



# Normally – OFF Silicon Carbide Junction Transistor

 $V_{DS}$  = 300 V  $R_{DS(ON)}$  = 240 m $\Omega$   $I_{D (Tc = 25^{\circ}C)}$  = 9 A  $h_{FE (Tc = 25^{\circ}C)}$  = 110

#### **Features**

- 210°C maximum operating temperature
- · Gate Oxide Free SiC Switch
- Exceptional Safe Operating Area
- Excellent Gain Linearity
- Compatible with 5 V TTL Gate Drive
- Temperature Independent Switching Performance
- Low Output Capacitance
- Positive Temperature Coefficient of R<sub>DS,ON</sub>
- Suitable for Connecting an Anti-parallel Diode

#### **Advantages**

- Compatible with Si MOSFET/IGBT Gate Drive ICs
- > 20 µs Short-Circuit Withstand Capability
- Lowest-in-class Conduction Losses
- High Circuit Efficiency
- · Minimal Input Signal Distortion
- High Amplifier Bandwidth

### **Package**

• RoHS Compliant





**TO-46** 

## **Applications**

- Down Hole Oil Drilling
- Geothermal Instrumentation
- Solenoid Actuators
- General Purpose High-Temperature Switching
- Amplifiers
- Solar Inverters
- Switched-Mode Power Supply (SMPS)
- Power Factor Correction (PFC)

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## **Section I: Absolute Maximum Ratings**

Parameter	Symbol	Conditions	Value	Unit	Notes
Drain – Source Voltage	V <sub>DS</sub>	V <sub>GS</sub> = 0 V	300	V	
Continuous Drain Current	Ι <sub>D</sub>	$T_J = 210^{\circ}\text{C}, T_C = 25^{\circ}\text{C}$	5.8	Α	
Continuous Gate Current	I <sub>GM</sub>		0.5	Α	
Turn-Off Safe Operating Area	RBSOA	$T_{VJ} = 210$ °C, $I_G = 0.5$ A, Clamped Inductive Load	$I_{D,max} = 9$ $\emptyset V_{DS} \le V_{DSmax}$	Α	Fig. 18
Short Circuit Safe Operating Area	SCSOA	$T_{VJ} = 210$ °C, $I_G = 0.5$ A, $V_{DS} = 200$ V, Non Repetitive	>20	μs	
Reverse Gate – Source Voltage	$V_{SG}$	·	30	V	
Reverse Drain – Source Voltage	$V_{SD}$		25	V	
Power Dissipation	P <sub>tot</sub>	$T_J = 210^{\circ}C, T_C = 25^{\circ}C$	20	W	Fig. 16
Storage Temperature	T <sub>stg</sub>		-55 to 210	°C	

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## **Section II: Electrical Characteristics**

