## MAX16946/MAX16947

# Remote Antenna, Current-Sense and LDO/Switches 


#### Abstract

General Description


The MAX16946/MAX16947 high-voltage, high-side, cur-rent-sense LDO/switches feature internal current limiting to prevent system damage due to fault conditions. The MAX16946 provides a fixed regulated 8.5V output voltage or an adjustable 3.3 V to 15 V output voltage. The MAX16946 can also be configured as a switch, while the MAX16947 is only available as a switch. The input voltage range for both devices extends from 4.5 V to 18 V (45V tolerant), making the devices ideal for providing phantom power to remote radio-frequency low-noise amplifiers (LNAs) in automotive applications.
The devices monitor the load current and provide an analog output voltage proportional to the sensed load current. Accurate internal current limit protects the input supply against both overload and short-circuit conditions. Two open-drain fault indicator outputs indicate to the microprocessor when a short circuit, an open-load condition, or a short-to-battery condition exists. An overtemperature shutdown is also indicated by means of the current-sense amplifier's output voltage.
A fault-blanking feature allows the devices to ignore momentary faults such as those caused by the charging of capacitive loads during hot-swapping, preventing false alarms to the system. The devices feature short-to-battery protection to latch off the internal LDO/pass switch during a short-to-battery event. During a thermal overload, the devices reduce power dissipation by going into thermal shutdown. They include an active-low, high-voltage-compatible shutdown input to place them in lowpower shutdown mode.
The MAX16946 is available in thermally enhanced, 16-pin TQFN-EP and QSOP-EP packages. The MAX16947 is available in a 16 -pin QSOP package. Both devices operate over the $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ temperature range.

## Ordering Information

| PART | PIN-PACKAGE | OUTPUT |
| :--- | :--- | :---: |
| MAX16946GEE/V+ | 16 QSOP-EP* | Switch or LDO |
| MAX16946GTE/V+ | 16 TQFN-EP* | Switch or LDO |
| MAX16947GEE/V+ ${ }^{* *}$ | 16 QSOP | Switch |

Note: All devices are specified over the $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ operating temperature range.
/V Denotes an automotive qualified part.
+Denotes a lead(Pb)-free/RoHS-compliant package.
*EP = Exposed pad.
${ }^{* *}$ Future product-contact factory for availability.

Features

- Switch Phantom Power-On/Off Under $\mu \mathrm{C}$ Control
- Precision Adjustable Current Limit $300 \mathrm{~mA}(\max ), \mathrm{T}_{\mathrm{A}}=+105^{\circ} \mathrm{C}$ 500 mA (max), $\mathrm{T}_{\mathrm{A}}=+85^{\circ} \mathrm{C}$ (MAX16946 in SW Mode Only)
- Regulated Output Voltage (MAX16946)-8.5V

Fixed or Adjustable Between 3.3V and 15V

- Current Measurement Analog Voltage Output
- Detect Open-Load and Short-Circuit Conditions
- Provide Open-Drain Fault Signals ( $\overline{\mathrm{SC}}$ and $\overline{\mathrm{OL}})$
- Overcurrent Blanking During Startup
- Thermal Shutdown
- AEC-Q100 Qualified
$-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ Operating Temperature Range


## Applications

Remote LNA Phantom Power
Automotive Safety and Infotainment
Automotive Remote Module Power
Functional Diagram


## MAX16946/MAX16947 <br> Remote Antenna, Current-Sense and LDO/Switches

## ABSOLUTE MAXIMUM RATINGS




Note 1: Package thermal resistances were obtained using the method described in JEDEC specification JESD51-7, using a four-layer board. For detailed information on package thermal considerations, refer to www.maximintegrated.com/thermal-tutorial.

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## ELECTRICAL CHARACTERISTICS

$\left(\mathrm{VIN}=12 \mathrm{~V}, \mathrm{VGND}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}\right.$ to $+105^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=\mathrm{TJ}=+25^{\circ} \mathrm{C}$.)

| PARAMETER | SYMBOL | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| POWER SWITCH/LDO |  |  |  |  |  |  |  |
| IN Operating Supply Range | VIN | Full performance |  | 4.5 |  | 18 | V |
|  |  | Output switched off (Note 2) |  |  |  | 28 | V |
|  |  | Output switched off for < 1s (Note 2) |  |  |  | 45 | V |
| IN Supply Current | ICC | $\mathrm{V} \overline{\mathrm{SHDN}}>2.4 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  |  | 2.1 | 2.6 | mA |
| IN Shutdown Supply Current | ISD | $V \overline{\text { SHDN }}=\mathrm{V}_{\mathrm{GND}}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{VIN}^{\prime}=12 \mathrm{~V}$ |  |  |  | 7 | $\mu \mathrm{A}$ |
| Undervoltage Lockout (Rising) | VUVLO | Falling VIN |  |  | 3.5 |  | V |
|  |  | Rising VIN |  |  | 3.9 |  |  |
|  |  | Hysteresis |  |  | 0.4 |  |  |
| Internal Switch Voltage Drop | VSW | Measured between SENS and OUT while sourcing 100 mA , FB grounded, SW operation, $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, 4.5 \mathrm{~V}<\mathrm{V}_{\mathrm{IN}}<18 \mathrm{~V}$ |  |  |  | 0.20 | V |
|  |  | Measured between SENS and OUT while sourcing 100 mA , FB grounded, SW operation, $\mathrm{T}_{\mathrm{A}}=+105^{\circ} \mathrm{C}, 4.5 \mathrm{~V}<\mathrm{V}$ IN $<18 \mathrm{~V}$ (Note 2) |  |  | 0.2 | 0.25 | V |
| Internal Voltage Regulator | VREG | $I_{\text {REG }}=0 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  |  | 5 |  | V |
| Feedback Voltage | VFB | MAX16946 only, LDO mode with FB connected to external resistive divider | $\begin{aligned} & \text { IOUT }=5 \mathrm{~mA} \text { to } \\ & 150 \mathrm{~mA}, 4.5 \mathrm{~V} \leq \mathrm{V} \mathrm{IN} \leq \\ & 18 \mathrm{~V} \end{aligned}$ | 0.97 | 1 | 1.03 | V |
|  |  |  | $\begin{aligned} & \text { IOUT }=2 \mathrm{~mA} \text { to } \\ & 200 \mathrm{~mA}, 4.5 \mathrm{~V}<\mathrm{V} \text { IN } \\ & \leq 18 \mathrm{~V} \end{aligned}$ | 0.95 | 1 | 1.05 | V |

