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August 2014

# FAN21SV04 — TinyBuck<sup>™</sup> 4 A, 24 V Single-Input Integrated Synchronous Buck Regulator

### Features

- Single-Supply Operation with 4 A Output Current
- Wide Input Range with Dual Supply: 3.0 V to 24 V
- Wide Output Voltage Range: 0.8 V to 80% V<sub>IN</sub>
- Over 94% Peak Efficiency
- 1% Reference Accuracy Over Temperature
- Fully Synchronous Operation with Integrated Schottky Diode on Low-Side MOSFET Boosts Efficiency
- Single Supply Device for V<sub>IN</sub> > 6.5 V 24 V
- Programmable Frequency Operation (200-600 KHz)
- Synchronizable to External Clock with Master/Slave Provisions
- Power-Good Signal
- Accepts Ceramic Capacitors on Output
- External Compensation for Flexible Design
- Starts on Pre-Bias Outputs
- Integrated Bootstrap Diode
- Programmable Over-Current Protection
- Under-Voltage, Over-Voltage, and Thermal-Shutdown Protections
- 5 x 6 mm, 25-Pin, 3-Pad MLP Package

### **Applications**

- Servers & Telecom
- Graphics Cards & Displays
- Computing Systems
- Set-Top Boxes & Game Consoles
- Point-of-Load Regulation

### Description

The FAN21SV04 TinyBuck<sup>™</sup> is a highly efficient, small-footprint, programmable-frequency, 4 A, integrated synchronous buck regulator.

FAN21SV04 contains both synchronous MOSFETs and a controller/driver with optimized interconnects in one package, which enables designers to solve highcurrent requirements in a small area with minimal external components, thereby reducing cost. Onboard internal 5 V regulator enables single-supply operation for input voltages >6.5 V.

The FAN21SV04 can be configured to drive multiple slave devices OR synchronize to an external system clock. In slave mode, FAN21SV04 may be set up to be free-running in the absence of a master clock signal.

External compensation, programmable switching frequency, and current-limit features allow for design optimization and flexibility. High-frequency operation allows for all-ceramic solutions.

Fairchild's advanced BiCMOS power process, combined with low- $R_{DS(ON)}$  internal MOSFETs and a thermally efficient MLP package, provide the ability to dissipate high power in a small package. Integration helps minimize critical inductances, making layout simpler and more efficient compared to discrete solutions.

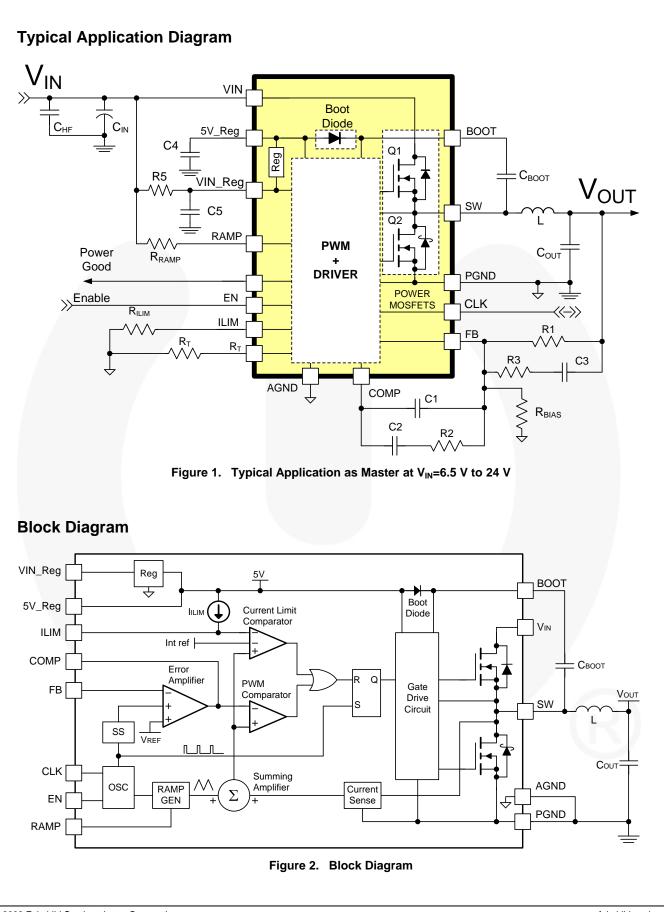
Output over-voltage, under-voltage, over-current, and thermal-shutdown protections help protect the device from damage during fault conditions. FAN21SV04 prevents pre-biased output discharge during startup in point-of-load applications.

### **Related Resources**

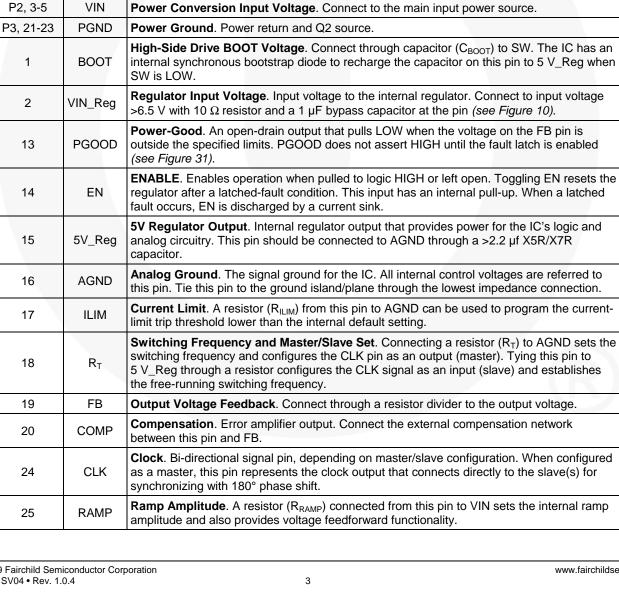
- <u>TinyCalc™ Calculator Design Tool</u>
- AN-8022 TinyCalc™ Calculator User Guide

### **Ordering Information**

Part Number	Operating Temperature Range	Package	Packing Method
FAN21SV04MPX	-10°C to 85°C	Maldad Laadlaas Daakaga (MLD) 5 x 6 mm	Tapa and Daal
FAN21SV04EMPX	-40°C to 85°C	Molded Leadless Package (MLP) 5 x 6 mm	Tape and Reel



FAN21SV04 — TinyBuck™ 4 A, 24 V Single-Input Integrated Synchronous Buck Regulator



٨N

1 2 3 3 5

P3 PGND

 19

 15

 14

 15

AGND LIM R m

Figure 3. MLP 5 x 6 mm Pin Configuration (Bottom View)

Switching Node. Junction of high-side and low-side MOSFETs.