Davamatar	Symbol	Conditions	Value		11	Nistes	
Parameter		Conditions	Min.	Typical	Max.	- Unit	Notes
A: On State							
Drain – Source On Resistance	R <sub>DS(ON)</sub>	$\begin{split} I_D &= 5 \text{ A, } T_j = 25 \text{ °C} \\ I_D &= 5 \text{ A, } T_j = 125 \text{ °C} \\ I_D &= 5 \text{ A, } T_j = 175 \text{ °C} \\ I_D &= 5 \text{ A, } T_j = 175 \text{ °C} \\ I_D &= 5 \text{ A, } T_j = 210 \text{ °C} \end{split}$		240 368 455 580		mΩ	Fig. 5
Gate – Source Saturation Voltage	$V_{GS,sat}$	$I_D = 5 \text{ A}, I_D/I_G = 40, T_j = 25 \text{ °C}$ $I_D = 5 \text{ A}, I_D/I_G = 30, T_j = 175 \text{ °C}$		3.45 3.22		V	Fig. 7
DC Current Gain	h <sub>FE</sub>	$\begin{array}{c} V_{DS} = 5 \text{ V, } I_{D} = 5 \text{ A, } T_{j} = 25 \text{ °C} \\ V_{DS} = 5 \text{ V, } I_{D} = 5 \text{ A, } T_{j} = 125 \text{ °C} \\ V_{DS} = 5 \text{ V, } I_{D} = 5 \text{ A, } T_{j} = 175 \text{ °C} \\ V_{DS} = 5 \text{ V, } I_{D} = 5 \text{ A, } T_{j} = 210 \text{ °C} \\ \end{array}$		113 79 72 70		_	Fig. 5
B: Off State							
Drain Leakage Current	I <sub>DSS</sub>	$\begin{array}{l} V_R = 300 \text{ V}, V_{GS} = 0 \text{ V}, T_j = 25 \text{ °C} \\ V_R = 300 \text{ V}, V_{GS} = 0 \text{ V}, T_j = 125 \text{ °C} \\ V_R = 300 \text{ V}, V_{GS} = 0 \text{ V}, T_j = 210 \text{ °C} \end{array}$		10 50 100	100 500 1000	nA	Fig. 6
Gate Leakage Current	I <sub>sg</sub>	V <sub>SG</sub> = 20 V, T <sub>j</sub> = 25 °C		20		nA	
C: Thermal							
Thermal resistance, junction - case	R <sub>thJC</sub>	Assumes thermal conduction through baseplate only actual value may be lower		9.86		°C/W	Fig. 19

## **Section III: Dynamic Electrical Characteristics**

Doromotor	Cumbal	Symbol Conditions -		Value			Notes
Parameter	Symbol	Conditions	Min.	Typical	Max.	Unit	Notes
A: Capacitance and Gate Charge	9						
Input Capacitance	C <sub>iss</sub>	$V_{GS} = 0 \text{ V}, V_{D} = 300 \text{ V}, f = 1 \text{ MHz}$		527		pF	Fig. 9
Reverse Transfer/Output Capacitance	$C_{rss}/C_{oss}$	$V_D = 300 \text{ V}, f = 1 \text{ MHz}$		24		рF	Fig. 9
Output Capacitance Stored Energy	Eoss	$V_{GS} = 0 \text{ V}, V_{D} = 300 \text{ V}, f = 1 \text{ MHz}$		1.1		μJ	Fig. 10
