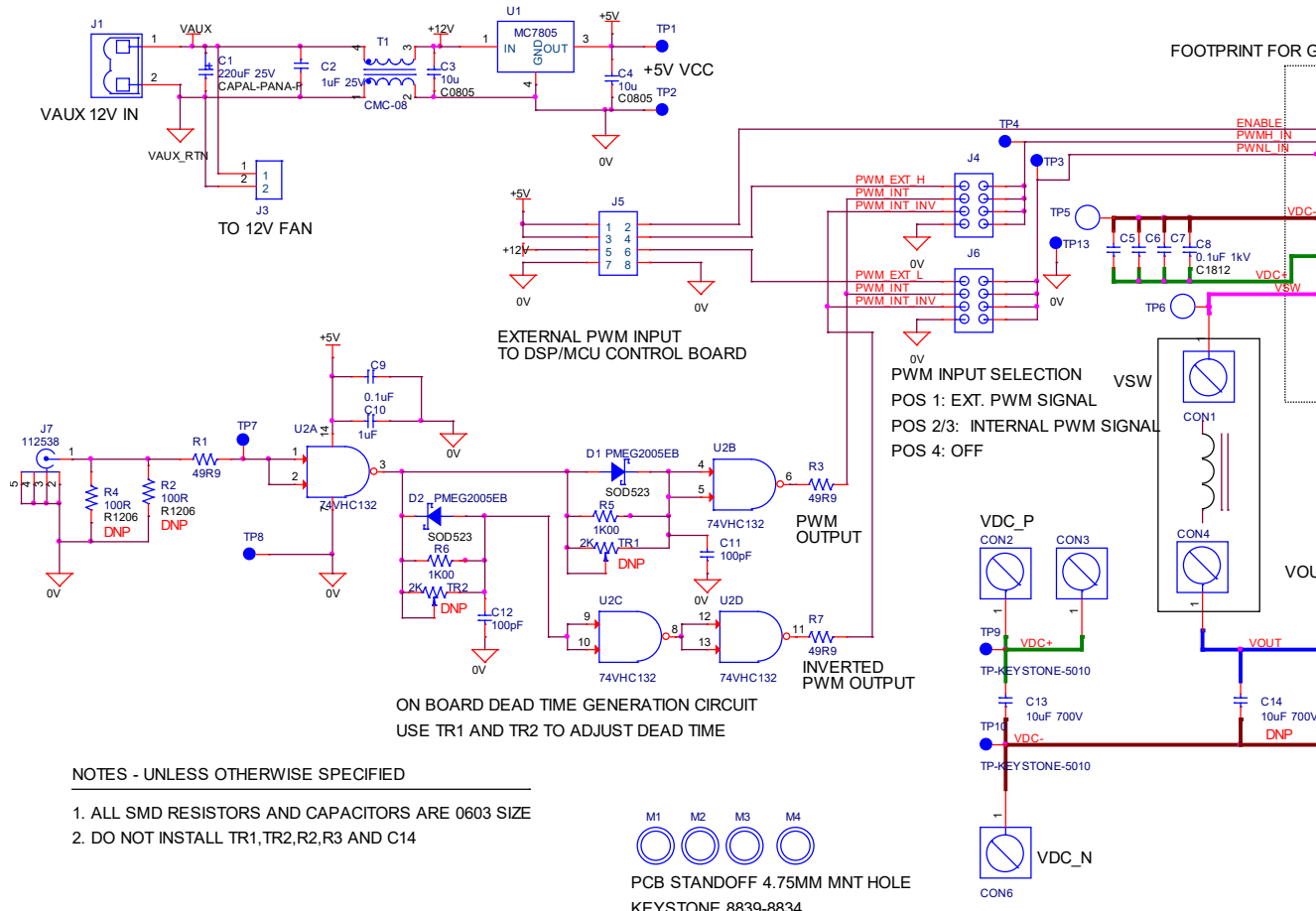
Bill of Materials GS66508B-EVBDB1

ADuM4121_HBD_BOM
For GS66508B-EVBDB1

Qty	DESCRIPTION	VALUE	JEDEC_TYPE	LOCATION	Manufacturer
6	CAP CER X7R	4.7UF	C0805H53	C1-C3,C14-C16	TAIYO YUDEN
8	CAP CER X7R, HIGH VOLTAGE	0.1uF	C1812H71	C4-C11	KEMET CORPORATION
4	CAP CER 0603 X7R	0.1uF	C0603	C12,C13,C17,C18	KEMET CORPORATION
2	CAP CER X5R	10uF	C0805-2	C19,C20	TAIYO YUDEN
2	CAP CER X7R 0603	0.47uF	C0603	C21,C22	MURATA MANUFACTUR
3	CONN-PCB 1POS BRD EDGE RIVET MOUNT FOR 62MILS BRD, 40MILS PIN SIZE, 200MILS PIN LENGTH	3620-2-32-15-00-00-08-0	CNMILLMAX3620	CON1-CON3	MILL-MAX
11	RES FILM SMD 0603	0	R0603	R7,FB1-FB3,R17-R22	MULTICOMP
1	CONN-PCB BERG HDR DOUBLE STR MALE 6P	TSW-103-08-G-D-RA	CNSAMTEC2X3H330LD36	J1	SAMTEC
1	CONN-PCB BERG HDR ST FEM 6P	SSW-106-01-G-S	CNBERGF1X6H330LD31	J2	SAMTEC
1	CONN-PCB JUMPER MICRO-MINI 6.9MM	5102	CNKEYSTONE5102	JP1	KEYSTONE
2	LED GREEN CLEAR	QTLP600C4TR	LED0603	LED1,LED2	FAIRCHILD SEMICONDR
