# Positive Doubling Charge Pumps with Shutdown in a SOT-23 Package 

## Features

- Charge Pumps in 6-Pin SOT-23A Package
- >99\% Typical Voltage Conversion Efficiency
- Voltage Doubling
- Input Voltage Range, TC1240: +2.5 V to +4.0 V ,

TC1240A: +2.5 V to +5.5 V

- Low Output Resistance, TC1240: $17 \Omega$ (Typical)

TC1240A: $12 \Omega$ (Typical)

- Only Two External Capacitors Required
- Low Supply Current, TC1240: $180 \mu \mathrm{~A}$ (Typical)

TC1240A: $550 \mu \mathrm{~A}$ (Typical)

- Power-Saving Shutdown Mode ( $1 \mu \mathrm{~A}$ Maximum)
- Shutdown Input Fully Compatible with 1.8V Logic Systems


## Applications

- Cellular Phones
- Pagers
- PDAs, Portable Data Loggers
- Battery Powered Devices
- Handheld Instruments


## Package Type

## 6-Pin SOT-23A



NOTE: 6-Pin SOT-23A is equivalent to the EIAJ (SC-74A)

## General Description

The TC1240/TC1240A is a doubling CMOS charge pump voltage converter in a small 6-Pin SOT-23A package. The TC1240 doubles an input voltage that can range from +2.5 V to +4.0 V , while the TC1240A doubles an input voltage that can range from +2.5 V to +5.5 V . Conversion efficiency is typically $>99 \%$. Internal oscillator frequency is 160 kHz for both devices. The TC1240 and TC1240A have an active-high shutdown that limits the current consumption of the devices to less than $1 \mu \mathrm{~A}$.

External component requirement is only two capacitors for standard voltage doubler applications. All other circuitry (including control, oscillator and power MOSFETs) are integrated on-chip. Typical supply current is $180 \mu \mathrm{~A}$ for the TC1240 and $550 \mu \mathrm{~A}$ for the TC1240A. Both devices are available in a 6-Pin SOT23A surface mount package.

Typical Application Circuit


### 1.0 ELECTRICAL CHARACTERISTICS

| Absolute Maximum Ratings † |
| :---: |
| Input Voltage ( $\mathrm{V}_{\text {IN }}$ to GND) |
| TC1240 ....................................... +4.5V, -0.3 |
| TC1240A...................................... $+5.8 \mathrm{~V},-0.3 \mathrm{~V}$ |
| Output Voltage ( $\mathrm{V}_{\text {OUT }}$ to GND) |
| $\begin{aligned} & \text { TC1240 ................................................................................... } \mathrm{V}_{\text {IN }}-0.3 \mathrm{~V} \\ & \text { TC1240A }-0.3 \mathrm{~V} \end{aligned}$ |
|  |  |
|  |
| Short-Circuit Duration: $\mathrm{V}_{\text {OUT }}$ to GND ............Indefinite |
| Thermal Resistance ................................... $210^{\circ} \mathrm{C} / \mathrm{W}$ |
| Power Dissipation ( $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ ).................... 600 mW |
| Operating Temperature Range............ $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Storage Temperature (Unbiased) ....... $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |

$\dagger$ Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions above those indicated in the operation sections of the specifications is not implied. Exposure to Absolute Maximum Rating conditions for extended periods may affect device reliability.

## TC1240 ELECTRICAL SPECIFICATIONS

Electrical Specifications: Unless otherwise noted, typical values apply at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$. Minimum and maximum values apply for $\mathrm{T}_{\mathrm{A}}=-40^{\circ}$ to $+85^{\circ} \mathrm{C}$, and $\mathrm{V}_{\text {IN }}=+2.8 \mathrm{~V}, \mathrm{C}_{1}=\mathrm{C}_{2}=3.3 \mu \mathrm{~F}$, SHDN $=$ GND.

