

# **MPM3840**

2.8V-5.5V, 4A, Power Module, Synchronous Step-Down Converter with Integrated Inductor

# DESCRIPTION

The MPM3840 is a DC/DC module that includes a monolithic, step-down, switch-mode converter with built-in, internal power MOSFETs and an inductor. The MPM3840 can provide 4A of continuous output current from a 2.8V to 5.5V input voltage with excellent load and line regulation. The MPM3840 is ideal for powering portable equipment that run on a single-cell Lithium-ion (Li+) battery. The output voltage can be regulated as low as 0.6V. Only input capacitors, output capacitors, and feedback (FB) resistors are required to complete the design.

The constant-on-time (COT) control scheme provides a fast transient response, high light-load efficiency, and easy loop stabilization.

Full protection features include cycle-by-cycle current limiting and thermal shutdown.

The MPM3840 requires a minimal number of readily available, standard, external components and is available in an ultra-small QFN-20 (3mmx5mmx1.6mm) package.

# FEATURES

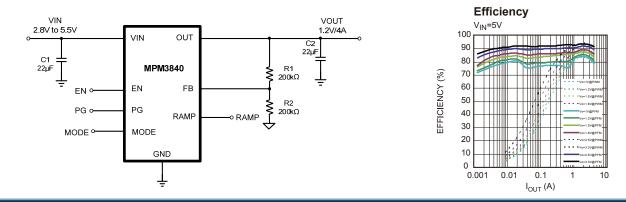
- >80% Light-Load Efficiency
- Low I<sub>Q</sub>: 40µA
- Wide 2.8V to 5.5V Operating Input Range
- Output Voltage as Low as 0.6V
- 100% Duty Cycle in Dropout
- 4A Output Current
- $25m\Omega$  and  $12m\Omega$  Internal Power MOSFETs
- 1.2MHz Frequency
- External Mode Control
- External Mode Control (PWM.PFM) and Dynamic Analog Voltage
- EN and Power Good for Power Sequencing
- Cycle-by-Cycle Over-Current Protection (OCP)
- 1.5ms Internal Soft-Start Time with Pre-Biased Start-Up
- Short-Circuit Protection (SCP) with Hiccup Mode
- Thermal Shutdown
- Stable with Low ESR Output Ceramic Capacitors
- Available in a QFN-20 (3mmx5mmx1.6mm) Package

# **APPLICATIONS**

- Networking/Servers
- Space-Constraint Applications
- Industrial Products
- Low-Voltage I/O System Power

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# **TYPICAL APPLICATION**



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### **ORDERING INFORMATION**

Part Number*	Package	Top Marking
MPM3840GQV	QFN-20 (3mmx5mmx1.6mm)	See Below

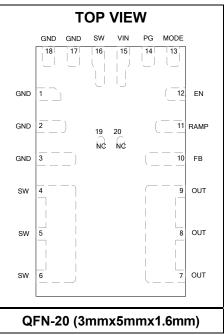
\* For Tape & Reel, add suffix -Z (e.g. MPM3840GQV-Z)

# **TOP MARKING**

MPYW
3840
LLL
М

MP: MPS prefix Y: Year code W: Week code 3840: First four digits of the part number LLL: Lot number M: Module

# PACKAGE REFERENCE





# ABSOLUTE MAXIMUM RATINGS (1)

Supply voltage (VIN)	6V
V <sub>SW</sub> 0	0.3V (-5V for <10ns) to
	6V (10V for <10ns)
All other pins	0.3V to 6V
Junction temperature	150°C
Lead temperature	260°C
Continuous power dissipa	tion (T <sub>A</sub> = +25°C) <sup>(2)</sup>
Storage temperature	65°C to +150°C

#### **Recommended Operating Conditions** <sup>(3)</sup>

Supply voltage (VIN)	2.8V to 5.5V
Operating junction temp. $(T_J)$ .	40°C to +125°C

Thermal Resistance  $^{(4)}$   $\theta_{JA}$   $\theta_{JC}$ 

QFN-20 (3mmx5mmx1.6mm)... 46.... 10... °C/W

#### NOTES:

- 1) Exceeding these ratings may damage the device.
- 2) The maximum allowable power dissipation is a function of the maximum junction temperature  $T_J$  (MAX), the junction-toambient thermal resistance  $\theta_{JA}$ , and the ambient temperature  $T_A$ . The maximum allowable continuous power dissipation at any ambient temperature is calculated by  $P_D$  (MAX) = ( $T_J$  (MAX)- $T_A$ )/ $\theta_{JA}$ . Exceeding the maximum allowable power dissipation produces an excessive die temperature, causing the regulator to go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- The device is not guaranteed to function outside of its operating conditions.
- 4) Measured on JESD51-7, 4-layer PCB.



