# +48V Quad Hot-Swap Controllers For Power-Over-LAN 


#### Abstract

General Description The MAX5913A/MAX5914A are quadruple hot-swap controllers. The MAX5913A/MAX5914A independently control four external n-channel switches to hot-swap system loads from a single VCC supply line. The devices allow the safe insertion and removal of power devices from live network ports. The operating supply voltage range is between +35 V and +72 V . The devices are intended for applications in Power-Over-Media-Dependent Interface (MDI), but are not limited to such usage.

The MAX5913A/MAX5914A feature an internal undervoltage lockout (UVLO) function that prevents the FET from turning on, if $V_{C C}$ does not exceed the default value of +32 V . The devices also feature $\mathrm{a}+12 \mathrm{~V}$ relay driver with 100 mA current drive capable of driving lowvoltage +3.3 V relays. The MAX5913A features an active-low relay driver that sinks current when the relay output is enabled. The MAX5914A features an activehigh relay driver output that sources 1 mA to drive an external FET relay driver when the relay output is enabled. Control circuitry ensures the relays and the FETs are off until VCC reaches the UVLO threshold. The MAX5913A/MAX5914A use an external sense resistor to enable all the internal current-sense functions. The MAX5913A/MAX5914A feature a programmable analog current-limit circuit. If the switch remains in current limit for more than a programmable time, the $n$-channel FET latches off and the supply can be restarted either by autoretry or by an external command after the preset offtime has elapsed. The MAX5913A/MAX5914A are available in a 44-pin MQFP package and are specified for the extended $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ operating temperature range.


Applications
Power-Over-LAN
Power-Over-MDI
IP Phone Switches/Routers
Telecom Line Cards
Network Switches/Routers
Midspan Power-Over-MDI

Typical Operating Circuit appears at end of data sheet.

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Features

- Wide Operating Input Voltage Range: +35 V to +72 V
- IEEE ${ }^{\circledR}$ 802.3af Compatible
- Four Independent Power Switch Controllers
- Open-Circuit Detector
- On-Board Charge Pumps to Drive External n-Channel FETs
- Current Sense with External Resistor
- Foldback Current Limiting
- +32V Input Undervoltage Lockout
- On-Chip +12V, 100mA Voltage Relay Drivers

Ordering Information

| PART | TEMP RANGE | PIN-PACKAGE |
| :--- | :--- | :---: |
| MAX5913AEMH + | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 44 MQFP |
| MAX5913AEMH +T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 44 MQFP |
| MAX5914AEMH + | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 44 MQFP |
| MAX5914AEMH +T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 44 MQFP |

+Denotes a lead(Pb)-free/RoHS-compliant package. $T$ = Tape and reel.

Pin Configuration


## +48V Quad Hot-Swap Controllers For Power-Over-LAN

## ABSOLUTE MAXIMUM RATINGS



VDD to DGND ........................................................... 0.3 V to +7 V DGND to AGND..........................................................-5V to +5 V Current into RLYD_ .........................................-50mA to +150 mA Current into Any Other Pin............................................... $\pm 50 \mathrm{~mA}$ Continuous Power Dissipation $\left(\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}\right)$ 44-Pin MQFP (derate $12.7 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $+70^{\circ} \mathrm{C}$ )......... 1.013 W Operating Temperature Range ........................... $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ Storage Temperature Range ............................. $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ Lead Temperature (soldering, 10s) ................................ $+300^{\circ} \mathrm{C}$

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## ELECTRICAL CHARACTERISTICS

$\left(\mathrm{V}_{C C}=\mathrm{V}_{\text {CSP }}=+48 \mathrm{~V}, \mathrm{~V}_{\text {AGND }}=\mathrm{V}_{\text {DGND }}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD}}=+3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{RLY}}=+12 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}\right.$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{CSP}}=+48 \mathrm{~V}$ and $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.)

| PARAMETER | SYMBOL | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| POWER SUPPLIES |  |  |  |  |  |  |  |
| Analog Supply Voltage | VCC | Measured with respect to AGND |  | 35 |  | 72 | V |
|  | Is | $\mathrm{V}_{\text {CC }}=\mathrm{V}_{\text {CSP }}=72 \mathrm{~V}$ | $\mathrm{T}_{\mathrm{A}}=0^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |  | 2.7 | 4 |  |
|  | Is | IS $=$ ICC + ICSP | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $0^{\circ} \mathrm{C}$ |  |  | 5 |  |
| Digital Supply Voltage | VDD | Measured with respect to DGND |  | 2.5 | 3.3 | 3.7 | V |
| Digital Supply Current | IDD | All logic outputs high, RTIM unconnected |  |  | 1.1 | 3 | mA |
| Analog Supply Undervoltage Lockout | VUVLO | VCC rising, circuits enabled |  | 29 | 32 | 35 | V |
| UVLO Hysteresis | Vuvio, H |  |  |  | 3 |  | V |
| UVLO Deglitch Delay | tD,UVLO | VON $=3.3 \mathrm{~V}, \mathrm{~V}_{\text {RLYON }}=3.3 \mathrm{~V}$ (Figure 1) |  | 12.8 | 25.6 | 38.4 | ms |
| Relay Driver Supply | $V_{\text {RLY }}$ | Measured with respect to DGND |  |  |  | 14 | V |
| Ground Potential Difference | VGG | Voltage difference between DGND and AGND |  | -4 |  | 4 | V |
| FEEDBACK INPUT AND CURRENT SENSE |  |  |  |  |  |  |  |
| OUT Sense Bias Current | IFP | VoUT_ = VCC |  |  |  | 2 | $\mu \mathrm{A}$ |
| Initial Feedback Voltage | $V_{\text {FB_S }}$ | Voltage under which the foldback circuit starts reducing the current-limit value (Note 1) |  |  | 18 |  | V |
| Current-Limit Threshold Voltage | VSC | Maximum $\Delta \mathrm{V}$ across RSENSE at $\mathrm{V}_{\text {OUT }}>\mathrm{V}_{\text {FB_S }}$ |  | 125 | 142.5 | 160 | mV |
| Foldback Voltage | $V_{\text {FLBK }}$ | Maximum $\Delta \mathrm{V}$ across RSENSE at V OUT $=0 \mathrm{~V}$ |  | 42 | 48 | 54 | mV |
| Fast Discharge Threshold | $\mathrm{V}_{\mathrm{FC}}$ |  |  | 360 | 420 | 480 | mV |
| Switch-On Threshold | VSWON | Maximum $\mathrm{V}_{\mathrm{CC}}$ - $\mathrm{V}_{\text {OUT }}$ at which the switch is defined as fully on, Vout increasing |  | 1.2 | 1.5 | 1.8 | V |
| Switch-On Comparator Hysteresis | VSWON_H |  |  |  | 160 |  | mV |
| MOSFET DRIVERS |  |  |  |  |  |  |  |
| Gate Overdrive Voltage | VGS | $\mathrm{V}_{\text {GATE }}-\mathrm{V}_{\mathrm{CC}}$ when switch is fully on $0^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |  | 7 | 9 | 11 | V |
|  |  | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $0^{\circ} \mathrm{C}$ |  | 7 | 9 | 12 |  |
| Gate Charge Current | IGATE | $\mathrm{V}_{\text {GATE }}=0 \mathrm{~V}$ |  | 7 | 10 | 13 | $\mu \mathrm{A}$ |

