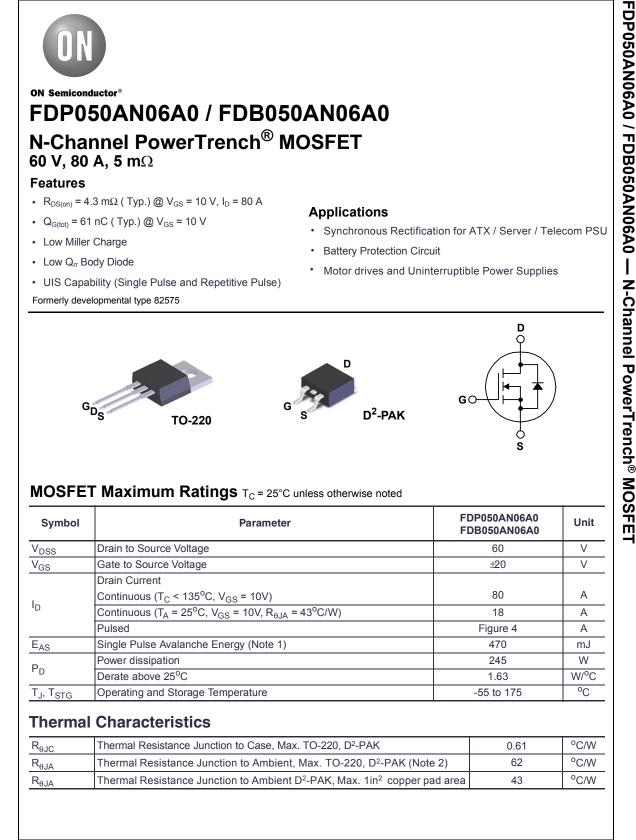
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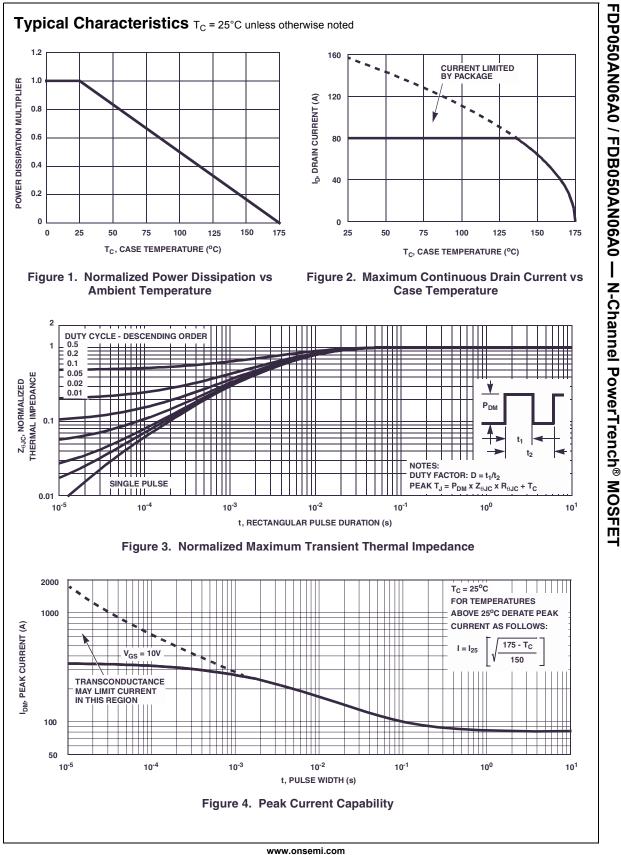
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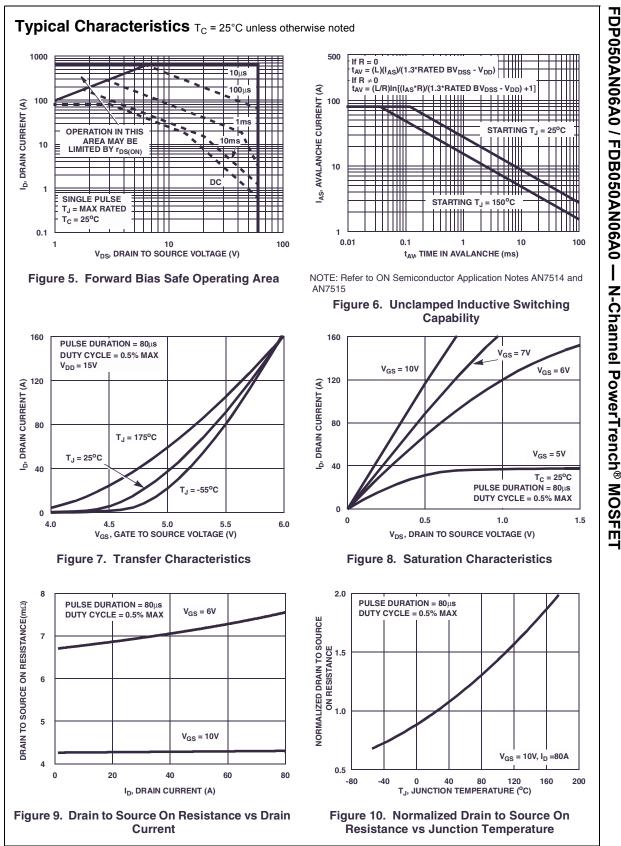
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Device Marking FDB050AN06A0		Device	Package	Reel Size	Tape \	Vidth	Quar	ntity
		FDB050AN06A0	D <sup>2</sup> -PAK	330 mm	24 mm		800 units	
FDP050AN06A0 FDP050AN06A0		FDP050AN06A0	TO-220 Tube		N/A		50 units	
Electric	al Char	acteristics T <sub>c</sub> = 25°C	unless otherwi	se noted				
Symbol	Parameter		Test Conditions		Min	Тур	Max	Unit
Off Chara	cteristic	S						
B <sub>VDSS</sub>	Drain to S	Drain to Source Breakdown Voltage		I <sub>D</sub> = 250μA, V <sub>GS</sub> = 0V		-	-	V
	Zero Gate Voltage Drain Current		V <sub>DS</sub> = 50V			-	1	
I <sub>DSS</sub>	Zero Gale	e voltage Drain Current	$V_{GS} = 0V$	T <sub>C</sub> = 150°C	-	-	250	μΑ
I <sub>GSS</sub>	Gate to Source Leakage Current		V <sub>GS</sub> = ±20V		-	-	±100	nA
On Chara	cteristic	S						
V <sub>GS(TH)</sub>	Gate to S	ource Threshold Voltage	rce Threshold Voltage $V_{GS} = V_{DS}, I_D = 250 \mu A$		2	-	4	V
	Drain to Source On Resistance		I <sub>D</sub> = 80A, V <sub>0</sub>	$I_{D} = 80A, V_{GS} = 10V$ $I_{D} = 40A, V_{GS} = 6V$ $I_{D} = 80A, V_{GS} = 10V,$ $T_{J} = 175^{\circ}C$		0.0043	0.005	
r <sub>DS(ON)</sub>						0.007	0.011	Ω
			I <sub>D</sub> = 80A, V <sub>0</sub> T <sub>J</sub> = 175°C			0.0085	0.010	