# **ELECTRICAL CHARACTERISTICS**

 $V_{IN}$  = 3.6V,  $V_{OUT}$  = 1.2V,  $T_J$  = -40°C to +125°C, typical value is tested at  $T_J$  = +25°C. The limit over temperature is guaranteed by characterization, unless otherwise noted.

Parameter	Symbol	Condition	Min	Тур	Max	Units
Feedback voltage	V <sub>FB</sub>	$2.8V \le V_{IN} \le 5.5V$	0.594	0.600	0.606	V
Feedback current	I <sub>FB</sub>	V <sub>FB</sub> = 0.65V		50		nA
P-FET switch on resistance	R <sub>DSON P</sub>			25		mΩ
N-FET switch on resistance	R <sub>DSON N</sub>			12		mΩ
Dropout resistance	R <sub>DR</sub>	100% on duty		47		mΩ
Switch leakage		T <sub>J</sub> = 25°C		0	1	μA
P-FET peak current limit			4.5	5.5	6.5	А
N-FET valley current limit				4		А
		T <sub>J</sub> = 25°C	216	070	324	
On time		T <sub>J</sub> = -40°C to 85°C	202	270	338	ns
Switching frequency	f <sub>s</sub>	V <sub>OUT</sub> = 1.2V		1200		kHz
Minimum off time	T <sub>MIN-OFF</sub>			60		ns
Minimum on time <sup>(5)</sup>	T <sub>MIN-On</sub>			50		ns
Soft-start time	T <sub>SS-ON</sub>			1.5		ms
PG UV threshold rising	PGTH_Hi			0.9		VFB
PG UV threshold falling	PGTH_Lo			0.85		VFB
PG OV threshold rising	PGTH_Hi			1.15		VFB
PG OV threshold falling	PGTH_Lo			1.1		VFB
Power good delay				140		μs
Power good sink current capability	V <sub>PG LO</sub>	Sink 1mA			0.4	V
Power good logic-high voltage	V <sub>PG HI</sub>	V <sub>IN</sub> = 5V, V <sub>FB</sub> = 0.6V	4.9			V
Power good internal pull-up resistor	R <sub>PG</sub>			500		kΩ
Under-voltage lockout threshold rising			2.4	2.55	2.7	V
Under-voltage lockout threshold hysteresis				300		mV
EN input logic-low voltage					0.4	V
EN input logic-high voltage			1.2			V
		V <sub>EN</sub> = 2V		2		μA
EN input current		V <sub>EN</sub> = 0V		0		μA
Supply current (shutdown)		$V_{EN} = 0V, T_{J} = 25^{\circ}C$		0.1	1	μA
Supply current (quiescent)		V <sub>IN</sub> = 3.6V, V <sub>EN</sub> = 2V, V <sub>FB</sub> = 0.65V, T <sub>J</sub> = 25°C		40	60	μA
Thermal shutdown <sup>(5)</sup>				150		°C
Thermal hysteresis <sup>(5)</sup>				20		°C
Inductor L value				0.47		μH
Inductor DC resistance				22		mΩ

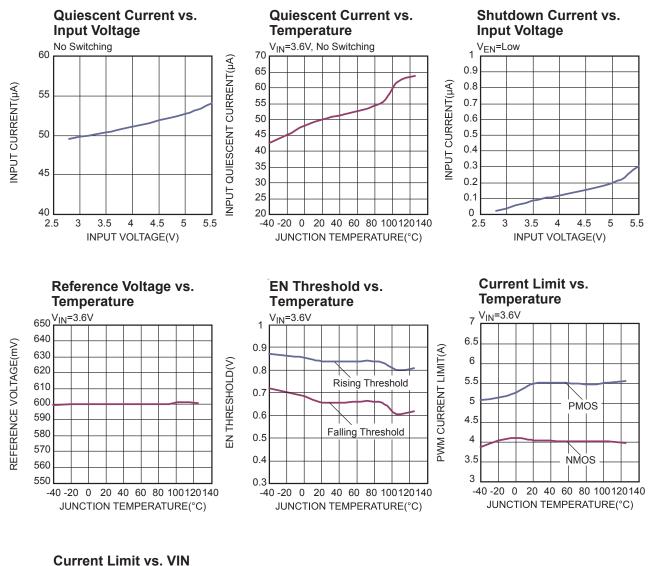
NOTE:

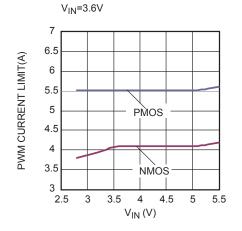
5) Guaranteed by design.



# **TYPICAL PERFORMANCE CHARACTERISTICS**

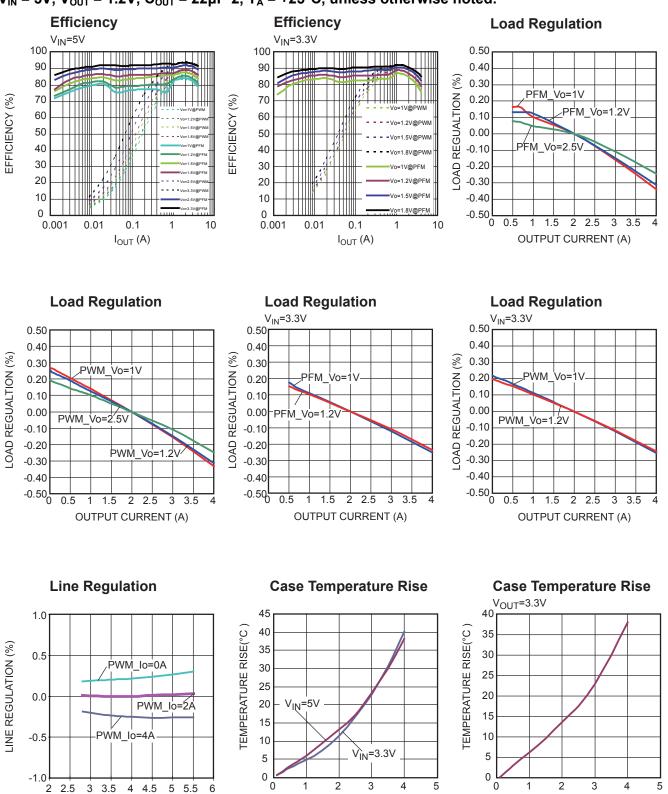
 $V_{IN}$  = 5V,  $V_{OUT}$  = 1.2V,  $C_{OUT}$  = 22µF\*2,  $T_A$  = +25°C, unless otherwise noted.







 $V_{IN} = 5V$ ,  $V_{OUT} = 1.2V$ ,  $C_{OUT} = 22\mu F^{*}2$ ,  $T_A = +25^{\circ}C$ , unless otherwise noted.



**INPUT VOLTAGE (V)** 

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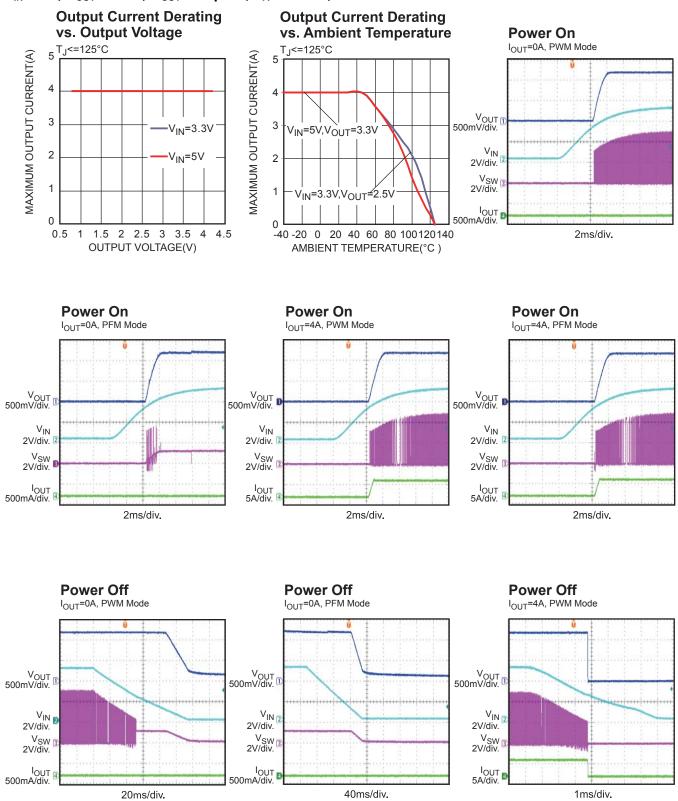
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 $I_{OUT}(A)$ 

