

## 13.56 MHz, CLASS-E, 1KW RF Generator using a Microsemi DRF1200 Driver/MOSFET Hybrid

Gui Choi Sr. Application Engineer Phone: 541-382-8028, ext. 1205 <u>gchoi@microsemi.com</u>

The DRF1200/Class-E Reference design is available to expedite the evaluation of the DRF1200 Driver MOSFET hybrid. This Application Note or Reference Design Kit does not represent a finished commercial-ready design. It is only a teaching tool to demonstrate the capability of the DRF1200 under 50 Ohm, flat line condition. Each reference design kit has been verified to perform to the specifications of the application note. The application note contains a parts list, PCB layout and schematic that enables the user to facilitate any repairs resulting beyond its intended use. By purchasing the reference design kit the user takes full responsibility for repair and any modification. No warranties, repair or returns will be accepted.

## The reference design kit contains lethal voltages and high power RF. Use safety precautions.



#### **Contents**

INTRODUCTION DESIGN CONSIDERATIONS OVERALL CONCEPT CIRCUIT DESCRIPTION

- a. RF PULSE GENERATION CIRCUIT
- b. RF OUTPUT MATCHING CIRCUIT
- c. DC SUPPLY

TEST REQUIREMENTS PERFORMANCE (DATA SUMMARY) CONCLUSIONS APPENDIX I (SCHEMATIC) APPENDIX II (PCB LAYOUT) APPENDIX III (PARTS LIST) REFERENCES



### INTRODUCTION

This application note discusses the design procedures and test results for a 13.56MHz, 1KW, CLASS-E generator ideal for ISM applications. To achieve high efficiency and low cost, a Microsemi DRF1200 Driver/MOSFET was selected. The DRF1200 can generate over 1KW of output power and consists of a MOSFET driver, high power MOSFET and internal bypass capacitors in an air cavity flangeless package. The flangeless package was designed to optimize reliability, provide increased flexibility while still providing a low cost solution. A reference design board (DRF1200/CLASS-E) is available for purchase to facilitate the immediate evaluation of the principles of this application note.

To optimize efficiency performance, a CLASS-E RF generator was chosen. It is essential that care is taken to use adequate circuitry, clean PCB layout and good ground connections on the PCB to ensure proper output waveforms.

#### **DESIGN CONSIDERATIONS**

The following issues were considered in the design of a high efficiency, high power RF generator.

- a. CLASS-E operation for high-efficiency.
- b. Adequate output matching circuit. Matching tools were used to achieve the required power and efficiency.
- c. Parts that are capable of handling RF output of 1KW. This includes the bypass capacitor in the DC circuit and selecting a toroidal inductor and capacitors for output matching circuit.
- d. PCB designed for good ground connections, especially for the output matching circuit.
- e. PCB layout optimizing the isolation between power output and input signal generation circuit.

Table 1 shows the output achieved for this RF Power Generator.

Freq	<b>Output Power</b>	Voltage	Current	Efficiency				
13.56Mhz	1KW	320V	3.7A	86%				

 Table 1. Key Specification

#### **OVERALL CONCEPT**

This high efficiency RF power generator uses a DRF1200 to minimize layout parasitics and optimize efficiency for CLASS-D and CLASS-E operation.

a. **RF pulse generator circuit** 

The pulse oscillator and pulse control circuit is designed to create an ISM frequency of 13.56MHz and adjust the pulse width and phase according to circuit power requirements.

#### b. RF output matching circuit

The matching circuit was calculated with a RF matching software tool to maximize power transfer to 50 Ohm load. The circuit was then tuned using the inductor, capacitor and RF choke coil (RFC).

#### CIRCUIT DESCRIPTIONS

a. **RF Pulse Generation** 

The Pulse generation circuit employs 13.56MHz TCXO and Flip Flop IC to adjust Pulse Width from 14nS to 35nS at the signal input of DRF1200. For this application, the pulse width is set at **15nS**. To minimize conductive EMI, it is crucial to use a good ground plane layout with respect to the signal lines.