Dynamic	Characte	eristics	·					
C <sub>ISS</sub>	Input Capacitance		$V_{DS} = 25V, V_{GS} = 0V,$		-	3900	-	pF
C <sub>OSS</sub>	Output Capacitance				-	750	-	pF
C <sub>RSS</sub>	Reverse 1	Fransfer Capacitance	f = 1MHz		-	270	-	pF
Q <sub>g(TOT)</sub>	Total Gate	e Charge at 10V	V <sub>GS</sub> = 0V to	10V		61	80	nC
Q <sub>g(TH)</sub>	Threshold	I Gate Charge	V <sub>GS</sub> = 0V to	2V <sub>VDD</sub> = 30V	-	8	11	nC
Q <sub>gs</sub>	Gate to S	Gate to Source Gate Charge		I <sub>D</sub> = 80A	-	24	-	nC
Q <sub>gs2</sub>	Gate Charge Threshold to Plateau Gate to Drain "Miller" Charge			I <sub>g</sub> = 1.0mA		16	-	nC
Q <sub>gd</sub>					-	15	-	nC
Switching	g Charac	teristics (V <sub>GS</sub> = 10V)						
t <sub>ON</sub>	Turn-On Time					-	264	ns
t <sub>d(ON)</sub>	Turn-On E	Delay Time			-	16	-	ns
t <sub>r</sub>	Rise Time Turn-Off Delay Time			$V_{DD}$ = 30V, $I_{D}$ = 80A $V_{GS}$ = 10V, $R_{GS}$ = 4.3 $\Omega$		160	-	ns
t <sub>d(OFF)</sub>			V <sub>GS</sub> = 10V,			28	-	ns
t <sub>f</sub>	Fall Time	Fall Time Turn-Off Time				29	-	ns
t <sub>OFF</sub>	Turn-Off T				-	-	86	ns
Drain-Sou	urce Diod	de Characteristics						
V <sub>SD</sub>	Source to	Source to Drain Diode Voltage		I <sub>SD</sub> = 80A		-	1.25	V
			I <sub>SD</sub> = 40A			-	1.0	V
t <sub>rr</sub>		everse Recovery Time		$I_{SD}$ = 75A, $dI_{SD}/dt$ = 100A/µs		-	34	ns
Q <sub>RR</sub>	Reverse Recovered Charge		$I_{SD}$ = 75A, $dI_{SD}/dt$ = 100A/µs		-	-	25	nC