 $I_{OUT}(A)$ 



 $V_{IN} = 5V$ ,  $V_{OUT} = 1.2V$ ,  $C_{OUT} = 22\mu F^*2$ ,  $T_A = +25^{\circ}C$ , unless otherwise noted.





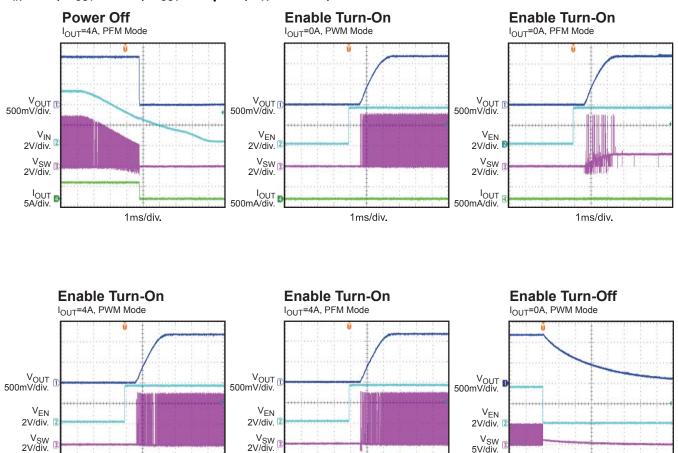
I<sub>OUT</sub> 500mA/div.

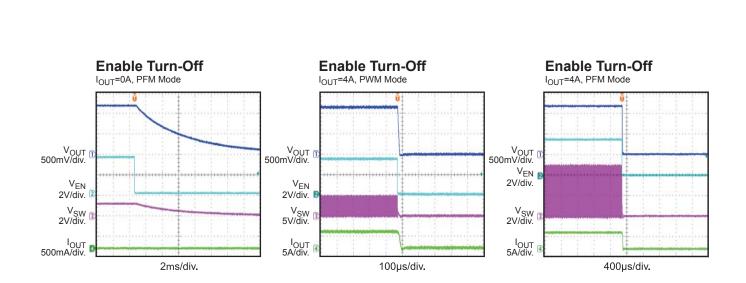
2ms/div.

# **TYPICAL PERFORMANCE CHARACTERISTICS** (continued)

 $V_{IN} = 5V$ ,  $V_{OUT} = 1.2V$ ,  $C_{OUT} = 22\mu F^*2$ ,  $T_A = +25^{\circ}C$ , unless otherwise noted.

I<sub>OUT</sub> 5A/div.





1ms/div.

MPM3840 Rev. 1.1 3/10/2017

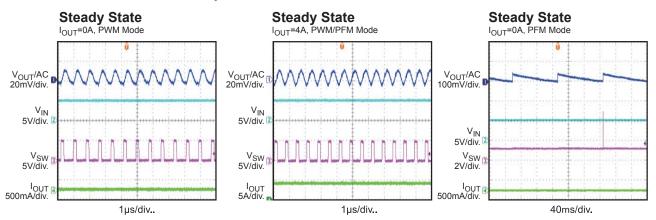
I<sub>OUT</sub> 5A/div.

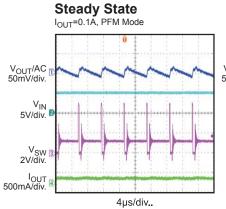
1ms/div.

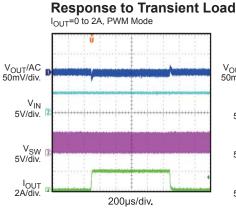
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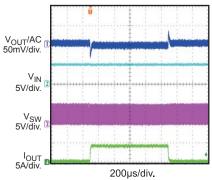
 $V_{IN} = 5V$ ,  $V_{OUT} = 1.2V$ ,  $C_{OUT} = 22\mu F^*2$ ,  $T_A = +25^{\circ}C$ , unless otherwise noted.

