## Dual-Output (+ and -) DC-DC Converters for CCD

## General Description

The MAX8614A/MAX8614B dual-output step-up DC-DC converters generate both a positive and negative supply voltage that are each independently regulated. The positive output delivers up to 50 mA while the inverter supplies up to 100 mA with input voltages between 2.7 V and 5.5 V . The MAX8614A/MAX8614B are ideal for powering CCD imaging devices and displays in digital cameras and other portable equipment.
The MAX8614A/MAX8614B generate an adjustable positive output voltage up to +24 V and a negative output down to 16 V below the input voltage. The MAX8614B has a higher current limit than the MAX8614A. Both devices operate at a fixed 1 MHz frequency to ease noise filtering in sensitive applications and to reduce external component size.

Additional features include pin-selectable power-on sequencing for use with a wide variety of CCDs, True Shutdown ${ }^{\mathrm{TM}}$, overload protection, fault flag, and internal soft-start with controlled inrush current.

The MAX8614A/MAX8614B are available in a space saving $3 \mathrm{~mm} \times 3 \mathrm{~mm}$, 14 -pin TDFN package and are specified over the $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C} / 125^{\circ} \mathrm{C}$ extended temperature ranges.

## Applications

- CCD Bias Supplies and OLED Displays
- Digital Cameras
- Camcorders and Portable Multimedia
- PDAs and Smartphones

True Shutdown is a trademark of Maxim Integrated Products, Inc.

## Pin Configuration



## Features

- Dual Output Voltages (+ and -)
- Adjustable Up to +24 V and Down to -10 V at $5.5 \mathrm{~V}_{\mathrm{IN}}$
- Output Short/Overload Protection
- True Shutdown on Both Outputs
- Controlled Inrush Current During Soft-Start
- Selectable Power-On Sequencing
- Up to $90 \%$ Efficiency
- $1 \mu \mathrm{~A}$ Shutdown Current
- 1MHz Fixed-Frequency PWM Operation
- Fault-Condition Flag
- Thermal Shutdown
- Small, 3mm x 3mm, 14-Pin TDFN Package


## Ordering Information

| PART | TEMP <br> RANGE | PIN- <br> PACKAGE | TOP MARK | ILIM BST/ <br> INV |
| :---: | :---: | :---: | :---: | :---: |
| MAX8614AETD+ | $\begin{gathered} -40^{\circ} \mathrm{C} \text { to } \\ +85^{\circ} \mathrm{C} \end{gathered}$ | 14 TDFN | ABG | $\begin{gathered} 0.44 / \\ 0.33 \end{gathered}$ |
| MAX8614BETD+ | $\begin{aligned} & -40^{\circ} \mathrm{C} \text { to } \\ & +85^{\circ} \mathrm{C} \end{aligned}$ | 14 TDFN | ABH | $\begin{aligned} & 0.8 / \\ & 0.75 \end{aligned}$ |
| MAX8614BATD/V+ | $\begin{aligned} & -40^{\circ} \mathrm{C} \text { to } \\ & +125^{\circ} \mathrm{C} \end{aligned}$ | 14 TDFN | ABT | $\begin{aligned} & \hline 0.8 / \\ & 0.75 \end{aligned}$ |

+Denotes a lead(Pb)-free/RoHS-compliant package.
$N$ denotes an automotive qualified part that conforms to AEC-Q100.

## Typical Operating Circuit



## Dual-Output (+ and -) DC-DC Converters for CCD

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Absolute Maximum Ratings
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$V_{C C}$, AVCC to GND $\qquad$ -0.3 V to +6 V
LXN to $\mathrm{V}_{\mathrm{CC}}$............................................................... -18 V to +0.3 V
LXP to PGND
-0.3 V to +33 V

## REF, ONINV, ONBST, SEQ, FBN, FBP

FLT to GND $\qquad$ -0.3 V to (AVCC + 0.3) V PVP to GND ............................................ -0.3 V to $\left(\mathrm{V}_{\mathrm{CC}}+0.3\right) \mathrm{V}$ AVCC to $\mathrm{V}_{\mathrm{CC}} \ldots . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . ~-~ 0.3 V ~ t o ~+0.3 V ~$ PGND to GND -0.3 V to +0.3 V

Continuous Power Dissipation ( $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ Multilayer Board) 14 -Pin $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ TDFN (derate $18.2 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ )...........................................................1454.4mW Operating Temperature Range $\qquad$ $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C} / 125^{\circ} \mathrm{C}$ Junction Temperature ..................................................... $+150^{\circ} \mathrm{C}$ Storage Temperature Range ............................ $65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ Lead Temperature (soldering, 10s). $\qquad$ $+300^{\circ} \mathrm{C}$

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## Electrical Characteristics