2	MOD DC-DC CONVERTER 5VIN 9VOUT 1W	PES1-S5-S9-M	MPES1-SX-SX-M	PS1,PS2	CUI INC
2	TRAN GANFET BOTTOM-SIDE COOLED 650V E-MODE, PRELIM	GS66508B	DIE4_8_38X6_98	Q1,Q2	GANSYSTEMS
7	RES FILM SMD 0603	3.3K	R0603	R2-R4,R8-R10,R13	MULTICOMP
2	RES PRECISION THICK FILM CHIP R0603	20	R0603	R6, R12	ROHM
4	RES PRECISION THICK FILM CHIP R0603	10	R0603	R5,R11,R15,R16	PANASONIC
2	IC MICROPOWER LOW-NOISE ULTRA LOW DROPOUT REGULATOR	LP2985IM5-6.1/NOPB	SOT23-5L-2	U1,U3	TEXAS INSTRUMENTS
2	IC-ADI HV ISOLATED GATE DRIVER WITH MILLER CLAMP PRELIM	ADUM4121ARZ	SO8WB_A	U2,U4	ADI
1	IC-ADI LDO REGULATOR 3.3V OUT	ADP3309ARTZ-3.3	SOT23-5L-2	U5	ADI
1	RES FILM SMD 0603	0	R0603	R1, R14	MULTICOMP
1	DIODE TVS UNIDIRECTIONAL	SMAJ7.5A	DO214AC_A	D1	LITTELFUSE, INC.
6	CONN-PCB TST PNT BLK	5001	CNKEY5001TP	TP1-TP6	KEYSTONE ELECTRON
1	heatsink, 35x35mmx25.4mm, black anodized				Cool Innovation
1	Thermal sheet cut to 35x35mm square				BOND PLY