Effective Output Capacitance, time related	$C_{\text{oss,tr}}$	$I_D$ = constant, $V_{GS}$ = 0 V, $V_{DS}$ = 0800 V		51		pF	
Effective Output Capacitance, energy related	$C_{oss,er}$	$V_{GS} = 0 \text{ V}, V_{DS} = 080 \text{ V}$		41		pF	
Gate-Source Charge	$Q_{GS}$	V <sub>GS</sub> = -53 V		3.7		nC	
Gate-Drain Charge	$Q_{GD}$	$V_{GS} = 0 \text{ V}, V_{DS} = 0200 \text{ V}$		10.9		nC	
Gate Charge - Total	$Q_G$			14.6		nC	
B: Switching							
Internal Gate Resistance – zero bias	$R_{G(INT\text{-}ZERO)}$	$f = 1 \text{ MHz}, V_{AC} = 50 \text{ mV}, V_{DS} = V_{GS} = 0 \text{ V}, $ $T_i = 210  {}^{\circ}\text{C}$		14.5		Ω	
Internal Gate Resistance – ON	R <sub>G(INT-ON)</sub>	$V_{GS} > 2.5 \text{ V}, V_{DS} = 0 \text{ V}, T_j = 210 ^{\circ}\text{C}$		0.37		Ω	
Turn On Delay Time	t <sub>d(on)</sub>	$T_i = 25  {}^{\circ}\text{C},  V_{DS} = 200  \text{V},$		13.0		ns	
Fall Time, V <sub>DS</sub>	t <sub>f</sub>	_I <sub>D</sub> = 5 A, Resistive Load		12.4		ns	Fig. 11, 13
Turn Off Delay Time	$t_{d(off)}$	Refer to Section V: for additional driving		12.0		ns	
Rise Time, V <sub>DS</sub>	t <sub>r</sub>	information		6.6		ns	Fig. 12, 14
Turn On Delay Time	t <sub>d(on)</sub>	$_{\rm T_i}$ = 210 °C, $V_{\rm DS}$ = 200 V,		7.0		ns	_
Fall Time, V <sub>DS</sub>	t <sub>f</sub>	_I <sub>D</sub> = 5 A, Resistive Load		12.2		ns	Fig. 11
Turn Off Delay Time	$t_{d(off)}$	Refer to Section V: for additional driving		30.0		ns	
Rise Time, V <sub>DS</sub>	t <sub>r</sub>	information		6.9		ns	Fig. 12
Turn-On Energy Per Pulse	$E_{on}$	$T_i = 25  {}^{\circ}\text{C},  V_{DS} = 200  \text{V},$		20.6		μJ	Fig. 11, 13
Turn-Off Energy Per Pulse	$E_{off}$	-I <sub>j</sub> = 25 ℃, V <sub>DS</sub> = 200 V, -I <sub>D</sub> = 5 A, Inductive Load		1.0		μJ	Fig. 12, 14
Total Switching Energy	$E_{tot}$	ID = 071, madelive zead		21.6		μJ	
Turn-On Energy Per Pulse	E <sub>on</sub>	T 240.0C V 200.V		18.4		μJ	Fig. 11
Turn-Off Energy Per Pulse	$E_{off}$	−T <sub>j</sub> = 210 °C, V <sub>DS</sub> = 200 V, −I <sub>D</sub> = 5 A, Inductive Load		0.6		μJ	Fig. 12
Total Switching Energy	$E_{tot}$	ip = 074, iliduotive Eddu		19.0		μJ	