## +48V Quad Hot-Swap Controllers For Power-Over-LAN

## ELECTRICAL CHARACTERISTICS (continued)

$\left(\mathrm{V}_{C C}=\mathrm{V}_{C S P}=+48 \mathrm{~V}, \mathrm{~V}_{\text {AGND }}=\mathrm{V}_{\mathrm{DGND}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD}}=+3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{RLY}}=+12 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}\right.$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{V}_{C C}=\mathrm{V}_{\text {CSP }}=+48 \mathrm{~V}$ and $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.)

| PARAMETER | SYMBOL | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Gate Discharge Current | IGATE,DIS | During current regulation |  |  | 8 |  | $\mu \mathrm{A}$ |
|  |  | VoN $=0 \mathrm{~V}$ |  |  | 1 |  | mA |
|  |  | $\left(\mathrm{V}_{\text {CSP_ }}-\mathrm{V}_{\text {DRAIN_ }}\right)>\mathrm{V}_{\text {FC }}$ |  |  | 15 |  | mA |
| Source-Gate Clamp Voltage | VSGZ | $\mathrm{V}_{\text {OUT_ }}=0 \mathrm{~V}$, force 30 m measure VGATE - Vout | A into GATE_, | 14 | 16.5 | 18 | V |
| OPEN-CIRCUIT DETECTOR |  |  |  |  |  |  |  |
| Open-Circuit Current-Threshold Voltage | Voc | Minimum $\Delta \mathrm{V}$ across RSENSE to detect an open circuit |  | 1.5 | 3 | 4.5 | mV |
| Delay to Open-Circuit Detect | toc | (Figure 2) |  | 450 | 900 | 1350 | ms |
| Deglitch Delay | tLPFD | $($ VCSP_ - VDRAIN_) < Voc (Figure 2) |  | 106 | 204 | 302 | ms |
| RELAY DRIVERS |  |  |  |  |  |  |  |
| Maximum Low Voltage (MAX5913A) | VRLOW | RLYON $=$ high, $\mathrm{IRLYD}_{-}=100 \mathrm{~mA}$ |  |  |  | 0.5 | V |
| Relay Pullup Current (MAX5914A) | IRPLUP | RLYON = high, $\mathrm{V}_{\text {RLYD_ }}=0 \mathrm{~V}$ |  | 0.3 | 0.8 | 1.3 | mA |
| Clamp Diode Voltage | $V_{\text {RCLAMP }}$ | Force 100 mA into RLYD, measure $V_{\text {RLYD }}$ VRLY |  |  |  | 2 | V |
| Relay Output Leakage |  | RLYON_ = low, $\mathrm{V}_{\text {RLYD_- }}=\mathrm{V}_{\text {RLY }}$ |  |  | 1 |  | $\mu \mathrm{A}$ |
| TIMING |  |  |  |  |  |  |  |
| Short-Circuit and Startup Timer (Note 2) | to | On time for continuous overcurrent conditions | RRTIM $=2 \mathrm{k} \Omega$ | 4.8 | 6.4 | 8.0 | ms |
|  |  |  | RRTIM $=40 \mathrm{k} \Omega$ | 76 | 128 | 180 |  |
|  |  |  | RRTIM $=\infty$ | 3.2 | 6.4 | 9.6 |  |
| Auto-Retry Duty Cycle |  | DC = logic low |  |  | 1 |  | \% |
|  |  | DC = logic high |  |  | 2 |  |  |
|  |  | DC = unconnected |  |  | 4 |  |  |
| Port Turn-On Delay | ton_DEL | Von $=3.3 \mathrm{~V}$ (Figure 3) |  | 12.8 | 25.6 | 38.4 | ms |
| Relay Turn-Off Delay | toff_DEL | After RLYON_ goes low (Figure 3) |  | 1.6 | 3.2 | 4.8 | ms |
| DIGITAL INTERFACE |  |  |  |  |  |  |  |
| DC Pin Input-Voltage High | $\mathrm{V}_{\text {IH_DC }}$ | $2.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{DD}} \leq 3.7 \mathrm{~V}$ |  | $0.7 \times \mathrm{V}$ |  |  | V |
| DC Pin Input-Voltage Low | VIL_DC | $2.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{DD}} \leq 3.7 \mathrm{~V}$ |  |  | $0.3 \times \mathrm{V}_{\mathrm{DD}}$ |  | V |
| DC Pin Input Impedance | RIN_DC |  |  |  | 1 |  | $\mathrm{k} \Omega$ |
| Logic Input High | $\mathrm{V}_{\mathrm{IH}}$ | $2.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{DD}} \leq 3.7 \mathrm{~V}$ |  | $0.8 \times \mathrm{V}$ |  |  | V |
| Logic Input Low | VIL | $2.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{DD}} \leq 3.7 \mathrm{~V}$ |  |  | $0.3 \times \mathrm{VDD}$ |  | V |
| Logic Input Leakage |  |  |  |  |  | 1 | $\mu \mathrm{A}$ |
| FAULT Output-Voltage Low | $\mathrm{V}_{\mathrm{FL}}$ | ISINK $=4 \mathrm{~mA}$ |  |  |  | 0.4 | V |
| FAULT High Input Leakage |  |  |  |  |  | 1 | $\mu \mathrm{A}$ |
| Logic Output-Voltage High | VOH | STAT_ outputs sourcing 0.5 mA |  | VDD - 0.4 |  |  | mV |
| Logic Output-Voltage Low | VOL | STAT_ outputs sinking 0.5 mA |  |  |  | 0.4 | V |