Appendix B - GS665MB-EVB

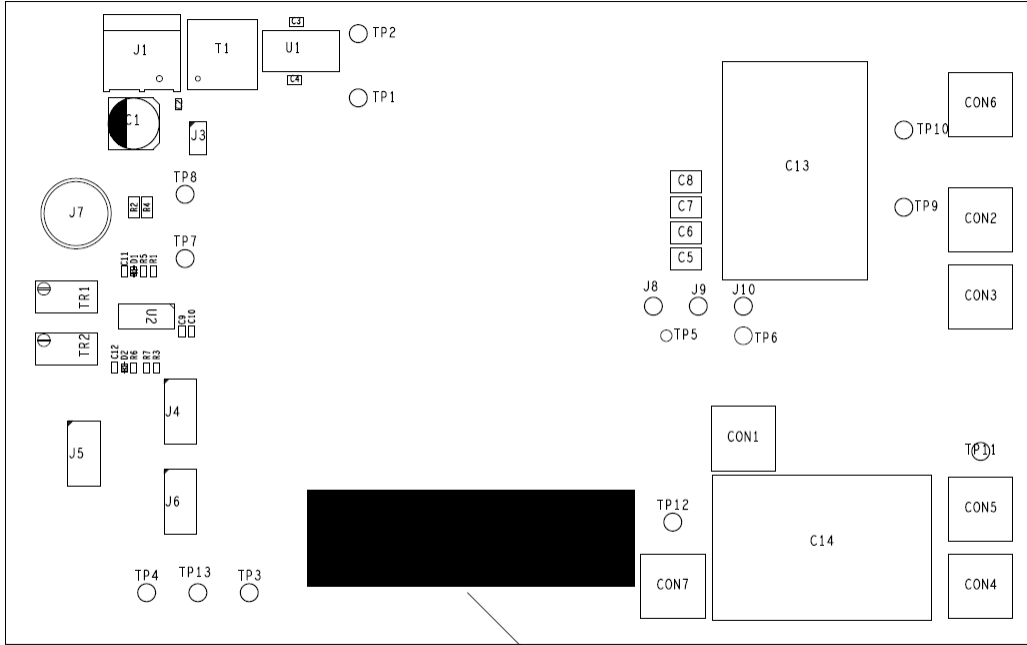
Circuit schematics



Assembly drawing

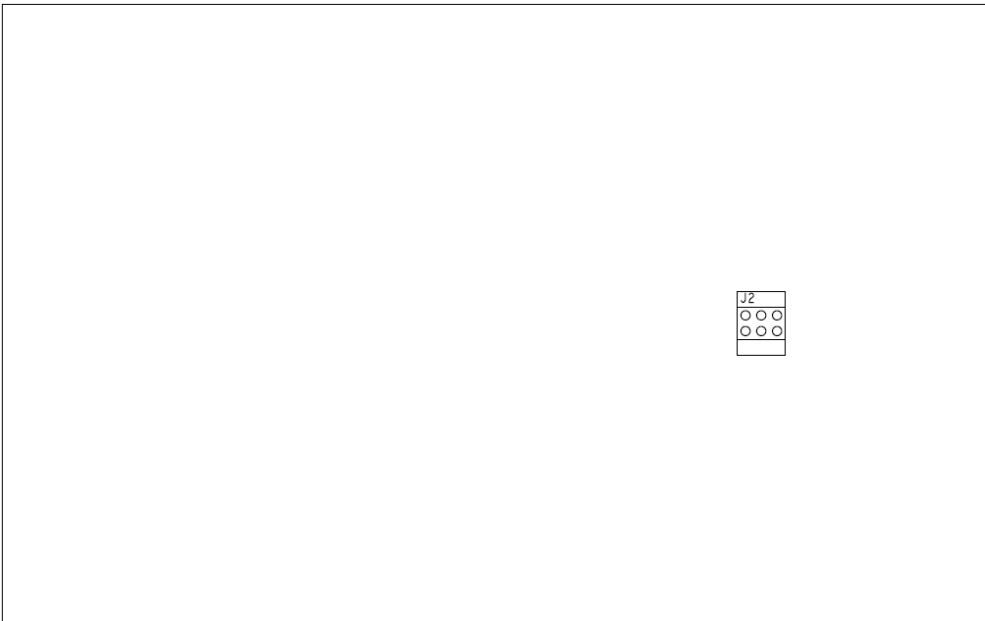
Assembly Top

TOP COMPONENT SIDE



SUGGESTED LOCATION FOR S/N LABEL

Assembly Bottom



Bill of Materials

GAN SYSTEMS 650V GAN UNIVERSAL MOTHER BOATRD						
BOARD P/N:	GS665EVBMB					
Revision	B1					
Last Update	6/30/2016					
Quantity	Reference	Description	Value	Manufacturer	Part number	
	1	PCB	PCB bare 2-layer 2oz Cu.			
1	CON1,CON2,CON3,CON4,CON5,CON6,CON7	TERMINAL SCREW VERTICAL PC MNT	CON-10-32-SCRWMNT	KEYSTONE	8191	D
2	C1	CAP ALUM 220UF 20% 25V SMD	220uF 25V	Panasonic	EEE-FK1E221P	
3	C2,C10	GENERIC 1UF/25V, 10% X7R SMD 0603	1uF	TAIYO YUDEN	TMK107B7105KA-T	
4	C3,C4	GENERIC 10UF/25V, 10% SMD 0805	10uF	TAIYO YUDEN	TMK212BBJ106KG-T	
5	C5,C6,C7,C8	GENERIC 0.1uF/1000V, SMD 1812	0.1uF 1kV	KEMET	C1812C104KDRAC7800	
6	C9	GENERIC 0.1UF/25V, 10% X7R SMD 0603	0.1uF	TAIYO YUDEN	TMJ107BB7104KAHT	
7	C11,C12	GENERIC 100PF/25V 5% NP0 SMD 0603	100pF	KEMET	C0603C101J3GACTU	
8	C13,C44	CAP FILM 10UF/600VDC 5%, 27.5MM LEAD SPACING	10uF 700V	KEMET	C4AEHBU5100A11J	D
9	D1,D2	DIODE SCHOTTKY 20V 500MA SOD523	PMEG2005EB	NXP	PMEG2005EB,115	
10	J1	TERM BLOCK HDR 2POS R/A 5.08MM	CON-TERM-BLK-2POS-RA	TE CONNECTIVITY	796638-2	