5V\_Reg

Z

P2 VIN

RAMP

CLK

PGND

PGND

PGND

22

24

VIN VIN SW SW

678

P1 SW

sw

sw

sw

sw

2

-GOOD

### **Pin Configuration**

Pad / Pin Definitions

Name

SW

Description

Pad / Pin

P1, 6-12

### **Absolute Maximum Ratings**

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.

Parameter	Conditions			Max.	Units
VIN, VIN_Reg to AGND	AGND=PGND			28	V
5V_Reg to AGND	AGND=PGND			6	V
BOOT to PGND				35	V
BOOT to SW			-0.5	6.0	V
	Continuous		-0.5	24.0	V
SW to PGND	Transient (t < 20 ns, f < 600 Kl	Hz)	-5	30	V
All other pins			-0.3	6.0	V
505	Electrostatic Discharge	Human Body Model, JESD22-A114	1.5		
ESD	Protection Level	Charged Device Model, JESD22-C101	2.5		kV

### **Recommended Operating Conditions**

The Recommended Operating Conditions table defines the conditions for actual device operation. Recommended operating conditions are specified to ensure optimal performance to the datasheet specifications. Fairchild does not recommend exceeding them or designing to Absolute Maximum Ratings.

Symbol	Parameter	Conditions	Min.	Тур.	Max	Units
f <sub>SW</sub>	Switching Frequency		200	500	600	KHz
V <sub>IN,</sub> VIN_Reg	Supply Voltage for Power and Bias	VIN to PGND	3.0		24.0	V
VIN_Reg	Supply voltage for Fower and bias	VIN_Reg to AGND	6.5		24.0	
т	Ambient Temperature	FAN21SV04MPX	-10		+85	°C
T <sub>A</sub>	Ambient Temperature	FAN21SV04EMPX	-40		+85	
TJ	Junction Temperature				+125	°C

### **Thermal Information**

Symbol	Parameter		Min.	Тур.	Max.	Units
T <sub>STG</sub>	Storage Temperature		-65		+150	°C
TL	Lead Soldering Temperature, 30 Seconds				+300	°C
		P1 (Q2)		4		
$\theta_{\text{JC}}$	Thermal Resistance: Junction-to-Case	P2 (Q1)		7		°C/W
		P3		4		
$\theta_{J-PCB}$	Thermal Resistance: Junction-to-Mounting Surface <sup>(1)</sup>			35		°C/W
P <sub>D</sub>	Total Power Dissipation in the package, $T_A=25^{\circ}C^{(1)}$				2.8	W

Note:

1. Typical thermal resistance when mounted on a four-layer, two-ounce PCB, as shown in Figure 38. Actual results are dependent upon mounting method and surface related to the design.

### **Electrical Characteristics**

Recommended operating conditions and using the circuit shown in Figure 1, with  $V_{IN}$ , VIN\_Reg=12 V, unless otherwise noted.

Parameter	Conditions	Min.	Тур.	Max.	Units	
Power Supplies						
Operating Current (VIN+VIN_Reg)	V <sub>IN</sub> =12 V, 5V_Reg Open, CLK Open, f <sub>SW</sub> =500 KHz, No Load		22	30	mA	
VIN_Reg Operating Current	EN=High, 5 V_Reg Open, CLK Open, f <sub>SW</sub> =500 KHz		11		mA	
VIN_Reg Quiescent Current	EN=High, FB=0.9 V		4	5	mA	
VIN_Reg Standby Current	EN=0, V <sub>IN</sub> =12 V			1	mA	
5V_Reg Output Voltage	Internal V <sub>CC</sub> Regulator, No Load, 6.5 V <vin_reg<24 td="" v<=""><td>4.7</td><td>5.0</td><td>5.3</td><td>V</td></vin_reg<24>	4.7	5.0	5.3	V	
5V_Reg Max. Current Load	VIN_Reg=12 V			5	mA	
	Rising V <sub>IN</sub> , V <sub>IN</sub> =VIN_Reg		5.6	6.3	V	
VIN_Reg UVLO Threshold	Falling V <sub>IN</sub> , V <sub>IN</sub> =VIN_Reg			5	V	
Reference						
Reference Voltage measured	FAN21SV04MPX, T <sub>A</sub> =25°C	794	800	806		
at FB (See Figure 4 for Temperature Coefficient)	FAN21SV04EMPX, T <sub>A</sub> =25°C	795	800	805	mV	
Oscillator					0	
_	$R_T$ =50 k $\Omega$ to GND (Master Mode)	255	300	345		
Frequency	$R_T=24 \text{ k}\Omega$ to GND (Master Mode)	540	600	660	KHz	
Frequency in Slave Mode Compared to Master Mode	$R_T$ =24 kΩ to 50 kΩ to 5 V_Reg (Slave Mode) -15			+15	%	
Minimum On Time <sup>(2)</sup>			40	65	ns	
Duty Cycle	V <sub>IN</sub> =6.5 V, f <sub>SW</sub> =600 KHz		80	85	%	
Ramp Amplitude, Peak–to-Peak <sup>(2)</sup>	V <sub>IN</sub> =16 V, 1.8 V <sub>OUT</sub> , R <sub>T</sub> =30 kΩ, R <sub>RAMP</sub> =200 kΩ		0.5		V	
Minimum Off Time <sup>(2)</sup>			100	150	ns	
Synchronization				•		
CLK Output Pulse Width	Master (R <sub>T</sub> to GND)	70	85	100	ns	
CLK Output Sink Current	Master, V <sub>CLK</sub> =0.4 V	0.25		0.35	mA	
CLK Output Source Current	Master, V <sub>CLK</sub> =2 V	-2.5		-2.0	mA	
CLK Input Pulse Width	Slave: $V_{CLK} \ge 2 V$	50		/	ns	
CLK Input Source Current	Slave: V <sub>CLK</sub> =1 V	-230	-200	-170	μA	
CLK Input Threshold, Rising	Slave	1.73	1.83	1.93	V	
Soft-Start						
$V_{OUT}$ to Regulation (T <sub>0.8</sub> )	Fraguenov 500 KHz		2.5		ms	
Fault Enable/SSOK (T <sub>1.0</sub> )	Frequency=500 KHz		3.1		ms	
Error Amplifier					~ 1	
DC Gain <sup>(2)</sup>		80	85		dB	
Gain Bandwidth Product <sup>(2)</sup>	VIN_Reg > 6.5 V	12	15		MHz	
Output Voltage Swing (V <sub>COMP</sub> )		0.4		4.0	V	
Output Current, Sourcing	5V_Reg=5 V, V <sub>COMP</sub> =2.2 V	1.5	2.2	2.5	mA	
Output Current, Sinking	5V_Reg=5 V, V <sub>COMP</sub> =1.2 V	0.8	1.2	1.5	mA	
FB Bias Current	V <sub>FB</sub> =0.8 V, T <sub>A</sub> =25°C	-850	-650	-450	nA	