## Remote Antenna, Current-Sense and LDO/Switches

## ELECTRICAL CHARACTERISTICS (continued)

$\left(V_{I N}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{GND}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}\right.$ to $+105^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=\mathrm{T}_{\mathrm{J}}=+25^{\circ} \mathrm{C}$.)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Feedback Input Bias Current | IfB | $V_{\text {FB }}=1.0 \mathrm{~V}, \mathrm{LDO}$ mode, $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | -0.5 |  | +0.5 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\mathrm{FB}}=1.0 \mathrm{~V}, \mathrm{LDO}$ mode, $\mathrm{T}_{\mathrm{A}}=+105^{\circ} \mathrm{C}$ |  | 0 |  |  |
| Fixed 8.5V to LDO Mode Feedback Threshold | VFB_TH | Switching to LDO mode from fixed 8.5V | 3.3 |  | 4.2 | V |
| Adjustable Output Voltage Range | Vout | LDO mode with external resistive divider, VIN > VOUT + VDROPOUT (Note 3) | 3.3 |  | 15 | V |
| FB Load Regulation |  | VIN - VOUT $\geq 2 \mathrm{~V}$, IOUT $=5 \mathrm{~mA}$ to 100 mA , LDO mode |  | -2 |  | \% |
| FB Line Regulation |  | VIN - VOUT $\geq 2 \mathrm{~V}$, IOUT $=6 \mathrm{~mA}$, LDO mode |  | 20 |  | mV/V |
| Fixed 8.5V Output Voltage | Vout_8.5V | IOUT $=5 \mathrm{~mA}$, LDO mode with internal resistive divider, $9 \mathrm{~V} \leq \mathrm{V}$ IN $\leq 18 \mathrm{~V}$ | 8.33 | 8.5 | 8.67 | V |
| Power-Supply Rejection Ratio | PSRR | VIN - VOUT $\geq 2 \mathrm{~V}, \mathrm{f}=100 \mathrm{~Hz}$, LDO mode |  | 50 |  | dB |
| Startup Response Time | tST | $\overline{\text { SHDN }}$ rising to switch/LDO on, time needed to charge $\mathrm{CCOMP}=0.1 \mu \mathrm{~F}$ |  | 10 |  | ms |
| OUT Pulldown Resistor Value | ROUT_OFF | V $\overline{\text { SHDN }}=\mathrm{V}_{\text {GND }}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  |  | 250 | k $\Omega$ |
| COMP Power-Down Resistor Value | RCOMP_OFF | $V \overline{\text { SHDN }}=\mathrm{V}_{\text {GND }}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  |  | 120 | $\mathrm{k} \Omega$ |
| CURRENT-SENSE AMPLIFIER |  |  |  |  |  |  |
| AOUT Gain | Av | $\begin{aligned} & \text { VAOUT/(VIN }- \text { VSENS }^{\text {S }} \text {, measured with } \\ & \text { VIN }- \text { VSENS }^{2} 20 \mathrm{mV} \text { and } 100 \mathrm{mV}, \\ & 4.5 \mathrm{~V} \text { VIN }<18 \mathrm{~V} \end{aligned}$ | 25.35 | 26 | 26.65 | V/V |
| Current-Sense Amplifier Input Voltage Range | VINR | Drop across the shunt resistor, normal operation | 0 |  | 125 | mV |
| AOUT Zero-Current Output Voltage | VAOUT_ZS | $\left(\mathrm{V}_{\text {IN }}-\mathrm{V}_{\text {SENS }}\right)=0 \mathrm{~V}, 4.5 \mathrm{~V}<\mathrm{V}_{\text {IN }}<18 \mathrm{~V}$ | 0.368 | 0.4 | 0.432 | V |
| Maximum AOUT Voltage | VAOUT_FS | $\left(\mathrm{V}\right.$ IN $\left.-\mathrm{V}_{\text {SENS }}\right)=125 \mathrm{mV}$, if V LIM $=\mathrm{V}_{\text {REF }}$ then $V_{\text {AOUT }}(\mathrm{MAX})=3 \mathrm{~V}$ |  | 3.65 |  | V |
| AOUT Drive Capability | IAOUT | $\left(\mathrm{VIN}-\mathrm{V}_{\text {SENS }}\right)=30 \mathrm{mV}$ | 1.0 |  |  | mA |
| AOUT Leakage Current | IAOUT_LEAK | $V_{\text {SHDN }}=V_{G N D}, T_{A}=+25^{\circ} \mathrm{C}$ | 2 |  |  | $\mu \mathrm{A}$ |
| SENS Leakage Current | ISENS_LEAK | $V_{\text {SHDN }}=V_{\text {GND }}, T_{A}=+25^{\circ} \mathrm{C}$ |  |  | 2 | $\mu \mathrm{A}$ |
| REFERENCE |  |  |  |  |  |  |
| REF Output Voltage | VREF | $4.5 \mathrm{~V}<\mathrm{V}_{\text {IN }}<18 \mathrm{~V}$ | 2.94 | 3 | 3.06 | V |
| REF Undervoltage | VREF_UV | $V_{\text {REF }}$ falling | 2.18 |  | 2.72 | V |
| REF Output Current | IREF |  | 100 |  |  | $\mu \mathrm{A}$ |
| REF Leakage Current | IREF_LEAK | $\mathrm{V} \overline{\mathrm{SHDN}}=\mathrm{V}_{\mathrm{GND}}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  |  | 2 | $\mu \mathrm{A}$ |
| FAILURE DETECTION COMPARATORS |  |  |  |  |  |  |
| Open-Load Comparator Input Common-Mode Range | Volt_CMR | (Note 2) | 0.4 |  | 1.7 | V |
| Open-Load Comparator Offset Voltage | Volt_os | VOLT $=1.05 \mathrm{~V}$ | -40 | 0 | +40 | mV |

