# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

## **General Description**

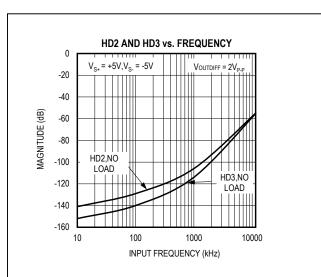
The MAX44206 is a low-noise, low-distortion fully differential operational amplifier suitable for driving high-speed, high-resolution, 20-/18-/16-bit SAR ADCs, including the MAX11905 ADC family. Featuring a combination of wide 2.7V to 13.2V supply voltage range and wide 400MHz bandwidth, the MAX44206 is suitable for low-power, highperformance data acquisition systems.

The MAX44206 offers a VOCM input to adjust the output common-mode voltage, eliminating the need for a coupling transformer or AC-coupling capacitors. This adjustable output common-mode voltage allows the MAX44206 to match the input common-mode voltage range of the ADC following it. Shutdown mode consumes only  $6.8\mu$ A and extends battery life in battery-powered applications or reduces average power in systems cycling between shutdown and periodic data readings.

The MAX44206 is available in an 8-pin  $\mu$ MAX<sup>®</sup> package and is specified for operation over the -40°C to +125°C temperature range.

## **Applications**

- Single-Ended to Differential Conversion
- High-Speed Process Control
- Medical Imaging
- Fully-Differential Signal Conditioning
- Active Filters



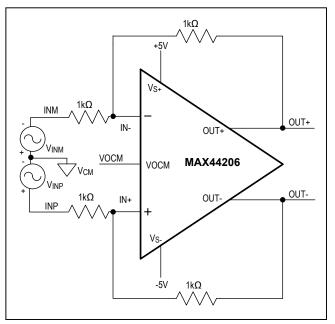
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## **Features and Benefits**

- Low Input Noise Drives Precision SAR ADCs
  - 3.1nV/√Hz at 1kHz
  - + 200nVP-P from 0.1Hz to 10Hz
- High Speed for DC and AC Applications
  - Gain-Bandwidth Product 400MHz
  - -3dB Gain-Bandwidth Product 180MHz
  - Slew Rate 180V/µs
- Ultra-Low Distortion Drives AC Inputs to 20-Bit SAR ADCs
  - + HD2 = -141dB, HD3 = -152dB at  $f_{IN}$  = 10kHz, V<sub>OUT,DIFF</sub> = 2V<sub>P-P</sub>
  - + HD2 = -106dB, HD3 = -115dB at  $f_{IN}$  = 1MHz, V<sub>OUT,DIFF</sub> = 2V<sub>P-P</sub>
- Wide Supply Range (2.7V to 13.2V) Drives Unipolar or Bipolar (±6.6V) Signals
- 3.7mA Quiescent Supply Current with Only 6.8µA Shutdown Current
- 8-Pin µMAX Package Saves Board Space

Ordering Information appears at end of data sheet.

## **Typical Application Circuit**





# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

## **Absolute Maximum Ratings**

V <sub>S</sub> + to V <sub>S</sub> 0.3V to +15V
All Other Pins $(V_{S}) - 0.3V$ to $(V_{S}) + 0.3V$
IN+ to IN0.3V to +0.3V
Continuous Input Current into Any Pin (Note 1)±20mA
Output Short-Circuit Duration (Note 1) 10s
Continuous Power Dissipation ( $T_A = +70^{\circ}C$ )
µMAX (derate 10.3mW/°C above +70°C)824.7mW

Operating Temperature Range	-40°C to +125°C
Junction Temperature	+150°C
Storage Temperature Range	-65°C to +150°C
Lead Temperature (soldering, 10s)	+300°C
Soldering Temperature (reflow)	+260°C

## Package Thermal Characteristics (Note 1)

#### μΜΑΧ

Note 1: Package thermal resistances were obtained using the method described in JEDEC specification JESD51-7, using a four-layer board. For detailed information on package thermal considerations, refer to www.maximintegrated.com/thermal-tutorial.

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## **Electrical Characteristics (±5V Supply)**

 $(V_{S+} = +5V, V_{S-} = -5V, V_{OCM} = 0V, \overline{SHDN} = V_{S+}, EP = 0V (Note 2), R_F = R_G = 1k\Omega, R_L = 1k\Omega (between OUT+ and OUT-), T_A = -40°C to +125°C, unless otherwise noted. Typical values are at T_A = +25°C.) (Note 3)$ 

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
POWER SUPPLY						
Supply Voltage Range	V <sub>S</sub>	$V_{S}$ + to $V_{S}$ -, guaranteed by PSRR (EP = $V_{S}$ -)	2.7		13.2	V
Quippont Current		No load, R <sub>L</sub> = ∞		3.7	6.8	mA
Quiescent Current	۱ <sub>S</sub>	SHDN = 0V		6.8	20	μA
Power-Supply Rejection Ratio	PSRR	$V_{S}$ + to $V_{S}$ - = 2.7V to 13.2V (EP = $V_{S}$ )	90	123		dB
DIFFERENTIAL PERFORMANCE-DC SPECIFICATIONS						
Input Common-Mode Range	V <sub>ICM</sub>	Guaranteed by CMRR	(V <sub>S</sub> -) + 1.	1	(V <sub>S</sub> +) - 1.1	V
Input Common-Mode Rejection Ratio	CMRR	$V_{ICM} = (V_{S}-) + 1.1V$ to $(V_{S}+) - 1.1V$	94	130		dB
Input Offset Voltage	V <sub>OS</sub>			±0.2	±1.5	mV
Input Offset Voltage Drift	TCV <sub>OS</sub>			0.2		μV/°C
Input Bias Current	Ι <sub>Β</sub>			30	750	nA
Input Offset Current	I <sub>OS</sub>			±15	±350	nA
Open-Loop Gain	A <sub>VOL</sub>	V <sub>OUT,DIFF</sub> = 6.6V <sub>P-P</sub> , T <sub>A</sub> = +25°C	96	130		dB
Output Short-Circuit Current	I <sub>SC</sub>			60		mA
Output Voltage Swing	V <sub>S</sub> + - V <sub>OUT</sub>	Applies to V <sub>OUT+</sub> , V <sub>OUT</sub>		0.98	1.15	V
Output Voltage Swing	V <sub>OUT</sub> - V <sub>S</sub> -	Applies to V <sub>OUT+</sub> , V <sub>OUT-</sub>		0.92	1.10	v

# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

## **Electrical Characteristics (continued)**

 $(V_{S+} = +5V, V_{S-} = -5V, V_{OCM} = 0V, \overline{SHDN} = V_{S+}, EP = 0V (Note 2), R_F = R_G = 1k\Omega, R_L = 1k\Omega (between OUT+ and OUT-), T_A = -40°C to +125°C, unless otherwise noted. Typical values are at T_A = +25°C.) (Note 3)$ 