# FAN21SV04 — TinyBuck™ 4 A, 24 V Single-Input Integrated Synchronous Buck Regulator

### Note:

2. Specifications guaranteed by design and characterization; not production tested.

### Electrical Characteristics (Continued)

Recommended operating conditions using the circuit shown in Figure 1 with  $V_{IN}$ ,  $V_{IN\_Reg}$ =12 V, unless otherwise noted.

Parameter	Conditions	Min.	Тур.	Max.	Units
Control Functions				•	I
EN Threshold, Rising			1.35	2.00	V
EN Hysteresis			250		mV
EN Pull-Up Resistance	VIN_Reg >6.5 V		800		KΩ
EN Discharge Current	Auto-Restart Mode, VIN_Reg>6.5 V		1		μA
FB OK Drive Resistance			800	1000	KΩ
DOOD Law Thready Id	FB < V <sub>REF</sub> , 2 Consecutive Clock Cycles <sup>(3)</sup>	-14.0	-11.0	-8.0	0())
PGOOD Low Threshold	FB > V <sub>REF</sub> , 2 Consecutive Clock Cycles <sup>(3)</sup>	+7.0	+10.0	+13.5	%V <sub>REF</sub>
PGOOD Low Voltage	I <sub>OUT</sub> ≤ 2 mA			0.4	V
PGOOD Leakage Current	V <sub>PGOOD</sub> =5 V		0.2	1.0	μA
Protection and Shutdown					
Current Limit	$R_{ILIM}$ open, f <sub>SW</sub> =500 KHz, V <sub>OUT</sub> =1.8 V, R <sub>RAMP</sub> =200 kΩ, 16 Consecutive Clock Cycles <sup>(3)</sup>	5.5	6.5	7.5	A
I <sub>LIM</sub> Current	VIN_Reg > 6.5 V, T <sub>A</sub> =25°C	-11	-10	-9	μA
Over-Temperature Shutdown	Internal Temperature		+155		°C
Over-Temperature Hysteresis	Internal Temperature		+30		°C
Over-Voltage Threshold	2 Consecutive Clock Cycles <sup>(3)</sup>	110	115	120	%V <sub>OUT</sub>
Under-Voltage Shutdown	16 Consecutive Clock Cycles <sup>(3)</sup>	68	73	78	%V <sub>OUT</sub>
Fault-Discharge Threshold	Measured at FB pin		250		mV
Fault-Discharge Hysteresis	Measured at FB pin (V <sub>FB</sub> ~500 mV)		250		mV

### Note:

3. Delay times are not tested in production. Guaranteed by design.

### **Typical Characteristics**

 $V_{\text{IN}}\text{=}12\text{V},$   $V_{\text{CC}}\text{=}5\text{V},$   $T_{\text{A}}\text{=}25^{\circ}\text{C},$  unless otherwise specified.

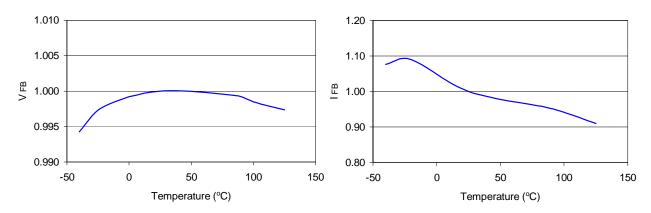


Figure 4. Reference Voltage (V<sub>FB</sub>) vs. Temperature, Figure 5. Reference Bias Current (I<sub>FB</sub>) vs. Temperature, Normalized Normalized

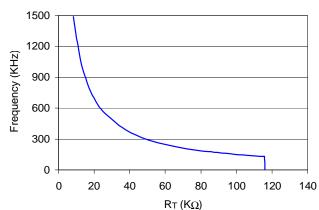


Figure 6. Frequency vs. R<sub>T</sub> (Master)