## MAX16946/MAX16947

## Remote Antenna, Current-Sense and <br> LDO/Switches

## ELECTRICAL CHARACTERISTICS (continued)

$\left(\mathrm{VIN}=12 \mathrm{~V}, \mathrm{VGND}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}\right.$ to $+105^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=\mathrm{TJ}=+25^{\circ} \mathrm{C}$.)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OLT Input Bias Current | IOLT | $\mathrm{V}_{\text {OLT }}=1.05 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | -0.5 |  | +0.5 | $\mu \mathrm{A}$ |
|  |  | VOLT $=1.05 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+105^{\circ} \mathrm{C}$ |  | 0 |  |  |
| Initial Open-Load Blanking Time | toL | A switched open load is blanked for toL | 100 |  |  | ms |
| Open-Load Glitch Immunity | tOL_GLITCH | IOUT < IOL | 10 |  | 100 | $\mu \mathrm{s}$ |
| Current-Limit Comparator Input Common-Mode Range | VLIM_CMR | If VLIM is derived from REF then maximum voltage at LIM is 3V (Note 2) | 1.7 |  | 3.65 | V |
| Current-Limit Comparator Input Offset Voltage | VLIM_OS | VLIM $=2.675 \mathrm{~V}$ | -80 | 0 | +80 | mV |
| LIM Input Bias Current | ILIM_BIAS | $\mathrm{V}_{\text {LIM }}=2.675 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | -0.5 |  | +0.5 | $\mu \mathrm{A}$ |
|  |  | VLIM $=2.675 \mathrm{~V}, \mathrm{~T}_{\text {A }}=+105^{\circ} \mathrm{C}$ |  | 0 |  |  |
| Short-Circuit AOUT Voltage Threshold | VSC | Rising VAOUT at which the $\overline{\mathrm{SC}}$ output asserts low, hysteresis of 40 mV , $4.5 \mathrm{~V}<\mathrm{V}_{\mathrm{IN}}<18 \mathrm{~V}$ | 1.65 | 1.7 | 1.75 | V |
| Short-Circuit Current Blanking Time | tBLANK | IOUT > ISC | 100 |  |  | ms |
| Delay Time Before Retry After Short-Circuit Current Turn-Off | tretry | IOUT > ISC | 1100 |  |  | ms |
| IN Overvoltage Lockout Threshold | VoVLO | VIN rising, hysteresis $=0.5 \mathrm{~V}$ (typ) | 19 | 21 | 23 | V |
| Short-to-BAT Threshold in Off-State | Vout_BAT | Short to battery detected when VOUT - VIN > Vout_BAT | 0 | 250 | 500 | mV |
| Reverse-Current Detection Level | Vrev | Power switch on (SW or LDO mode), VREV <br> $=V_{I N}-V_{S E N S}, V_{\text {REV }}=-9.6 m V$ produces <br> $V_{\text {AOUT }}=150 \mathrm{mV}$, $\mathrm{V}_{\text {REV }}=-5.7 \mathrm{mV}$ <br> produces $V_{\text {AOUT }}=250 \mathrm{mV}$ | -9.6 |  | -5.7 | mV |
| Reverse-Current Shutdown Time | tSD_REV | Delay to shut down switch or LDO after VREV exceeds -7.7 mV (typ), $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  |  | 5 | $\mu \mathrm{s}$ |
| Feedback Voltage Out of Range | $V_{\text {FB_ERR }}$ | LDO mode | 1.12 |  | 1.28 | V |
| Reverse-Current Blanking Time for Short-Circuit Events | trev_BLANK | Switching on and off into a temporary load (short-circuit events) |  | 16 |  | ms |
| OVERTEMPERATURE PROTECTION |  |  |  |  |  |  |
| Thermal Shutdown Threshold | TSHDN |  |  | +170 |  | ${ }^{\circ} \mathrm{C}$ |
| Thermal Shutdown Hysteresis | THYST |  |  | 15 |  | ${ }^{\circ} \mathrm{C}$ |
| LOGIC |  |  |  |  |  |  |
| $\overline{\mathrm{SC}}, \overline{\mathrm{OL}}$ Output-Voltage Low | VOL | Sinking current $=1 \mathrm{~mA}$ |  |  | 0.4 | V |
| $\overline{\mathrm{SC}}, \overline{\mathrm{OL}}$ Open-Drain Leakage Current | ISC_LEAK, <br> IOL_LEAK | $\overline{S C}, \overline{O L}$ not asserted, $\sqrt{S C}=\sqrt{O L}=5 \mathrm{~V}$, $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  |  | 1 | $\mu \mathrm{A}$ |