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
DIFFERENTIAL PERFORMANC	E—AC SPEC	IFICATIONS				
Input Voltage-Noise Density	e <sub>N</sub>	f = 1kHz		3.1		nV/√Hz
Input Voltage Noise		0.1Hz < f < 10Hz	200			nV <sub>P-P</sub>
Input Current-Noise Density	i <sub>N</sub>	f = 1kHz		1.5		pA/√Hz
1/f Noise Due to Input Current		0.1Hz < f < 10Hz		220		pA <sub>P-P</sub>
-3dB Small-Signal Bandwidth		V <sub>OUT,DIFF</sub> = 0.1V <sub>P-P</sub>		180		MHz
0.1dB Gain Flatness Bandwidth		V <sub>OUT,DIFF</sub> = 0.1V <sub>P-P</sub>		25		MHz
-3dB Large-Signal Bandwidth		V <sub>OUT,DIFF</sub> = 2V <sub>P-P</sub>		38		MHz
0.1dB Gain Flatness Bandwidth		V <sub>OUT,DIFF</sub> = 2V <sub>P-P</sub>		19		MHz
Slew Rate (Differential)	SR	V <sub>OUT,DIFF</sub> = 2V <sub>P-P</sub>		180		V/µs
Capacitive Loading	CL	No sustained oscillations		5		pF
		V <sub>OUT,DIFF</sub> = 2V <sub>P-P</sub> , f = 10kHz		-129/-14	5	
UD2/UD2 Crestiantions		V <sub>OUT,DIFF</sub> = 2V <sub>P-P</sub> , f = 1MHz		-90/-98		dDa
HD2/HD3 Specifications		$V_{OUT,DIFF} = 6.6V_{P-P}$ , f = 10kHz	-124/-142		dBc	
		V <sub>OUT,DIFF</sub> = 6.6V <sub>P-P</sub> , f = 1MHz		-86/-90		1
o	1	Settling to 0.1%, $V_{OUT,DIFF} = 4V_{P-P}$	58		ns	
Settling Time	t <sub>S</sub>	Settling to 0.1%, V <sub>OUT,DIFF</sub> = 6.6V <sub>P-P</sub>	107			
Output Impedance	R <sub>OUT,DIFF</sub>	f <sub>C</sub> = 1MHz	0.1			Ω
Output Balance Error		V <sub>OUT,DIFF</sub> = 1V <sub>P-P</sub> , f = 1MHz	-54		dB	
SHDN INPUT						
Innut \ /oltogo	V <sub>IH</sub>		1.25			V
Input Voltage	VIL				0.65	
land to constant	IIН	V <sub>SHDN</sub> = 2V		0.2	1.5	
Input Current	١ <sub>IL</sub>	V <sub>SHDN</sub> = 0V	-1.5	-0.2		μA
Turn-On Time	t <sub>ON</sub>	Output condition		1.2		μs
Turn-Off Time	tOFF	Output condition		0.8		μs
VOCM INPUT to VOUT, CM PERF	ORMANCE					
Input Voltage Range		Guaranteed by gain parameter	(V <sub>S</sub> -) + 1	.2 (\	/ <sub>S</sub> +) - 1.2	V
Output Common-Mode Gain	G <sub>OCM</sub>	$\Delta$ (V <sub>OUT,CM</sub> )/ $\Delta$ (V <sub>OCM</sub> ), V <sub>OCM</sub> = (V <sub>S</sub> -) + 1.2 to (V <sub>S</sub> +) - 1.2	0.99	1	1.01	V/V
Input Offset Voltage				±13	±38	mV
Input Bias Current			-2	-0.30		μA
Output Common-Mode Rejection Ratio (Note 4)	OCMRR	$2 \times \Delta(V_{OS})/\Delta(V_{OCM}), V_{OCM} = (V_{S}) + 1.2$ to $(V_{S}) - 1.2$	100	130		dB
-3dB Small-Signal Bandwidth		V <sub>OUT,CM</sub> = 100mV <sub>P-P</sub>		16		MHz
Slew Rate		V <sub>OUT,CM</sub> = 1V <sub>P-P</sub>	1	6		V/µs

# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

## **Electrical Characteristics (+5V Supply)**

 $(V_{S+} = +5V, V_{S^-} = 0V, VOCM = 2.5V, \overline{SHDN} = V_{S+}, EP = 0V (Note 2), R_F = R_G = 1k\Omega, R_L = 1k\Omega$  (between OUT+ and OUT-),  $T_A = -40^{\circ}C$  to +125°C, unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ .) (Note 3)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
POWER SUPPLY		•				
Supply Voltage Range	V <sub>S</sub>	$V_{S}$ + to $V_{S}$ -, guaranteed by PSRR (EP = $V_{S}$ -)	2.7		13.2	V
Outer eart Ourse of		No load, R <sub>L</sub> = ∞		3.7	6.8	mA
Quiescent Current	I <sub>S</sub>	V <sub>SHDN</sub> = 0V		5.9	20	μA
DIFFERENTIAL PERFORMANC	E-DC SPEC	IFICATIONS				
Input Common-Mode Range	V <sub>ICM</sub>	Guaranteed by CMRR	(V <sub>S</sub> -) + ′	1.1 (	V <sub>S</sub> +) - 1.1	V
Input Common-Mode Rejection Ratio	CMRR	$V_{ICM}$ = (V <sub>S</sub> -) + 1.1V to (V <sub>S</sub> +) - 1.1V	94	130		dB
Input Offset Voltage	V <sub>OS</sub>			±0.2	±1.5	mV
Input Offset Voltage Drift	TC V <sub>OS</sub>			0.2		µV/°C
Input Bias Current	Ι <sub>Β</sub>			30	750	nA
Input Offset Current	I <sub>OS</sub>			±15	±350	nA
Open-Loop Gain	A <sub>VOL</sub>	V <sub>OUT,DIFF</sub> = 2.8V <sub>P-P</sub> , T <sub>A</sub> = +25°C	95	120		dB
Output Short-Circuit Current	I <sub>SC</sub>			60		mA
Output Voltage Swing	V <sub>S</sub> + - V <sub>OUT</sub>	Applies to V <sub>OUT+</sub> , V <sub>OUT</sub>		0.95	1.1	- V
	V <sub>OUT</sub> - V <sub>S</sub> -	Applies to V <sub>OUT+</sub> , V <sub>OUT</sub>		0.85	1.1	
DIFFERENTIAL PERFORMANC	E-AC SPEC	IFICATIONS				
Input Voltage-Noise Density	e <sub>N</sub>	f = 1kHz		3.1		nV/√Hz
Input Voltage Noise		0.1Hz < f < 10Hz		200		$nV_{P-P}$
Input Current-Noise Density	i <sub>N</sub>	f = 1kHz		1.5		pA/√Hz
1/f Noise Due to Input Current		0.1Hz < f < 10Hz		220		pA <sub>P-P</sub>
-3dB Small-Signal Bandwidth		$V_{OUT,DIFF} = 0.1 V_{P-P}$		180		MHz
0.1dB Gain Flatness Bandwidth		$V_{OUT,DIFF} = 0.1 V_{P-P}$		25		MHz
-3dB Large-Signal Bandwidth		V <sub>OUT,DIFF</sub> = 2V <sub>P-P</sub>		38		MHz
0.1dB Gain Flatness Bandwidth		V <sub>OUT,DIFF</sub> = 2V <sub>P-P</sub>		19		MHz
Slew Rate (Differential)	SR	V <sub>OUT,DIFF</sub> = 2V <sub>P-P</sub>		120		V/µs
Capacitive Loading	CL	No sustained oscillations		5		pF
UD2/UD2 Specifications		V <sub>OUT</sub> = 4V <sub>P-P</sub> , f = 10kHz		-123/-14	3	dPo
HD2/HD3 Specifications		V <sub>OUT</sub> = 4V <sub>P-P</sub> , f = 1MHz		-88.5/-95	5.5	dBc
Sottling Time	Settling to 0.1%, $V_{OUT,DIFF} = 4V_{P-P}$			58		200
Settling Time	t <sub>S</sub>	Settling to 0.1%, V <sub>OUT,DIFF</sub> = 6.6V <sub>P-P</sub>		100		ns
Output Impedance	R <sub>OUT,DIFF</sub>	f <sub>C</sub> = 1MHz (V <sub>OUT,DIFF</sub> )		0.1		Ω
Output Balance Error		V <sub>OUT.DIFF</sub> = 1V <sub>P-P</sub> , f = 1MHz		-52		dB

# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

## **Electrical Characteristics (continued)**

 $(V_{S+} = +5V, V_{S-} = 0V, VOCM = 2.5V, \overline{SHDN} = V_{S+}, EP = 0V (Note 2), R_F = R_G = 1k\Omega, R_L = 1k\Omega$  (between OUT+ and OUT-),  $T_A = -40^{\circ}C$  to +125°C, unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ .) (Note 3)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
SHDN INPUT						
Input Voltage	VIH		1.25			V
	V <sub>IL</sub>				0.65	v
Input Current	IIН	V <sub>SHDN</sub> = 2V		0.2	1.5	
input Current	IIL	V <sub>SHDN</sub> = 0V	-1.5	-0.2		μA
Turn-On Time	t <sub>ON</sub>	Output condition		1.2		μs
Turn-Off Time	tOFF	Output condition		0.8		μs
VOCM INPUT to VOUT, CM PER	FORMANCE					
Input Voltage Range		Guaranteed by gain parameter	(V <sub>S</sub> -) +1.2		(V <sub>S</sub> +)-1.2	V
Output Common-Mode Gain	G <sub>OCM</sub>	$ \Delta(V_{OUT,CM})/\Delta(V_{OCM}), V_{OCM} = (V_S-) + 1.2 $ to (V <sub>S</sub> +) - 1.2	0.99	1	1.01	V/V
Input Offset Voltage				±13	±38	mV
Input Bias Current			-2	-0.3		μA
Output Common-Mode Rejection Ratio (Note 4)	OCMRR	$2 \times \Delta(V_{OS})/\Delta(V_{OCM}),$ V <sub>OCM</sub> = (V <sub>S</sub> -) + 1.2 to (V <sub>S</sub> +) - 1.2	90	130		dB
-3dB Small-Signal Bandwidth		V <sub>OUT,CM</sub> = 100mV <sub>P-P</sub>		16		MHz
Slew Rate		V <sub>OUT,CM</sub> = 1V <sub>P-P</sub>		6		V/µs