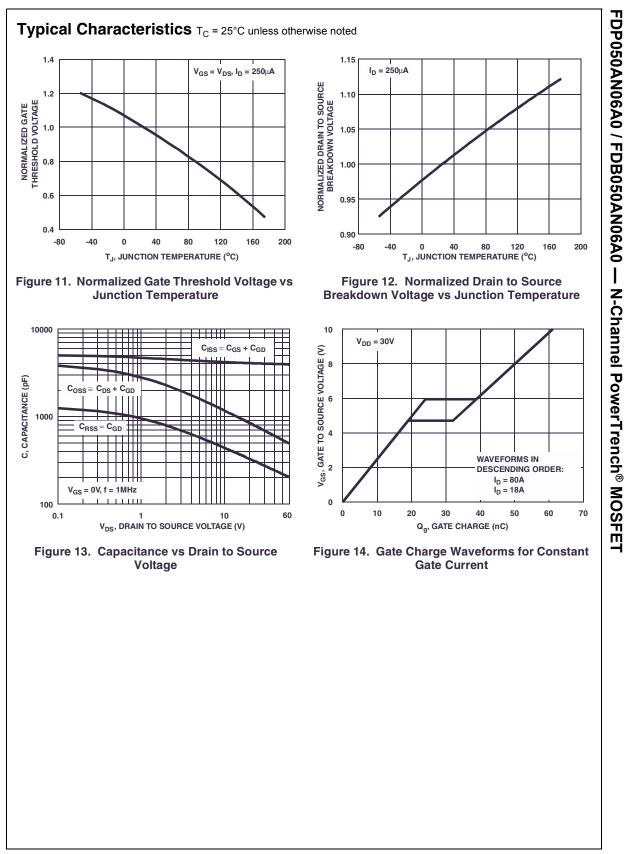
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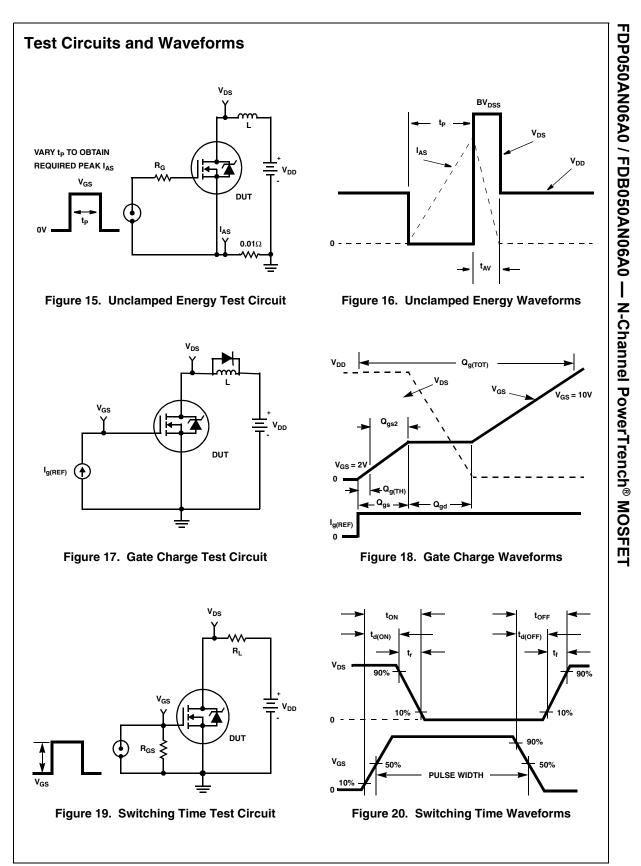