# MAX16946/MAX16947 Remote Antenna, Current-Sense and LDO/Switches 

## ELECTRICAL CHARACTERISTICS (continued)

$\left(V_{I N}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{GND}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}\right.$ to $+105^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=\mathrm{T}_{J}=+25^{\circ} \mathrm{C}$.)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\overline{\text { SHDN }}$ Input-Voltage High | VSHDN_HI |  | 2.7 |  |  | V |
| $\overline{\text { SHDN }}$ Input-Voltage Low | VSHDN_LO |  |  |  | 0.8 | V |
| $\overline{\text { SHDN }}$ Input Current | ISHDN | VSHDN $>6 \mathrm{~V}$ |  | 5 |  | $\mu \mathrm{A}$ |
| SHDN Off-Time | tSHDN_OFF |  | 150 | 256 | 420 | $\mu \mathrm{s}$ |

Note 2: Guaranteed by design and not production tested.
Note 3: VDROPOUT is voltage from VIN to VOUT and includes drop across the sense resistor and internal power FET. Additionally, VOUT + VDROPOUT $<\operatorname{VOVLO}(\mathrm{MIN})=19 \mathrm{~V}$.
$\left(\mathrm{VIN}=14 \mathrm{~V}\right.$, RSENSE $=0.5 \Omega, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted. $)$


## MAX16946/MAX16947

Remote Antenna, Current-Sense and LDO/Switches

Typical Operating Characteristics (continued)
$\left(\mathrm{V} \mid \mathrm{N}=14 \mathrm{~V}\right.$, RSENSE $=0.5 \Omega, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted. $)$


# MAX16946/MAX16947 Remote Antenna, Current-Sense and LDO/Switches 

Typical Operating Characteristics (continued)
$\left(\mathrm{V}_{\mathrm{I}}=14 \mathrm{~V}, \mathrm{R}\right.$ SENSE $=0.5 \Omega, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted. $)$


# MAX16946/MAX16947 <br> Remote Antenna, Current-Sense and LDO/Switches 

Typical Operating Characteristics (continued)
$\left(\mathrm{V} \mid \mathrm{N}=14 \mathrm{~V}\right.$, RSENSE $=0.5 \Omega, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted. $)$
high-voltage line transient response (MAX16947)


CURRENT-SENSE AMPLIFIER GAIN
vs. TEMPERATURE


OVERCURRENT BLANKING TIME
vs. SUPPLY VOLTAGE


AOUT GAIN
vs. TEMPERATURE


OVERCURRENT BLANKING TIME
vs. TEMPERATURE


DROPOUT VOLTAGE (VSENS - VOUT) vs. TEMPERATURE (MAX16946 SWITCH CONFIGURATION)


# MAX16946/MAX16947 <br> Remote Antenna, Current-Sense and LDO/Switches 

Typical Operating Characteristics (continued)
$\left(\mathrm{V}_{\text {IN }}=14 \mathrm{~V}\right.$, RSENSE $=0.5 \Omega, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted. $)$




Pin Description

| PIN |  | NAME | FUNCTION |
| :---: | :---: | :---: | :---: |
| MAX16946 | MAX16947 |  |  |
| 1 | 1 | IN | Input Voltage. Bypass IN to GND with a low-ESR ceramic capacitor with a minimum value of $0.1 \mu \mathrm{~F}$. |
| 2 | 2 | SENS | Current-Sense Amplifier Input. Connect the sense resistor between SENS and IN. |
| 3 | 3 | $\overline{\text { SHDN }}$ | Active-Low Shutdown Input. Drive $\overline{\text { SHDN }}$ low for more than 360 us to turn off the device. Pulsing $\overline{\text { SHDN }}$ low for less than tSHDN_OFF clears the $\overline{\text { OL }}$ output. $\overline{\text { SHDN }}$ is high-voltage compatible and is connected to IN for normal operation. |
| 4, 9, 15 | 4, 9, 14, 15 | GND | Ground |
| 5 | 5 | COMP | LDO Compensation. Connect a $0.1 \mu \mathrm{~F}$ ceramic capacitor between COMP and GND to compensate the LDO. |
| 6 | 6 | $\overline{\mathrm{SC}}$ | Open-Drain Short-Circuit Indicator Output. $\overline{\mathrm{SC}}$ goes low when the load current is greater than the set short-circuit current threshold or when there is a short-to-battery fault. Connect $\overline{\mathrm{SC}}$ to a $10 \mathrm{k} \Omega$ pullup resistor. See Table 1. |
| 7 | 7 | $\overline{\mathrm{OL}}$ | Open-Drain Open-Load Indicator Output. $\overline{\mathrm{OL}}$ goes low when the load current is lower than the set open-load current threshold or when there is a short-to-battery fault. Connect $\overline{\mathrm{OL}}$ to a $10 \mathrm{k} \Omega$ pullup resistor. See Table 1. |
| 8 | 8 | AOUT | Current Monitor Voltage Output. AOUT can be used to measure the load current by means of an external ADC. AOUT has a current drive capability of 1mA. Bypass AOUT to GND with a 15 nF ceramic capacitor. See Table 1. |
| 10 | 10 | OLT | Open-Load Current Threshold Setting Input. A resistive divider between REF, OLT, and GND sets the open-load current threshold. |
| 11 | 11 | LIM | Current-Limit Setting input. Connect a resistive divider from REF, LIM, and GND to set the current limit of the switch or LDO. Alternatively, externally drive LIM (not to exceed 3.65 V ) to set the current limit. |