Note 1: See Typical Operating Characteristics for Current-Limit Foldback, and refer to Current Sensing and Regulation section.
Note 2: The resistor at RTIM can range from $2 \mathrm{k} \Omega$ to $40 \mathrm{k} \Omega$.
Note 3: Limits are $100 \%$ tested at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ and $\mathrm{T}_{\mathrm{A}}=+85^{\circ} \mathrm{C}$. Limits at $-40^{\circ} \mathrm{C}$ are guaranteed by design and characterization, but are not production tested.

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$\left(\mathrm{V}_{\mathrm{CSP}}^{-}, ~=~ V_{C C}=+48 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD}}=+3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{RLY}}=+12 \mathrm{~V}, \mathrm{~V}_{\text {AGND }}=\mathrm{V}_{\mathrm{DGND}}=0 \mathrm{~V}, \mathrm{RTIM}=\right.$ open, $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified. $)$

SUPPLY CURRENT
vs. INPUT VOLTAGE


GATE OVERDRIVE VOLTAGE
vs. INPUT VOLTAGE


TURN-OFF WAVEFORMS


A: $V_{O N}=V_{\text {RLYON, }} 5 \mathrm{~V} /$ div
B: VRlyD, 20V/div
C: Vout, 20V/div
D: VGATE, 20V/div

SUPPLY CURRENT
vs. TEMPERATURE


GATE OVERDRIVE VOLTAGE
vs. TEMPERATURE


GATE TURN-OFF WAVEFORM


A: VRLYD, 20V/div
B: $V_{\text {RLYON }}, 5 \mathrm{~V} / \mathrm{div}$
C: Von, $5 \mathrm{~V} / \mathrm{div}$
D: VGATE, 20V/div

UNDERVOLTAGE LOCKOUT
vs. TEMPERATURE


STARTUP WAVEFORMS


A: $V_{O N}=V_{\text {RLYON }}, 5 \mathrm{~V} / \mathrm{div}$
B: VRLYD, 20V/div
C: Vout, 20V/div
D: VGATE, 20V/div
UVLO TURN-ON DELAY


RLYON $=V_{D D}$
A: $\mathrm{V}_{\text {ON }}, 5 \mathrm{~V} / \mathrm{div}$
B: $V_{C C}, 10 \mathrm{~V} / \mathrm{div}$
C: Vout, 50V/div
D: VGATE, 50V/div

# +48V Quad Hot-Swap Controllers For Power-Over-LAN 

Typical Operating Characteristics (continued)
$\left(\mathrm{V}_{C S P}=\mathrm{V}_{\mathrm{CC}}=+48 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD}}=+3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{RLY}}=+12 \mathrm{~V}, \mathrm{~V}_{\text {AGND }}=\mathrm{V}_{\mathrm{DGND}}=0 \mathrm{~V}, \mathrm{RTIM}=\right.$ open, $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified. $)$


RLYON $=V_{D D}, R L=100 \Omega$, RRTIM $=40 \mathrm{k} \Omega$, CLOAD $=470 \mu \mathrm{~F}$ A: Von, 5V/div
B: Vout, 10V/div
C: Iout, $200 \mathrm{~mA} / \mathrm{div}$


CURRENT-LIMIT FOLDBACK


RLYON $=$ VDD, RL $=139 \Omega$, RRTIM $=40 \mathrm{k} \Omega, C L O A D=470 \mu \mathrm{~F}$ A: Von, 5V/div
B: Vout, 10V/div
C: Iout, $200 \mathrm{~mA} /$ div

TURN-ON INTO CAPACITIVE LOAD


RLYON $=V_{D D}$, RRTIM $=40 \mathrm{k} \Omega$
A: Von, 5V/div
B: $V_{G A T E}$, 20V/div
C: Vout, 20V/div
D: Iout, 200mA/div


RLYON $=V_{D D}, \operatorname{RL}=162 \Omega$, RRTIM $=40 \mathrm{k} \Omega$, CLOAD $=470 \mu \mathrm{~F}$ A: Von, 5V/div
B: Vout, 10V/div
C: Iout, $200 \mathrm{~mA} / \mathrm{div}$

## +48V Quad Hot-Swap Controllers For Power-Over-LAN

## $\left(\mathrm{V}_{\mathrm{CSP}},=\mathrm{V}_{C C}=+48 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD}}=+3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{RLY}}=+12 \mathrm{~V}, \mathrm{~V}_{\text {AGND }}=\mathrm{V}_{\mathrm{DGND}}=0 \mathrm{~V}, \mathrm{RTIM}=\right.$ open, $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified. $)$


RLYON $=V_{D D}, R_{L}=200 \Omega$, RRTIM $=40 \mathrm{k} \Omega$
A: $V_{0 N}, 5 \mathrm{~V} /$ div
B: Vout, 10V/div
C: Iout, $200 \mathrm{~mA} / \mathrm{div}$