#### b. **RF Output Matching**

The DRF1200 has a switching speed of 3~4nS, BVds of 1KV and Ids of 13A max. To achieve highefficiency operation, the RF generator uses CLASS-E operation. At full power, the efficiency is approximately 86% at 13.56MHz. The MOSFET output capacitance was considered when tuning the external shunt capacitance to get the desired performance. See DRF1200 data sheet for output capacitance. The RF output matching circuit was designed using a RF matching tool and was optimized to achieve maximize power transfer to 50 Ohm Load. The output matching circuit is a series resistive circuit combined with a reactive circuit consisting of an "L" match Toroidal Inductor and Capacitors in series and shunt to ground.

#### c. DC Supply

The PS HV DC supply input circuit utilizes a RFC and by-pass capacitors to minimize interference with AC signal. The RFC was calculated to be approximately 1K Ohm impedance at 13.56MHz using 30 turns of 20AWG wire. The bypass capacitor should have a minimum 1KV rating.



#### **TEST REQUIREMENTS**



#### b. Hardware and power sequencing requirements

- Cooling requirement: Testing is recommended to be performed using a water cooling system. If not available, should use enough heat sink to maintain continuous testing with sufficient fan capability. A space of approximately 2.5 inches or higher between the fans and the bench floor should be allowed so that air flow is not impeded.
- Sequential steps for Turn-On/Turn Off of Power Supplies.
  - 1. Turn on Driver power supply PS\_1 (14V via JP1).
  - 2. Then, turn on MOSFET supply (PS\_2) and slowly increase to 40V (via JP2).
  - 3. While monitoring the RF power from power meter and output waveform of the Drain, ramp up MOSFET power supply (PS\_2) to the values per Table 2 making sure that output is stable for each supply voltage before proceeding to the next higher voltage.
  - 4. To turn-off, turn power supplies off in the reverse order.
- If RF output waveform, Vds and/or RF power level from power meter fluctuate, immediately shut down of PS\_2 for safety and determine fault before resuming test.



#### PERFORMANCE

a. Data summary

No\Para.	PS HV (V)	Id (A)	Pin (W)	Pout (W)	H (%)	Vds (V)
1	100	1.1	110.00	104	94.5	276
2	110	1.19	130.90	124	94.7	
3	120	1.3	156.00	149	95.5	
4	130	1.4	182.00	175	96.2	
5	140	1.51	211.40	204	96.5	
6	150	1.63	244.50	235	96.1	
7	160	1.75	280.00	268	95.7	
8	170	1.87	317.90	303	95.3	
9	180	2	360.00	342	95.0	
10	190	2.13	404.70	383	94.6	
11	200	2.25	450.00	424	94.2	576
12	210	2.4	504.00	472	93.7	
13	220	2.52	554.40	515	92.9	
14	230	2.66	611.80	564	92.2	
15	240	2.8	672.00	615	91.5	
16	250	2.95	737.50	669	90.7	
17	260	3.09	803.40	723	90.0	
18	270	3.23	872.10	775	88.9	
19	280	3.38	946.40	830	87.7	
20	290	3.52	1,020.80	882	86.4	
21	300	3.66	1,098.00	940	85.6	
22	320	3.7	1,155.00	1000	86.1	925

**Table 2.** Power Sequencing Data Summary

Table 2 shows the effects of varying the PS HV on MOSFET current, RF power, efficiency, and peak Vds. Efficiency vs. Pout is shown in Figure 2 and peak Vds vs. PS HV is shown in Figure 3. The efficiency is calculated using RF power output and DC input power of the power MOSFET. Efficiency remains higher than 94% up to RF power of 500W and 90% up to 800W. At RF output power of 1KW, the efficiency is reduced slightly to approximately 86%.

Figure 3 shows that the peak drain voltage (Vds) is approximately 3 times the PS HV voltage. This is close to the ideal value of 3.5 times PS HV voltage.

Figure 4 shows that the peak Vds is 276V when the PS HV voltage is 100V. Figure 5 shows that a peak Vds of 576V is achieved with a PS HV voltage setting of 200V. Figure 6 shows that a peak Vds of 876V is achieved with a PS HV voltage setting of 300V.