# Remote Antenna, Current-Sense and LDO/Switches 

Pin Description (continued)

| PIN |  | NAME | FUNCTION |
| :---: | :---: | :---: | :---: |
| MAX16946 | MAX16947 |  |  |
| 12 | 12 | REF | +3V Nominal Reference Output. REF has a current drive capability of 100 A A. |
| 13 | 13 | REG | Internal Regulator +5 V Output. REG powers all internal blocks. Do no use REG to supply power to external circuitry. Bypass REG to GND with a $1 \mu \mathrm{~F}$ capacitor. |
| 14 | - | FB | Feedback Input (MAX16946 Only). Connect FB to GND to configure the MAX16946 as a switch. Connect FB to REG for an LDO with a fixed 8.5 V output. Connect to the center tap of an external resistive divider connected between OUT and GND to adjust the output voltage of the LDO. |
| 16 | - | OUT | Switch or LDO Output (MAX16946 Only). OUT is either a switch or LDO output depending on the connection of FB. |
| - | 16 | OUT | Switch Output |
| - | - | EP | Exposed Pad (MAX16946 Only). Connect EP to the ground plane for optimal heat dissipation. Do not use EP as the only electrical ground connection. |

## Detailed Description

The MAX16946/MAX16947 high-voltage, high-side, cur-rent-sense LDO/switches feature internal current limiting to prevent system damage due to fault conditions. The MAX16946 provides a regulated 8.5 V output voltage fixed or adjustable from 3.3 V to 15 V . The MAX16946 can also be configured as a switch, while the MAX16947 is only available as a switch. The input voltage range for both devices extends from 4.5 V to 18 V (45V tolerant), making the devices ideal for providing phantom power to remote radio-frequency low-noise amplifiers (LNAs) in automotive applications.
The devices monitor the load current and provide an analog output voltage proportional to the sensed load current. Accurate internal current-limit protects the input supply against both overload and short-circuit conditions. Two open-drain fault indicator outputs indicate to the microprocessor when a short circuit, an open-load condition, or a short-to-battery condition exists. An overtemperature shutdown is also indicated by means of the current-sense amplifier's output voltage.
A fault-blanking feature allows the devices to ignore momentary faults such as those caused by the charging of capacitive loads during hot-swapping, preventing false alarms to the system. The devices feature short-to-battery protection to latch off the internal LDO/ pass switch during a short-to-battery event and thermal
overload. They include an active-low, high-voltagecompatible shutdown input to place them in low-power shutdown mode.

Current-Sense Amplifier The integrated current-sense amplifier employs a differential amplifier that amplifies the voltage between IN and SENS. A sense resistor, RSENSE, is connected across IN and SENS. Typical sense resistor values range between $0.25 \Omega$ and $2 \Omega$. When the load current passes through the sense resistor, a voltage drop develops across it. The current-sense amplifier amplifies this voltage.
The current-sense amplifier features an internally fixed gain of $A v=26 \mathrm{~V} / \mathrm{V}$ (typ). The following equations show the relationship between the current-sense amplifier output voltage (VAOUT) and load current:

$$
\begin{gathered}
\left(V_{\text {IN }}-V_{\text {SENS }}\right)(V)=I_{\text {LOAD }}(A) \times R_{\text {SENSE }}(\Omega) \\
V_{\text {AOUT }}(V)=A_{V}(V / V) \times\left(V_{\text {IN }}-V_{\text {SENS }}\right)(V)+0.4 V
\end{gathered}
$$

If LIM is connected to REF, the maximum output voltage of AOUT is VAOUT_FS $=3 \mathrm{~V}$. If LIM is externally driven to 3.65 V , the maximum output voltage of AOUT extends to $V_{\text {AOUT_FS }}=3.65 \mathrm{~V}$. The maximum AOUT voltage is always equal to VLIM, the voltage at LIM.
AOUT is the output of an internal buffer with 1 mA current drive capability. Bypass AOUT to ground with a $15 n F$ ceramic capacitor.

## MAX16946/MAX16947

## Remote Antenna, Current-Sense and LDO/Switches

## Load Protection

The devices monitor the load current through an external sense resistor and perform the following actions:

- If the monitored current is lower than the set openload current, the devices signal that there is an openload (see the Open Load section).
- If the monitored current is greater than the set shortcircuit current (ISC), the devices enter the shortcircuit mode (see the Short Circuit and Current Limit section).
The devices also perform a short-to-battery detection before the internal switch turns on. During normal operation, reverse-current detection protects the devices from short-to-battery events (see the Short-to-Battery and Reverse-Current Detection section).
In addition, thermal shutdown protects the devices from overheating (see the Thermal Shutdown section).
Two open-drain fault indicator outputs ( $\overline{\mathrm{OL}}$ and $\overline{\mathrm{SC}}$ ) and the AOUT voltage indicate the devices' status (Table 1).

Open Load
If the load current drops below the open-load current threshold, the $\overline{\mathrm{OL}}$ output latches low. An openload condition does not turn off the internal switch. To unlatch the $\overline{\mathrm{OL}}$ output, pulse $\overline{\mathrm{SHDN}}$ low for less than t $\overline{\text { SHDN_OFF }}(150 \mu \mathrm{~s}$ min $)$. Keeping $\overline{\text { SHDN }}$ low for longer than tsHDN_OFF shuts down the device.
The open-load current threshold is adjustable. Connect a resistive divider between REF, the open-load current threshold adjustment input (OLT), and GND to set the open-load current threshold (see the Open-Load Current Threshold Selection section).