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## Thermal Resistance vs. Mounting Pad Area

The maximum rated junction temperature,  $T_{JM}$ , and the thermal resistance of the heat dissipating path determines the maximum allowable device power dissipation,  $P_{DM}$ , in an application. Therefore the application's ambient temperature,  $T_A$  (°C), and thermal resistance  $R_{\theta JA}$  (°C/W) must be reviewed to ensure that  $T_{JM}$  is never exceeded. Equation 1 mathematically represents the relationship and serves as the basis for establishing the rating of the part.

$$P_{DM} = \frac{(T_{JM} - T_A)}{R_{\theta JA}}$$
(EQ. 1)

In using surface mount devices such as the TO-263 package, the environment in which it is applied will have a significant influence on the part's current and maximum power dissipation ratings. Precise determination of  $P_{DM}$  is complex and influenced by many factors:

- Mounting pad area onto which the device is attached and whether there is copper on one side or both sides of the board.
- 2. The number of copper layers and the thickness of the board.
- 3. The use of external heat sinks.
- 4. The use of thermal vias.
- 5. Air flow and board orientation.
- 6. For non steady state applications, the pulse width, the duty cycle and the transient thermal response of the part, the board and the environment they are in.

ON Semiconductor provides thermal information to assist the designer's preliminary application evaluation. Figure 21

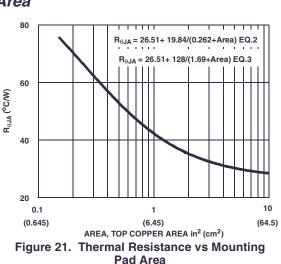
defines the  $R_{0JA}$  for the device as a function of the top copper (component side) area. This is for a horizontally positioned FR-4 board with 1oz copper after 1000 seconds of steady state power with no air flow. This graph provides the necessary information for calculation of the steady state junction temperature or power dissipation. Pulse applications can be evaluated using the ON Semiconductor device Spice thermal model or manually utilizing the normalized maximum transient thermal impedance curve.