$\left(\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\text {AVCC }}=\mathrm{V}_{\text {ONINV }}=\mathrm{V}_{\text {ONBST }}=3.6 \mathrm{~V}, \mathrm{PGND}=\mathrm{SEQ}=\mathrm{GND}, \mathrm{C} 6=0.22 \mu \mathrm{~F}, \mathrm{C} 1=2.2 \mu \mathrm{~F}, \mathrm{C} 2=4.7 \mu \mathrm{~F}\right.$, Figure $1, \mathrm{~T}_{\mathrm{A}}=0^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.)

| PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AVCC and $\mathrm{V}_{\mathrm{CC}}$ Voltage Range | (Note 1) | 2.7 |  | 5.5 | V |
| UVLO Threshold | $\mathrm{V}_{\text {CC }}$ rising | 2.42 | 2.55 | 2.66 | V |
| UVLO Hysteresis |  |  | 25 |  | mV |
| Step-Up Output-Voltage Adjust Range |  | $\mathrm{V}_{\text {AVCC }}$ |  | 24 | V |
| Inverter Output-Voltage Adjust Range | $\mathrm{V}_{\text {INV }}-\mathrm{V}_{\text {CC }}$ (Note 2) | -16 |  | 0 | V |
| LXP Current Limit | MAX8614B | 0.7 | 0.8 | 0.9 | A |
|  | MAX8614A | 0.34 | 0.44 | 0.52 |  |
| LXP Short-Circuit Current Limit | MAX8614B | 0.90 | 1.05 | 1.20 | A |
|  | MAX8614A | 0.52 | 0.61 | 0.70 |  |
| LXN Current Limit | MAX8614B | 0.65 | 0.75 | 0.85 | A |
|  | MAX8614A | 0.28 | 0.33 | 0.38 |  |
| LXN On-Resistance | $\mathrm{V}_{\mathrm{CC}}=3.6 \mathrm{~V}$ |  | 0.6 | 1.1 | $\Omega$ |
| LXP On-Resistance | $\mathrm{V}_{\mathrm{CC}}=3.6 \mathrm{~V}$ |  | 0.625 |  | $\Omega$ |
| PVP On-Resistance | $\mathrm{V}_{\mathrm{CC}}=3.6 \mathrm{~V}$ |  | 0.15 | 0.3 | $\Omega$ |
| Maximum Duty Cycle | Step-up and inverter | 82 | 90 |  | \% |
| Quiescent Current (Switching, No Load) | $I_{\text {AVCC }}$ |  | 0.75 | 1.4 | mA |
|  | IVCC |  | 2 | 3 |  |
| Quiescent Current (No Switching, No Load) | $I_{\text {AVCC }}$ |  | 400 | 800 | $\mu \mathrm{A}$ |
|  | IVCC |  | 8 | 15 |  |
| Shutdown Supply Current | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  | 0.1 | 5 | $\mu \mathrm{A}$ |
|  | $\mathrm{T}_{\mathrm{A}}=+85^{\circ} \mathrm{C}$ |  | 0.1 |  |  |
| FBP Line Regulation | $\mathrm{V}_{\mathrm{CC}}=2.7 \mathrm{~V}$ to 5.5 V |  | -20 |  | mV/D |
| FBN Line Regulation | $\mathrm{V}_{\mathrm{CC}}=2.7 \mathrm{~V}$ to 5.5 V |  | 20 |  | $\begin{gathered} \mathrm{mV} / \\ (\mathrm{D}-0.5) \end{gathered}$ |

## Electrical Characteristics (continued)

$\left(\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{AVCC}}=\mathrm{V}_{\text {ONINV }}=\mathrm{V}_{\text {ONBST }}=3.6 \mathrm{~V}, \mathrm{PGND}=\mathrm{SEQ}=\mathrm{GND}, \mathrm{C} 6=0.22 \mu \mathrm{~F}, \mathrm{C} 1=2.2 \mu \mathrm{~F}, \mathrm{C} 2=4.7 \mu \mathrm{~F}\right.$, Figure $1, \mathrm{~T}_{\mathrm{A}}=0^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.)

| PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FBP Load Regulation | $I_{\text {LXP }}=I_{\text {ILIMMIN }}$, MAX8614B |  |  | -15 |  | mV/A |
|  | ILXP $=$ IILIMMIN , MAX8614A |  |  | -35 |  |  |
| FBN Load Regulation | ILXN $=I_{\text {ILIMMIN }}$, MAX8614B |  |  | 17.5 |  | mV/A |
|  | $I_{\text {LXN }}=I_{\text {ILIMMIN }}$, MAX8614A |  | 65 |  |  |  |
| Oscillator Frequency |  |  | 0.93 | 1 | 1.07 | MHz |
| Soft-Start Interval | Step-up and inverter |  | 10 |  |  | ms |
| Overload-Protection Fault Delay |  |  |  | 100 |  | ms |
| FBP, FBN, REFERENCE |  |  |  |  |  |  |
| REF Output Voltage | No load |  | 1.24 | 1.25 | 1.26 | V |
| REF Load Regulation | $0 \mu \mathrm{~A}<\mathrm{I}_{\text {REF }}<50 \mu \mathrm{~A}$ |  |  | 10 |  | mV |
| REF Line Regulation | $3.3 \mathrm{~V}<\mathrm{V}_{\mathrm{AVCC}}<5.5 \mathrm{~V}$ |  |  | 2 | 5 | mV |
| FBP Threshold Voltage | No load |  | 0.995 | 1.010 | 1.025 | V |
| FBN Threshold Voltage | No load |  | -10 | 0 | +10 | mV |
| FBP Input Leakage Current | $\mathrm{V}_{\mathrm{FBP}}=1.025 \mathrm{~V}$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | -50 | +5 | +50 | nA |
|  |  | $\mathrm{T}_{\mathrm{A}}=+85^{\circ} \mathrm{C}$ |  | +5 |  |  |
| FBN Input Leakage Current | $\mathrm{FBN}=-10 \mathrm{mV}$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | -50 | +5 | +50 | nA |
|  |  | $\mathrm{T}_{\mathrm{A}}=+85^{\circ} \mathrm{C}$ |  | +5 |  |  |
| LXN Input Leakage Current | $\mathrm{V}_{\mathrm{LXN}}=-12 \mathrm{~V}$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | -5 | +0.1 | +5 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{T}_{\mathrm{A}}=+85^{\circ} \mathrm{C}$ |  | +0.1 |  |  |
| LXP Input Leakage Current | $V_{\text {LXP }}=23 \mathrm{~V}$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | -5 | +0.1 | +5 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{T}_{\mathrm{A}}=+85^{\circ} \mathrm{C}$ |  | +0.1 |  |  |
| PVP Input Leakage Current | $V_{P V P}=0 V$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | -5 | +0.1 | +5 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{T}_{\mathrm{A}}=+85^{\circ} \mathrm{C}$ |  | +0.1 |  |  |
| $\overline{\text { FLT }}$ Input Leakage Current | $\mathrm{V}_{\overline{\mathrm{FLT}}}=3.6 \mathrm{~V}$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | -1 | +0.1 | +1 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{T}_{\mathrm{A}}=+85^{\circ} \mathrm{C}$ |  | +0.1 |  |  |
| $\overline{\text { FLT Input Resistance }}$ | Fault mode, $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  |  | 10 | 20 | $\Omega$ |
| ONINV, ONBST, SEQ LOGIC INPUTS |  |  |  |  |  |  |
| Logic-Low Input | $2.7 \mathrm{~V}<\mathrm{V}_{\text {AVCC }}<5.5 \mathrm{~V}$ |  |  |  | 0.5 | V |
| Logic-High Input | $2.7 \mathrm{~V}<\mathrm{V}_{\mathrm{AVCC}}<5.5 \mathrm{~V}$ |  | 1.6 |  |  | V |
| Bias Current | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  |  | 0.1 | 1 | $\mu \mathrm{A}$ |

## Electrical Characteristics

$\left(V_{C C}=V_{A V C C}=V_{\text {ONINV }}=V_{\text {ONBST }}=V_{E N}=3.6 \mathrm{~V}, \mathrm{PGND}=\mathrm{SEQ}=\mathrm{GND}, \mathrm{C} 6=0.22 \mu \mathrm{~F}, \mathrm{C} 1=2.2 \mu \mathrm{~F}, \mathrm{C} 2=6.7 \mu \mathrm{~F}\right.$, Figure $1, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted.) (Note 3)

| PARAMETER | CONDITIONS | MIN | TYP MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: |
| AVCC $=\mathrm{V}_{\mathrm{CC}}$ Voltage Range | (Note 1) | 3 | 5.5 | V |
| UVLO Threshold | $\mathrm{V}_{\mathrm{CC}}$ rising | 2.42 | 2.82 | V |
| Step-Up Output Voltage Adjust Range |  | $\mathrm{V}_{\text {AVCC }}$ | 24 | V |
| Inverter Output Voltage Adjust Range | $\mathrm{V}_{\text {INV }}-\mathrm{V}_{\text {CC }}$ (Note 2) | -16 | 0 | V |
| LXP Current Limit | MAX8614B | 0.7 | 0.9 | A |
|  | MAX8614A | 0.34 | 0.52 |  |
| LXP Short-Circuit Current Limit | MAX8614B | 0.9 | 1.2 | A |
|  | MAX8614A | 0.52 | 0.70 |  |
| LXN Current Limit | MAX8614B | 0.65 | 0.85 | A |
|  | MAX8614A | 0.28 | 0.38 |  |
| LXN On-Resistance | $\mathrm{V}_{\mathrm{CC}}=3.6 \mathrm{~V}$ |  | 1.1 | $\Omega$ |
| PVP On-Resistance | $\mathrm{V}_{\mathrm{CC}}=3.6 \mathrm{~V}$ |  | 0.3 | $\Omega$ |
| Maximum Duty Cycle | Step-up and inverter | 82 |  | \% |
| Quiescent Current (Switching, No Load) | $\mathrm{I}_{\text {AVCC }}$ |  | 1.4 | mA |
|  | Ivcc |  | 3 |  |
| Quiescent Current (No Switching, No Load) | $I_{\text {AVCC }}$ |  | 800 | $\mu \mathrm{A}$ |
|  | Ivcc |  | 15 |  |
| Oscillator Frequency |  | 0.93 | 1.07 | MHz |
| FBP, FBN, REFERENCE |  |  |  |  |
| REF Output Voltage | No load | 1.235 | 1.260 | V |
| FBP Threshold Voltage | No load | 0.995 | 1.025 | V |
| FBN Threshold Voltage | No load | -10 | +10 | mV |
| ONINV, ONBST SEQ LOGIC INPUTS |  |  |  |  |
| Logic-Low Input | $2.7 \mathrm{~V}<\mathrm{V}_{\mathrm{AVCC}}<5.5 \mathrm{~V}$ |  | 0.5 | V |
| Logic-High Input | $2.7 \mathrm{~V}<\mathrm{V}_{\text {AVCC }}<5.5 \mathrm{~V}$ | 1.6 |  | V |