## Short Circuit and Current Limit

If the load current exceeds the set short-circuit current threshold (ISC), the tBLANK timer begins counting. During this period, the load current is limited to the current limit set by the voltage at LIM. If the overcurrent condition persists beyond tBLANK, $\overline{\mathrm{SC}}$ asserts low and the internal switch turns off. The timer resets if the overcurrent condition disappears before the blanking time (tBLANK) has elapsed.
If the switch is turned off at the end of tBLANK, a retry timer (tRETRY) starts immediately after the blanking time has elapsed, and during that time the switch stays off. At the end of tretry, the switch turns on again while $\overline{\mathrm{SC}}$ stays low. If the fault still exists, the cycle repeats. If the fault has been removed, the switch stays on and $\overline{\mathrm{SC}}$ goes high after the blanking time tBLANK. During retry when the switch is off, the current through the switch is zero. Blanking time and retry time have fixed values of 100 ms (min) and 1100ms (min), respectively.
Figures 1-4 show the response of the devices to the presence and removal of overcurrent conditions.
The current-limit threshold is adjustable. Connect a resistive divider between REF, the current-limit setting input (LIM), and GND to set the current-limit threshold. Alternatively, externally drive LIM (not to exceed 3.65V) to set the current-limit threshold (see the Current-Limit Threshold Selection section).
The short-circuit current threshold depends on the value of the sense resistor and is calculated as follows:

$$
I_{S C}=\frac{1.3 \mathrm{~V}}{R_{\text {SENSE }} \times \mathrm{A}_{V}}
$$

where $A v$ is the gain of the internal current-sense amplifier and is equal to $26 \mathrm{~V} / \mathrm{V}$ and RSENSE is the sense resistor value.

## MAX16946/MAX16947 Remote Antenna, Current-Sense and LDO/Switches



Figure 1. Turn-On into Temporary Short Circuit


Figure 2. Turn-On into Hard Short Circuit

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Figure 3. Turn-On into Temporary Heavy Load


Figure 4. Turn-On into Heavy Load

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## Short-to-Battery and Reverse-Current Detection

 It is possible for OUT to be shorted to the battery due to a fault in the system. The devices detect this failure by comparing the OUT voltage and the IN voltage before the switch turns on. Every time the switch turns on, such as at the end of the retry time, or once the thermal shutdown condition disappears, the short-to-battery detection is performed. At this point, if the device detects the short-to-battery fault, the switch stays off and both $\overline{\mathrm{SC}}$ and $\overline{O L}$ assert low (Table 1).Series inductance and the output capacitor can produce ringing during a short-circuit condition, resulting in an output voltage that temporarily exceeds the input voltage. Blanking is implemented during and immediately after a short-circuit event to prevent false triggering of the reverse-current detection. The reverse-current blanking time (tREV_BLANK) is 16 ms (typ). If the reverse current produces a VSENSE (VIN - VSENSE) less than -7.7 mV (typ) for a duration greater than the blanking time, the device latches off the switch and both $\overline{\mathrm{SC}}$ and $\overline{\mathrm{OL}}$ assert low.

Thermal Shutdown
Thermal-shutdown circuitry protects the devices from overheating. The switch turns off immediately when the junction temperature exceeds $+170^{\circ} \mathrm{C}$ (typ) (Table 1). The switch turns on again after the device temperature drops by approximately $+15^{\circ} \mathrm{C}$ (typ). Thermal shutdown is indicated by OV on AOUT.

## Undervoltage and Overvoltage Lockout

 The devices include undervoltage lockout circuitry (UVLO) to prevent erroneous switch operation when theinput voltage goes below 3.5 V (typ) during startup and brownout conditions. Input voltages of less than 3.5 V inhibit operation of the device by turning off the internal charge pump and the switch.
These devices also feature an overvoltage lockout (OVLO) threshold of 21 V (typ). When VIN is greater than VOVLO, the device immediately turns off the switch and the internal charge pump.

## Shutdown ( $\overline{\text { SHDN }}$ )

The devices feature an active-low shutdown input ( $\overline{\mathrm{SHDN}}$ ) to place them into a low-power shutdown mode. The devices turn off and consume a $7 \mu \mathrm{~A}$ maximum (at $\mathrm{V} I \mathrm{~N}=12 \mathrm{~V}$ ) of shutdown current when $\overline{\text { SHDN }}$ is driven low for greater than $360 \mu$ s. Driving $\overline{\text { SHDN }}$ high initiates a device turn-on with short-to-battery detection. Pulsing $\overline{\text { SHDN }}$ low for less than t $\overline{\text { SHDN_OFF }}$ clears the $\overline{O L}$ output.

Internal Reference (REF) The devices feature a $3 V$ bandgap reference output, stable over supply voltage and temperature. The reference has a current drive capability of $100 \mu \mathrm{~A}$. Use resistive dividers connected to REF to set the open-load current threshold and the current-limit threshold. Do not use REF to drive external circuitry.

## Internal +5V Linear Regulator (REG)

The devices feature an internal regulator that regulates the input voltage to +5 V to power all internal circuitry. Bypass the regulator output (REG) to GND with a $1 \mu \mathrm{~F}$ ceramic capacitor. Do not use this regulator to power external circuitry.