#### b. Chart of data sheet



Figure 2. Efficiency vs. Pout



Figure 3. Vds vs. HV



#### c. Waveform at MOSFET Drain for various settings of the HV PS









Figure 6. Peak VDS (PS HV = 300V)

#### CONCLUSIONS

This application note is for a reference design using a DRF1200 as a CLASS-E RF generator. The high performance DRF1200 Hybrid was used because it includes both the driver, Power MOSFET, and bypass capacitors optimized to reduce inductance and achieve a single low-cost solution. A reference design board is available to demonstrate this high efficiency, 1KW, 13.56MHz RF generator with 86% efficiency using a drain supply voltage up to 320Vdc.

The critical aspects such as the layout of components for efficient power generation, testing, and air cooling requirements are also discussed.

#### **Test Setup**

It is highly recommended that a Common Mode Choke (CMC) is used on all power and measurement inputs and outputs. This approach provides the best stability and the most accurate measurements.

Construction of CMC's are illustrated below. The CMC on the left should be used for PS 1 and the PS 2 inputs. These lines are tightly twisted pairs (5-8 twists per inch). The CMC on the right should be used for the Scope Probe Cable. Three to five turns on each is sufficient. The CMC's should be placed as close to the DRF1200/CLASS-E Board as practical. **Bench test pictures are included where Fair-Rite part number 0431164181 has been used in three places for power supply isolation.** 









Figure 7. Overall schematic



## **Appendix II. PCB Layout**

PCB size: 3.5W \* 7.5L in inch PCB: FR-4, 65mil T



Figure 8. PCB Layout



#### **Appendix III. Parts List** Supplier **Supplier PN** Manufacture Part ID Description Size Manuf. PN Microsemi U1 **RF MOSFET Hybrid** тзв Microsemi **DRF1200 DRF1200** C1 10uF/35V 1812 Digi-key pcc2183ct-nd 140-XRL16V10-RC 10uF/16V 5\*11 Mouser 140-XRL16V10-RC Xicon C2 0805 .47uF/50V Digi-key 490-3328-1-ND GRM21BR71H474KA88L C3 .47uF/50V 0805 Digi-key 490-3328-1-ND GRM21BR71H474KA88L C4 .47uF/50V 0805 490-3328-1-ND GRM21BR71H474KA88L C5 Digi-key 100pF/50V 0805 Digi-key PCC101CGCT-ND C6 C7 1.0uF/50V 0805 Digi-key 587-1438-1-ND Taiyo Yuden GMK212BJ105KG-T C8 4.7uF35V 6032-28 Digi-key 478-1717-1-ND C9 0.1uF 0805 Taiyo Yuden UMK212B7104KG-T C10 1.0uF/50V 0805 Digi-key 587-1438-1-ND Taiyo Yuden GMK212BJ105KG-T C11 4.7uF35V 6032-28 478-1717-1-ND Digi-key C13 0.01uF/1KV Cer. Disc Newark 18M6914 Newark C14 0.01uF/1KV 18M6914 Cer. Disc C15 0.01uF/1KV Cer. Disc Newark 18M6914 C16 0.01uF/1KV Cer. Disc Newark 18M6914 C17 NC. C18 NC 47PF/2500V 3838 ATC 700C470JW2500X ATC 700C470JW2500X C19 3838 C20 82PF/2500V 700C820JW2500X ATC 700C820JW2500X ATC C21 220PF/3600V 3838 ATC 100E221KW3600X ATC 100E221KW36ooX 270PF/3600V ATC 100E271KW3600X ATC 100E271KW36ooX C22 3838 10~220pF C23 3838 ATC 100E Series 220PF/3600V 3838 ATC 100E221KW3600X ATC 100E221KW36ooX C24 220PF/3600V C25 3838 ATC 100E221KW3600X ATC 100E221KW36ooX 510ohm/1/8W 0805 Digi-key P510ATR-ND Panasonic ERJ-6GEYJ511V R1 0805 R2 100ohm 1/8W RЗ 3.30hm 1/8W 0805 Digi-key P3.3ACT-ND Panasonic ERJ-6GEYJ3R3V R4 3.30hm 1/8W 0805 Digi-key P3.3ACT-ND Panasonic ERJ-6GEYJ3R3V P1.00KCCT-ND R5 1.0K ohm 1/8W 0805 Digi-key Panasonic ERJ-ENF1001V 0805 1.0K ohm 1/8W Digi-key P1.00KCCT-ND ERJ-ENF1001V R6 Panasonic 51.1ohm 1/8W R7 0805 Digi-key P51.1CCT-ND Panasonic ERJ-6ENF51R1V R8 511ohm 1/8W 0805 Digi-key P511CCT-ND Panasonic ERJ-6ENF5110V R9 1ohm 1/2W Axial Digi-key P1.0BBCT-ND Panasonic ERD-S1TJ1ROV R10 1ohm 1/2W Digi-key P1.0BBCT-ND Panasonic ERD-S1TJ1ROV Axial 1ohm 1/2W Digi-key P1.0BBCT-ND ERD-S1TJ1ROV R11 Axial Panasonic <u>Digi-key</u> P1.0BBCT-ND R12 1ohm 1/2W Axial Panasonic ERD-S1TJ1R0V Digi-key 3292W-501-ND POT 500ohm Bourns SM:3269W-1 501 VR1 3/8" sq VR2 POT 500ohm 3/8" sq Digi-key 3292W-501-ND Bourns SM:3269W-1 501 D1 LED, green 5mm Digi-key P375-ND Panasonic LN31GPH 30V/300mA SOT23 MMBD301LT1GOSCT-ND On Semi. MMBD301LT1G D2 Digi-key J1 RFout port Newark 12M4398 161V504E Bomar DC Terminal Allied 839-0309 8191 JP1 Keystone JP2 DC Terminal Allied 839-0309 Keystone 8191 мсм 18PE 1/4LB Inductor w/ 2T Newark 05H7486 L12643540302 AWG18 Fair-Rite 2643540302 Fair-Rite Inductor w/ 20T Newark 05H7486 MCM 18PE 1/4LB L2 AWG18 T106-2 Micrometals T106-1 Micrometals Toroid Inductor Micrometals T225-6 5 --- 2ea Micrometals T225-6 5 L3 5T 12AWG Mouser 602-289-100 Alpha 289 2643540302 Toroid Inductor Allied Elec. Fair-Rite 2643540302 L4 Diq<u>ikey</u> 2T 18AWG A5857R-100-ND Alpha 5857 RD005