| Parameters | Sym | Min | Typ | Max | Units | Conditions |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| Supply Current | $\mathrm{I}_{\mathrm{DD}}$ | - | 180 | 300 | $\mu \mathrm{~A}$ | $\mathrm{R}_{\mathrm{LOAD}}=\infty$ |
| Shutdown Supply Current | $\mathrm{I}_{\mathrm{SHDN}}$ | - | 0.1 | 1.0 | $\mu \mathrm{~A}$ | $\mathrm{SHDN}=\mathrm{V}_{\mathrm{IN}}$ |
| Minimum Supply Voltage | $\mathrm{V}_{\mathrm{MIN}}$ | 2.5 | - | - | V | $\mathrm{R}_{\mathrm{LOAD}}=1.0 \mathrm{k} \Omega$ |
| Maximum Supply Voltage | $\mathrm{V}_{\mathrm{MAX}}$ | - | - | 4.0 | V | $\mathrm{R}_{\mathrm{LOAD}}=1.0 \mathrm{k} \Omega$ |
| Oscillator Frequency | $\mathrm{F}_{\mathrm{OSC}}$ | - | 160 | - | kHz | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Switching Frequency (Note 1) | $\mathrm{F}_{\mathrm{SW}}$ | 40 | 80 | 125 | kHz | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Shutdown Input Logic High | $\mathrm{V}_{\mathrm{IH}}$ | 1.4 | - | - | V | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\mathrm{MIN}}$ to $\mathrm{V}_{\mathrm{MAX}}$ |
| Shutdown Input Logic Low | $\mathrm{V}_{\mathrm{IL}}$ | - | - | 0.4 | V | $\mathrm{~V}_{\text {IN }}=\mathrm{V}_{\mathrm{MIN}}$ to $\mathrm{V}_{\mathrm{MAX}}$ |
| Power Efficiency | $\mathrm{P}_{\mathrm{EFF}}$ | 86 | 93 | - | $\%$ | $\mathrm{R}_{\mathrm{LOAD}}=1.0 \mathrm{k} \Omega$ |
| Voltage Conversion Efficiency | $\mathrm{V}_{\mathrm{EFF}}$ | 97.5 | 99.96 | - | $\%$ | $\mathrm{R}_{\mathrm{LOAD}}=\infty$ |
| Output Resistance (Note 2) | $\mathrm{R}_{\mathrm{OUT}}$ | - | 17 | - | $\Omega$ | $\mathrm{R}_{\mathrm{LOAD}}=1.0 \mathrm{k} \Omega$ |
|  |  | - | - | 30 |  | $\mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |

Note 1: Switching frequency is one-half internal oscillator frequency.
2: Capacitor contribution is approximately $26 \%$ of the output impedance [ESR = 1 / switching frequency $x$ capacitance].

## TC1240A ELECTRICAL SPECIFICATIONS

Electrical Specifications: Unless otherwise noted, typical values apply at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$. Minimum and maximum values apply for $\mathrm{T}_{\mathrm{A}}=-40^{\circ}$ to $+85^{\circ} \mathrm{C}$, and $\mathrm{V}_{\mathrm{IN}}=+5.0 \mathrm{~V}, \mathrm{C}_{1}=\mathrm{C}_{2}=3.3 \mu \mathrm{~F}, \mathrm{SHDN}=\mathrm{GND}$.