## Electrical Characteristics

$\left(\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{AVCC}}=\mathrm{V}_{\mathrm{ONINV}}=\mathrm{V}_{\mathrm{ONBST}}=\mathrm{V}_{\mathrm{EN}}=3.6 \mathrm{~V}, \mathrm{PGND}=\mathrm{SEQ}=\mathrm{GND}, \mathrm{C} 6=0.22 \mu \mathrm{~F}, \mathrm{C} 1=2.2 \mu \mathrm{~F}, \mathrm{C} 2=6.7 \mu \mathrm{~F}\right.$, Figure 1, MAX8614BATD $/ \mathrm{V}+$, $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+\mathbf{1 2 5}{ }^{\circ} \mathrm{C}$, unless otherwise noted)(Note 3)

| PARAMETER | CONDITIONS | MIN | TYP MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: |
| AVCC $=\mathrm{V}_{\text {CC }}$ Voltage Range | (Note 1) | 3 | 5.5 | V |
| UVLO Threshold | $\mathrm{V}_{\mathrm{CC}}$ rising | 2.42 | 2.82 | V |
| Step-Up Output Voltage Adjust Range |  | $\mathrm{V}_{\text {AVCC }}$ | 24 | V |
| Inverter Output Voltage Adjust Range | $\mathrm{V}_{\text {INV }}-\mathrm{V}_{\text {CC }}$ (Note 2) | -16 | 0 | V |
| LXP Current Limit |  | 0.7 | 0.9 | A |
|  |  | 0.34 | 0.52 |  |
| LXP Short-Circuit Current Limit |  | 0.9 | 1.2 | A |
|  |  | 0.52 | 0.70 |  |
| LXN Current Limit |  | 0.65 | 0.85 | A |
|  |  | 0.28 | 0.38 |  |
| LXN On-Resistance | $\mathrm{V}_{\mathrm{CC}}=3.6 \mathrm{~V}$ |  | 1.1 | $\Omega$ |
| PVP On-Resistance | $\mathrm{V}_{\mathrm{CC}}=3.6 \mathrm{~V}$ |  | 0.3 | $\Omega$ |
| Maximum Duty Cycle | Step-up and inverter | 82 |  | \% |
| Quiescent Current (Switching, No Load) | $I_{\text {AVCC }}$ |  | 1.4 | mA |
|  | Ivce |  | 3 |  |
| Quiescent Current <br> (No Switching, No Load) | IAVCC |  | 800 | $\mu \mathrm{A}$ |
|  | IVcc |  | 15 |  |
| Oscillator Frequency |  | 0.93 | 1.07 | MHz |
| FBP, FBN, REFERENCE |  |  |  |  |
| REF Output Voltage | No load | 1.235 | 1.260 | V |
| FBP Threshold Voltage | No load | 0.995 | 1.025 | V |
| FBN Threshold Voltage | No load | -10 | +10 | mV |
| ONINV, ONBST SEQ LOGIC INPUTS |  |  |  |  |
| Logic-Low Input | $2.7 \mathrm{~V}<\mathrm{V}_{\text {AVCC }}<5.5 \mathrm{~V}$ |  | 0.5 | V |
| Logic-High Input | $2.7 \mathrm{~V}<\mathrm{V}_{\text {AVCC }}<5.5 \mathrm{~V}$ | 1.6 |  | V |

Note 1: Output current and on-resistance are specified at 3.6 V input voltage. The IC operates to 2.7 V with reduced performance.
Note 2: The specified maximum negative output voltage is referred to $\mathrm{V}_{\mathrm{CC}}$, and not to GND . With $\mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}$, the maximum negative output is then -12.7 V .
Note 3: Specifications to $-40^{\circ} \mathrm{C}$ are guaranteed by design, not production tested.