 $<sup>^{1}</sup>$  – All times are relative to the Drain-Source Voltage  $V_{\text{DS}}$ 



## **Section IV: Figures**

#### A: Static Characteristics

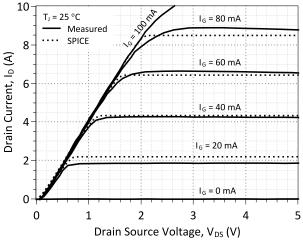


Figure 1: Typical Output Characteristics at 25 °C

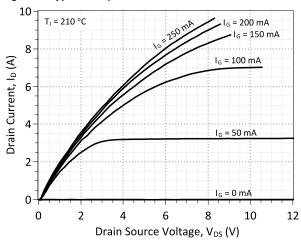


Figure 3: Typical Output Characteristics at 210 °C

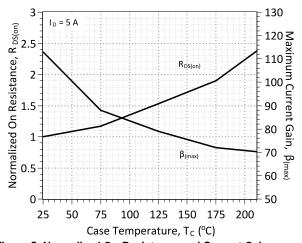


Figure 5: Normalized On-Resistance and Current Gain vs. Temperature

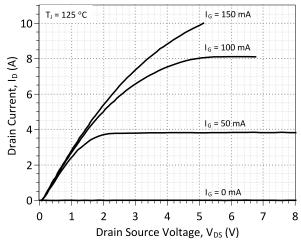


Figure 2: Typical Output Characteristics at 125 °C

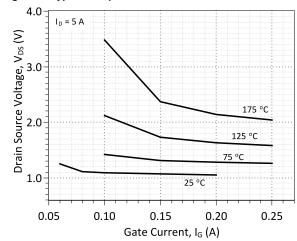


Figure 4: Drain-Source Voltage vs. Gate Current

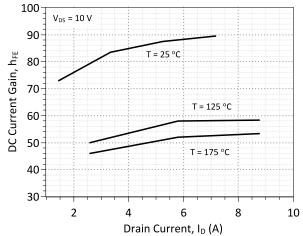


Figure 6: DC Current Gain vs. Drain Current

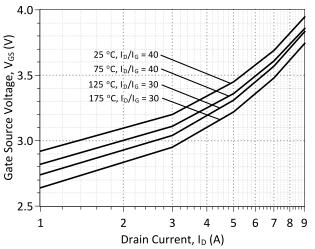


Figure 7: Typical Gate - Source Saturation Voltage

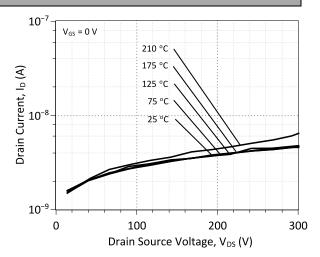


Figure 8: Typical Blocking Characteristics

## **B: Dynamic Characteristics**

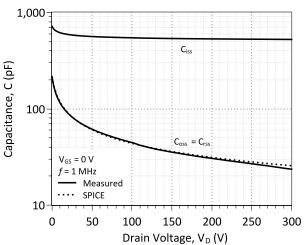


Figure 9: Input, Output, and Reverse Transfer Capacitance

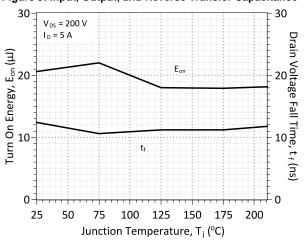


Figure 11: Typical Turn On Energy Losses and Switching Times vs. Temperature

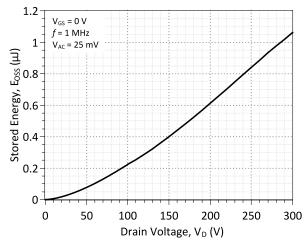


Figure 10: Energy stored in Output Capacitance

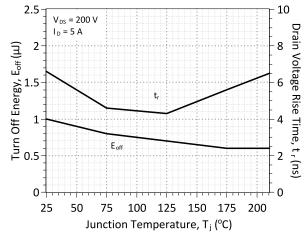


Figure 12: Typical Turn Off Energy Losses and Switching Times vs. Temperature





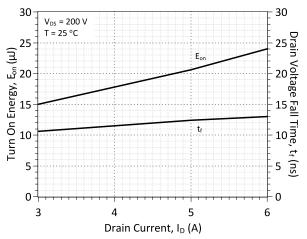


Figure 13: Typical Turn On Energy Losses and Switching Times vs. Drain Current

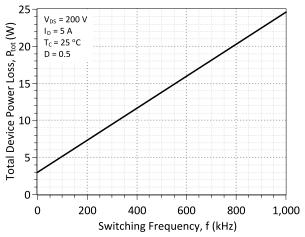


Figure 15: Typical Hard Switched Device Power Loss vs. Switching Frequency <sup>2</sup>

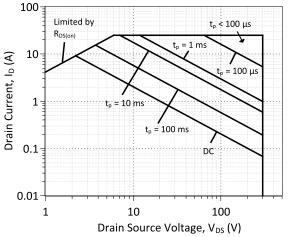


Figure 17: Forward Bias Safe Operating Area at T<sub>c</sub>= 25 °C

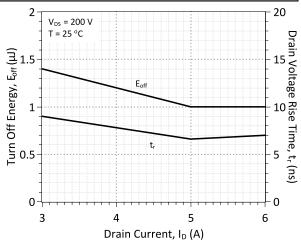


Figure 14: Typical Turn Off Energy Losses and Switching Times vs. Drain Current

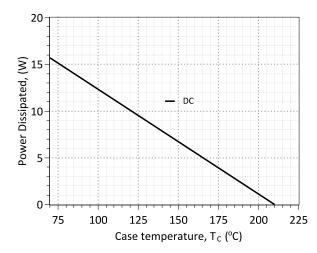


Figure 16: Power Derating Curve

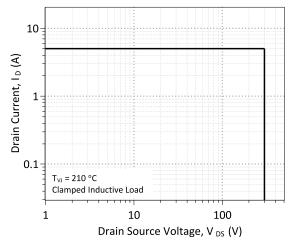


Figure 18: Turn-Off Safe Operating Area

<sup>&</sup>lt;sup>2</sup> – Representative values based on device conduction and switching loss. Actual losses will depend on gate drive conditions, device load, and circuit topology.