| Parameters | Sym | Min | Typ | Max | Units | Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supply Current | $\mathrm{I}_{\mathrm{DD}}$ | - | 550 | 900 | $\mu \mathrm{A}$ | $\mathrm{R}_{\text {LOAD }}=\infty$ |
| Shutdown Supply Current | $\mathrm{I}_{\text {SHDN }}$ | - | 0.01 | 1.0 | $\mu \mathrm{A}$ | SHDN $=\mathrm{V}_{\text {IN }}$ |
| Minimum Supply Voltage | $\mathrm{V}_{\text {MIN }}$ | 2.5 | - | - | V |  |
| Maximum Supply Voltage | $\mathrm{V}_{\text {MAX }}$ | - | - | 5.5 | V |  |
| Output Current | $\mathrm{I}_{\text {LOAD }}$ | 20 | - | - | mA |  |
| Sum of the $\mathrm{R}_{\mathrm{DS}(\mathrm{ON})}$ of the internal MOSFET Switches | $\mathrm{R}_{\text {SW }}$ | - | 4 | 8 | $\Omega$ | $\mathrm{I}_{\text {LOAD }}=20 \mathrm{~mA}$ |
| Oscillator Frequency | $\mathrm{F}_{\text {OSC }}$ | - | 160 | - | kHz | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Switching Frequency (Note 1) | $\mathrm{F}_{\text {SW }}$ | 40 | 80 | 125 | kHz | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Shutdown Input Logic High | $\mathrm{V}_{\mathrm{IH}}$ | 1.4 | - | - | V | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {MIN }}$ to $\mathrm{V}_{\text {MAX }}$ |
| Shutdown Input Logic Low | $\mathrm{V}_{\text {IL }}$ | - | - | 0.4 | V | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {MIN }}$ to $\mathrm{V}_{\text {MAX }}$ |
| Power Efficiency | $\mathrm{P}_{\text {EFF }}$ | 86 | 94 | - | \% | $\mathrm{I}_{\text {LOAD }}=5 \mathrm{~mA}$ |
| Voltage Conversion Efficiency | $\mathrm{V}_{\text {EFF }}$ | 99 | 99.96 | - | \% | $\mathrm{R}_{\text {LOAD }}=\infty$ |
| Output Resistance (Note 2) | $\mathrm{R}_{\text {OUT }}$ | - | 12 | $\overline{25}$ | $\Omega$ | $\begin{aligned} & \mathrm{I}_{\text {LOAD }}=20 \mu \mathrm{~A} \\ & \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C} \text { to }+85^{\circ} \mathrm{C} \end{aligned}$ |

Note 1: Switching frequency is one-half internal oscillator frequency.
2: Capacitor contribution is approximately $26 \%$ of the output impedance [ESR = 1 / switching frequency $x$ capacitance].

## TC1240/TC1240A

### 2.0 TYPICAL PERFORMANCE CURVES

Note: The graphs and tables provided following this note are a statistical summary based on a limited number of samples and are provided for informational purposes only. The performance characteristics listed herein are not tested or guaranteed. In some graphs or tables, the data presented may be outside the specified operating range (e.g., outside specified power supply range) and therefore outside the warranted range.

Note: Unless otherwise indicated, typical values apply at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.


FIGURE 2-1: Supply Current vs. Supply Voltage (No Load).


FIGURE 2-2:
Output Source Resistance vs. Supply Voltage (with $R_{\text {LOAD }}=1 \mathrm{k} \Omega$ )


FIGURE 2-3: Output Voltage Drop vs. Load Current.


FIGURE 2-4: Supply Current vs. Temperature (No Load).


FIGURE 2-5: Output Source Resistance vs. Temperature (with $R_{\text {LOAD }}=1 \mathrm{k} \Omega$ ).


FIGURE 2-6: Power Efficiency vs. Load
Current.

Note: Unless otherwise indicated, typical values apply at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.


FIGURE 2-7: Switching Frequency vs.
Temperature.

## TC1240/TC1240A

### 3.0 PIN DESCRIPTION

The description of the pins are listed in Table 3-1.
TABLE 3-1: PIN FUNCTION TABLE

| Pin No. | Symbol | Description |
| :---: | :---: | :--- |
| 1 | $\mathrm{~V}_{\text {IN }}$ | Power supply input |
| 2 | GND | Ground |
| 3 | C- | Commutation capacitor negative terminal |
| 4 | SHDN | Shutdown input (active high) |
| 5 | $\mathrm{~V}_{\text {OUT }}$ | Doubled output voltage |
| 6 | C+ | Commutation capacitor positive terminal |