#### References

13.56 MHz Osc

Dual Flip-Flop IC

U2

UЗ

• Solid State Radio Engineering - Herbert L. Krauss and Charles W. Bostian

Allied Elec.

Digi-key

Half

14SOP

 Application Note: Simple and Inexpensive High Efficiency Power Amp using New APT MOSFET – Kenneth Dierberger 1994

EP1100HSTSC-13.56M

296-13131-1-ND

Ecliptek Co

ΤĪ

• Application Note: PRF-1150 1KW 13.56MHz Class E RF Generator Evaluation Module - Matthew W. Vanis

EP1100HSTSC-13.560M

SN74ACT74NSR

# **X-ON Electronics**

Largest Supplier of Electrical and Electronic Components

Click to view similar products for Sub-GHz Development Tools category:

Click to view products by Microchip manufacturer:

Other Similar products are found below :

EVAL-ADF7021DBJZ EVAL-ADF7021-NDBZ2 EVAL-ADF7021-VDB3Z EVAL-ADF7023DB3Z MICRF219A-433 EV MICRF220-433 EV AD6679-500EBZ EVAL-ADF7901EBZ EVAL-ADF790XEBZ 110976-HMC453QS16G STEVAL-IKR002V7D MAX2602EVKIT+ MAX1472EVKIT-315 MAX1479EVKIT-315 STEVAL-IKR002V3D MAX7042EVKIT-315+ MAX2902EVKIT# MAX9947EVKIT+ MAX1470EVKIT-315 SKY66188-11-EK1 SKY66013-11-EVB EVAL-ADF7023DB5Z DRF1200/CLASS-E 1096 1098 MDEV-900-PRO DVK-SFUS-1-GEVK DVK-SFUS-API-1-GEVK US-SIGFOX-GEVB STEVAL-IKR002V2D 107755-HMC454ST89 DM182017-2 110961-HMC453ST89 DM182017-1 SX1272MB2DAS 3179 DC689A DC1513B-AB 3229 3230 3231 3232 DC963B DC1250A-AA DC1513B-AC DC1513B-AD DC1513B-AA TEL0075 131903-HMC921LP4E EU-SIGFOX-GEVB