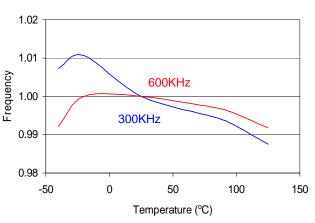
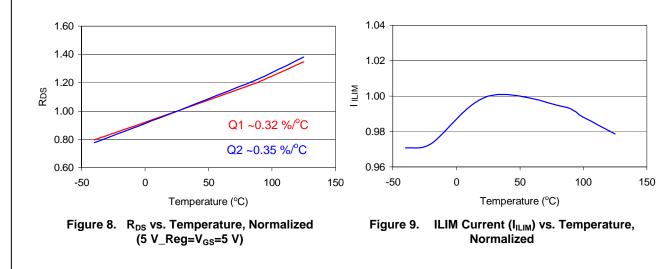
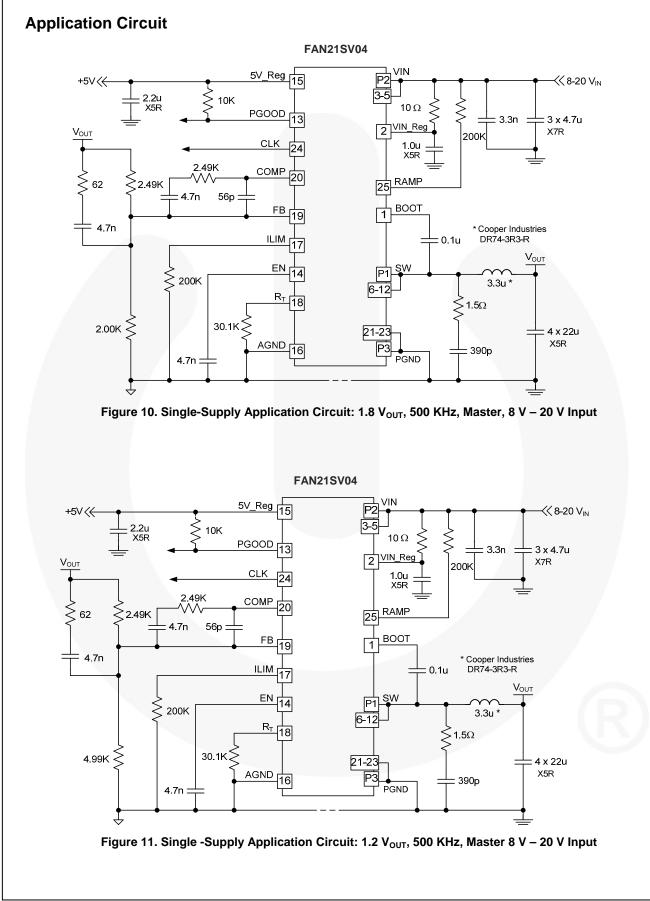


Figure 7. Frequency vs. Temperature, Normalized

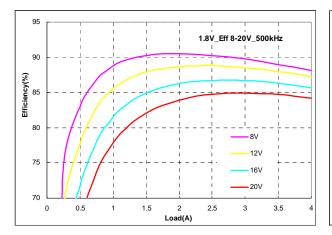




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### **Typical Performance Characteristics**

Typical operating characteristics using the Figure 10 circuit; V<sub>IN</sub>=12 V, V<sub>CC</sub>=5 V, T<sub>A</sub>=25°C, unless otherwise specified.





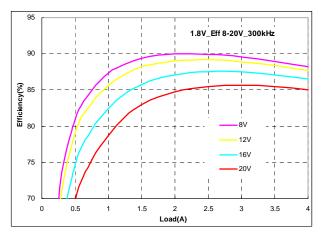


Figure 14. 1.8 V<sub>OUT</sub> Efficiency, 300 KHz<sup>(4)</sup>

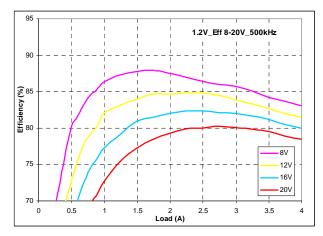


Figure 16. 1.2 V<sub>OUT</sub> Efficiency, 500 KHz (Figure 11)

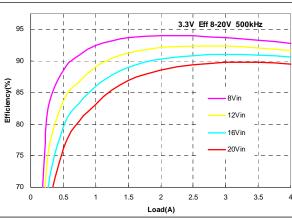
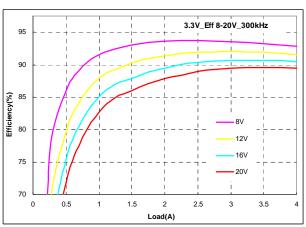


Figure 13. 3.3 V<sub>OUT</sub> Efficiency, 500 KHz<sup>(4)</sup>



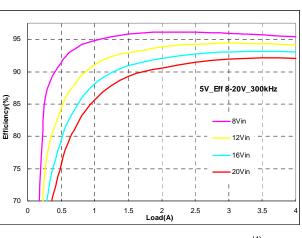
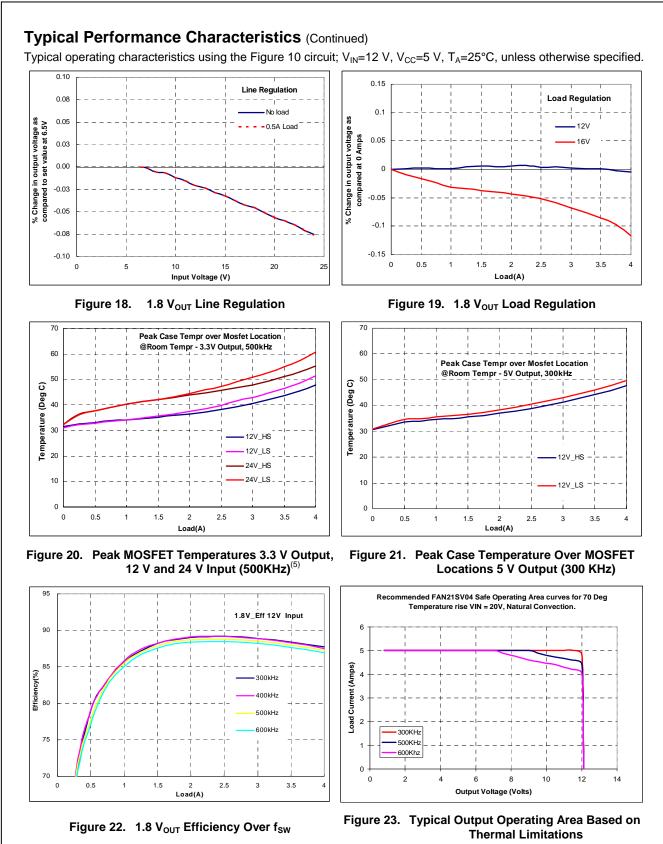