## Table 1. MAX16946/MAX16947 Status Truth Table

| $\overline{\mathrm{SC}}$ | $\overline{\mathrm{OL}}$ | $\mathrm{V}_{\text {AOUT }}(\mathrm{V})$ | DEVICE STATUS | ACTION TAKEN |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | (ILOAD $\times$ RSENSE) $\times 26+0.4$ | Normal operation | None |
| 0 | 1 | (ILOAD $\times$ RSENSE) $\times 26+0.4$ | Short circuit | Autoretry |
| 1 | 0 | (ILOAD $\times$ RSENSE) $\times 26+0.4$ | Open load | $\overline{\text { OL latched low }}$ |
|  |  |  | Reverse current (on-state) | Switch/LDO latched off |
| 0 | 0 | 0.4 after switching off | OUT short-to-battery (off-state), Vout too high ( LDO mode) | Switch/LDO turned off as long as condition persists |
| 1 | 1 | 0 | Thermal shutdown, VIN overvoltage, VIN undervoltage | Switch/LDO and AOUT turns off as long as condition persists |
| 1 | 1 | 0 | REF undervoltage | Switch/LDO, AOUT, and REF turned off as long as condition persists |

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## Applications Information

## Choosing the Sense Resistor

Ideally, the maximum load current develops the full-scale sense voltage across the current-sense resistor. The current-sense amplifier output voltage is given by:

$$
V_{\text {AOUT }}=A V \times\left(V_{I N}-V_{\text {SENS }}\right)+0.4 V
$$

where VAOUT is the output voltage of the current-sense amplifier, and $A V$ is the gain of the current-sense amplifier of 26V/V (typ).
Calculate the maximum value for RSENSE, so that the amplified differential voltage across IN and SENS does not exceed the short-circuit AOUT voltage threshold of $\mathrm{VSC}=1.7 \mathrm{~V}$ (typ), which is defined in the Electrical Characteristics table:

$$
R_{\text {SENSE }}=\frac{V_{S C}-0.4 V}{l_{\text {LOAD }}\left(F U L L \_S C A L E\right) \times A_{V}}
$$

Typical sense resistor values range between $0.25 \Omega$ and $2 \Omega$.
During normal operation, when the load current is less than the short-circuit current threshold, the maximum AOUT voltage is equal to VSC. When a short circuit to ground is present and the device goes into autoretry, the maximum AOUT voltage extends to VLIM, the voltage at LIM.

Keep inductance low if ISENSE has a large highfrequency component. Wire-wound resistors have the highest inductance, while metal film is somewhat better. Low-inductance, metal-film resistors are also available. Instead of being spiral wrapped around a core, as in


Figure 5. Open-Load Current Threshold Selection
metal-film or wire-wound resistors, they are a straight band of metal and are available in values under $1 \Omega$.
Because of the high current that flows through RSENSE, eliminate parasitic trace resistance from causing errors in the sense voltage.

Open-Load Current Threshold Selection
A resistive divider between REF, OLT, and GND sets the open-load current threshold. See Figure 5.
Use the following formula to set the desired open-load current threshold:

$$
\mathrm{R}_{2}=\frac{\mathrm{R}_{1}}{\left(\frac{\mathrm{~V}_{\mathrm{REF}}}{\mathrm{R}_{\mathrm{SENSE}} \times \mathrm{I}_{\mathrm{OL}} \times \mathrm{A}_{\mathrm{V}}+0.4 \mathrm{~V}}-1\right)}
$$

where IOL is the desired open-load current threshold, AV is the current-sense amplifier gain (26V/V typical), and VREF is the reference voltage (3V typ). Size $\mathrm{R}_{1}$ and $\mathrm{R}_{2}$ large enough so that the equivalent resistance of the resistive dividers used to set the open-load and currentlimit thresholds does not exceed the REF output $100 \mu \mathrm{~A}$ drive capability.
For example, to set the open-load current threshold at 10 mA , using a $0.5 \Omega$ sense resistor, use the following method to calculate the value of $\mathrm{R}_{1}$ and $\mathrm{R}_{2}$ :

$$
R_{2}=\frac{R_{1}}{\left(\frac{3 \mathrm{~V}}{0.5 \Omega \times 0.01 \mathrm{~A} \times 26 \mathrm{~V} / \mathrm{V}+0.4 \mathrm{~V}}-1\right)}
$$

Choose $\mathrm{R}_{1}=470 \mathrm{k} \Omega$ and calculate $\mathrm{R}_{2}$ as $100 \mathrm{k} \Omega$.


Figure 6. Current-Limit Threshold Selection

# Remote Antenna, Current-Sense and LDO/Switches 

## Current-Limit Threshold Selection

A resistive divider between REF, LIM, and GND sets the current-limit threshold. See Figure 6.
Use the following formula to set the desired current-limit threshold:

$$
R_{2}=\frac{R_{1}}{\left(\frac{V_{R E F}}{R_{\text {SENSE }} \times I_{C L} \times A_{V}+0.4 \mathrm{~V}}-1\right)}
$$

where ICL is the desired current-limit threshold, $A v$ is the current-sense amplifier gain ( $26 \mathrm{~V} / \mathrm{V}$ typ), and VREF is the reference voltage ( 3 V typ). Size $\mathrm{R}_{1}$ and $\mathrm{R}_{2}$ large enough so that the equivalent resistance of the resistive dividers used to set the open-load and current-limit thresholds does not exceed the REF output $100 \mu \mathrm{~A}$ drive capability.
For example, to set the current-limit threshold at 120 mA , using a $0.5 \Omega$ sense resistor, use the following method to calculate the value of $R_{1}$ and $R_{2}$ :

$$
\mathrm{R}_{2}=\frac{\mathrm{R}_{1}}{\left(\frac{3 \mathrm{~V}}{0.5 \Omega \times 0.120 \mathrm{~A} \times 26 \mathrm{~V} / \mathrm{V}+0.4 \mathrm{~V}}-1\right)}
$$

Choose $R_{1}=83 \mathrm{k} \Omega$ and calculate $\mathrm{R}_{2}$ as $156 \mathrm{k} \Omega$.