RLYON $=V_{D D}, R_{L}=O P E N$,
$R_{\text {RTII }}=40 \mathrm{k} \Omega, \mathrm{C}_{\text {LOAD }}=470 \mu \mathrm{~F}$
A: VON, $5 \mathrm{~V} / \mathrm{div}$
B: Vout, 10V/div
C. Iout, $200 \mathrm{~mA} / \mathrm{div}$


RTRYEN = $V_{D D}, \operatorname{RLYON}=0 N=V_{D D}$,
$D C=$ DON'T CARE, RRTIM $=2 k \Omega, R_{L}=100 \Omega$
A: VGate, 20V/div
B: Iout, $200 \mathrm{~mA} /$ div

CURRENT-LIMIT FOLDBACK

$R L Y O N=V_{D D}, R_{L}=O P E N, R_{R T I M}=40 \mathrm{k} \Omega, C_{L O A D}=470 \mu \mathrm{~F}$
A: Von, 5V/div
B: Vout, 20V/div
C: Iout, $200 \mathrm{~mA} /$ div

$O N=R L Y O N=V_{D D}, R=1 \Omega, \operatorname{RRTIM}=2 k \Omega$
A: Iout, $200 \mathrm{~mA} /$ div
B: $V_{G A T E}, 20 V /$ div

# +48V Quad Hot-Swap Controllers For Power-Over-LAN 

Typical Operating Characteristics (continued)
$\left(\mathrm{V}_{C S P}=\mathrm{V}_{\mathrm{CC}}=+48 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD}}=+3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{RLY}}=+12 \mathrm{~V}, \mathrm{~V}_{\text {AGND }}=\mathrm{V}_{\mathrm{DGND}}=0 \mathrm{~V}, \mathrm{RTIM}=\right.$ open, $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified. $)$


40 $\mu \mathrm{s} / \mathrm{div}$
$O N=R L Y O N=V_{D D}, R_{L}=1 \Omega, R_{R T I M}=2 \mathrm{k} \Omega$
A: Iout, $200 \mathrm{~mA} /$ div
B: $\mathrm{V}_{\mathrm{GAte}}, 20 \mathrm{~V} / \mathrm{div}$


$O N=R L Y O N=V_{D D}, R L=1 \Omega, R_{R T I M}=2 k \Omega$
A: lout, 5A/div
B: $V_{\text {Gate }}$ 20V/div

PEAK SHORT-CIRCUIT RESPONSE TIME

$1 \mu \mathrm{~s} / \mathrm{div}$
$O N=R L Y O N=V_{D D}, R_{L}=1 \Omega, R_{R T I M}=2 k \Omega$
A: Iout, 5A/div
B: $V_{G A T E}, 20 \mathrm{~V} / \mathrm{div}$

$O N=R L Y O N=V_{D D}$
A: Iout, $200 \mathrm{~mA} /$ div
B: $\mathrm{V}_{\mathrm{GATE}}, 20 \mathrm{~V} / \mathrm{div}$

$O N=R L Y O N=V_{D D}$
A: Iout, $200 \mathrm{~mA} /$ div
B: $V_{\text {Gate }}, 50 \mathrm{~V} / \mathrm{div}$

## +48V Quad Hot-Swap Controllers For Power-Over-LAN

$\left(V_{C S P}=V_{C C}=+48 \mathrm{~V}, V_{D D}=+3.3 V, V_{R L Y}=+12 \mathrm{~V}, V_{A G N D}=V_{D G N D}=0 \mathrm{~V}, \mathrm{RTIM}=\right.$ open, $T_{A}=+25^{\circ} \mathrm{C}$, unless otherwise specified. $)$

$O N=R L Y O N=V_{D D}, R=1 \Omega, R_{R T I M}=2 \mathrm{k} \Omega$
A: Iout, $200 \mathrm{~mA} /$ div
B: $V_{\text {gate }}$, $50 \mathrm{~V} / \mathrm{div}$


PEAK SHORT-CIRCUIT RESPONSE TIME (VCC = +72V, EXPANDED TIME SCALE)

$O N=R L Y O N=V_{D D}, R L=1 \Omega, R_{R T I M}=2 k \Omega$
A: Iout, 5A/div
B: VGAte, $50 \mathrm{~V} / \mathrm{div}$


OPEN-CIRCUIT THRESHOLD vs. INPUT VOLTAGE


# +48V Quad Hot-Swap Controllers For Power-Over-LAN 

Typical Operating Characteristics (continued)
$\left(\mathrm{V}_{C S P}=\mathrm{V}_{\mathrm{CC}}=+48 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD}}=+3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{RLY}}=+12 \mathrm{~V}, \mathrm{~V}_{\text {AGND }}=\mathrm{V}_{\mathrm{DGND}}=0 \mathrm{~V}, \mathrm{RTIM}=\right.$ open, $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified. $)$
to vs. INPUT VOLTAGE


RETRY DUTY CYCLE vs. DC

$V_{\text {GATE }}=20 \mathrm{~V} / \mathrm{div}$, RRTIM $=2 \mathrm{k} \Omega$
A: $\mathrm{V}_{\text {GATE }}, 20 \mathrm{~V} / \mathrm{div}, \mathrm{DC}=\mathrm{UNCONNECTED} \mathrm{(4} \mathrm{\%)}$
B: $\mathrm{V}_{\text {GATE }}, 20 \mathrm{~V} / \mathrm{div}, \mathrm{DC}=\mathrm{V}_{\mathrm{DD}}(2 \%)$
C: VGAte, $20 \mathrm{~V} / \mathrm{div}, \mathrm{DC}=\mathrm{GND}(1 \%)$