Figure 15. 3.3 V<sub>OUT</sub> Efficiency, 300 KHz<sup>(4)</sup>

Figure 17. 5 V<sub>OUT</sub> Efficiency, 300 KHz<sup>(4)</sup>

### Note:

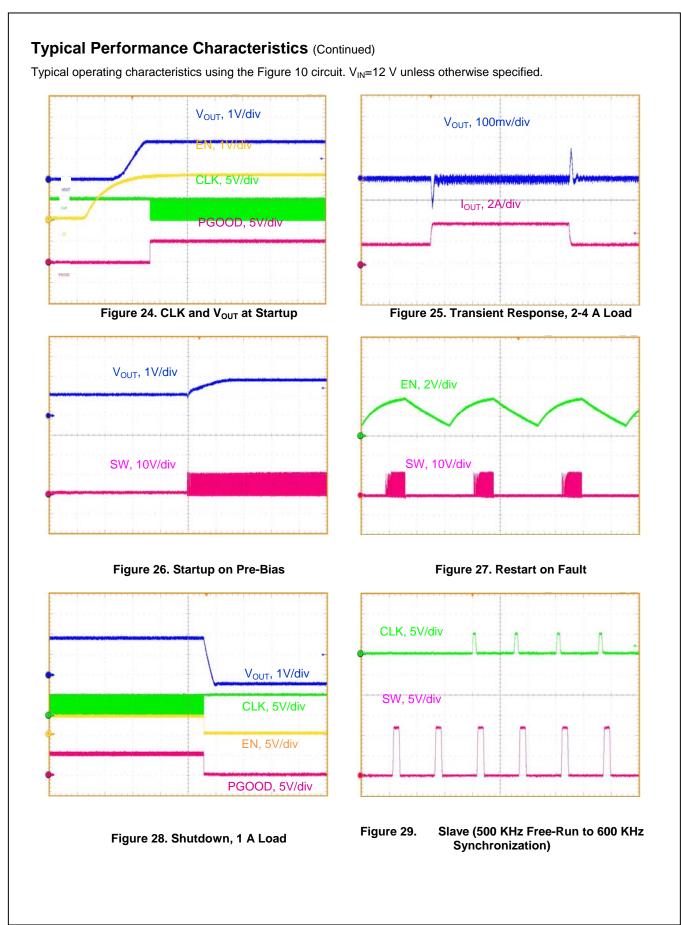
4. Circuit values for this configuration change in Figure 10.



Note:

5. Circuit values for this configuration change in Figure 10.





### **Circuit Operation**

### **PWM Generation**

Refer to Figure 2 for the PWM control mechanism. FAN21SV04 uses the summing-mode method of control to generate the PWM pulses. An amplified currentsense signal is summed with an internally generated ramp and the combined signal is compared with the output of the error amplifier to generate the pulse width to drive the high-side MOSFET. Sensed current from the previous cycle is used to modulate the output of the summing block. The output of the summing block is also compared against a voltage threshold set by the R<sub>LIM</sub> resistor to limit the inductor current on a cycle-by-cycle basis. R<sub>RAMP</sub> resistor helps set the charging current for the internal ramp and provides input voltage feed-forward function. The controller facilitates external compensation for enhanced flexibility.

### Initialization

Once VIN\_Reg voltage exceeds the UVLO threshold and EN is HIGH, the IC checks for a shorted FB pin before releasing the internal soft-start ramp (SS).

If the parallel combination of R1 and  $R_{BIAS}$  is  $\leq$  1 k\Omega, the internal SS ramp is not released and the regulator does not start.

### Enable

FAN21SV04 has an internal pull-up to the enable (EN) pin so that the IC is enabled once VIN\_Reg exceeds the UVLO threshold. Connecting a small capacitor across EN and AGND delays the rate of voltage rise on the EN pin. The EN pin also serves for the restart whenever a fault occurs *(refer to the Auto-Restart section).* If the regulator is enabled externally, the external EN signal should go HIGH only after 5 V\_Reg is established. For applications where such sequencing is required, FAN21SV04 can be enabled (after the V<sub>CC</sub> comes up) with external control, as shown in Figure 30.

If auto-restart is not desired, tie the EN pin HIGH with a logic gate to keep the 1  $\mu A$  current sink from discharging EN to 1.1 V. Figure 32 shows one method to pull up EN to V<sub>CC</sub> for a latch configuration.

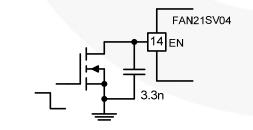


Figure 30. Enabling with External Control

### **Internal Regulator**

FAN21SV04 facilitates single-supply operation for input voltages >6.5 V. At startup, the output of the internal regulator tracks the input voltage and comes into regulation (5 V) when VIN\_Reg exceeds the UVLO threshold. The EN pin is released at the same time. The output voltage of the internal regulator (5 V\_Reg) is set to 5 V. The internal regulator supplies power to all the control circuits including the drivers.

For applications with V<sub>IN</sub><6.5 V, FAN21SV04 can be used if VIN\_Reg is provided with a separate low-power source >6.5 V. VIN\_Reg supply should come up after V<sub>IN</sub> during dual-supply operation. The VIN\_Reg pin should always be decoupled with at least a 10  $\Omega$  resistor and a 1  $\mu$ F ceramic capacitor (see Figure 10, Figure 11).

Since 5 V\_Reg is used to drive the internal MOSFET gates, high peak currents are present on the 5 V\_Reg pin. Connect a  $\geq$ 2.2 µf X5R or X7R decoupling capacitor between the 5 V\_Reg pin and AGND. For V<sub>IN</sub>>20 V operation, use a 3.3  $\Omega$  resistor in series with the boot capacitor to reduce noise into the regulator.

In addition to supplying power for the control circuits internally,  $5 V_Reg$  output can be used as a reference voltage for other applications requiring low noise reference voltage.  $5 V_Reg$  is capable of sourcing up to 5 mA of output current.