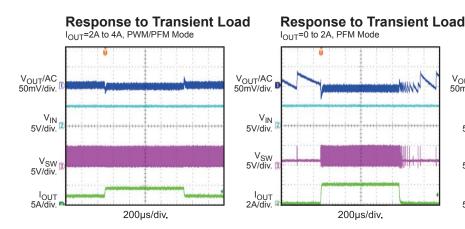




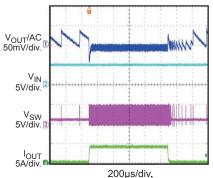


Response to Transient Load



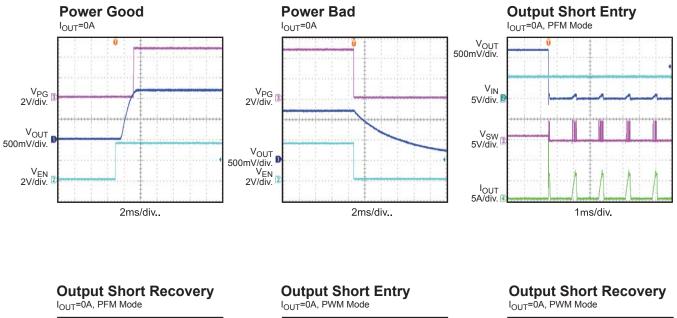


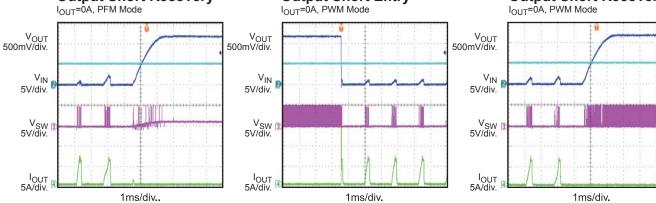
# Response to Transient Load





 $V_{IN} = 5V$ ,  $V_{OUT} = 1.2V$ ,  $C_{OUT} = 22\mu F^*2$ ,  $T_A = +25^{\circ}C$ , unless otherwise noted.







# **PIN FUNCTIONS**

Pin #	Name	Description
1, 2, 3, 17, 18	GND	<b>IC ground.</b> Connect the GND pins to larger copper areas to the negative terminals of the input and output capacitors.
4, 5, 6, 16	SW	<b>Switch node.</b> Connect SW to the inductor. SW also connects to the internal high-side and low-side power MOSFET switches.
7, 8, 9	OUT	Output voltage sense.
10	FB	<b>Feedback.</b> An external resistor divider from the output to GND tapped to FB sets the output voltage.
11	RAMP	<b>External ramp.</b> RAMP sets the ramp to optimize transient performance. Connect a ceramic capacitor (10pF to 47pF) between OUT and RAMP to improve transient performance.
12	EN	<b>Enable.</b> Set EN to a high voltage level to enable the MPM3840. For automatic start- up, connect EN to VIN with a pull-up resistor.
13	MODE	Multi-use pin.MODE is also denoted as $V_{CON.}$ For PWM and PFM selection: When $V_{MODE}$ is more than 1.2V, the MPM3840 entersPWM, and the internal reference is 0.6V. When $V_{MODE}$ is lower than 0.4V or isfloating, the MPM3840 enters PFM.For analog voltage dynamic regulation: When $V_{MODE}$ is between 0.6V and 1.1V, thereference voltage can be controlled by $V_{MODE}$ , and the MPM3840 works in PWM.Avoid setting $V_{MODE}$ between 0.4V and 0.6V as the MPM3840 may operate in an unknown mode.
14	PG	<b>Power good.</b> PG has an internal, $500k\Omega$ , pull-up resistor. PG is pulled up to VIN when the FB voltage is within 10% of the regulation level; otherwise, PG is low. There is a 140µs delay between the moment when V <sub>FB</sub> reaches the PG threshold and when PG goes high.
15	VIN	<b>Input supply.</b> VIN requires a decoupling capacitor to ground to reduce switching spikes.
19, 20	NC	Do not connect. NC must be left floating.