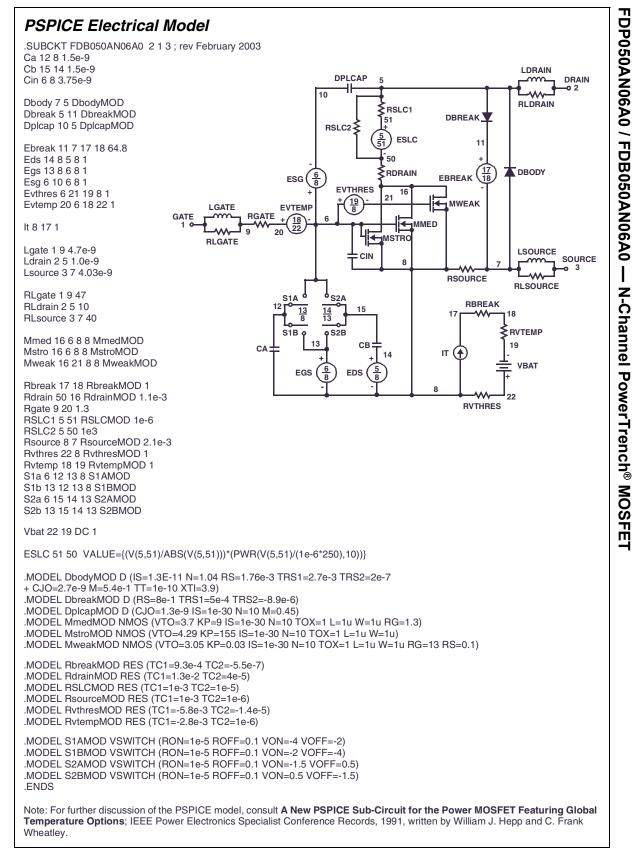
Thermal resistances corresponding to other copper areas can be obtained from Figure 21 or by calculation using Equation 2 or 3. Equation 2 is used for copper area defined in inches square and equation 3 is for area in centimeters square. The area, in square inches or square centimeters is the top copper area including the gate and source pads.

$$R_{\Theta JA} = 26.51 + \frac{19.84}{(0.262 + Area)}$$
 (EQ. 2)

Area in Inches Squared

$$R_{\theta JA} = 26.51 + \frac{128}{(1.69 + Area)}$$
(EQ. 3)  
Area in Centimeters Squared