CHANNEL-TO-CHANNEL CROSSTALK


SEE FIGURE 4 FOR TEST CIRCUIT

Pin Description

| PIN | NAME | FUNCTION |
| :---: | :---: | :---: |
| 1 | $\overline{\text { FAULT }}$ | Active-Low Fault Output. $\overline{\text { FAULT }}$ is an open-drain output that goes low when a fault is detected on any of the four channels. FAULT is low when an OC (open circuit) is detected, or when the MAX5913A/MAX5914A is in auto-retry caused by an overcurrent condition. When RTRYEN is low, and the channel switch is latched off due to an overcurrent condition, $\overline{\text { FAULT }}$ remains low until $\mathrm{ON}_{-}$is driven low. |
| 2, 3, 4, 5 | STAT1, <br> STAT2, <br> STAT3, <br> STAT4 | Status Outputs. STAT_ are push-pull outputs. Depending on the STATOUT pin status, STAT_ flags either the Power-OK_ or Port-OC_ status. <br> Power-OK_ high indicates: <br> a) $\mathrm{ON}_{-}$input is high. <br> b) The switch port is fully on and startup is completed (VCSP_- Vout_) < VSWON. <br> c) Input voltage is above VuvLO. <br> d) Switch is not in current limit. <br> Power-OK_ low indicates a fault with any of the above conditions. Port-OC_ output high indicates that the switch is latched off because the switch current is less than the opencurrent threshold, Port-OC is low otherwise. |
| 6, 10, 24, 28 | $\begin{gathered} \text { CSP4, CSP3, CSP2, } \\ \text { CSP1 } \end{gathered}$ | Current-Sense Positive Input. Connect to VCC and place a current-sense resistor from CSP_ to DRAIN_. Use a Kelvin sense trace from a current-sense resistor to CSP_ (see Figure 7). |
| 7, 11, 23, 27 | DRAIN4, DRAIN3, DRAIN2, DRAIN1 | MOSFET Drain Current-Sense Negative Input. Connect to drain of power MOSFET and connect a current-sense resistor from CSP_ to DRAIN_. Use Kelvin sense trace from current-sense resistor to DRAIN_ (see Figure 7). |

## +48V Quad Hot-Swap Controllers For Power-Over-LAN

Pin Description (continued)

| PIN | NAME | FUNCTION |
| :---: | :---: | :---: |
| 8, 12, 21, 25 | OUT4, OUT3, OUT2, OUT1 | MOSFET Source Output Voltage Sense. Connect to a power MOSFET source through a $100 \Omega$ series resistor. |
| 9, 13, 22, 26 | GATE4, GATE3, GATE2, GATE1 | MOSFET Gate Driver Output. The MAX5913A/MAX5914A regulate the gate-drive voltage to (VCC +9 V ) to fully turn on the power n-channel MOSFET. GATE_ sources $10 \mu \mathrm{~A}$ during startup to slowly turn on the MOSFET switch. GATE_ sinks 1 mA to turn off the MOSFET switch. |
| 14 | $V_{\text {RLY }}$ | Relay Supply-Voltage Input. Referenced to DGND. |
| $\begin{gathered} 15,16,18 \\ 19 \end{gathered}$ | RLYD3, RLYD4, RLYD1, RLYD2 | Relay-Drive Output. For the MAX5913A, RLYD_ sinks 100 mA when the relay driver is enabled. For the MAX5914A, RLYD_ sources 1mA when the relay driver is enabled. |
| 17, 30 | DGND | Digital Ground. All logic voltages are referred to DGND. The voltage difference between DGND and AGND can be up to $\pm 4 \mathrm{~V}$. |
| 20 | AGND | Analog Ground. All analog voltages are referred to AGND. |
| 29 | VCC | Analog Power Supply. Connect $\mathrm{V}_{\mathrm{C}}$ to +35 V to +72 V power supply. UVLO circuitry turns off the MOSFET switch and relay for $\mathrm{V}_{\mathrm{CC}}<\mathrm{V}_{\text {UVLO }}$. Bypass $\mathrm{V}_{\mathrm{CC}}$ to AGND with a $1 \mu \mathrm{~F}$ capacitor. |
| 31 | OCEN | Open-Circuit Detector Enable Input. Drive OCEN high to enable open-circuit detector, or drive low to disable. When enabled, the open-circuit detector waits for a 900ms delay after Power-OK conditions are met before enabling the open-circuit detector function. |
| 32 | STATOUT | Status Output Multiplexer (MUX) Control Input. Controls the signal MUX into the STAT_ outputs. Drive STATOUT high to route Power-OK_ status to STAT_ outputs, or drive STATOUT low to route Port-OC_ status to STAT_ outputs. |
| 33 | RTRYEN | Auto-Retry Enable Input. Drive RTRYEN high to enable auto-retry. Drive RTRYEN low to enable switch latch-off mode. When switch is latched off, a high-to-low transition on the ON_ control input clears the latch. |
| 34 | DC | Duty-Cycle Programming Input. DC sets the minimum off-time after an overcurrent condition latches off the switch. When RTRYEN is high, DC sets the auto-retry duty cycle. Drive DC low for $1 \%$ duty cycle, drive DC high for $2 \%$, or leave DC unconnected for $4 \%$ duty cycle. |
| $\begin{gathered} 35,37,39, \\ 41 \end{gathered}$ | RLYON1, RLYON2, RLYON3, RLYON4 | Relay-Driver Control Input. Drive RLYON_ high to enable RLYD_, drive RLYON_ low to turn off the MOSFET switch for the channel and disable RLYD_. |
| $\begin{gathered} 36,38,40, \\ 42 \end{gathered}$ | ON1, ON2, ON3, ON4 | MOSFET Switch Control Input. Drive ON_ high to enable GATE_ to turn on the MOSFET switch. RLYON_ must be high to enable the switch. Drive ON_ low to disable the switch. Pulling ON_ low also resets the latch when RTRYEN is low or if the switch is latched off due to open-circuit detection. |
| 43 | RTIM | Timing Oscillator Frequency Set Input. Connect a $2 \mathrm{k} \Omega$ to $40 \mathrm{k} \Omega$ resistor from RTIM to DGND to set the maximum continuous overcurrent time, to. Leave RTIM unconnected to set default 6.4 ms to. |
| 44 | $V_{\text {DD }}$ | Digital Power Supply. Bypass VDD to DGND with a $1 \mu \mathrm{~F}$ capacitor. |

# +48V Quad Hot-Swap Controllers For Power-Over-LAN 

## Detailed Description

The MAX5913A/MAX5914A quadruple hot-swap controllers provide Power-Over-MDI, also known as Power-Over-LAN systems (Figure 5). The MAX5913A/ MAX5914A enable control of four external n-channel MOSFET switches from a single VCC ranging from +35 V to +72 V , with timing control and current-limiting functions built in.
The MAX5913A/MAX5914A features include undervoltage lockout (UVLO), 100mA relay drivers, dual-level current sense, foldback current limit, programmable overcurrent time and auto-retry periods, internal charge pumps to drive external MOSFET and soft-start, port status output indicating power-OK (POK) or open-circuit conditions (Figure 6).