# **BLOCK DIAGRAM**

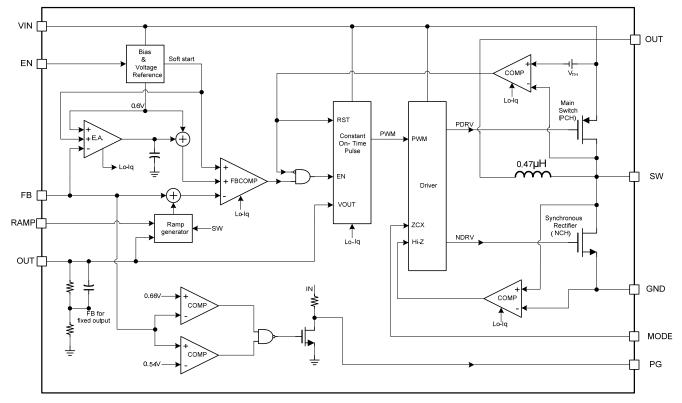


Figure 1: Functional Block Diagram



# **OPERATION**

The MPM3840 uses a constant-on-time (COT) control with input voltage feed-forward to stabilize the switching frequency over the full input range. At light load, the MPM3840 employs a proprietary control of low-side switching and inductor current on the switching node to improve efficiency. The module has an integrated inductor that makes the schematic and layout design very simple. Only input capacitors, output capacitors, and FB resistors are required to complete the design.

#### **Constant-On-Time (COT) Control**

Compared to fixed-frequency PWM control, constant-on-time (COT) control offers a simpler control loop and faster transient response. By using an input voltage feed-forward, the MPM3840 maintains a nearly constant switching frequency across the input and output voltage ranges. The switching pulse on time can be estimated with Equation (1):

$$t_{\rm ON} = \frac{V_{\rm OUT}}{V_{\rm IN}} \cdot 0.83\mu s \tag{1}$$

To prevent inductor current runaway during the load transient, the MPM3840 has a constant minimum off-time of 60ns. This minimum off time limit will not affect operation in steady state in any way.

#### **Light-Load Operation**

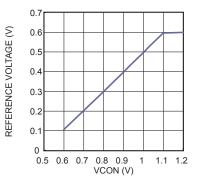
During light loads, the MPM3840 uses a proprietary control scheme to save power and improve efficiency. A zero-current cross detection (ZCD) circuit is used to detect when the inductor current starts to reverse. The lowside MOSFET (LS-FET) turns off immediately when the inductor current starts to reverse and triggers ZCD in discontinuous conduction mode (DCM) operation. Considering the internal circuit propagation time, the typical delay is 50ns. This means that the inductor current continues falling after the ZCD is triggered in this delay time. If the inductor current falling slew rate is fast (V<sub>OUT</sub> is high or close to VIN), the LS-FET is turned off, and the inductor current may be negative. This prevents the MPM3840 from entering DCM operation. For example, if VIN is 3.6V, and  $V_{OUT}$  is 3.3V, then the off time in CCM is 70ns. It is difficult to enter DCM at light load.

#### Enable (EN)

When the input voltage is greater than the under-voltage lockout (UVLO) threshold (typically 2.55V), the MPM3840 can be enabled by pulling EN higher than 1.2V. Leave EN floating or pull EN down to ground to disable the MPM3840. There is an internal  $1M\Omega$  resistor from EN to ground.

# MODE Selection and Analog Voltage Dynamic Regulation

The MPM3840 has programmable pulse-width modulation (PWM) and pulse-frequency modulation (PFM) work modes. When the voltage on MODE ( $V_{MODE}$ ) is higher than 1.2V, the MPM3840 operates in PWM. When  $V_{MODE}$  is lower than 0.4V or is floating, the MPM3840 operates in PFM, which can achieve high efficiency in light-load condition. PWM mode can maintain a constant switching frequency and small  $V_{OUT}$  ripple, but has low efficiency at light load.