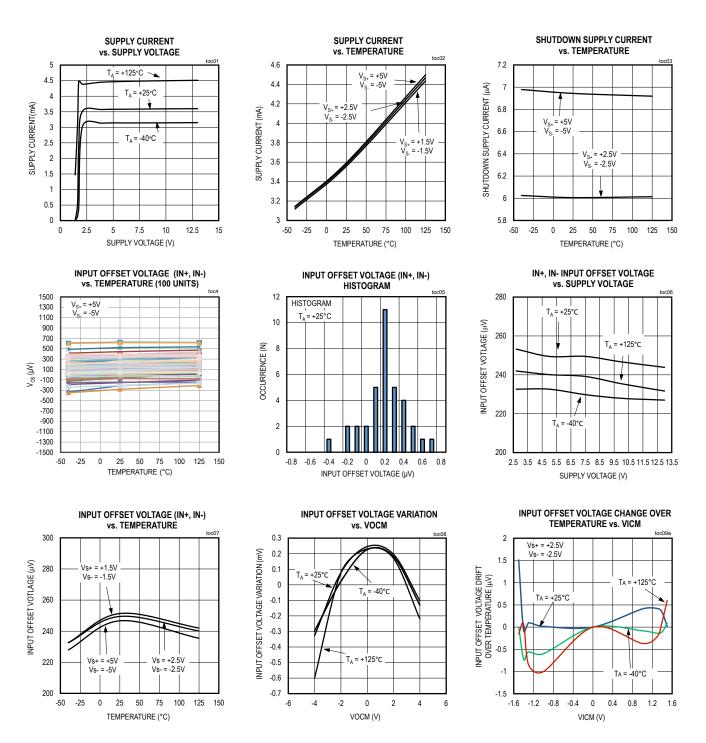
**Note 2:** EP is the logic ground reference to the  $\overline{\text{SHDN}}$  pin.

Note 3: All devices are 100% production tested at  $T_A = +25^{\circ}C$ . Temperature limits are guaranteed by design.

**Note 4:** OCMRR is mainly determined by external gain resistors matching. The formula used for OCMRR calculation assumes that gain resistors are perfectly matched. Therefore, OCMRR =  $(1 + R_F/R_G) \times \Delta V_{OS}/\Delta V(VOCM)$ .

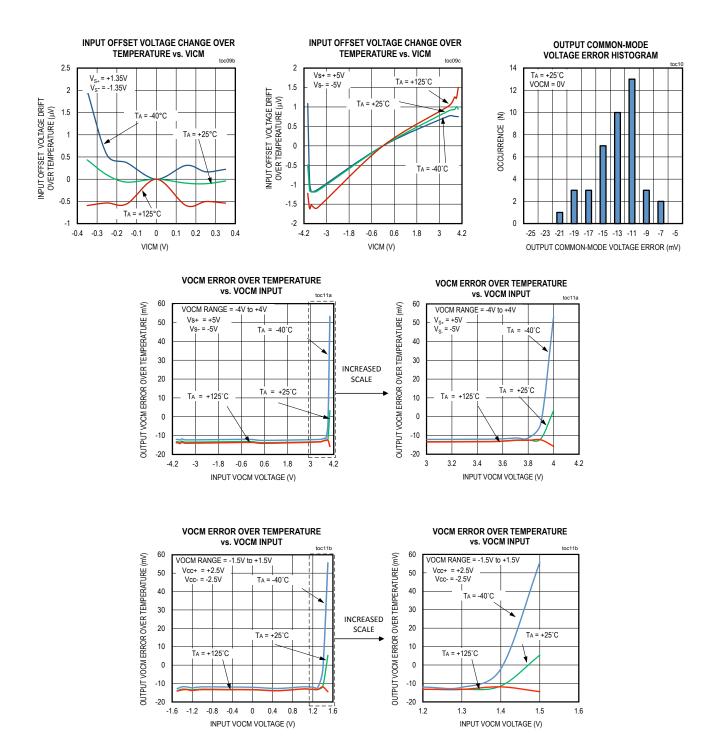
# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

## **Typical Operating Characteristics**



# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

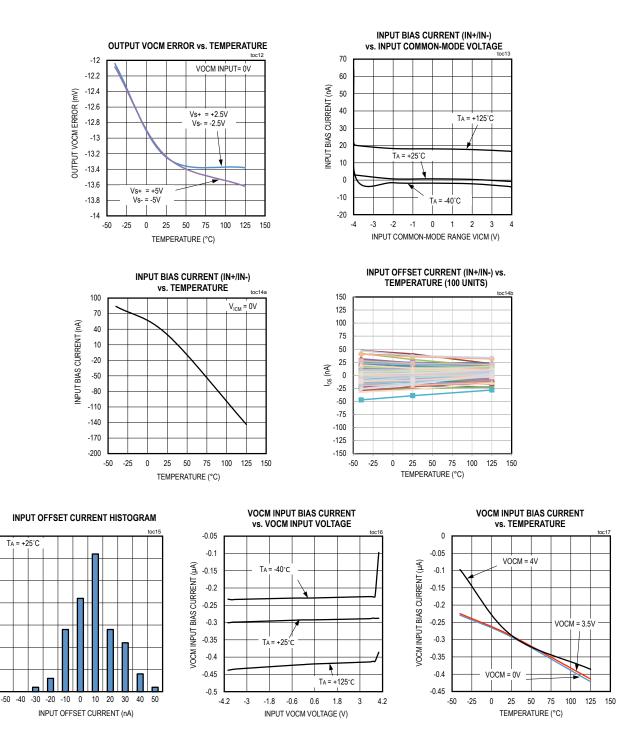
### **Typical Operating Characteristics (continued)**



# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

## **Typical Operating Characteristics (continued)**

 $(V_{S+} = +5V, V_{S-} = -5V, V_{OCM} = 0V, \overline{SHDN} = V_{S+}, EP = 0V, R_F = R_G = 1k\Omega, R_L = 1k\Omega$  (between OUT+ and OUT-),  $T_A = -40^{\circ}C$  to +125°C, unless otherwise noted.)