When EN is pulled LOW externally, 5 V\_Reg output is still present, but the IC is in standby mode with no switching.

### Soft-Start

FAN21SV04 uses an internal digital soft-start circuit to slowly ramp up the output voltage and limit inrush current during startup. When 5 V\_Reg is in regulation and EN is HIGH, the circuit releases SS and enables the PWM regulator. Soft-start time is a function of the switching frequency (number of clock cycles).

Once internal SS ramp has charged to 0.8 V (T0.8), the output voltage is in regulation. Until SS ramp reaches 1.0 V (T1.0), only the over-current-protection circuit is active during soft-start and all other output protections are inhibited.

In dual-supply operation mode, it is necessary to apply VIN before VIN\_Reg reaches its UVLO threshold to avoid skipping the soft-start cycle.

VIN\_Reg UVLO or toggling the EN pin discharges the SS and resets the IC.

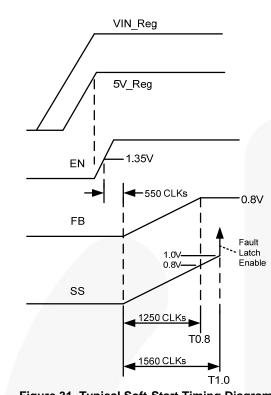


Figure 31. Typical Soft-Start Timing Diagram

### **Startup on Pre-Bias**

The regulator does not allow the low-side MOSFET to operate in full synchronous mode until SS reaches 95% of V<sub>REF</sub> (~0.76 V). This enables the regulator to startup on a pre-biased output and ensures that output is not discharged during the soft-start cycle.

### Protections

The converter output is monitored and protected against extreme overload, short-circuit, over-voltage, and undervoltage conditions.

### **Under-Voltage Protection**

If FB remains below the under-voltage threshold for 16 consecutive clock cycles, the fault latch is set and the converter shuts down. This protection is not active until the internal SS ramp reaches 1.0 V during soft-start.

### **Over-Voltage Protection**

If FB exceeds 115% •  $V_{REF}$  for two consecutive clock cycles, the fault latch is set and shutdown occurs.

A shorted high-side MOSFET condition is detected when SW voltage exceeds ~0.7 V while the low-side MOSFET is fully enhanced. The fault latch is set immediately upon detection.

The OV/UV fault conditions are not allowed to set the fault latch during soft-start. They are active only after T1.0 (see Figure 31).

### **Over-Temperature Protection**

The chip incorporates an over-temperature protection circuit that sets the fault latch when a die temperature of about 155°C is reached. The IC is allowed to restart when the die temperature falls below 125°C.

### Auto-Restart

After a fault, the EN pin is discharged with 1  $\mu$ A current pull-down to a 1.1 V threshold before the internal 800 k $\Omega$  pull-up is restored. A new soft-start cycle begins when EN charges above 1.35 V.

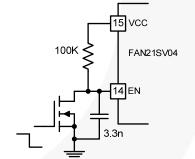
Depending on the external circuit, the FAN21SV04 can be configured to remain latched off or automatically restart after a fault, as listed in Table 1.

Table 1.	Fault /	Restart	Configurations
Tuble I.	i uuit /	1.Cotul t	ooningurutions

EN Pin	Controller / Restart State
Pull to GND	OFF (Disabled)
Connected to 5V_Reg with 100KΩ	No Restart – Latched OFF
Open	Immediate Restart After Fault
Cap to GND	New Soft-Start Cycle After EN is HIGH (Auto Restart Mode)

With EN left open, restart is immediate.

If auto-restart is not desired, tie the EN pin HIGH with a logic gate to keep the 1  $\mu$ A current sink from discharging EN to 1.1 V. Figure 32 shows one method to pull up EN to V<sub>CC</sub> for a latch configuration.





### Power Good (PGOOD) Signal

PGOOD is an open-drain output that asserts LOW when  $V_{OUT}$  is out of regulation, as measured at the FB pin. The thresholds are specified in the Electrical Specifications section. PGOOD does not assert HIGH until soft start is complete (T1.0) (see Figure 31).

### **Application Information**

### 5 V\_Reg Output

The 5 V\_Reg pin is the output of the internal regulator that supplies all power to the control circuit. It is important to keep this pin decoupled to AGND with a  $\geq$ 2.2 µf X5R or X7R decoupling capacitor. In addition, for operation with V<sub>IN</sub>>20 V, add a 3.3  $\Omega$  resistor in series with the boot capacitor to reduce the switching noise into the regulator.

### Setting the Output Voltage

The output voltage of the regulator can be set from 0.8 V to ~80% of V<sub>IN</sub> by an external resistor divider (R1 and R<sub>BIAS</sub> in Figure 1). For output voltages >3.3 V, output current rating may need to be de-rated depending on the ambient temperature, power dissipated in the package, and the PCB layout (refer to Thermal Information table on page 4, Figure 20, Figure 21, and Figure 23).

The internal reference is set to 0.8 V with 650 nA sourced from the FB pin to ensure that the regulator does not start if the pin is left open.

The external resistor divider is calculated using:

$$\frac{0.8V}{R_{BIAS}} = \frac{V_{OUT} - 0.8V}{R1} + 650nA$$
 (1)

Connect R<sub>BIAS</sub> between FB and AGND.

If R1 is open (see Figure 1), the output voltage is not regulated and a latched fault occurs after the SS is complete (T1.0).

If the parallel combination of R1 and  $R_{\text{BIAS}}$  is  $\leq$  1 K\Omega, the internal SS ramp is not released and the regulator does not start.

### **Setting the Switching Frequency**

Switching frequency is determined by a resistor,  $R_T$ , connected between the  $R_T$  pin and AGND (Master Mode) or 5 V\_Reg (Slave Mode):

where  $R_T$  is expressed in k $\Omega$ :

$$R_{T(K\Omega)} = \frac{(10^6 / f) - 135}{65}$$
(2)

where frequency (f) is expressed in KHz.

In Slave Mode, the switching frequency is about 10% slower for the same  $R_{T}.$  The regulator does not start if  $R_{T}$  is open in Master Mode.