#### Figure 2: Reference Voltage Change with VCON

The MPM3840 can regulate the output voltage by dynamically changing the MODE voltage ( $V_{CON}$ ) to meet a situation where the output voltage must be adjusted directly. When  $V_{CON}$  is an appropriate value (0.6V to 1.1V), the MPM3840 works in PWM, and the internal reference voltage changes smoothly as  $V_{CON}$ changes to provide a new output voltage without changing the external resistor divider. When the  $V_{CON}$  function is enabled, set the reference voltage ( $V_{ref}$ ) to be from 0.35V to 0.6V. The accuracy is typically 3%. When setting the  $V_{ref}$  value from 0.1V to 0.35V, the accuracy is



typically 10%. The detailed  $V_{Ref}$  curve is shown in Figure 2. Calculate  $V_{ref}$  with Equation (2):

 $Ref(V)=0.985 \times VCON(V)-0.486$  (2)

#### Soft Start (SS)

The MPM3840 has a built-in soft start (SS) that ramps up the output voltage at a constant slew rate to avoid overshooting at start-up. The softstart time is about 1.5ms, typically.

#### **Pre-Bias Start-Up**

The MPM3840 can start up with a pre-biased output voltage. If the internal SS voltage is lower than the FB voltage, the HS-FET and LS-FET remain off until the SS voltage crosses the FB voltage.

#### Power Good (PG) Indicator

The MPM3840 has an open drain with a  $500k\Omega$  pull-up resistor as a power good (PG) indicator.

PG is pulled up to VIN when the FB voltage is within 10% of the regulation level; otherwise, PG is low. There is a 140 $\mu$ s delay between the moment when V<sub>FB</sub> reaches the PG threshold and when PG goes high. The MOSFET has a maximum R<sub>DS(ON)</sub> of 100 $\Omega$ .

#### **Current Limit**

The MPM3840 has a 5.5A current limit for the HS-FET. When the HS-FET reaches its current limit, the MPM3840 enters hiccup mode until the current drops to prevent the inductor current from rising and damaging the components.

#### Short Circuit and Recovery

The MPM3840 enters short-circuit protection (SCP) mode when it reaches the current limit and attempts to recover with hiccup mode. The MPM3840 disables the output power stage, discharges the soft-start capacitor, and attempts to soft start. If the short-circuit condition remains after the soft start ends, the MPM3840 repeats this operation until the short circuit is removed and the output rises back to regulation levels.



# **APPLICATION INFORMATION**

#### Setting the Output Voltage

The external resistor divider sets the output voltage (see the Typical Application Circuit on page 17). Select the feedback resistor (R1) to reduce  $V_{OUT}$  leakage current, typically between  $40k\Omega$  to  $200k\Omega$ . There is no strict requirement on the feedback resistor. R1 >  $10k\Omega$  is reasonable for most applications. R2 can be calculated with Equation (2):

$$R2 = \frac{R1}{\frac{V_{out}}{0.6} - 1}$$
 (2)

The feedback circuit is shown in Figure 3.

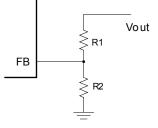


Figure 3: Feedback Network

Table 1 lists the recommended resistor values for common output voltages.

Table 1: Resistor Values for Common OutputVoltages

0				
V <sub>OUT</sub> (V)	R1 (kΩ)	R2 (kΩ)		
1.0	200 (1%)	300 (1%)		
1.2	200 (1%)	200 (1%)		
1.8	200 (1%)	100 (1%)		
2.5	200 (1%)	63.2 (1%)		
3.3	200 (1%)	44.2 (1%)		

#### Selecting the Input Capacitor

The input current to the step-down converter is discontinuous and therefore requires а capacitor to supply AC current to the step-down converter while maintaining the DC input voltage. Use low ESR capacitors for the best performance. Ceramic capacitors with X5R or X7R dielectrics are highly recommended because of their low ESR values and small temperature coefficients. For most applications, a 22µF capacitor is sufficient. For higher output voltages, a 47µF capacitor may be needed to improve system stability.

Since the input capacitor absorbs the input switching current, it requires an adequate ripple current rating. The RMS current in the input capacitor can be estimated with Equation (3):

$$I_{C1} = I_{LOAD} \times \sqrt{\frac{V_{OUT}}{V_{IN}}} \sqrt{\frac{1 - \frac{V_{OUT}}{V_{IN}}}{V_{IN}}}$$
(3)

The worst-case condition occurs at VIN =  $2V_{OUT}$ , shown in Equation (4):

$$I_{C1} = \frac{I_{LOAD}}{2}$$
(4)

For simplification, choose an input capacitor with an RMS current rating greater than half of the maximum load current.