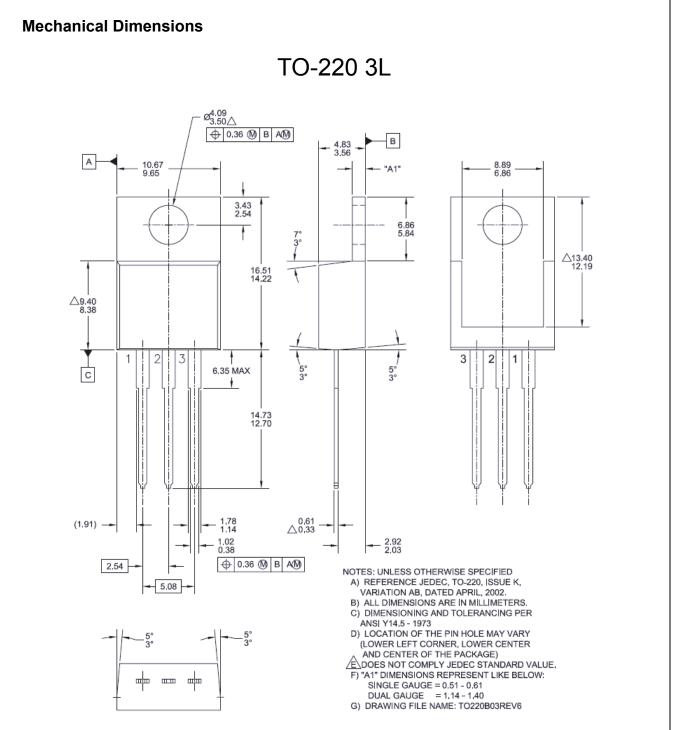


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### SABER Electrical Model DP050AN06A0 / FDB050AN06A0 --rev February 2003 template FDB050AN06A0 n2,n1,n3 electrical n2,n1,n3 var i iscl dp..model dbodymod = (isl=1.3e-11,nl=1.04,rs=1.76e-3,trs1=2.7e-3,trs2=2e-7,cjo=2.7e-9,m=5.4e-1,tt=1e-10,xti=3.9) dp..model dbreakmod = (rs=8e-1,trs1=5e-4,trs2=-8.9e-6) dp..model dplcapmod = (cjo=1.3e-9,isl=10e-30,nl=10,m=0.45)m..model mmedmod = (type=\_n,vto=3.7,kp=9,is=1e-30, tox=1) m..model mstrongmod = (type=\_n,vto=4.29,kp=155,is=1e-30, tox=1) m..model mweakmod = (type=\_n,vto=3.05,kp=0.03,is=1e-30, tox=1,rs=0.1) sw\_vcsp..model s1amod = (ron=1e-5,roff=0.1,von=-4,voff=-2) DPLCAP DRAIN sw\_vcsp..model s1bmod = (ron=1e-5,roff=0.1,von=-2,voff=-4) 02 10 sw\_vcsp..model s2amod = (ron=1e-5,roff=0.1,von=-1.5,voff=0.5) RLDRAIN sw\_vcsp..model s2bmod = (ron=1e-5,roff=0.1,von=0.5,voff=-1.5) ₹RSLC1 c.ca n12 n8 = 1.5e-9 51 RSLC2 ₹ c.cb n15 n14 = 1.5e-9 ISCL c.cin n6 n8 = 3.75e-9 DBREAK 50 dp.dbody n7 n5 = model=dbodymod RDRAIN dp.dbreak n5 n11 = model=dbreakmod 6 ESG 11 dp.dplcap n10 n5 = model=dplcapmod DBODY EVTHRES **N-Channel PowerTrench® MOSFET** 16 21 <u>19</u> 8 4 MWFAK LGATE spe.ebreak n11 n7 n17 n18 = 64.8 EVTEMP RGATE GATE $\mathbf{m}$ 18 22 spe.eds n14 n8 n5 n8 = 1 EBREAK ••• I 9 spe.egs n13 n8 n6 n8 = 1 20 MSTR RLGATE spe.esg n6 n10 n6 n8 = 1 LSOURCE spe.evthres n6 n21 n19 n8 = 1 CIN SOURCE 8 $\mathbf{m}$ spe.evtemp n20 n6 n18 n22 = 1 3 RSOURCE RLSOURCE i.it n8 n17 = 1 RBREAK l.lgate n1 n9 = 4.7e-9 <u>13</u> 8 <u>14</u> 13 15 17 18 I.ldrain n2 n5 = 1.0e-9 RVTEMP l.lsource n3 n7 = 4.03e-9 S1B o S2B СВ 19 CA IT 4 14 res.rlgate n1 n9 = 47 VBAT res rldrain n2 n5 = 105 EGS FDS res.rlsource n3 n7 = 40 8 22 m.mmed n16 n6 n8 n8 = model=mmedmod, l=1u, w=1u RVTHRES m.mstrong n16 n6 n8 n8 = model=mstrongmod, l=1u, w=1u m.mweak n16 n21 n8 n8 = model=mweakmod, l=1u, w=1u res.rbreak n17 n18 = 1, tc1=9.3e-4,tc2=-5.5e-7 res.rdrain n50 n16 = 1.1e-3, tc1=1.3e-2,tc2=4e-5 res.roate n9 n20 = 1.3res.rslc1 n5 n51 = 1e-6, tc1=1e-3,tc2=1e-5 res.rslc2 n5 n50 = 1e3res.rsource n8 n7 = 2.1e-3, tc1=1e-3,tc2=1e-6 res.rvthres n22 n8 = 1, tc1=-5.8e-3,tc2=-1.4e-5 res.rvtemp n18 n19 = 1, tc1=-2.8e-3,tc2=1e-6 sw\_vcsp.s1a n6 n12 n13 n8 = model=s1amod sw\_vcsp.s1b n13 n12 n13 n8 = model=s1bmod sw\_vcsp.s2a n6 n15 n14 n13 = model=s2amod sw\_vcsp.s2b n13 n15 n14 n13 = model=s2bmod v.vbat n22 n19 = dc=1 equations { i (n51->n50) +=iscl iscl: v(n51,n50) = ((v(n5,n51)/(1e-9+abs(v(n5,n51))))\*((abs(v(n5,n51)\*1e6/250))\*\*10)))}