## Switch and Relay Control Inputs

The MAX5913A/MAX5914A ON_inputs turn on the corresponding MOSFET switch. Driving ON_ high turns on the switch if the corresponding RLYON is driven high, and VCC > VUVLO for more than 25.6 ms . Driving RLYON_ high immediately turns on the corresponding relay, and activates the 25.6 ms delay after which the corresponding ON_ input is active. Driving RLYON_ low immediately turns off the switch and activates a 3.2 ms delay, after which the relay is turned off. These internal delays safely allow driving ON_ and RLYON_ simultaneously. The relay is turned on while the switch is off so that there is no voltage across the relay contacts. The relay is turned off while the switch is off so that there is no current flowing when the relay contacts are opened (see Figure 3).

## Input Voltage and UVLO

 The MAX5913A/MAX5914A operate from a +35 V to +72 V supply voltage. VCC powers the MAX5913A/MAX5914A analog circuitry and is monitored continuously during startup and normal operation. The MAX5913A/MAX5914A keep all MOSFET switches and relay drivers securely off before VCc rises above VuVLo. The MAX5913A/ MAX5914A turn off all MOSFET switches and relay drivers after VCC falls below VUVLO - VUVLO,H.Startup
When the turn-on condition is met (see the Input Voltage and UVLO and Switch and Relay Control Inputs sections), the MAX5913A/MAX5914A slowly turn on the external MOSFET switch by charging its gate using a constant current source, IGATE (10 AA typ). The gate voltage slope is determined by the total gate capacitance CGATE connected to this node. Since the output voltage follows the gate voltage, thus the output rises with a slope determined by:

$$
\frac{\Delta \mathrm{V}_{\mathrm{OUT}}}{\Delta \mathrm{t}}=\frac{\mathrm{I}_{\mathrm{GATE}}}{\mathrm{C}_{\mathrm{GATE}}}
$$

If a capacitor load is connected to the output, the total current through the FET is:

$$
I=I_{G A T E} \frac{C_{L}}{C_{G A T E}}+I_{L}
$$

where $C_{L}$ is the load capacitance and $I_{L}$ is the current required by any load connected to the output during the startup phase.
If the current through the FET reaches the programmed current-limit value:

$$
l_{\operatorname{MAX}}=\frac{V_{S C}}{R_{S E N S E}}
$$

the internal current-limit circuitry activates and regulates this FET current to be a value, ILIM, that depends on Vout (IFLBK) (Figure 8). See the Current Sensing and Regulation section. In this case, the maximum rate of change of the output is determined by:

$$
\frac{\Delta \mathrm{V}_{\mathrm{OUT}}}{\Delta \mathrm{t}}=\frac{\mathrm{L} \mathrm{LIM}-\mathrm{l}_{\mathrm{L}}}{\mathrm{C}_{\mathrm{L}}}
$$

The formula shows the necessity for ILIM to be larger than $I_{\mathrm{L}}$ in order to allow the output voltage to rise. The foldback function is active as long as the circuit is in overcurrent condition. Should the overcurrent condition persist for a period longer than the maximum time to, the switch is latched off and GATE_ is discharged to ground with a 1 mA pulldown current.
If auto-retry is enabled, the switch turns on again after a waiting period, tOFF, which is determined by the programmed duty cycle.
After the startup, the internal charge pumps provide (VCC +9 V ) typical gate overdrive to fully turn on the switch. When the switch is fully on (voltage drop across the switch is $\leq 1.5 \mathrm{~V}$ ), and the switch is not in current limit, the POK signal is asserted.

## Current Sensing and Regulation

The MAX5913A/MAX5914A control port current with using two voltage comparators (dual-level detection) that sense the voltage drop across an external currentsense resistor. Connect CSP_ to Vcc and connect a current-sense resistor between CSP_ and DRAIN_. Kelvin sensing should be used as shown in Figure 7.

## +48V Quad Hot-Swap Controllers For Power-Over-LAN

Test Circuits and Timing Diagrams


Figure 1. UVLO Deglitch Delay


Figure 3. Port Turn-On Delay, Relay Turn-Off Delay

The first comparator compares the sensed voltage against the VSC threshold (typically 142.5 mV ). Choose a sense resistor as follows:
RSENSE = VSC / IMAX
where IMAX is the maximum current allowed through the switch.
When Imax is reached, foldback current-limit circuitry regulates the current limit as a function of Vout (Figure 8). As VOUT approaches zero, the maximum voltage drop


Figure 2. Open-Circuit Detector Deglitch Delay


Figure 4. Channel-to-Channel Crosstalk Test Circuit
across the sense resistor is lowered to a minimum value of 48 mV (typ). This foldback feature helps reduce the power dissipation in the external power FET during output overload and output short-circuit conditions. If a load with very low activation voltage is permanently connected to the output, make the minimum limit current sufficiently larger than the load current. If the load current indeed exceeds the foldback-limit value, the MAX5913A/ MAX5914A are not able to power up the switch.

# +48V Quad Hot-Swap Controllers For <br> Power-Over-LAN 



Figure 5. Typical Application Circuit

A second comparator with a detection threshold of $3 V_{\text {SC }}$ activates a fast 15 mA pulldown of the gate. The purpose of this comparator is to rapidly discharge the gate when a momentary current peak overstresses the external FET, helping the regulation to act more rapidly.
The sense resistor is also used to detect an open-circuit or low-current condition with a typical threshold of 3 mV .