### 4.0 DETAILED DESCRIPTION

The TC1240/TC1240A charge pump converter doubles the voltage applied to the $\mathrm{V}_{\text {IN }}$ pin. Conversion consists of a two-phase operation (Figure 4-1). During the first phase, switches $S_{2}$ and $S_{4}$ are open and $S_{1}$ and $S_{3}$ are closed. During this time, $\mathrm{C}_{1}$ charges to the voltage on $\mathrm{V}_{\text {IN }}$ and load current is supplied from $\mathrm{C}_{2}$. During the second phase, $S_{2}$ and $S_{4}$ are closed, while $S_{1}$ and $S_{3}$ are open.
During this second phase, $\mathrm{C}_{1}$ is level-shifted upward by $\mathrm{V}_{\text {IN }}$ volts. This connects $\mathrm{C}_{1}$ to the reservoir capacitor $\mathrm{C}_{2}$, allowing energy to be delivered to the output as needed. The actual voltage is slightly lower than $2 \times V_{\text {IN }}$ since the four switches $\left(\mathrm{S}_{1}-\mathrm{S}_{4}\right)$ have an on-resistance and the load drains charge from reservoir capacitor $\mathrm{C}_{2}$.


FIGURE 4-1: Ideal Switched Capacitor Charge Pump Doubler.

### 5.0 TYPICAL APPLICATIONS

### 5.1 Output Voltage Considerations

The TC1240/TC1240A performs voltage doubling but does not provide regulation. The output voltage will droop in a linear manner with respect to load current. The value of this equivalent output resistance is approximately $12 \Omega$ nominal at $+25^{\circ} \mathrm{C}$ and $\mathrm{V}_{\mathrm{IN}}=+5.0 \mathrm{~V}$ for the TC1240A and $17 \Omega$ nominal at $+25^{\circ} \mathrm{C}$ and $\mathrm{V}_{\text {IN }}=+2.8 \mathrm{~V}$ for the TC1240. $\mathrm{V}_{\text {OUT }}$ is approximately +10.0 V at light loads for the TC1240A and +5.6 V for the TC1240, and droops according to the equation below:

## EQUATION

$$
\begin{gathered}
V_{\text {DROOP }}=I_{O U T} \times R_{\text {OUT }} \\
V_{O U T}=2 \times V_{I N}-V_{\text {DROOP }}
\end{gathered}
$$

### 5.2 Charge Pump Efficiency

The overall power efficiency of the charge pump is affected by four factors:

1. Losses from power consumed by the internal oscillator, switch drive, etc. (which vary with input voltage, temperature and oscillator frequency).
2. $I^{2} R$ losses due to the on-resistance of the MOSFET switches on-board the charge pump.
3. Charge pump capacitor losses due to effective series resistance (ESR).
4. Losses that occur during charge transfer (from commutation capacitor to the output capacitor) when a voltage difference between the two capacitors exist.
Most of the conversion losses are due to factors (2) and (3) above. These losses are given by Equation 5-1.

## EQUATION 5-1:

a) $P_{\text {LOSS( } 2,3)}=I_{O U T}^{2} \times R_{\text {OUT }}$
b) $R_{\text {OUT }}=\left[\frac{1}{F_{S W}\left(C_{1}\right)}\right]+8 R_{\text {SWITCH }}+4 E S R_{C 1}+E S R_{C 2}$

## TC1240/TC1240A

The switching frequency in Equation $5-1 \mathrm{~b}$ is defined as one-half the oscillator frequency (i.e., $\mathrm{F}_{\mathrm{SW}}=\mathrm{F}_{\mathrm{OSC}} / 2$ ). The $1 /\left(F_{S W}\right)\left(C_{1}\right)$ term in Equation $5-1 b$ is the effective output resistance of an ideal switched capacitor circuit (Figure 5-1 and Figure 5-2).

The output voltage ripple is given by Equation 5-2.
EQUATION 5-2:

$$
V_{R I P P L E}=\frac{I_{O U T}}{2\left(F_{S W}\right)\left(C_{2}\right)}+2\left(I_{O U T}\right)\left(E S R_{C 2}\right)
$$



FIGURE 5-1: Ideal Switched Capacitor Model.


FIGURE 5-2: Equivalent Output
Resistance.

