ON Semiconductor

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ON Semiconductor®

FDB3652-F085

N-Channel PowerTrench® MOSFET 100V, 61A, 16m Ω

Features

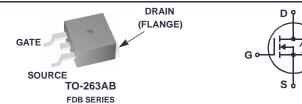
- $r_{DS(ON)} = 14m\Omega$ (Typ.), $V_{GS} = 10V$, $I_D = 61A$
- $Q_q(tot) = 41nC (Typ.), V_{GS} = 10V$
- Low Miller Charge
- Low Q_{RR} Body Diode
- · UIS Capability (Single Pulse and Repetitive Pulse)
- Qualified to AEC Q101
- RoHS Compliant

Formerly developmental type 82769



Applications

- DC/DC Converters and Off-line UPS
- Distributed Power Architectures and VRMs
- Primary Switch for 24V and 48V Systems
- · High Voltage Synchronous Rectifier
- Direct Injection / Diesel Injection Systems
- 42V Automotive Load Control
- Electronic Valve Train Systems



MOSFET Maximum Ratings $T_C = 25^{\circ}C$ unless otherwise noted

Symbol	Parameter	Ratings	Units
V _{DSS}	Drain to Source Voltage	100	V
V _{GS}	Gate to Source Voltage	±20	V
	Drain Current		
I_D	Continuous ($T_C = 25^{\circ}C$, $V_{GS} = 10V$)	61	А
	Continuous ($T_C = 100^{\circ}C$, $V_{GS} = 10V$)	43	А
	Continuous ($T_{amb} = 25^{\circ}C$, $V_{GS} = 10V$) with $R_{\theta JA} = 43^{\circ}C/W$)	9	А
	Pulsed	Figure 4	А
E _{AS}	Single Pulse Avalanche Energy (Note 1)	182	mJ
	Power dissipation	150	W
P_{D}	Derate above 25°C	1.0	W/°C
T_J, T_{STG}	Operating and Storage Temperature	-55 to 175	°C

Thermal Characteristics

$R_{\theta JC}$	Thermal Resistance Junction to Case TO-263		1.0	°C/W
	Thermal Resistance Junction to Ambient TO-263	(Note 2)	62	°C/W
$R_{\theta JA}$	Thermal Resistance Junction to Ambient TO-263, 1in	copper pad area	43	°C/W

This product has been designed to meet the extreme test conditions and environment demanded by the automotive industry. For a copy of the requirements, see AEC Q101 at: http://www.aecouncil.com/

All ON Semiconductor products are manufactured, assembled and tested under ISO9000 and QS9000 quality systems certification.

Package Marking and Ordering Information

Device Marking	Device	Package	Reel Size	Tape Width	Quantity
FDB3652	FDB3652-F085	TO-263AB	330mm	24mm	800 units

Electrical Characteristics $T_C = 25^{\circ}C$ unless otherwise noted

Symbol	Parameter	Test Co	nditions	Min	Тур	Max	Units	
Off Characteristics								
B _{VDSS}	Drain to Source Breakdown Voltage	$I_D = 250 \mu A, V_G$	S = 0V	100	-	-	V	
1	Zero Gate Voltage Drain Current	$V_{DS} = 80V$		-	-	1	^	
IDSS	Zero Gate voltage Diam Current	$V_{GS} = 0V$	$T_{C} = 150^{\circ}C$	-	-	250	μΑ	
I_{GSS}	Gate to Source Leakage Current	$V_{GS} = \pm 20V$		-	-	±100	nA	

On Characteristics

V _{GS(TH)}	Gate to Source Threshold Voltage	$V_{GS} = V_{DS}, I_{D} = 250 \mu A$	2	-	4	V
r _{DS(ON)}	Drain to Source On Resistance	$I_D = 61A, V_{GS} = 10V$	-	0.014	0.016	
		$I_D = 30A, V_{GS} = 6V$	-	0.018	0.026	0
		$I_D = 61A, V_{GS} = 10V,$ $T_J = 175$ °C	-	0.035	0.043	3.2