## Typical Operating Characteristics

$\left(\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{AVCC}}=3.6 \mathrm{~V}, \mathrm{SEQ}=\mathrm{GND}\right.$, Figure 1, unless otherwise noted. $)$


## Typical Operating Characteristics (continued)

$\left(\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{AVCC}}=3.6 \mathrm{~V}, \mathrm{SEQ}=\mathrm{GND}\right.$, Figure 1, unless otherwise noted. $)$



SWITCHING WAVEFORMS (POSITIVE OUTPUT)


SWITCHING WAVEFORMS (NEGATIVE OUTPUT)


## Typical Operating Characteristics (continued)

$\left(\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{AVCC}}=3.6 \mathrm{~V}, \mathrm{SEQ}=\mathrm{GND}\right.$, Figure 1, unless otherwise noted. $)$


## Pin Description

| PIN | NAME | FUNCTION |
| :---: | :---: | :--- |
| 1 | ONBST | Enable Logic Input. Connect ONBST to AVCC for automatic startup of the step-up converter, <br> or use ONBST as an independent control of the step-up converter. |
| 2 | FBN | Negative Output Feedback Input. Connect a resistor-divider between the negative output and <br> REF with the center to FBN to set the negative output voltage. |
| 3 | AVCC | Bias Supply. AVCC powers the IC. AVCC must be connected to V Cc. |
| 4 | REF | $1.25 V$ Reference Voltage Output. Bypass with a 0.22uF ceramic capacitor to GND. |
| 5 | GND | Ground. Connect GND to PGND with a short trace. |
| 6 | $\overline{\text { FLT }}$ | Fault Open-Drain Output. Connect a 100k resistor from FLT to AVCC. <br> FLT is active low during a fault event and is high impedance in shutdown. |
| 7 | FBP | Positive Output-Voltage Feedback Input. Connect a resistor-divider between the positive output and GND <br> with the center to FBP to set the positive output voltage. FBP is high impedance in shutdown. |
| 8 | SEQ | Sequence Logic Input. When SEQ = low, power-on sequence can be independently controlled by ONBST <br> and ONINV. When SEQ = high, the positive output powers up before the negative output. |
| 9 | ONINV | Enable Logic Input. Connect ONINV to AVCC for automatic startup of the inverter, <br> or use ONINV as an independent control of the inverter. |
| 10 | LXP | Positive Output Switching Inductor Node. LXP is high impedance in shutdown. |
| 11 | PGND | Power Ground. Connect PGND to GND with a short trace. |
| 12 | PVP | True-Shutdown Load Disconnect Switch. Connect one side of the inductor to PVP and the other side to LXP. <br> PVP is high impedance in shutdown. |
| 13 | VCC | Power Input Supply. VCC supplies power for the step-up and inverting DC-DC converters. <br> VCc must be connected to AVCC. |
| 14 | LXN | Negative Output Switching Inductor Node. LXN is high impedance in shutdown. <br> - |
| EP | Exposed Pad. Connect exposed pad to ground. |  |

## Functional Diagram



## Detailed Description

The MAX8614A/MAX8614B generate both a positive and negative output voltage by combining a step-up and an inverting DC-DC converter on one IC. Both the step-up converter and the inverter share a common clock. Each output is independently regulated.
Each output is separately controlled by a pulse-widthmodulated (PWM) current-mode regulator. This allows the converters to operate at a fixed frequency $(1 \mathrm{MHz})$ for use in noise-sensitive applications. The 1 MHz switching rate allows for small external components. Both converters are internally compensated and are optimized for fast transient response (see the Load Transient/Voltage Positioning section).

## Step-Up Converter

The step-up converter generates a positive output voltage up to 24 V . An internal power switch, internal True-Shutdown load switch (PVP), and external catch diode allow conversion efficiencies as high as $90 \%$. The internal load switch disconnects the battery from the load by opening the battery connection to the inductor, providing True Shutdown. The internal load switch stays on at all times during normal operation. The load switch is used in the control scheme for the converter and cannot be bypassed.

## Inverter

The inverter generates output voltages down to -16 V below $\mathrm{V}_{\mathrm{CC}}$. An internal power switch and external catch diode allow conversion efficiencies as high as $85 \%$.

## Control Scheme

Both converters use a fixed-frequency, PWM currentmode control scheme. The heart of the current-mode PWM controllers is a comparator that compares the error-amp voltage-feedback signal against the sum of the amplified current-sense signal and a slopecompensation ramp. At the beginning of each clock cycle, the internal power switch turns on until the PWM comparator trips. During this time the current in the inductor ramps up, storing energy in the inductor's magnetic field. When the power switch turns off, the inductor releases the stored energy while the current ramps down, providing current to the output.