35

30

Ê 25

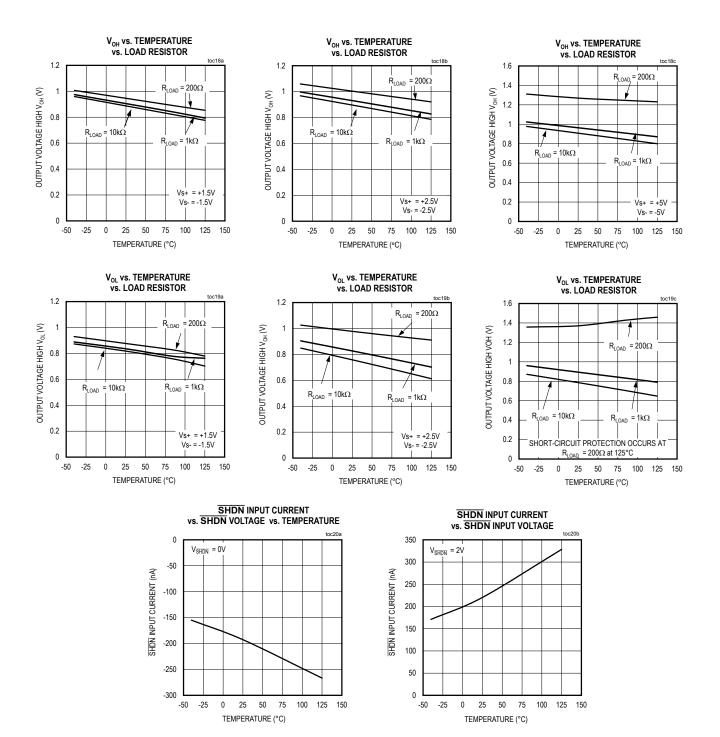
10

5

0

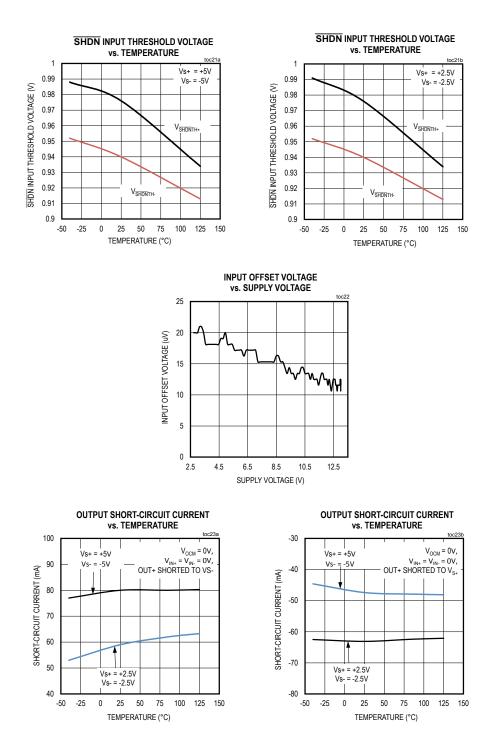
# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

## **Typical Operating Characteristics (continued)**



# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

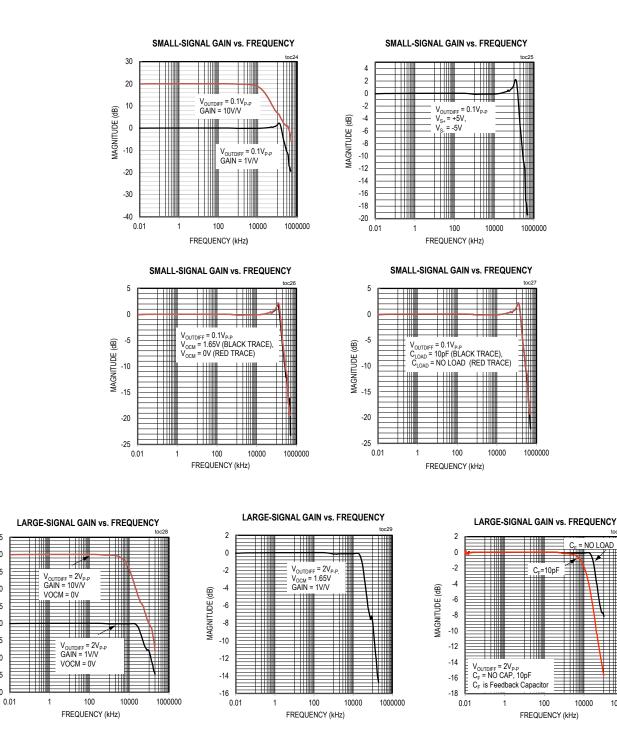
### **Typical Operating Characteristics (continued)**



# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

## **Typical Operating Characteristics (continued)**

 $(V_{S+} = +5V, V_{S-} = -5V, V_{OCM} = 0V, \overline{SHDN} = V_{S+}, EP = 0V, R_F = R_G = 1k\Omega, R_L = 1k\Omega$  (between OUT+ and OUT-),  $T_A = -40^{\circ}C$  to +125°C, unless otherwise noted.)



25

20

15

10

5

0

-5

-10

-15

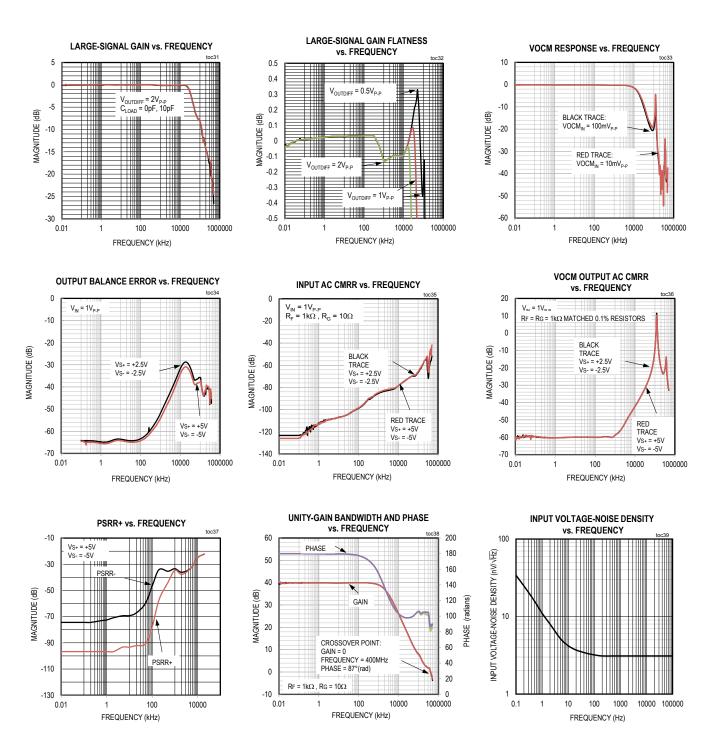
-20

MAGNITUDE (dB)

1000000

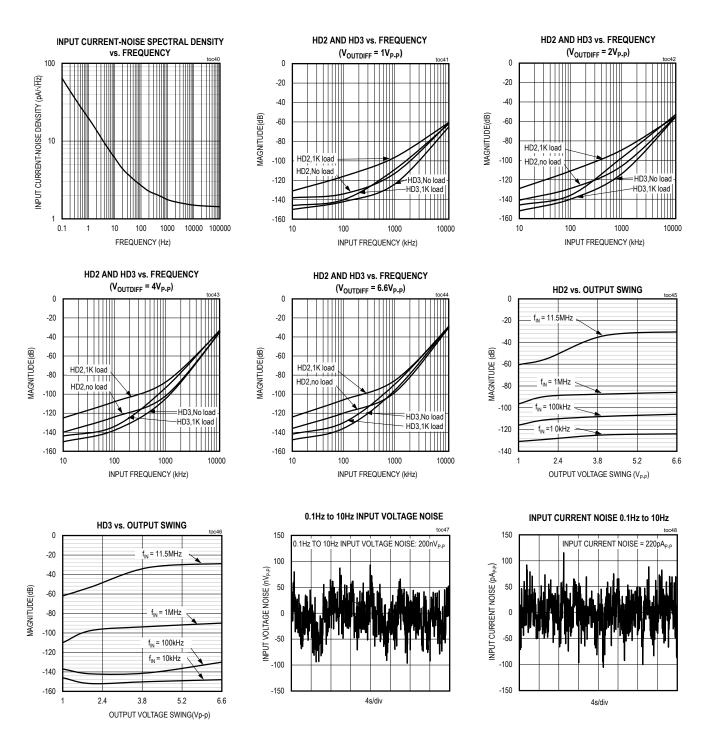
# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

## **Typical Operating Characteristics (continued)**



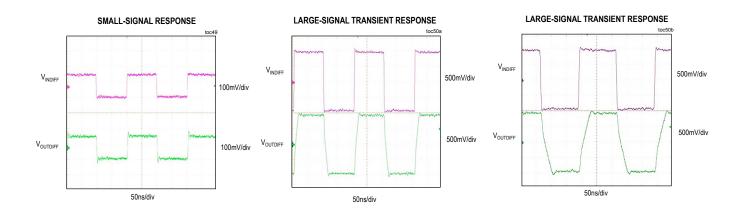
# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

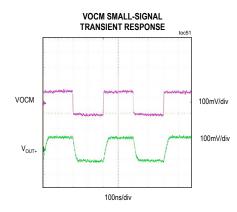
## **Typical Operating Characteristics (continued)**