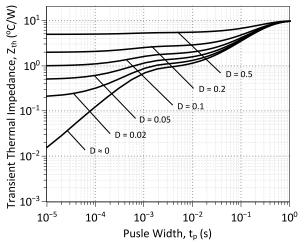


Figure 19: Transient Thermal Impedance

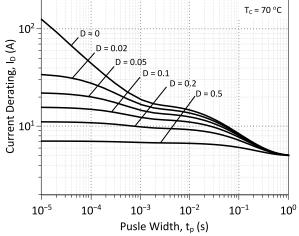


Figure 20: Drain Current Derating vs. Pulse Width



## Section V: Driving the GA05JT03-46

The GA05JT03-46 is a current controlled SiC transistor which requires a positive gate current for turn-on and to remain in on-state. It may be driven by different drive topologies depending on the intended application.

Table 1: Estimated Power Consumption and switching frequencies for various Gate Drive topologies.

Drive Topology	Gate Drive Power Consumption	Switching Frequency
Simple TTL	High	Low
Constant Current	Medium	Medium
High Speed – Boost Capacitor	Medium	High
High Speed – Boost Inductor	Low	High
Proportional	Lowest	Medium
Pulsed Power	Medium	N/A

#### A: Simple TTL Drive

The GA05JT03-46 may be driven by 5 V TTL logic by using a simple current amplification stage. The current amplifier output current must meet or exceed the steady state gate current,  $I_{G,steady}$ , required to operate the GA05JT03-46. An external gate resistor  $R_G$ , shown in the Figure 21 topology, sets  $I_{G,steady}$  to the required level which is dependent on the SJT drain current  $I_D$  and DC current gain  $h_{FE}$ ,  $R_G$  may be calculated from the equation below. The values of  $h_{FE}$  and  $V_{GS,sat}$  may be read from Figure 6 and Figure 7, respectively.  $V_{EC,sat}$  can be taken from the PNP datasheet, a partial list of high-temperature PNP and NPN transistors options is given below. High-temperature MOSFETs may also be used in the topology.

$$R_{G,max} = \frac{\left(5.0 \ V - V_{EC,sat}(PNP) - V_{GS,sat}(SJT)\right) * h_{FE}(T, I_D)}{I_D * 1.5}$$

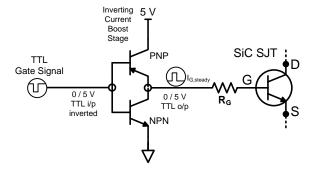


Figure 21: Simple TTL Gate Drive Topology

Table 2: Partial List of High-Temperature BJTs for TTL Gate Driving

BJT Part Number	Туре	T <sub>j,max</sub> (°C)
PHPT60603PY	PNP	175
PHPT60603NY	NPN	175
2N2222	NPN	200
2N6730	PNP	200
2N2905	PNP	200
2N5883	PNP	200
2N5885	NPN	200



#### **B: High Speed Driving**

For ultra high speed GA05JT03-46 switching ( $t_r$ ,  $t_r$  < 20 ns) while maintaining low gate drive losses the supplied gate current should include a positive current peak during turn-on, a negative voltage peak during turn-off, and continuous gate current I<sub>G</sub> to remain on.

An SJT is rapidly switched from its blocking state to on-state, when the necessary gate charge for turn-on,  $Q_G$ , is supplied by a burst of high gate current until the gate-source capacitance,  $C_{GS}$ , and gate-drain capacitance,  $C_{GD}$ , are fully charged. Ideally, the burst should terminate when the drain voltage has fallen to its on-state value in order to avoid unnecessary drive losses. A negative voltage peak is recommended for the turn-off transition in order to ensure that the gate current is not being supplied under high dV/dt due to the Miller effect. While satisfactory turn off can be achieved with  $V_{GS} = 0$  V, a negative  $V_{GS}$  value may be used in order to speed up the turn-off transition.