### 5.3 Capacitor Selection

In order to maintain the lowest output resistance and output ripple voltage, it is recommended that low ESR capacitors be used. Additionally, larger values of $C_{1}$ will lower the output resistance and larger values of $C_{2}$ will reduce output ripple (see Equation 5-1b).
Table 5-1 shows various values of $\mathrm{C}_{1}$ and the corresponding output resistance values @ $+25^{\circ} \mathrm{C}$. It assumes a $0.1 \Omega \mathrm{ESR}_{\mathrm{C} 1}$ and $0.9 \Omega \mathrm{R}_{\mathrm{Sw}}$. Table 5-2 shows the output voltage ripple for various values of $\mathrm{C}_{2}$. The $\mathrm{V}_{\text {RIPPLE }}$ values assume 5 mA output load current and $0.1 \Omega \mathrm{ESR}_{\mathrm{C} 2}$.

TABLE 5-1: OUTPUT RESISTANCE
VS. $C_{1}(E S R=0.1 \Omega)$

| $\mathbf{C}_{\mathbf{1}}(\boldsymbol{\mu F})$ | $\mathbf{T C 1 2 4 0}$ <br> $\mathbf{R}_{\mathbf{O U T}}(\Omega)$ | $\mathbf{T C 1 2 4 0 A}$ <br> $\mathbf{R}_{\mathbf{O U T}}(\Omega)$ |
| :---: | :---: | :---: |
| 0.47 | 47 | 35 |
| 1 | 28.5 | 20.5 |
| 2.2 | 19.5 | 14 |
| 3.3 | 17 | 12 |
| 4.7 | 15.5 | 10.5 |
| 10 | 13.6 | 9.3 |
| 47 | 12.5 | 8.3 |
| 100 | 12.2 | 8.1 |

TABLE 5-2: OUTPUT VOLTAGE RIPPLE VS. $C_{2}(E S R=0.1 \Omega)$
lout 5 mA

| $\mathbf{C}_{\mathbf{1}}(\boldsymbol{\mu F})$ | TC1240/TC1240A <br> $\mathbf{V}_{\text {RIPPLE }}(\mathbf{m V})$ |
| :---: | :---: |
| 0.47 | 142 |
| 1 | 67 |
| 2.2 | 30 |
| 3.3 | 20 |
| 4.7 | 14 |
| 10 | 6.7 |
| 47 | 2.5 |
| 100 | 1.6 |

### 5.4 Input Supply Bypassing

The $\mathrm{V}_{\mathrm{IN}}$ input should be capacitively bypassed to reduce AC impedance and minimize noise effects due to the switching internal to the device. The recommended capacitor should be a large value (at least equal to $\mathrm{C}_{1}$ ) connected from the input to GND.

### 5.5 Shutdown Input

The TC1240 and TC1240A are disabled when SHDN is high, and enabled when SHDN is low. This input cannot be allowed to float.


FIGURE 5-3: Test Circuit.

### 5.6 Voltage Doubler

The most common application for charge pump devices is the doubler (Figure 5-3). This application uses two external capacitors $-\mathrm{C}_{1}$ and $\mathrm{C}_{2}$ (plus a power supply bypass capacitor, if necessary). The output is equal to $2 \times V_{\text {IN }}$ minus any voltage drops due to loading. Refer to Table 5-1 and Table 5-2 for capacitor selection.

### 5.7 Cascading Devices

Two or more TC1240/TC1240As can be cascaded to increase output voltage (Figure 5-4). If the output is lightly loaded, it will be close to $\left((\mathrm{n}+1) \times \mathrm{V}_{\mathrm{IN}}\right)$, but will droop at least by $R_{\text {Out }}$ of the first device multiplied by the $\mathrm{I}_{\mathrm{Q}}$ of the second. It can be seen that the output resistance rises rapidly for multiple cascaded devices. For the case of the two-stage 'tripler', output resistance can be approximated as $\mathrm{R}_{\text {OUT }}=2 \times \mathrm{R}_{\text {OUT1 }}+\mathrm{R}_{\text {OUT2 }}$, where $\mathrm{R}_{\text {OUT1 }}$ is the output resistance of the first stage and $R_{\text {OUT2 }}$ is the output resistance of the second stage.