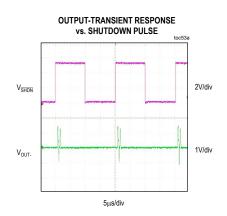


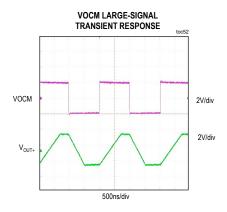
# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

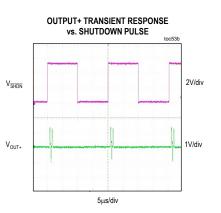
## **Typical Operating Characteristics (continued)**





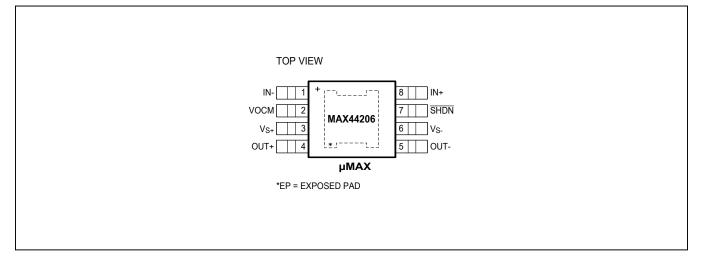






# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

## **Pin Configuration**

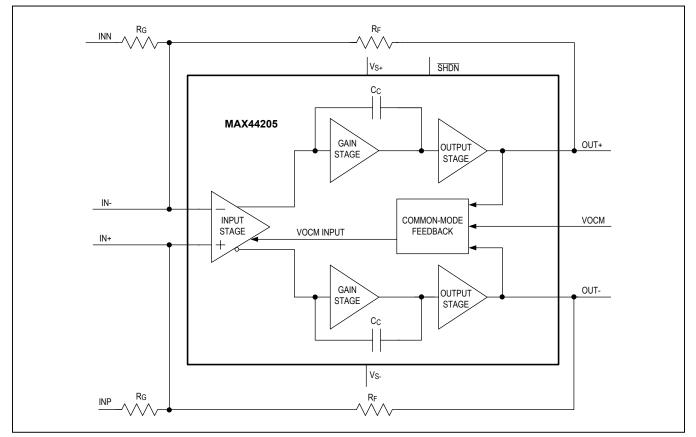


## **Pin Description**

PIN	NAME	FUNCTION
1	IN-	Inverting Input
2	VOCM	Output Common-Mode Voltage Input
3	V <sub>S+</sub>	Positive Supply Voltage Input
4	OUT+	Noninverting Differential Output
5	OUT-	Inverting Differential Output
6	V <sub>S-</sub>	Negative Supply Voltage Input
7	SHDN	Shutdown Mode Input (Active-Low). SHDN is referred to the exposed pad.
8	IN+	Noninverting Input
_	EP	Exposed Pad. EP is the logic ground reference to the SHDN pin.

# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

## **Functional Diagram**



### **Detailed Description**

The MAX44206 is a low-noise, low-power, very low-distortion fully differential (input and output) op amp capable of driving high-resolution 16-/18-/20-bit SAR ADCs with input signal frequencies from DC to 1MHz. These highresolution signal chain ICs are used in test and measurement applications, as well as medical instrumentation and industrial control systems.

This fully differential op amp accepts either single-ended or fully differential input signals at its inputs and converts the input signal into fully differential outputs that are exactly equal in amplitude and 180° apart in phase. Ideally, the noise and distortion performance of the amplifier should match or exceed the linearity of the ADC to preserve the overall system accuracy.

Four precisely matched resistors (two for feedback and two for gain setting) set the differential closed-loop gain as shown in the *Functional Diagram*.

The MAX44206 has an output voltage common-mode (VOCM) input to set the DC common-mode voltage level of the differential outputs without affecting the balance of the AC differential output signal on each output. The MAX44206 also features a low-power shutdown mode that consumes only  $6.8\mu$ A of supply current from the V<sub>S</sub>+ pin. Note that while the outputs are high impedance during shutdown, the feedback networks may provide paths for current to flow from the input source(s).

#### +5V Vs RG INM SHDN OUT+ IN-OUT VOCM MAX44206 VOCM OUT-RG OU. IN+ INF -5V

**Terminology and Definitions** 

Figure 1. Differential Input, Differential Output Configuration (Decoupling Capacitors Not Shown for Simplicity)

#### **Differential Voltage**

The differential voltage at the input is the voltage applied across INP to INM and the differential voltage at the output is the voltage across OUT+ to OUT-. Equations for input and output differential voltages are listed below:

 $V_{IN,dm} = (V_{INP} - V_{INM})$ 

$$V_{OUT,dm} = (V_{OUT+} - V_{OUT-})$$

 $V_{OUT+}$  and  $V_{OUT-}$  are voltages at the OUT+ and OUTterminals with respect to output common-mode voltage set by the VOCM input voltage.

#### **Common-Mode Voltage**

The common-mode voltage at the input is the average of the input pins (IN+ and IN-) and at the output, it is the average of two outputs. Equations for input and output common-mode voltages are listed below:

$$V_{IN,cm} = (V_{IN+} + V_{IN-})/2$$
  
 $V_{OUT,cm} = V_{OCM} = (V_{OUT+} + V_{OUT-})/2$ 

Though it was mentioned that the input common-mode voltage is the average of the voltage seen on both input pins, the range is slightly different depending on if the input signal is fully differential or single ended.

For fully differential input applications, where  $V_{INP} = -V_{INM}$ , the common-mode input voltage is:

$$\begin{split} \mathsf{V}_{\text{IN,cm}} &= (\mathsf{V}_{\text{IN+}} + \mathsf{V}_{\text{IN-}})/2 \cong \text{VOCM x } \mathsf{R}_{\text{G}}/(\mathsf{R}_{\text{F}} + \mathsf{R}_{\text{G}}) \\ &+ \mathsf{V}_{\text{CM}} \text{ x } \mathsf{R}_{\text{F}}/(\mathsf{R}_{\text{F}} + \mathsf{R}_{\text{G}}) \end{split}$$

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With single-ended input applications, there will be an input signal component to the input common-mode voltage, as there is no out-of-phase signal not applied on the other input. Applying V<sub>INP</sub> (connecting V<sub>INM</sub> to zero), the common-mode input voltage is:

 $V_{IN,cm} = (V_{IN+} + V_{IN-})/2 \cong VOCM \times R_G/(R_F + R_G) + V_{CM} \times R_F/(R_F + R_G) + V_{INP}/2 \times R_F/(R_F + R_G)$ 

#### Common-Mode Offset Voltage

The common-mode offset voltage is defined as the difference between the voltage applied to the VOCM terminal and the output common-mode voltage.

 $V_{OS,cm} = (V_{OUT,cm} - V_{OCM})$ 

#### Input Offset Voltage, CMRR, and VOCM CMRR

Input offset voltage is the differential voltage error (V<sub>OS,dm</sub>) between the input pins (IN+ and IN-). CMRR performance is affected by both the input offset voltage error at the input due to change in input common-mode voltage (V<sub>IN\_,cm</sub>) and the change in input offset voltage V<sub>OS,dm</sub>) due to VOCM change. So, there are two CMRR terms:

 $CMRR_{VIN,cm} = \Delta(V_{IN\_,cm})/\Delta(V_{OS,dm})$  $CMRR_{VOCM} = \Delta(V_{OCM})/\Delta(V_{OS,dm})$ 

The output common-mode rejection ratio is strongly affected by the matching of gain-setting feedback network.

#### **Output Balance Error**

An ideal differential output implies the two outputs of the amplifier should be exactly equal in amplitude but 180° apart in phase. Output balance is the measure of how well the outputs are balanced and is defined as the ratio of the output common-mode voltage to the output differential signal. It is generally expressed as dB in log scale.