## Fault Protection

The MAX8614A/MAX8614B have robust fault and overload protection. After power-up, the device is set to detect an out-of-regulation state that could be caused by an overload or short condition at either output. If either output remains in overload for more than 100 ms , both converters turn off and the FLT flag asserts low. During a short-circuit condition longer than 100 ms on the positive output, foldback current limit protects the output. During a short-circuit condition longer than 100ms on the negative output, both converters turn off and the FLT flag asserts low. The converters then remain off until the device is reinitialized by resetting the controller.
The MAX8614A/MAX8614B also have thermal shutdown. When the device temperature reaches $+170^{\circ} \mathrm{C}$ (typ), the device shuts down. When it cools down by $20^{\circ} \mathrm{C}$ (typ), the converters turn on.

## Enable (ONBST/ONINV)

Applying a high logic-level signal to ONBST/ONINV turns on the converters using the soft-start and pow-er-on sequencing described below. Pulling ONBST/ ONINV low puts the IC in shutdown mode, turning off the internal circuitry. When ONBST/ONINV goes high (or if power is applied with ONBST/ONINV high), the power-on sequence is set by SEQ. In shutdown, the device consumes only $0.1 \mu \mathrm{~A}$ and both output loads are disconnected from the input supply.

## Soft-Start and Inrush Current

The step-up converter and inverter in the MAX8614A/ MAX8614B feature soft-start to limit inrush current and minimize battery loading at startup. This is accomplished by ramping the reference voltage at the input of each error
amplifier. The step-up reference is ramped from 0 to 1 V (where 1 V is the desired feedback voltage for the step-up converter), while the inverter reference is ramped down from 1.25 V to 0 (where 0 is the desired feedback voltage for the inverter).
During startup, the step-up converter True-Shutdown load switch turns on before the step-up-converter reference voltage is ramped up. This effectively limits inrush current peaks to below 500 mA during startup.

## Undervoltage Lockout (UVLO)

The MAX8614A/MAX8614B feature undervoltagelockout (UVLO) circuitry, which prevents circuit operation and MOSFET switching when AVCC is less than the UVLO threshold ( 2.55 V , typ). The UVLO comparator has 25 mV of hysteresis to eliminate chatter due to the source supply output impedance.

## Power-On Sequencing (SEQ)

The MAX8614A/MAX8614B have pin-selectable internally programmed power-on sequencing. This sequencing covers all typical sequencing options required by CCD imagers.
When SEQ $=0$, power-on sequence can be independently controlled by ONINV and ONBST. When SEQ = 0 and ONINV and ONBST are pulled high, both outputs reach regulation simultaneously. The inverter is held off while the step-up True-Shutdown switch slowly turns on to pull PVP to $\mathrm{V}_{\mathrm{CC}}$. The positive output rises to a diode drop below $\mathrm{V}_{\mathrm{CC}}$. Once the step-up output reaches this voltage, the step-up and the inverter then ramp their respective references over a period of 7 ms . This brings the two outputs into regulation at approximately the same time.
When SEQ = 1 and ONBST and ONINV are pulled high, the step-up output powers on first. The inverter is held off until the step-up completes its entire soft-start cycle and the positive output is in regulation. Then the inverter starts its soft-start cycle and achieves regulation in approximately 7 ms .

## True Shutdown

The MAX8614A/MAX8614B completely disconnect the loads from the input when in shutdown mode. In most step-up converters, the external rectifying diode and inductor form a DC current path from the battery to the output. This can drain the battery even in shutdown if a load is connected at the step-up converter output. The MAX8614A/MAX8614B have an internal switch between the input $\mathrm{V}_{\mathrm{CC}}$ and the inductor node, PVP. When this switch turns off in shutdown there is no DC path from the input to the output of the step-up converter. This load disconnect is referred to as "True Shutdown." At the

## Dual-Output (+ and -) DC-DC Converters for CCD

inverter output, load disconnect is implemented by turning off the inverter's internal power switch.

## Current-Limit Select

The MAX8614B allows an inductor current limit of 0.8A on the step-up converter and 0.75 A on the inverter. The MAX8614A allows an inductor current limit of 0.44A on the step-up converter and 0.33 A on the inverter. This allows flexibility in designing for higher loadcurrent applications or for smaller, more compact designs when less power is needed. Note that the currents listed above are peak inductor currents and not output currents. The MAX8614B output current is 50 mA at +15 V and 100 mA at -7.5 V . The MAX8614A output current is 25 mA at +15 V and 50 mA at -7.5 V .

## Load Transient/Voltage Positioning

The MAX8614A/MAX8614B match the load regulation to the voltage droop seen during load transients. This is sometimes called voltage positioning. This results in minimal overshoot when a load is removed and minimal voltage drop during a transition from light load to full load.
The use of voltage positioning allows superior loadtransient response by minimizing the amplitude of overshoot and undershoot in response to load transients. DC-DC converters with high control-loop gains maintain tight DC load regulation, but still allow large voltage drops of $5 \%$ or greater for several hundred microseconds during transients. Load-transient variations are seen only with an oscilloscope (see the Typical Operating Characteristics). Since DC load regulation is read with a voltmeter, it does not show how the power supply reacts to load transients.