### 5.8 Paralleling Devices

To reduce the value of $\mathrm{R}_{\text {OUT }}$, multiple TC1240/ TC1240As can be connected in parallel (Figure 5-5). The output resistance will be reduced by a factor of $N$, where N is the number of TC1240/TC1240As. Each device will require its own pump capacitor (C1x), but all devices may share one reservoir capacitor (C2). However, to preserve ripple performance, the value of C2 should be scaled according to the number of paralled TC1240/TC1240As, respectively.

### 5.9 Layout Considerations

As with any switching power supply circuit good layout practice is recommended. Mount components as close together as possible to minimize stray inductance and capacitance. Also use a large ground plane to minimize noise leakage into other circuitry.


FIGURE 5-4: Cascading Multiple Devices To Increase Output Voltage.


FIGURE 5-5: $\quad$ Paralleling Multiple Devices To Reduce Output Resistance.

### 6.0 PACKAGING INFORMATION

### 6.1 Package Marking Information



| Device | Code |
| :--- | :---: |
| TC1240 | DN |
| TC1240A | EN |

ex: 1240AECH =(E) $\mathbb{N} \bigcirc \bigcirc$
(3) represents year and 2-month code
(4) represents production lot ID code

## TC1240/TC1240A

## 6-Lead Plastic Small Outline Transistor (CH) (SOT-23)

Note: For the most current package drawings, please see the Microchip Packaging Specification located at http://www.microchip.com/packaging


| Units |  | INCHES* |  |  | MILLIMETERS |  |  |
| :--- | :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Dimension Limits | MIN | NOM | MAX | MIN | NOM | MAX |  |
| Number of Pins | n |  | 6 |  |  | 6 |  |
| Pitch | p |  | .038 |  |  | 0.95 |  |
| Outside lead pitch (basic) | p 1 |  | .075 |  |  | 1.90 |  |
| Overall Height | A | .035 | .046 | .057 | 0.90 | 1.18 | 1.45 |
| Molded Package Thickness | A 2 | .035 | .043 | .051 | 0.90 | 1.10 | 1.30 |
| Standoff | A 1 | .000 | .003 | .006 | 0.00 | 0.08 | 0.15 |
| Overall Width | E | .102 | .110 | .118 | 2.60 | 2.80 | 3.00 |
| Molded Package Width | E 1 | .059 | .064 | .069 | 1.50 | 1.63 | 1.75 |
| Overall Length | D | .110 | .116 | .122 | 2.80 | 2.95 | 3.10 |
| Foot Length | L | .014 | .018 | .022 | 0.35 | 0.45 | 0.55 |
| Foot Angle | $\phi$ | 0 | 5 | 10 | 0 | 5 | 10 |
| Lead Thickness | C | .004 | .006 | .008 | 0.09 | 0.15 | 0.20 |
| Lead Width | B | .014 | .017 | .020 | 0.35 | 0.43 | 0.50 |
| Mold Draft Angle Top | $\alpha$ | 0 | 5 | 10 | 0 | 5 | 10 |
| Mold Draft Angle Bottom | $\beta$ | 0 | 5 | 10 | 0 | 5 | 10 |
| *Controlling Parameter |  |  |  |  |  |  |  |

## *Controlling Parameter

Notes:
Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed .005 " 0.127 mm ) per side.

JEITA (formerly EIAJ) equivalent: SC-74A
Drawing No. C04-120

## TC1240/TC1240A

### 7.0 REVISION HISTORY

Revision D (December 2012)
Added a note to each package outline drawing.

## TC1240/TC1240A

NOTES:

## PRODUCT IDENTIFICATION SYSTEM



## Sales and Support

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Data Sheets
Products supported by a preliminary Data Sheet may have an errata sheet describing minor operational differences and
recommended workarounds. To determine if an errata sheet exists for a particular device, please contact one of the following:
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```


## TC1240/TC1240A

NOTES:

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