#### B:1: High Speed, Low Loss Drive with Boost Capacitor

The GA05JT03-46 may be driven using a High Speed, Low Loss Drive with Boost Capacitor topology in which multiple voltage levels, a gate resistor, and a gate capacitor are used to provide current peaks at turn-on and turn-off for fast switching and a continuous gate current while in on-state. As shown in Figure 22, in this topology two gate driver ICs are utilized. An external gate resistor R<sub>G</sub> is driven by a low voltage driver to supply the continuous gate current throughout on-state.and a gate capacitor C<sub>G</sub> is driven at a higher voltage level to supply a high current peak at turn-on and turn-off. A 3 kV isolated evaluation gate drive board (GA03IDDJT30-FR4) from GeneSiC Semiconductor utilizing this topology is commercially available for high and low-side driving, its datasheet provides additional details about this drive topology.

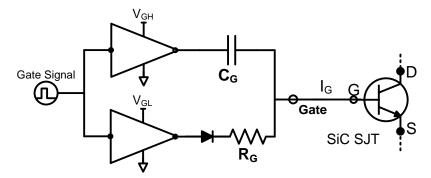


Figure 22: High Speed, Low Loss Drive with Boost Capacitor Topology

#### B:2: High Speed, Low Loss Drive with Boost Inductor

A High Speed, Low-Loss Driver with Boost Inductor is also capable of driving the GA05JT03-46 at high-speed. It utilizes a gate drive inductor instead of a capacitor to provide the high-current gate current pulses  $I_{G,on}$  and  $I_{G,off}$ . During operation, inductor L is charged to a specified  $I_{G,on}$  current value then made to discharge  $I_L$  into the SJT gate pin using logic control of  $S_1$ ,  $S_2$ ,  $S_3$ , and  $S_4$ , as shown in Figure 23. After turn on, while the device remains on the necessary steady state gate current  $I_{G,steady}$  is supplied from source  $V_{CC}$  through  $R_G$ . Please refer to the article "A current-source concept for fast and efficient driving of silicon carbide transistors" by Dr. Jacek Rąbkowski for additional information on this driving topology.<sup>3</sup>

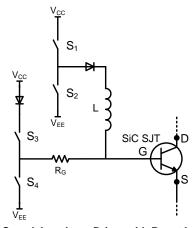


Figure 23: High Speed, Low-Loss Driver with Boost Inductor Topology

<sup>3 -</sup> Archives of Electrical Engineering. Volume 62, Issue 2, Pages 333-343, ISSN (Print) 0004-0746, DOI: 10.2478/aee-2013-0026, June 2013



#### C: Proportional Gate Current Driving

A proportional gate drive topology may be beneficial for applications in which the GA05JT03-46 will operate over a wide range of drain current conditions to lower the gate drive power consumption. A proportional gate driver relies on instantaneous drain current I<sub>D</sub> feedback to vary the steady state gate current I<sub>G,steady</sub> supplied to the GA05JT03-46.

#### C:1: Voltage Controlled Proportional Driver

A voltage controlled proportional driver relies on a gate drive integrated circuit to detect the GA05JT03-46 drain-source voltage  $V_{DS}$  during onstate to sense  $I_D$ . The integrated circuit will then increase or decrease  $I_G$  in response to  $I_D$ . This allows  $I_G$  and gate drive power consumption to reduce while  $I_D$  is low or for  $I_G$  to increase when  $I_D$  increases. A high voltage diode connected between the drain and sense protects the integrated circuit from high-voltage when blocking. A simplified version of this topology is shown in Figure 24. Additional information will be available in the future at http://www.genesicsemi.com/references/product-notes/.