Output Balance Error = 20 x log|(V<sub>OUT,cm</sub>)/(V<sub>OUT,dm</sub>)|

#### **Operation and Equations**

The *Functional Diagram* details the internal architecture of the differential op amp. The negative feedback loop across the outputs to respective inputs force voltages on IN+ and IN- pins equal to each other. That implies:

$$\frac{V_{INP}}{R_F} = \frac{-V_{OUT-}}{R_G}$$
$$\frac{V_{INN}}{R_F} = \frac{-V_{OUT+}}{R_G}$$

From above equations see the relationship between differential output voltage and inputs.

$$(V_{OUT+} - V_{OUT-}) = (V_{INP} - V_{INN}) \times \frac{R_F}{R_G}$$

# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

The VOCM input voltage with the help of the commonmode feedback circuit drives the output common-mode voltage level to VOCM. This results in the following output relations:

$$(V_{OUT+}) = (VOCM) + \frac{V_{OUT,DM}}{2}$$
$$(V_{OUT-}) = (VOCM) - \frac{V_{OUT,DM}}{2}$$

#### Input and ESD Protection

As shown in Figure 2, ESD diodes are present on all the pins with respect to the  $V_{S+}$  and  $V_{S-}$  pins so that these ESD diodes turn on and protect the part when voltages on these pins go out of range from either supplies by more than one diode drop. There are two series input resistors

and back-to-back diode protection between the inputs for protection against excessive differential voltages across the amplifier's inputs.

# SHDN and Exposed Pad Shutdown Operation

The MAX44206 offers a shutdown mode for low-power operation. Drive SHDN below 0.65V with respect to the  $\mu$ MAX exposed pad (EP) to shut down the part and only 6.8 $\mu$ A (typ) will be drawn from V<sub>S+</sub>. To keep the part active, SHDN needs to be at least 1.25V above EP.

#### **Exposed Pad**

EP is the logic ground reference to the SHDN pin. EP should be connected to the PCB ground plane for optimum thermal dissipation.

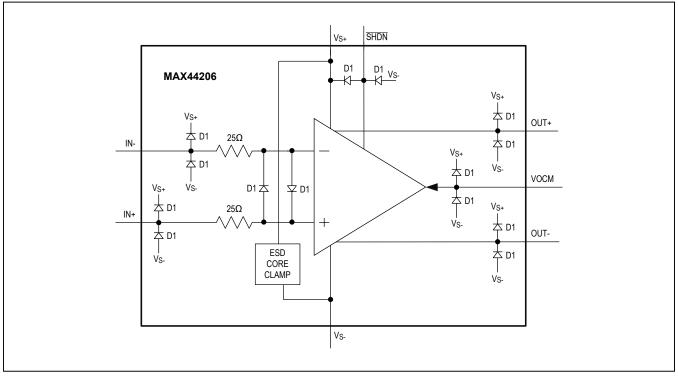


Figure 2. Showing ESD Protection Scheme in MAX44206

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# Shutdown Operation with External Components and Stimuli

In shutdown mode, quiescent supply current is low. However, there will be currents flowing into the IC pins depending on the external components and applied signals. Figure 3 shows the block diagram with these current paths and Figure 2 shows internal protection devices. In active operation mode (shutdown disabled), input signals are applied to INP and INN. The voltage applied to the VOCM pin sets the output common-mode voltage.

In shutdown mode, the voltages applied to INP, INN, and VOCM will interact with the IC internal components resulting in current flowing into the IC pins. It must be noted that the op amp's outputs, OUT+ and OUT-, exhibit highimpedance state in shutdown mode.

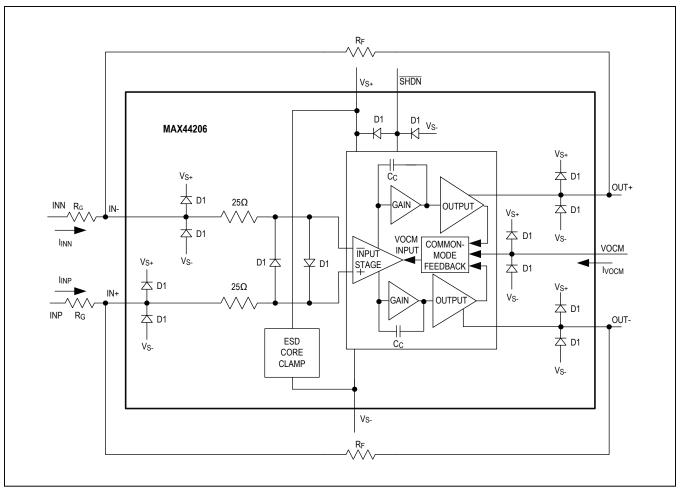


Figure 3. Currents Flowing when MAX44206 is in Shutdown

# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

#### **Applications Information**

The fully differential op amp is shown in Figure 4 for reference. Fully differential op amps provide a lot of advantages, including rejecting common-mode noise coupled to the input, the output, and from the power supply. The effective output swing is increased by a factor of two as the outputs are equal in amplitude and 180° apart in phase.

For example, by applying a fully differential input signal of  $1V_{P-P}$  across INP and INN on Figure 1 there is a  $1V_{P-P}$  differential output voltage swing. Another advantage of having fully differential outputs is that even order harmonics will be suppressed at the output.

# Input Impedance Mismatch Due to Source Impedance

The impedance looking into the IN+ and IN- nodes of Figure 5 depends on how the inputs are driven. For a fully differential input signal, i.e.,  $V_{INP} = V_{INM} + 180^{\circ}$ . The input impedance looking into inputs is shown in Figure 5.

 $R_{INP} = R_{INM} = R_G$ 

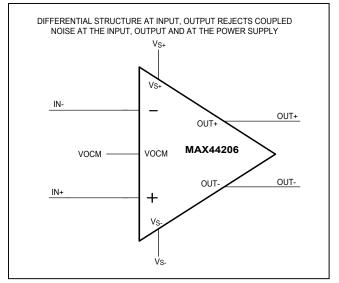


Figure 4. Fully Differential Op Amp

For a single-ended input signal, since the inputs are not balanced, the input impedance actually increases relative to the fully differential case. The input impedance looking into either input is:

$$R_{INP} = R_{INM} = \frac{R_G}{[1 - (\frac{1}{2}) \times \frac{R_F}{(R_G + R_F)}]}$$

Apart from the single-ended input and differential input signal cases, an input signal source from a nonzero source impedance may cause imbalance between feed-back resistor networks for single-ended input driving case as shown in the Figure 6. A terminating resistor RT as shown in Figure 6 is used to impedance match to the source such that:

$$R_{T} = R_{INM} \times \frac{R_{S}}{R_{INM} - R_{S}}$$

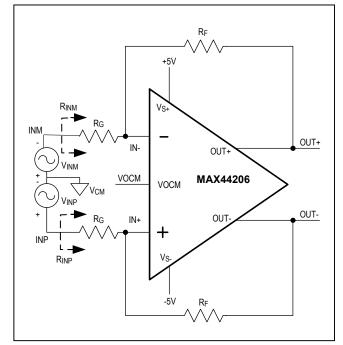


Figure 5. Showing Fully Differential Architecture

A terminating resistor is inserted to correct for impedance mismatch between the source and input. The gain resistor mismatch across feedback networks is created due to the parallel combination of  $R_T$  and  $R_S$ . So, to balance out the gain resistor mismatch on the other input, insert  $R_B$  such that:

$$R_B = R_T \times \frac{R_S}{R_T - R_S}$$

#### **Effects of Input Resistor Mismatch**

If there is a mismatch between the feedback resistor ( $R_F$ ) pair and gain resistor ( $R_G$ ) pair, there will be a small delta in the feedback factor across the input pins. This delta in the feedback factor is a source of common-mode error. To apply an AC CMRR test without a differential input signal, the common-mode rejection is proportional to the resistor mismatch. Using 0.1% or better resistors will mitigate most of the problems and will yield good CMRR performance.