## Open-Circuit Detection

The MAX5913A/MAX5914A detect when a port has low current or is open circuit, and turn off the switch to that port. After the switch is turned on and the POK conditions are met, the open-circuit detector is enabled after
a 900 ms delay. The open-circuit voltage threshold is set at 3 mV across the current-sense resistor. Drive OCEN high to enable open-circuit detectors for all four ports. Drive OCEN low to disable the detectors. Each port has an open-circuit flag that can be read from STAT_ outputs when the STATOUT is low. STAT_ output high indicates that the switch is latched off due to an open-circuit condition on that port. To reset the latch pull ON_ low and then high to restart (Table 1).

Output Voltage Sense and Power-OK
The MAX5913A/MAX5914A sense the output voltage of the port at the source of the external MOSFET switch.

## +48V Quad Hot-Swap Controllers For Power-Over-LAN



Figure 6. Functional Diagram

Internally the circuit compares the output voltage with $V_{C C}$ to determine when the FET is completely on. A POK condition is met when:

$$
\left(\mathrm{V}_{C C}-\mathrm{V}_{\text {OUT }}\right) \leq 1.5 \mathrm{~V}
$$

The internal circuit monitors VOUT to determine the value of the foldback current when the circuit goes into current-limit conditions. The value of the current limit decreases as the output voltage decreases in order to limit the power dissipation of the FET. The nonlinear relationship between VOUT and ILIM is depicted in Figure 8.
The foldback circuit is active whenever the MAX5913A/ MAX5914A are in current-limit mode after an overcurrent condition has been detected.

Connect a catch diode to analog ground and a $100 \Omega$ resistor in series with OUT_ to limit the current during negative inductive kicks that can bring OUT_ below the ground potential (Figure 5).

Relay Drivers
The MAX5913A/MAX5914A include on-chip relay drivers, RYLD_, capable of sinking 100mA. When RLYON_ goes high, the MAX5913A/MAX5914A immediately enable the relay driver, and the corresponding $O N$ _ switch control input is delayed 25.6 ms to allow the relay to close under a zero-voltage condition. When RLYON_ goes low, the MAX5913A/MAX5914A immediately turn off the corresponding switch, and then turn off the relay driver after a 3.2 ms delay, ensuring the relay contacts open under a zero-current condition. The polarity of the MAX5913A

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RLYD_ is opposite to that of the MAX5914A. For the MAX5913A, upon the assertion of the RLYON_ input, RLYD_ sinks 100 mA to DGND. For the MAX5914A, when RLYON_ is high, an internal 1mA current source pulls up RLYD_ to VDD. A 100 mA catch diode is internally connected between RYLD_ and $\mathrm{V}_{\text {RLY }}$ to protect the MAX5913A/MAX5914A from inductive kicks from the relay coil. VRLY must be connected to the high-side relay supply voltage.

Programmable Timing, RTIM
An external resistor from RTIM to DGND sets the frequency of the internal oscillator upon which to and the auto-retry times are based.
Use $2 \mathrm{k} \Omega$ to $40 \mathrm{k} \Omega$ resistors for RRTIM.

$$
\text { to }=(\operatorname{RRTIM} / 2 \mathrm{k} \Omega)(6.4 \mathrm{~ms})
$$

If RTIM is unconnected, an internal resistor sets to to a nominal 6.4 ms .

## Auto-Retry and Programmable Duty Cycle

The MAX5913A/MAX5914A feature auto-retry with adjustable duty cycle. Driving RTRYEN high enables the auto-retry function. When the switch encounters an overcurrent for a period greater than to, the switch is turned off, and remains off for a toff programmed by DC, a three-level input. After the toff period, the switch is automatically turned on again. When the port encounters a continuous overload or short-circuit condition, the switch turns on and off repeatedly with the on duty cycle of $1 \%, 2 \%$, or $4 \%$ depending on the DC input state (Table 2). When RTRYEN is low, the auto-retry is disabled, and a fault condition at the switch turns the switch off and the switch remains latched off. Driving the corresponding ON control input low resets the latch. Pulling ON high to turn on the switch. However, the MAX5913A/MAX5914A always wait a minimum time, toff, before restarting the switch.

## Logic Interface and Status Outputs

The MAX5913A/MAX5914A logic interface controls the device functionality. All the basic control functions for the four switches are separated. ON_ enables individual on/off control of each MOSFET (the corresponding relay must be on to turn on the switch). RLYON_ enables individual on/off control of each relay. STAT_ indicates POK or Port-OC (open circuit) status of each switch. The other logic pins are common to all four switches. A single FAULT output goes low when any of the four channels is latched off. Driving OCEN high enables the open-circuit detectors. Driving RTRYEN high enables the auto-retry function, RTRYEN low enables the switch latch-off function. DC, a three-level logic input, programs the duty cycle. The STATOUT input selects the signal multiplexed at STAT_ outputs (Table 1.). Driving STATOUT high routes POK status to the STAT_ outputs. Driving STATOUT low routes Port-OC status to the STAT_ outputs.

Fault Management UVLO and Power-OK
The MAX5913A/MAX5914A monitor the VCC input voltage and each switch's current and voltage to determine POK, overcurrent, or Port-OC status. When Vcc falls below the UVLO threshold, FAULT goes low and all four switches and relays are turned off. When the volage across the switch is less than 1.5 V , the switch is fully on, and if the switch is not in current limit or open circuit, POK status is good (high).

Open-Circuit Faults
With the open-circuit detector enabled, when any switch current falls below the open-circuit detector threshold current, the open-circuit detector turns off the switch after a 25.6 ms delay, FAULT goes low, and the Port-OC flag is set for that switch. To clear the switch latched-off condition, $\overline{F A U L T}$ and Port-OC flags drive the corresponding ON input low.