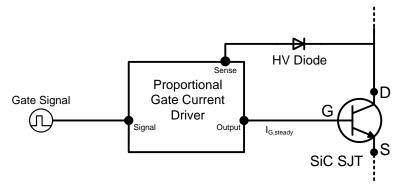


Figure 24: Simplified Voltage Controlled Proportional Driver

#### C:2: Current Controlled Proportional Driver

The current controlled proportional driver relies on a low-loss transformer in the drain or source path to provide feedback of the GA05JT03-46 drain current during on-state to supply  $I_{G,steady}$  into the gate.  $I_{G,steady}$  will increase or decrease in response to  $I_D$  at a fixed forced current gain which is set be the turns ratio of the transformer,  $h_{force} = I_D / I_G = N_2 / N_1$ . GA05JT03-46 is initially tuned-on using a gate current pulse supplied into an RC drive circuit to allow  $I_D$  current to begin flowing. This topology allows  $I_{G,steady}$  and the gate drive power consumption to reduce while  $I_D$  is relatively low or for  $I_{G,steady}$  to increase when  $I_D$  increases. A simplified version of this topology is shown in Figure 25. Additional information will be available in the future at http://www.genesicsemi.com/references/product-notes/.

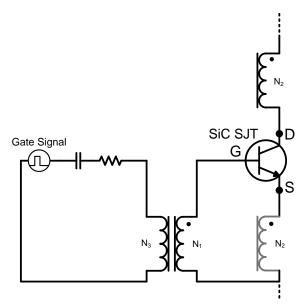


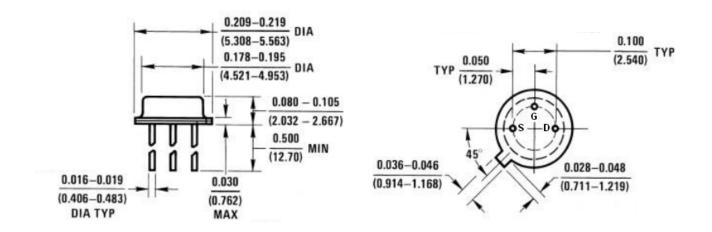
Figure 25: Simplified Current Controlled Proportional Driver



## **Section VI: Package Dimensions**

**TO-46** 

#### **PACKAGE OUTLINE**



- 1. CONTROLLED DIMENSION IS INCH. DIMENSION IN BRACKET IS MILLIMETER.
  2. DIMENSIONS DO NOT INCLUDE END FLASH, MOLD FLASH, MATERIAL PROTRUSIONS

Revision History						
Date Revision Comments Supersedes						
2014/12/12	1	Updated Electrical Characteristics				
2014/08/25	0	Initial release				

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#### **Section VII: SPICE Model Parameters**

This is a secure document. Please copy this code from the SPICE model PDF file on our website (http://www.genesicsemi.com/images/hit\_sic/sjt/GA05JT03-46\_SPICE.pdf) into LTSPICE (version 4) software for simulation of the GA05JT03-46.

```
MODEL OF GeneSiC Semiconductor Inc.
*
     $Revision:
                   1.0
                                  $
     $Date:
               12-DEC-2014
                                        $
     GeneSiC Semiconductor Inc.
     43670 Trade Center Place Ste. 155
     Dulles, VA 20166
     COPYRIGHT (C) 2014 GeneSiC Semiconductor Inc.
     ALL RIGHTS RESERVED
* These models are provided "AS IS, WHERE IS, AND WITH NO WARRANTY
 OF ANY KIND EITHER EXPRESSED OR IMPLIED, INCLUDING BUT NOT LIMITED
 TO ANY IMPLIED WARRANTIES OF MERCHANTABILITY AND FITNESS FOR A
 PARTICULAR PURPOSE."
 Models accurate up to 2 times rated drain current.
.model GA05JT03 NPN
           9.8338E-48
+ IS
+ ISE
           1.0733E-26
           3.23
+ EG
+ BF
           135
+ BR
           0.55
           200
+ IKF
           1
+ NF
           2.
+ NE
+ RB
           14.5
           0.002
+ IRB
+ RBM
           0.37
+ RE
           0.01
           0.23
+ RC
+ CJC
           2.16E-10
+ VJC
           3.656
+ MJC
           0.4717
+ CJE
           5.021E-10
           2.95
+ VJE
+ MJE
           0.4867
+ XTI
           3
+ XTB
           -1.0
                 1.050E-2
+ TRC1
+ VCEO
                 300
+ ICRATING 9
 MFG
           GeneSiC_Semiconductor
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End of GA05JT03 SPICE Model

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