### SPICE Thermal Model th 0 JUNCTION REV 23 February 2003 FDB050AN06A0T CTHERM1 TH 6 5e-3 CTHERM2 6 5 1.3e-2 CTHERM3 5 4 1.4e-2 ≶ RTHERM1 CTHERM1 CTHERM4 4 3 1.9e-2 CTHERM5 3 2 4.7e-2 CTHERM6 2 TL 9e-2 6 RTHERM1 TH 6 1e-2 RTHERM2 6 5 3.1e-2 RTHERM3 5 4 4.5e-2 RTHERM2 CTHERM2 ξ RTHERM4 4 3 1.2e-1 RTHERM5 3 2 1.3e-1 RTHERM6 2 TL 1.52e-1 5 SABER Thermal Model SABER thermal model FDB050AN06A0T RTHERM3 CTHERM3 template thermal\_model th tl ξ thermal\_c th, tl ctherm.ctherm1 th 6 =5e-3 4 ctherm.ctherm2 6 5 =1.3e-2 ctherm.ctherm3 5 4 =1.4e-2 ctherm.ctherm4 4 3 =1.9e-2 ctherm.ctherm5 3 2 =4.7e-2 **RTHERM4** ≶ CTHERM4 ctherm.ctherm6 2 tl =9e-2 rtherm.rtherm1 th 6 =1e-2 rtherm.rtherm2 6 5 = 3.1e-2 3 rtherm.rtherm3 5 4 =4.5e-2 rtherm.rtherm4 4 3 =1.2e-1 rtherm.rtherm5 3 2 =1.3e-1 RTHERM5 CTHERM5 ξ rtherm.rtherm6 2 tl =1.52e-1 } 2 RTHERM6 CTHERM6 ξ CASE tl 9

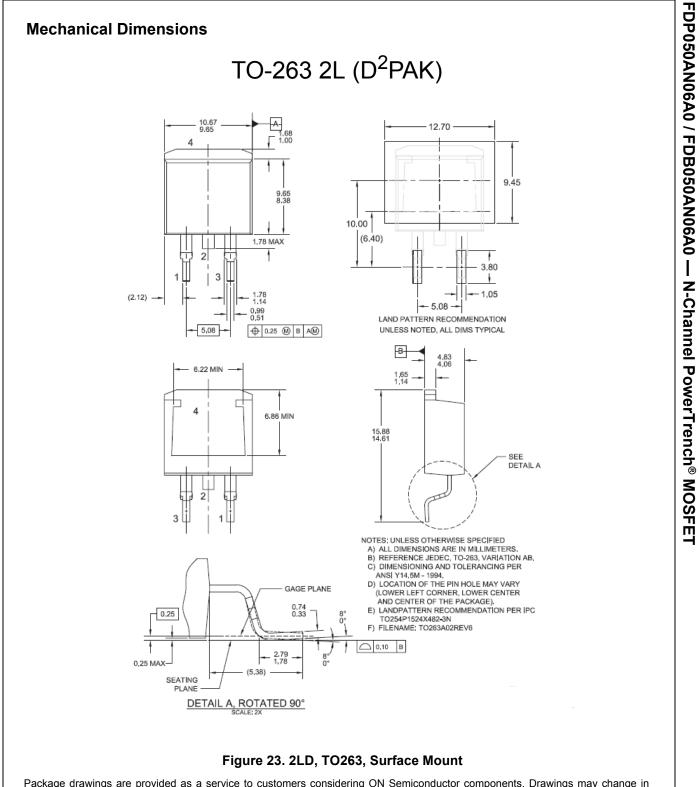
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# Figure 22. TO-220, Molded, 3Lead, Jedec Variation AB

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