## Using an External Reference

Use an external reference with resistive dividers as an alternative means of setting the current-limit and openload current thresholds. The equations shown in the Open-Load Current Threshold Selection and CurrentLimit Threshold Selection sections are still applicable when using an external reference. In those equations, set $V_{\text {REF }}$ equal to the voltage of the external reference.
When using the devices' $3 V$ reference, the maximum voltage at LIM is VLIM $=3 \mathrm{~V}$ and is obtained by connecting LIM to REF. When using an external reference, set the voltage at LIM to no greater than $\operatorname{VLIM}(\mathrm{MAX})=3.65 \mathrm{~V}$.

Fixed/Adjustable Output Voltage The MAX16946 is configurable to provide a fixed 8.5 V output or as an adjustable LDO with an output between 3.3 V and 15 V . Connect a resistive divider between OUT, FB, and GND to set the output to the desired voltage, as shown in Figure 7. Connect FB to REG to configure the MAX16946 as an 8.5V LDO, as shown in Figure 8. FB is regulated to 1.0 V with $\pm 3 \%$ accuracy for a load current between 5 mA and 150 mA . The accuracy falls to $\pm 5 \%$ for a load current between 2 mA and 200 mA . Select a value for $\mathrm{R}_{1}$ and calculate $\mathrm{R}_{2}$ as follows:

$$
R_{2}=\frac{R_{1}}{\left(\frac{V_{\text {OUT }}}{V_{F B}}-1\right)}
$$

Select $\mathrm{R}_{1}$ so that the maximum input bias current at FB is negligible compared to the total current going through $R_{1}$.

## Compensation Capacitor

 Compensate the LDO regulator by bypassing COMP to GND with a $0.1 \mu \mathrm{~F}$ ceramic capacitor.Input Capacitor
Connect a low-leakage ceramic capacitor from IN to GND to limit the input-voltage drop during momentary output short-circuit conditions and to protect the device against transients due to inductance in the IN line. For example, use at least a $0.1 \mu \mathrm{~F}$ ceramic capacitor if the input inductance (including any stray inductance) is estimated to be $20 \mu \mathrm{H}$. Larger capacitor values reduce the voltage undershoot and voltage overshoot in case of reverse current at the input.

## Output Capacitor

In an analogous fashion to the input capacitor, an output capacitor protects the device against transients due to any series inductance in the output. Under no conditions should the voltage on OUT go below -0.3 V as specified in the Absolute Maximum Ratings section. A Schottky diode is required to clamp transients that go below ground. For example, with a 2.2 mH series inductance, to avoid excessive ringing at the output, bypass OUT to GND with not more than $0.1 \mu \mathrm{~F}$ capacitance. Additionally, bypassing OUT to GND with a $2.2 \mu \mathrm{~F}$ ceramic capacitor in series with a $10 \Omega$ resistor reduces ringing caused by load current transients through a maximum 2.2 mH series inductance.


Figure 7. Adjustable Output-Voltage Selection

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## Remote Antenna, Current-Sense and LDO/Switches

## Layout and Thermal Dissipation

To optimize the switch response time to output shortcircuit condition, it is very important to keep all traces as short as possible to reduce the effect of undesirable parasitic inductance. Place input and output capacitors as close as possible to the device (no more than 5 mm ). IN and OUT must be connected with wide short traces to the power bus. During normal operation in switch mode, the power dissipation is small and the package temperature change is minimal. In LDO mode, the power dissipation is given by:

If the output is continuously shorted to ground at the maximum supply voltage, the devices are protected because the total power dissipated during the short is scaled down by the duty cycle imposed by the protection:

$$
P_{(\text {MAX })}=\frac{V_{\text {VIN }(\text { MAX }} \times I_{\text {OUT }(M A X)} \times t_{\text {BLANK }}}{t_{\text {RETRY }}+t_{\text {BLANK }}}
$$

$$
(\text { VIN }- \text { VOUT) } \times \text { ILOAD }+ \text { VIN x IIN }
$$



Figure 8. LDO with Adjustable Output Voltage (3.3V to 15V)

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Figure 9. LDO with Fixed 8.5V Output


Figure 10. Input Switched to Output

## MAX16946/MAX16947 <br> Remote Antenna, Current-Sense and LDO/Switches

## Chip Information

PROCESS: BiCMOS

## Package Information

For the latest package outline information and land patterns, go to www.maximintegrated.com/packages. Note that a "+", "\#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.

| PACKAGE <br> TYPE | PACKAGE <br> CODE | OUTLINE <br> NO. | LAND <br> PATTERN <br> NO. |
| :---: | :---: | :---: | :---: |
| 16 QSOP | $\mathrm{E} 16+5$ | $\underline{21-0055}$ | $90-0167$ |
| 16 QSOP-EP | $\mathrm{E} 16 \mathrm{E}+10$ | $\underline{21-0112}$ | $90-0239$ |
| 16 TQFN-EP | $\mathrm{T} 1644+4$ | $\underline{21-0139}$ | $90-0070$ |

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