### **Calculating the Inductor Value**

Typically the inductor value is chosen based on ripple current ( $\Delta I_L$ ), which is chosen between 10 to 35% of the maximum DC load. Regulator designs that require fast

transient response use a higher ripple-current setting while regulator designs that require higher efficiency keep ripple current on the low side and operate at a lower switching frequency. The inductor value is calculated by the following formula:

$$L = \frac{V_{OUT} \bullet (1 - \frac{V_{OUT}}{V_{IN}})}{\Delta I L \bullet f}$$
(3)

where f is the switching frequency.

### Setting the Ramp Resistor Value

 $R_{RAMP}$  resistor plays a critical role by providing charging current to the internal ramp capacitor and also serving as a means to provide input voltage feedforward.

R<sub>RAMP</sub> is calculated by the following formula:

$$R_{\text{RAMP}(K\Omega)} = \frac{(V_{\text{IN}} - 1.8) \bullet V_{\text{OUT}}}{(30.5 - 4.5 \bullet I_{\text{OUT}}) \bullet V_{\text{IN}} \bullet f \bullet 10^{-6}} - 2$$
(4)

where frequency (f) is expressed in KHz.

For wide input operation, first calculate  $R_{RAMP}$  for the minimum and maximum input voltage conditions and use larger of the two values calculated.

In all applications, current through the  $R_{RAMP}$  pin must be greater than 10  $\mu$ A from the equation below for proper operation:

$$\frac{V_{IN} - 1.8}{R_{RAMP} + 2} \ge 10\mu A \tag{5}$$

If the calculated R<sub>RAMP</sub> values in Equation (4) result in a current less than 10  $\mu$ A, use the R<sub>RAMP</sub> value that satisfies Equation (5). In applications with large Input ripple voltage, the R<sub>RAMP</sub> resistor should be adequately decoupled from the input voltage to minimize ripple on the ramp pin.

### Setting the Current Limit

The current limit system involves two comparators. The MAX I<sub>LIMIT</sub> comparator is used with a V<sub>ILIM</sub> fixed-voltage reference and represents the maximum current limit allowable. This reference voltage is temperature compensated to reflect the R<sub>DSON</sub> variation of the low-side MOSFET. The ADJUST I<sub>LIMIT</sub> comparator is used where the current limit needs to be set lower than the V<sub>ILIM</sub> fixed reference. The 10 µA current source does not track the R<sub>DSON</sub> changes over temperature, so change is added into the equations for calculating the ADJUST I<sub>LIMIT</sub> comparator reference voltage, as is shown below. Figure 33 shows a simplified schematic of the overcurrent system.

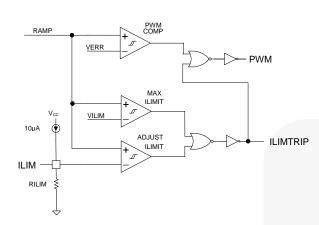


Figure 33. Current-Limit System Schematic

Since the  $I_{LIM}$  voltage is set by a 10  $\mu$ A current source into the  $R_{ILIM}$  resistor, the basic equation for setting the reference voltage is:

$$V_{\text{RILIM}} = 10\mu A^* R_{\text{ILIM}} \tag{6}$$

To calculate R<sub>ILIM</sub>:

$$R_{ILIM} = V_{RILIM} / 10\mu A \tag{7}$$

The voltage  $V_{\text{RILIM}}$  is made up of two components,  $V_{\text{BOT}}$  (which relates to the current through the low-side MOSFET) and  $V_{\text{RMPEAK}}$  (which relates to the peak current through the inductor). Combining those two voltage terms results in:

$$R_{ILIM} = (V_{BOT} + V_{RMPEAK})/10\mu A$$
(8)

$$R_{ILIM} = \{0.96 + (I_{LOAD} * R_{DSON} * K_{T} * 8)\} + \{D^{*}(V_{IN} - 1.8)/(f_{SW} * 0.03^{*}10^{-}3^{*}R_{RAMP})\}/10\mu A$$
where:

 $V_{BOT} = 0.96 + (I_{LOAD} * R_{DSON} * K_T * 8);$ 

 $V_{\text{RMPEAK}} = D^*(V_{\text{IN}} - 1.8)/(f_{\text{SW}}^* 0.03^* 10^{-3} R_{\text{RAMP}});$ 

I<sub>LOAD</sub> = the desired maximum load current;

 $R_{DSON}$  = the nominal  $R_{DSON}$  of the low-side MOSFET;

 $K_T$  = the normalized temperature coefficient for the low-side MOSFET (on datasheet graph);

 $D = V_{OUT}/V_{IN}$  duty cycle;

f<sub>SW</sub> = Clock frequency in kHz; and

 $R_{RAMP}$  = chosen ramp resistor value in k $\Omega$ .

After 16 consecutive, pulse-by-pulse, current-limit cycles, the fault latch is set and the regulator shuts down. Cycling  $V_{CC}$  or EN restores operation after a normal soft-start cycle (refer to the Auto-Restart section).

The over-current protection fault latch is active during the soft-start cycle. Use 1% resistor for  $R_{ILIM}$ .

### Loop Compensation

The control loop is compensated using a feedback network around the error amplifier. Figure 34 shows a

complete Type-3 compensation network. Type-2 compensation eliminates R3 and C3.

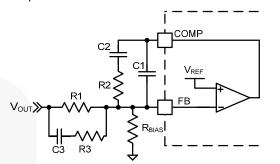


Figure 34. Compensation Network

Since the FAN21SV04 employs summing current-mode architecture, Type-2 compensation can be used for many applications. For applications that require wide loop bandwidth and/or use very low-ESR output capacitors, Type-3 compensation may be required.

 $R_{RAMP}$  provides feedforward compensation for changes in  $V_{IN}$ . With a fixed  $R_{RAMP}$  value, the modulator gain increases as  $V_{IN}$  is reduced, which can make it difficult to compensate the loop. For low-input-voltage-range designs (3 V to 8 V),  $R_{RAMP}$  and the compensation component values are different as compared to designs with  $V_{IN}$  between 8 V and 24 V.