#### **Noise Calculations**

The MAX44206 offers input voltage and current noise densities of  $3.1 \text{nV}/\sqrt{\text{Hz}}$  and  $1.5 \text{pA}/\sqrt{\text{Hz}}$ , respectively. From Figure 7, the total output noise is a combination of noise generated by the amplifier and the feedback and gain resistors. The total output noise generated by both the amplifier and the feedback components is given by the equation:

$$e_{nt} = \sqrt{\frac{\left[e_n \times (1 + \frac{R_F}{R_G})\right]^2 + 2 \times (i_n \times R_F)^2}{(1 + 2 \times (e_{nRG} \times \frac{R_F}{R_G})^2 + 2 \times (e_{nRF})^2}}$$

ent is total output noise of the circuit shown in Figure 7

en is the input voltage-noise density

in is the input current-noise density

 $\mathbf{e}_{nRG}$  is the noise voltage density contributed by the gain resistor RG

 $e_{\mbox{\scriptsize nRF}}$  is the noise voltage density contributed by the feedback resistor  $\mbox{\scriptsize RF}$ 

Resistor Noise =  $\sqrt{4 \times k \times T \times R \times \Delta f}$  in nV/ $\sqrt{Hz}$ 

T is absolute temperature in Kelvin

k is Boltzmann constant: k = 1.38 x 10<sup>-23</sup> in joules/Kelvin

R is resistance in ohms and  $\Delta f$  is frequency range in Hertz

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The MAX44206 input-referred voltage noise contributes the equivalent noise of a  $600\Omega$  resistor. For low noise, keep the source and feedback resistance at or below this value, i.e.  $R_S + R_G / / R_F \leq 600\Omega$ . At combinations of below  $600\Omega$ , amplifier noise is dominant, but in the region  $600\Omega$  to  $10k\Omega$ , the noise is dominated by resistor thermal noise. Any larger resistances beyond that, the noise current multiplied by the total resistance dominated the noise.

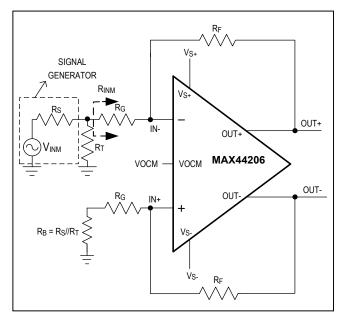


Figure 6. Compensation for Source Impedance

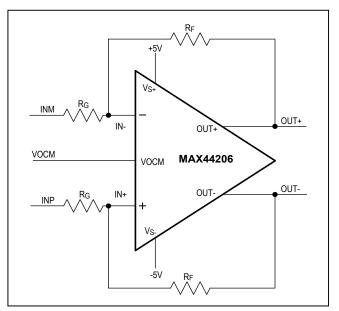


Figure 7. Fully Differential Amplifier

# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

Lower resistor values are ideal for low-noise performance at the cost of increased distortion due to increased loading of the feedback network on the output stage. Higher resistor values will yield better distortion performance due to less loading on the output stage but at the cost of increase in higher output noise.

#### Improving Stability Using Feedback Capacitors

When the MAX44206 is configured such that a combination of parasitic capacitances at the inverting input form a pole whose frequency lies within the closed-loop bandwidth of the amplifier, a feedback capacitor across the feedback resistor is needed to form a zero at a frequency close to the frequency of the parasitic pole to recover the lost phase margin.

Adding larger value feedback capacitors will reduce the peaking of the amplifier but decreases the closed-loop -3dB bandwidth.

#### Layout and Bypass Capacitors

For single-supply applications, it is recommended to place a 0.1 $\mu$ F NPO or COG ceramic capacitor within 1/8<sup>th</sup> of an inch from the V<sub>S+</sub> pin to ground and to also connect a 10 $\mu$ F ceramic capacitor within 1 inch of the V<sub>S+</sub> pin to GND.

In dual-supply applications, it is recommended to install 0.1µF NPO or C0G ceramic capacitor within 1/8<sup>th</sup> of an inch from the V<sub>S+</sub> and V<sub>S-</sub> pins to GND and place 10µF ceramic capacitors within 1 inch of the V<sub>S+</sub> and V<sub>S-</sub> pins to GND. Low ESR\ESL NPO capacitors are recommended for 0.1µF or smaller decoupling capacitors. A 0.1µF or 0.22µF capacitor is a good choice close to VOCM input pin to ground.

Signal routing into and out of the part should be direct and as short as possible into and out of the op amp inputs and outputs. The feedback path should be carefully routed with the shortest path possible without any parasitic capacitance forming between feedback trace and board power planes. Ground and power planes should be removed from directly under the amplifier input and output pins. Also, care should be taken such that there will be no parasitic capacitance formed around the summing nodes at the inputs that could affect the phase margin of the part.

Any load capacitance beyond a few picofarads needs to be isolated using series output resistors placed as close as possible to the output pins to avoid excessive peaking or instability.

#### **Driving a Fully Differential ADC**

The MAX44206 was designed to drive fully differential SAR ADCs such as the MAX11905. The MAX11905 is part of a family of 20-/18-/16-bit, 1.6Msps/1Msps ADCs that offer excellent AC and DC performance. Figure 8 details a fully differential input to the MAX44206, which then drives the fully differential MAX11905 ADC inputs through the ADC input filter shown in the dashed box.

The MAX6126 provides a 3V reference output voltage, which is fed to the ADC's reference. The MAX44206's common mode (VOCM) is created by dividing down the reference voltage by a factor of two. A pair of  $1k\Omega \ 0.1\%$  resistors are used for this purpose. The VOCM input is bypassed to GND with a combination of  $2.2\mu F$  (X7R) and  $0.1\mu F$  (NPO) capacitors.

The MAX44206 is connected in a unity-gain configuration. The input resistors and feedback resistors are all  $1k\Omega$  0.1% resistors. The feedback resistors are bypassed by a pair of 4.7nF (C0G, 100V) capacitors. These feedback components roll the amplifier off to about 60MHz corner frequency.

The ADC input filter uses a pair of  $10\Omega \ 0.1\%$  resistors and a 2.2nF (C0G) capacitor. This input filter assists the MAX44206's settling response with the MAX11905's fast acquisition window.

Figure 8 was used to test the AC performance in Figures 9 and 10. Data were taken with the input frequencies at 10kHz on the MAX11905 Evaluation Kit. Figures 9 to 13 detail the results of the MAX11905 Evaluation Kit (MAX11905DIFEVKIT#) GUI.

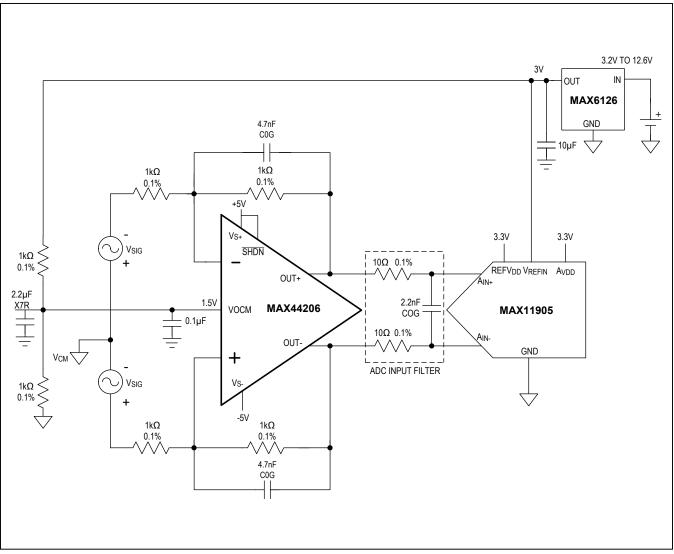


Figure 8. MAX44206 Driving a 20-Bit MAX11905 SAR ADC

# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

The sample rate for Figure 9 is 1Msps and the sample rate for Figure 10 is 1.6Msps, the MAX11905's maximum sample rate. As measured at the MAX11905 output, the signal-to-noise ratio is > 97dB for both sample rates, with total harmonic distortion > 112.9dB.

Figures 11 to 13 detail the DC performance of the MAX44206 and MAX11905. These three figures detail the results of shorting the inputs together to GND at the  $V_{SIG}$  sources and measuring the noise histogram at the output of the ADC. All data was measured at 1Msps, with 65,536 samples taken. Figure 11 shows the results at a 20-bit code level with no averaging. Effective number of bits (ENOB) is 17.9 bits.

One technique to improve a system's ENOB is to average multiple samples. The tradeoff is a reduced effective sample rate. The theoretical expected results of averaging are a 0.5 improvement in ENOB for every average factor of 2. Therefore, averaging by 16x should improve ENOB by 2 bits. Figure 12 details this example, and the ENOB is improved nearly 2 bits, from 17.9 bits to 19.8 bits. This shows that the noise from the ADC and the op amp are not limiting the ENOB.