11	J1-PLUG	TERM BLOCK BLUG 2POS 5.08MM		TE CONNECTIVITY	796634-2	
12	J2	CONN RCPT 6POS .100 DBL STR PCB	CON-RCPT-2X3-BOT	HARWIN	M20-7850342	M
13	J3		CON-2POS			C IN
14	J4,J6	CONN HEADER 8POS DUAL VERT PCB	CON-JMP-4POS	HARWIN	M20-9980445	
15	J5	CONN 8-POS, DUAL ROW 2.54MM	CON-HDR-4X2	AMPHENOL	75869-132LF	
16	J7	CONN BNC JACK STR 50 OHM PCB	112538	AMPHENOL	112538	
17	J8,J9,J10	CONN RECEIPT PIN .032-.046" .075"	CON-RCPT-EDGEMNT	MILLMAX	0312-0-15-15-34-27-10-0	M E
18	R1,R3,R7	generic 1% smd 0603	49R9	VISHAY DALE	CRCW060349R9FKEA	
19	R2,R4	generic 1% smd 1206	100R			D
20	R5,R6	generic 1% smd 0603	1K00	VISHAY DALE	CRCW06031K00FKEA	
21	TP1,TP2,TP3,TP4,TP7,TP8,TP9,TP10,TP11,TP12,TP13	TEST POINT PCB	TP-KEYSTONE-5010	KEYSTONE	5010	
22	TR1,TR2		2K	RECOM	CMC-08	D
23	T1	COMM MODE CHOKE 5.2A T/H	CMC-08			
24	U1	IC REG LDO 5V 1A DPAK	MC7805	ON SEMI	MC7805BDTRKG	
25	U2	1 IC GATE NAND 4CH 2-INP 14-SOIC	74VHC132	FAIRCHILD	74VHC132MX	
Off the board components:						
26	M1,M2,M3,M4,M5,M6	PCB STANDOFF NYLON STACKABLE 4.75M	MECH-STD0FF-KEYSTONE-8	KEYSTONE		8833
27	FAN	FAN AXIAL 38X20MM 12VDC WIRE		SUNON FANS	PMD1238PKB1-A.(2).GN	P S C IN J
28	JUMPER	JUMPER SHUNT GENERIC		TE CONNECTIVITY	382811-8	

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