### Master / Slave Configuration

When first enabled, the IC determines if it is configured as a master or slave for synchronization, depending on how  $R_T$  is connected.

### Table 2. Master / Slave Configuration

R <sub>T</sub> to:	Master / Slave	CLK Pin
GND	Master	Output
5V_Reg	Slave, free-running	Input

Slaves free-run in the absence of an external clock signal input when  $R_T$  is connected to 5 V\_Reg, allowing regulation to be maintained. It is not recommended to leave  $R_T$  open when running in Slave Mode to avoid noise pick up on the clock pin.

Slave free-running frequency should be set at least 25% lower than the incoming synchronizing pulse frequency. Maximum synchronizing clock frequency is recommended to be below 600 KHz.

### Synchronization

The synchronization method employed by the FAN21SV04 also provides the following features for maximum flexibility.

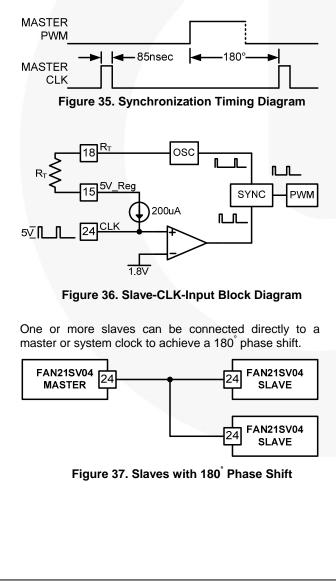
- Synchronization to an external system clock
- Multiple FAN21SV04s can be synchronized to a single master or system clock

- Independently programmable phase adjustment for one or multiple slaves
- Free-running capability in the absence of system clock or, if the master is disabled/faulted, the slaves can continue to regulate at a lower frequency

The FAN21SV04 master outputs an 85 ns-wide clock (CLK) signal, delayed 180° from its leading PWM edge. This feature allows out-of-phase operation for the slaves, thereby reducing the input capacitance requirements when more than one converter is operating on the same input supply. The leading SW-node edge is delayed ~40 ns from the rising PWM signal.

On a slave, synchronization is rising-edge triggered. The CLK input pin has a 1.8 V threshold and a  $200 \,\mu$ A current source pull-up.

In Master Mode, the clock signals go out after powergood signal asserts HIGH. Likewise, in Slave Mode, synchronization to an external clock signal occurs after the power-good signal goes HIGH. Until then, the converter operates in free-run mode.



Since the synchronizing circuit utilizes a narrow reset pulse, the actual phase delay is slightly more than 180°.

The FAN21SV04 is not intended for use in single-output, multi-phase regulator applications.

### PCB Layout

Good PCB layout and careful attention to temperature rise is essential for reliable operation of the regulator. Four-layer PCB with two-ounce copper on the top and bottom side and thermal vias connecting the layers is recommended. Keep power traces wide and short to minimize losses and ringing. Do not connect AGND to PGND below the IC. Connect AGND pin to PGND at the output OR to the PGND plane.

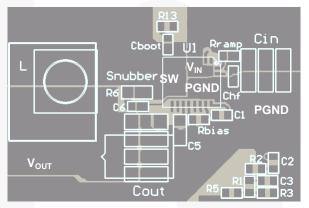
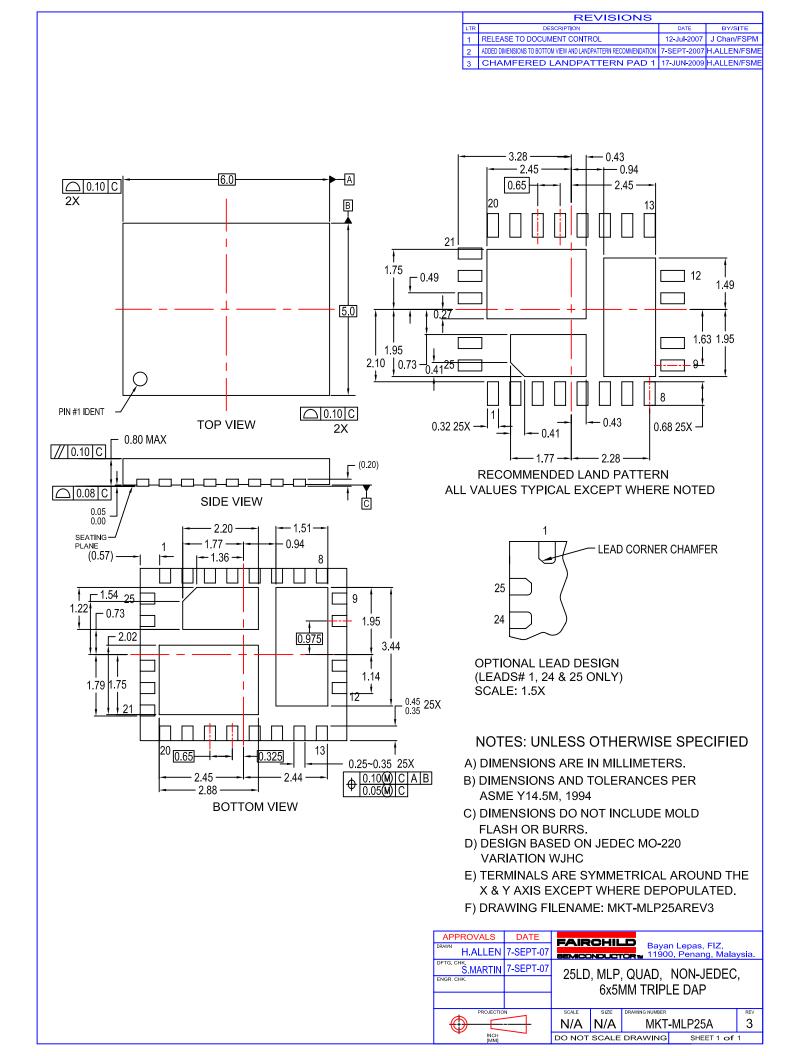


Figure 38. Recommended PCB Layout



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