Figure 13 shows the results of averaging by 64x, which will limit the effective sample rate to 15.6ksps (1Msps/64). ENOB is 20.8 bits in this mode, making the MAX11905 a lower power alternative to high-speed 24-bit delta-sigma ADCs.

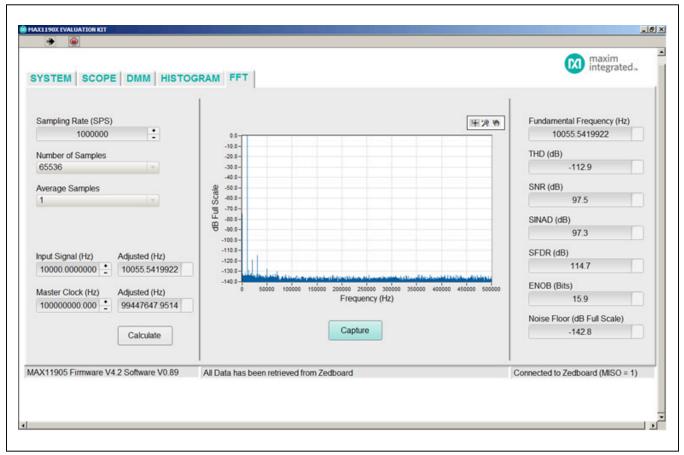


Figure 9. MAX11905 FFT (fSAMPLE = 1Msps, fIN = 10kHz)

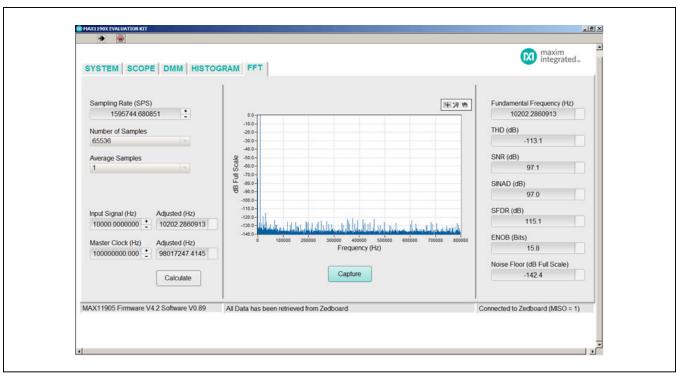


Figure 10. MAX11905 FFT (f<sub>SAMPLE</sub> = 1.6Msps, f<sub>IN</sub> = 10kHz)

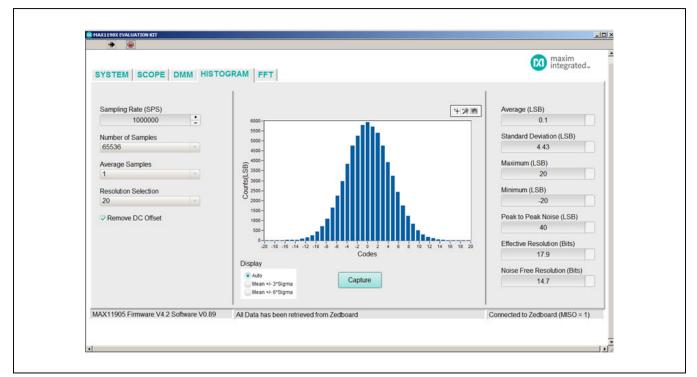


Figure 11. MAX11905 Output Data Histogram (Inputs Shorted, Averaging = 1, f<sub>SAMPLE</sub> = 1Msps)

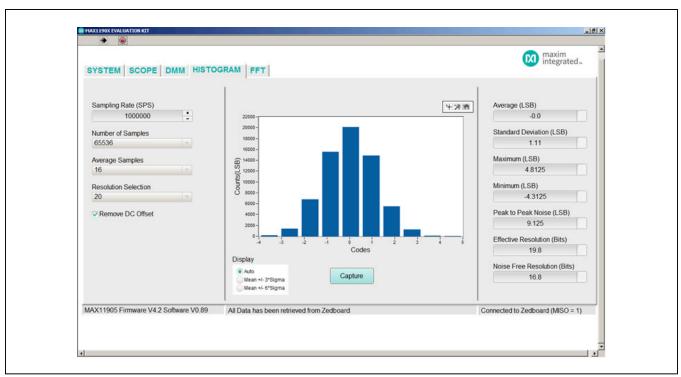


Figure 12. MAX11905 Output Data Histogram (Inputs Shorted, Averaging = 16, f<sub>SAMPLE</sub> = 1Msps)

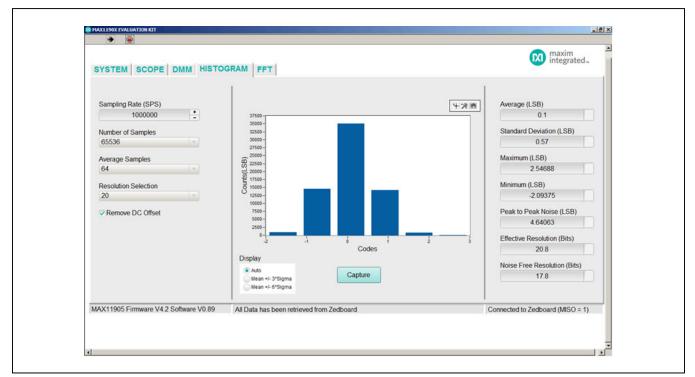


Figure 13. MAX11905 Output Data Histogram (Inputs Shorted, Averaging = 64, f<sub>SAMPLE</sub> = 1Msps)

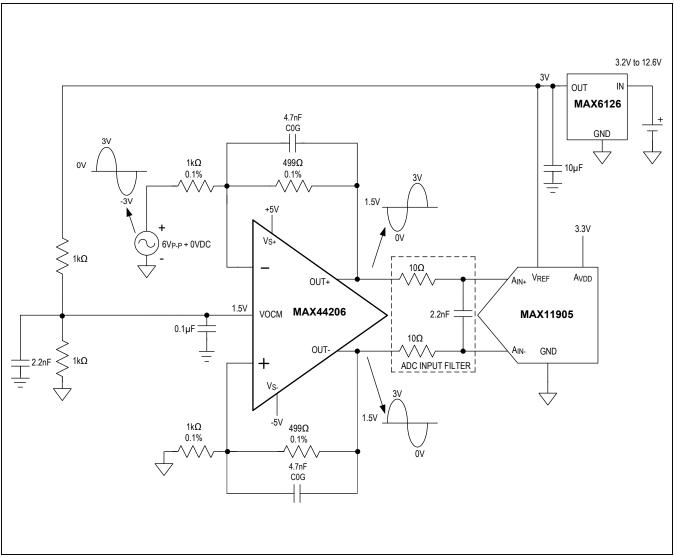


Figure 14. MAX44206 Used to Drive a Single-Ended Input into a Differential, 20-Bit SAR ADC

# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

## **Ordering Information**

PART	TEMP RANGE	PIN- PACKAGE	TOP MARK
MAX44206AUA+	-40°C to +125°C	8 µMAX-EP*	+AACT

+Denotes a lead(Pb)-free/RoHS-compliant package.

\*EP = Exposed pad.

## **Chip Information**

PROCESS: BICMOS

## **Package Information**

For the latest package outline information and land patterns (footprints), go to <u>www.maximintegrated.com/packages</u>. Note that a "+", "#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.

PACKAGE	PACKAGE	OUTLINE	LAND
TYPE	CODE	NO.	PATTERN NO.
8 µMAX-EP	U8E+2	<u>21-0107</u>	<u>90-0145</u>

# 180MHz, Low-Noise, Low-Distortion, Fully Differential Op Amp/ADC Driver

## **Revision History**

REVISION	REVISION	DESCRIPTION	PAGES
NUMBER	DATE		CHANGED
0	11/14	Initial release	—

For pricing, delivery, and ordering information, please contact Maxim Direct at 1-888-629-4642, or visit Maxim Integrated's website at www.maximintegrated.com.

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