## Applications Information

## Adjustable Output Voltage

The positive output voltage is set by connecting FBP to a resistive voltage-divider between the output and GND (Figure 1). Select feedback resistor R2 in the $30 \mathrm{k} \Omega$ to $100 \mathrm{k} \Omega$ range. R 1 is then given by:

$$
\mathrm{R} 1=\mathrm{R} 2\left(\frac{\mathrm{~V}_{\mathrm{BST}}}{\mathrm{~V}_{\mathrm{FBP}}}-1\right)
$$

where $\mathrm{V}_{\mathrm{FBP}}=1.01 \mathrm{~V}$.
The negative output voltage is set by connecting FBN to a resistive voltage-divider between the output and REF (Figure 1). Select feedback resistor R4 in the $30 \mathrm{k} \Omega$ to $100 \mathrm{k} \Omega$ range. R 3 is then given by:

$$
\mathrm{R} 3=\mathrm{R} 4 \times\left(\frac{\mathrm{V}_{\mathrm{FBN}}-\mathrm{V}_{\mathrm{IMV}}}{\mathrm{~V}_{\mathrm{REF}}-\mathrm{V}_{\mathrm{FBN}}}\right)
$$

where $\mathrm{V}_{\mathrm{REF}}=1.25 \mathrm{~V}$ and $\mathrm{V}_{\mathrm{FBN}}=0 \mathrm{~V}$.

## Inductor Selection

The MAX8614A/MAX8614B high switching frequency allows for the use of a small inductor. The $4.7 \mu \mathrm{H}$ and $2.2 \mu \mathrm{H}$ inductors shown in the Typical Operating Circuit is recommended for most applications. Larger inductances reduce the peak inductor current, but may result in skipping pulses at light loads. Smaller inductances require less board space, but may cause greater peak current due to current-sense comparator propagation delay.
Use inductors with a ferrite core or equivalent. Powder iron cores are not recommended for use with high switching frequencies. The inductor's incremental saturation rating must exceed the selected current limit. For highest efficiency, use inductors with a low DC resistance (under $200 \mathrm{~m} \Omega$ ); however, for smallest circuit size, higher resistance is acceptable. See Table 1 for a representative list of inductors and Table 2 for component suppliers.

## Diode Selection

The MAX8614A/MAX8614B high switching frequency demands a high-speed rectifier. Schottky diodes, such as the CMHSH5-2L or MBR0530L, are recommended. Make sure that the diode's peak-current rating exceeds the selected current limit, and that its breakdown voltage exceeds the output voltage. Schottky diodes are preferred due to their low forward voltage. However, ultra-highspeed silicon rectifiers are also acceptable. Table 2 lists component suppliers.

## Capacitor Selection

## Output Filter Capacitor

The primary criterion for selecting the output filter capacitor is low effective series resistance (ESR). The product of the peak inductor current and the output filter capacitor's ESR determines the amplitude of the high-frequency ripple seen on the output voltage. These requirements can be balanced by appropriate selection of the current limit.
For stability, the positive output filter capacitor (C1) should satisfy the following:

$$
\mathrm{C} 1>\left(6 \mathrm{~L} \mathrm{I}_{\mathrm{BSTMAX}}\right) /\left(\mathrm{R}_{\mathrm{CS}} \mathrm{D}+\mathrm{V}_{\mathrm{BST}^{2}}\right)
$$

where $R_{C S}=0.015$ (MAX8614B), and 0.035 (MAX8614A), and $D+$ is 1 minus the step-up switch duty cycle and is:

$$
\mathrm{D}+=\mathrm{V}_{\mathrm{CC}} / \mathrm{V}_{\mathrm{BST}}
$$

Table 1. Inductor Selection Guide

| OUTPUT VOLTAGES AND LOAD CURRENT | INDUCTOR | $\mathrm{L}(\mu \mathrm{H})$ | DCR (m ${ }^{\text {a }}$ ) | $I_{\text {SAT }}(\mathrm{A})$ | SIZE (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 15 \mathrm{~V}, 50 \mathrm{~mA} \\ & -7.5 \mathrm{~V}, 100 \mathrm{~mA} \end{aligned}$ | TOKO DB3018C, 1069AS-2R0 | 2.0 | 72 | 1.4 | $3 \times 3 \times 1.8$ |
|  | TOKO DB3018C, 1069AS-4R3 | 4.3 | 126 | 0.97 | $3 \times 3 \times 1.8$ |
|  | $\begin{array}{\|l\|} \hline \text { TOKO } \\ \text { S1024AS-4R3M } \end{array}$ | 4.3 | 47 | 1.2 | $4 \times 4 \times 1.7$ |
|  | Sumida CDRH2D14-4R7 | 4.7 | 170 | 1 | $3.2 \times 3.2 \times 1.55$ |
|  | $\begin{array}{\|l\|} \hline \text { TOKO } \\ \text { S1024AS-100M } \end{array}$ | 10 | 100 | 0.8 | $4 \times 4 \times 1.7$ |
| $\begin{aligned} & 15 \mathrm{~V}, 20 \mathrm{~mA} \\ & -7.5 \mathrm{~V}, 40 \mathrm{~mA} \end{aligned}$ | Sumida CDRH2D11-100 | 10 | 400 | 0.35 | $3.2 \times 3.2 \times 1.2$ |
|  | Sumida CDRH2D14-100 | 10 | 295 | 0.46 | $3.2 \times 3.2 \times 1.55$ |
|  | Murata LQH32CN100K33 | 10 | 300 | 0.45 | $3.2 \times 2.5 \times 2$ |