The input capacitor can be electrolytic, tantalum, or ceramic. When using electrolytic or tantalum capacitors, use a small, high-quality,  $0.1\mu$ F, ceramic capacitor placed as close to the IC as possible. When using ceramic capacitors, ensure that they have enough capacitance to prevent excessive voltage ripple at the input. The input voltage ripple caused by the capacitance can be estimated with Equation (5):

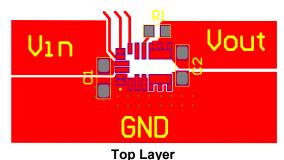
$$\Delta V_{\rm IN} = \frac{I_{\rm LOAD}}{f_{\rm S} \times C1} \times \frac{V_{\rm OUT}}{V_{\rm IN}} \times \left(1 - \frac{V_{\rm OUT}}{V_{\rm IN}}\right)$$
(5)

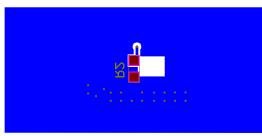


#### **PCB Layout Guidelines**

Efficient PCB layout of the switching power supplies is critical for stable operation. Especially considering the high-switching converter, if the layout is not done carefully, the regulator could show poor performance. For best results, refer to Figure 3 and follow the guidelines below.

- 1. Place the input capacitor as close to VIN and GND as possible.
- 2. Place the FB resistor very close to FB and GND. Ensure that the trace is not wide.
- 3. Place the output capacitor close to chip.
- 4. Make the VIN, VOUT, and GND traces wide enough to carry a high current.
- 5. Places several vias on the GND copper for better thermal performance.





Bottom Layer Figure 3: Recommended PCB Layout

#### **Design Example**

Table 2 is a design example following the application guidelines for the specifications below.

Table 2: Design Exan	mple
----------------------	------

V <sub>IN</sub>	2.8V - 5.5V
V <sub>OUT</sub>	1.2V
Ι <sub>ουτ</sub>	0A - 4A

The detailed application schematic is shown in Figure 4. The typical performance and circuit waveforms are shown in the Typical Performance Characteristics section. For more device applications, please refer to the related evaluation board datasheets.



# **TYPICAL APPLICATION CIRCUIT**

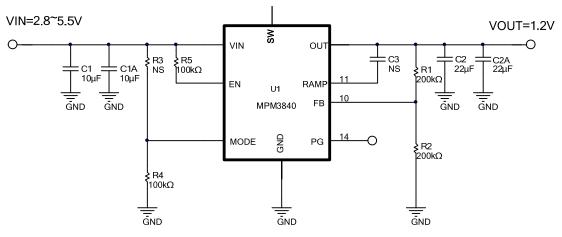
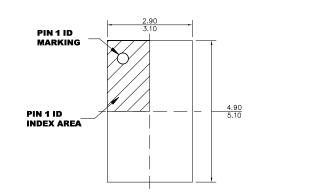


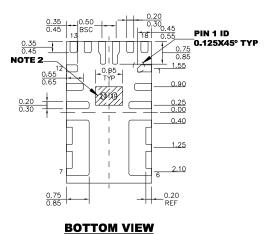
Figure 4: Application for 1.2V Output



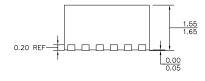
# PACKAGE INFORMATION

QFN-20 (3mmx5mmx1.6mm)

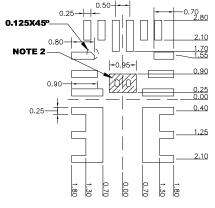




TOP VIEW



SIDE VIEW



#### **RECOMMENDED LAND PATTERN**

#### NOTE:

 ALL DIMENSIONS ARE IN MILLIMETERS.
SHADED AREA IS THE KEEP-OUT ZONE. ANY PCB METAL TRACE AND VIA ARE NOT ALLOWED TO CONNECT TO THIS AREA ELECTRICALLY OR MECHANICALLY.
EXPOSED PADDLE SIZE DOES NOT INCLUDE MOLD FLASH.
LEAD COPLANARITY SHALL BE 0.10 MILLIMETERS MAX.
JEDEC REFERENCE IS MO-220.
DRAWING IS NOT TO SCALE.

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