## Table 1. Status Output

| PORT_CONDITION | OCEN | STATOUT | STAT_ |
| :---: | :---: | :---: | :---: |
| Enabled. Switch fully on and not in current limit. | x | H | H (Power-OK_ is good) |
| Enabled. Switch in current limit, or $\mathrm{V}_{\mathrm{DS}}>1.5 \mathrm{~V}$. | x | H | $\begin{gathered} \mathrm{L} \\ (\text { Power-OK_ is not good) } \end{gathered}$ |
| Enabled. Switch current is less than OC threshold, port is latched off. | H | L | (Port-OC_, Port current is low or zero) |
| Enabled. Switch fully on and output current is greater than OC threshold. | H | L | L <br> (Port-OC_, Port current is good) |
| Disabled. | L | L | L |

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## Overcurrent Faults

When an on-switch current exceeds the current-limit threshold, foldback circuitry activates and regulates the switch current. When the current limit lasts for longer than to, the switch latches off. The POK status flag is set low, and the FAULT flag is set. If auto-retry is enabled, the switch remains off for a period toff. If auto-retry is disabled, the switch remains latched off, and FAULT is low. Reset the latch and FAULT by driving corresponding ON_low.

## Applications Information

Considerations for circuit design include output capacitor requirements, current-limit requirements, setting the maximum on-time in current limit, and choosing a suitable MOSFET and on-time duty cycle in auto-retry.

## Output Capacitor Requirements

The load capacitor requirements should be determined first, as this affects the required startup.

## Current-Limit Requirements

(Choosing Rsense)
The current limit should be set to at least 20\% higher than the expected full load current. If current limit is also used to control startup current, then set this limit high enough so that the output voltage can rise and settle before to elapses (see the Setting to (Choosing RRTIM) section).

Setting to (Choosing RRTIM)
Choose the to time by connecting a $2 k \Omega$ to $40 \mathrm{k} \Omega$ resistor from RTIM to DGND. The minimum 6.4 ms to is set with Rrtim $=2 \mathrm{k} \Omega$. The maximum 128 ms to is set with Rrtim $=40 \mathrm{k} \Omega$ set according to the following equation:

$$
\text { to }=(\text { RRTIM } / 2 \mathrm{k} \Omega)(6.4 \mathrm{~ms})
$$

to should be chosen appropriately, depending on the startup condition. There are two cases:

1) For startup without current limit, when:

$$
I=I_{\text {GATE }} \frac{C_{L}}{C_{G A T E}}+I_{L}<\frac{V_{S C}}{R_{\text {SENSE }}}
$$

The startup current does not reach the maximum current-limit threshold and to will not activate during startup condition. In this case, set to to a small
value, but large enough to allow the switch to remain on during large output load-current transients. The smaller the to, the faster the MAX5913A/MAX5914A turn off the external FET in case of output overload or short-circuit condition.
2) For startup with current limit, when:

$$
I=I_{G A T E}\left(\frac{C_{L}}{C_{G A T E}}+I_{L}\right) \geq \frac{V_{S C}}{R_{S E N S E}}
$$

which is expected when:

$$
\frac{C_{L}}{C_{G A T E}}
$$

is large, to must be set to be long enough to allow the output voltage to rise and settle before to elapses. In this case, to must satisfy the following equation:

$$
t_{O}=C_{L} \frac{18}{\frac{2}{3} I_{M A X}-I_{L}}+C_{L} \frac{V_{C C}-18 V}{I_{M A X}-I_{L}}
$$

where $\mathrm{V}_{\mathrm{CC}}$ is the input voltage and given that IL < ILIM.
Choosing Power MOSFET
The FET must withstand a short-circuit condition where its power dissipation is PDISS $=$ VCC $\times$ ILIM. The FET must have sufficient thermal capacitance to prevent thermal heating damage during the to time.

Choose Duty Cycle (Setting DC)
The duty cycle can be adjusted to allow time for heat to dissipate between to cycles, allowing use of smaller MOSFETs with lower thermal capacitance. For smaller duty cycle, a smaller FET is sufficient. See Table 2 for setting the duty cycle.
The auto-retry off-time should not be too long to keep the system wait time during retry period to a reasonable value. For example, when to is set to 128 ms and duty cycle is set to $1 \%$, the retry time is $99 \times 128 \mathrm{~ms}=12.7 \mathrm{~s}$.

## Application Circuits

In a typical LAN system there are two ways to deliver power over the LAN cable. Power can be supplied to the unused cable pairs, or power can be supplied over the signal pairs (Figures 9 and 10).

## +48V Quad Hot-Swap Controllers For Power-Over-LAN



Figure 7. Recommended Layout for Kelvin-Sensing Current Through Sense Resistor


Figure 8. Foldback Current-Limit Response

Table 2. Duty Programming Cycle

| DC | toFF | DUTY CYCLE |
| :---: | :---: | :---: |
| 0 | $99 \times$ to | $1 \%$ |
| 1 | $49 \times$ to | $2 \%$ |
| Open | $24 \times$ to | $4 \%$ |

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Figure 9. Power Sent Over Signal Pairs


Figure 10. Power Sent Over Spare Pairs

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Chip Information
PROCESS: BiCMOS

Package Information
For the latest package outline information and land patterns, go to www.maxim-ic.com/packages. Note that a " + ", "\#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.

| PACKAGE TYPE | $\begin{gathered} \hline \text { PACKAGE } \\ \text { CODE } \end{gathered}$ | OUTLINE NO. | LAND PATTERN NO. |
| :---: | :---: | :---: | :---: |
| 44 MQFP | M44+3 | 21-0826 | 90-0169 |

## +48V Quad Hot-Swap Controllers For Power-Over-LAN

| REVISION <br> NUMBER | REVISION <br> DATE | DESCRIPTION | PAGES <br> CHANGED |
| :---: | :---: | :--- | :---: |
| 0 | $5 / 04$ | Initial release | - |
| 1 | $1 / 11$ | Released the MAX5914A. Updated the Ordering Information, Electrical <br> Characteristics, Typical Operating Characteristics, Pin Description, and the <br> Programming Timing, RTIM section | $1-9,15$ |

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