## Table 2. Component Suppliers

| SUPPLIER | PHONE | WEBSITE |
| :--- | :---: | :--- |
| INDUCTORS |  | $770-436-1300$ |
| Murata | www.murata.com |  |
| Sumida | $847-545-600$ | www.sumida.com |
| TOKO | $631-435-1110$ | www.centralsemi.com |
| DIODES | www.tokoam.com |  |
| Central <br> Semiconductor <br> (CMHSH5-2L) | $602-303-5454$ | www.motorola.com |
| Motorola <br> (MBR0540L) | CAPACITORS |  |
| Taiyo Yuden | $408-573-4150$ | www.t-yuden.com |
| TDK | $888-835-6646$ | www.TDK.com |

For stability, the inverter output filter capacitor (C2) should satisfy the following:

$$
\begin{gathered}
C 2>\left(6 L V_{\text {REF }} \mathrm{I}_{\text {INVMAX }}\right) / \\
\left(\mathrm{R}_{\mathrm{CS}} \mathrm{D}-\left(\mathrm{V}_{\text {REF }}-\mathrm{V}_{\text {INV }}\right) \mathrm{V}_{\text {INV }}\right)
\end{gathered}
$$

where $R_{C S}=0.0175(\mathrm{MAX} 8614 \mathrm{~B})$, and 0.040 (MAX8614A), and D - is 1 minus the inverter switch duty cycle and is:

$$
\mathrm{D}-=\mathrm{V}_{\mathrm{CC}} / V_{\mathrm{INV}}
$$

Table 2 lists representative low-ESR capacitor suppliers.

## Input Bypass Capacitor

Although the output current of many MAX8614A/ MAX8614B applications may be relatively small, the input must be designed to withstand current transients equal to the inductor current limit. The input bypass capacitor reduces the peak currents drawn from the voltage source, and reduces noise caused by the MAX8614A/MAX8614B switching action. The input source impedance determines the size of the capacitor required at the input. As with the output filter capacitor, a low-ESR capacitor is recommended. A $22 \mu \mathrm{~F}$, low-ESR capacitor is adequate for most applications, although smaller bypass capacitors may also be acceptable with low-impedance sources, or if the source supply is already well filtered. Bypass AVCC separately from $\mathrm{V}_{\mathrm{CC}}$ with a $1.0 \mu \mathrm{~F}$ ceramic capacitor placed as close as possible to the AVCC and GND pins.

## PCB Layout and Routing

Proper PCB layout is essential due to high-current levels and fast-switching waveforms that radiate noise. Breadboards or protoboards should never be used when prototyping switching regulators.


Figure 1. Typical Application Circuit

It is important to connect the GND pin, the input bypass-capacitor ground lead, and the output filtercapacitor ground lead to a single point (star ground configuration) to minimize ground noise and improve regulation. Also, minimize lead lengths to reduce stray capacitance, trace resistance, and radiated noise, with
preference given to the feedback circuit, the ground circuit, and LX_. Place feedback resistors R1-R4 as close as possible to their respective feedback pins. Place the input bypass capacitor as close as possible to AVCC and GND.

MAX8614A/MAX8614B

## Dual-Output (+ and -) DC-DC <br> Converters for CCD

Chip Information
PROCESS: BiCMOS

## Package Information

For the latest package outline information and land patterns (footprints), go to www.maximintegrated.com/packages. Note that a "+", "\#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.

| PACKAGE <br> TYPE | PACKAGE <br> CODE | OUTLINE <br> NO. | LAND <br> PATTERN NO. |
| :---: | :---: | :---: | :---: |
| 14 TDFN | $\mathrm{T} 1433+2$ | $\underline{21-0137}$ | $\underline{90-0063}$ |

## Revision History

| REVISION <br> NUMBER | REVISION <br> DATE | DESCRIPTION | PAGES <br> CHANGED |
| :---: | :---: | :--- | :---: |
| 2 | $6 / 14$ | Added MAX8614ETD/V+ to Ordering Information | 1 |
| 3 | $12 / 19$ | Added EC table for MAX8614BATD/V+ | 3 |

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