Dynamic Characteristics

C _{ISS}	Input Capacitance		-	2880	-	pF
C _{OSS}	Output Capacitance	$V_{DS} = 25V, V_{GS} = 0V,$ f = 1MHz	-	390	-	pF
C _{RSS}	Reverse Transfer Capacitance	1 = 1101112	-	100	-	pF
$Q_{g(TOT)}$	Total Gate Charge at 10V	V _{GS} = 0V to 10V		41	53	nC
$Q_{g(TH)}$	Threshold Gate Charge	$V_{GS} = 0V \text{ to } 2V$ $V_{DD} = 50V$	-	5	6.5	nC
	Gate to Source Gate Charge	I _D = 61A	-	15	-	nC
Q _{gs} Q _{gs2}	Gate Charge Threshold to Plateau	I _g = 1.0mA	-	10	-	nC
Q_{gd}	Gate to Drain "Miller" Charge		-	10	-	nC

Switching Characteristics $(V_{GS} = 10V)$

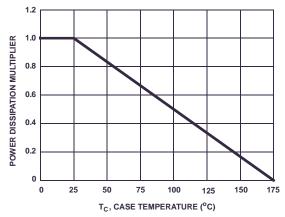
t _{ON}	Turn-On Time	$V_{DD} = 50V, I_{D} = 61A$ $V_{GS} = 10V, R_{GS} = 6.8\Omega$	-	-	146	ns
t _{d(ON)}	Turn-On Delay Time		-	12	-	ns
t _r	Rise Time		-	85	-	ns
t _{d(OFF)}	Turn-Off Delay Time		-	26	-	ns
t _f	Fall Time		-	45	-	ns
t _{OFF}	Turn-Off Time		-	-	107	ns

Drain-Source Diode Characteristics

V _{SD}	ISource to Drain Diode Voltage	I _{SD} = 61A	-	-	1.25	V
		I _{SD} = 30A	-	-	1.0	V
t _{rr}	Reverse Recovery Time	$I_{SD} = 61A$, $dI_{SD}/dt = 100A/\mu s$	-	-	62	ns
Q_{RR}	Reverse Recovered Charge	$I_{SD} = 61A$, $dI_{SD}/dt = 100A/\mu s$	-	-	45	nC

- Notes: 1: Starting $T_J = 25^{\circ}C$, L = 0.228mH, $I_{AS} = 40A$. 2: Pulse Width = 100s

Typical Characteristics $T_C = 25$ °C unless otherwise noted



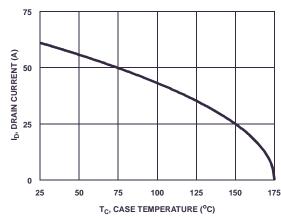


Figure 1. Normalized Power Dissipation vs Ambient Temperature

Figure 2. Maximum Continuous Drain Current vs Case Temperature

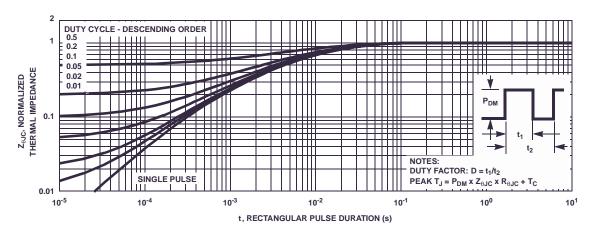


Figure 3. Normalized Maximum Transient Thermal Impedance

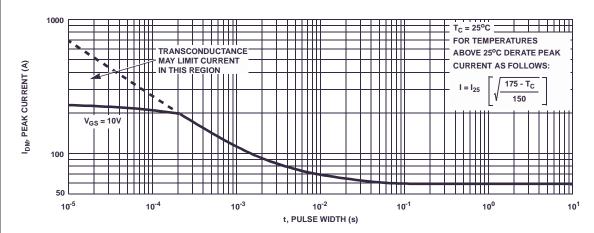
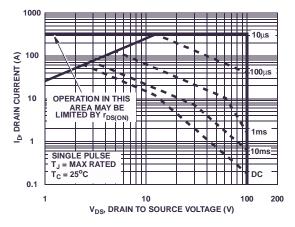


Figure 4. Peak Current Capability





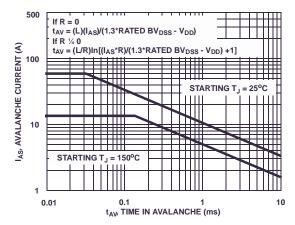
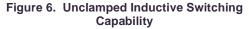
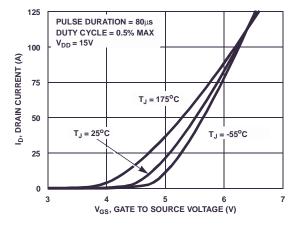


Figure 5. Forward Bias Safe Operating Area

NOTE: Refer to ON Semiconductor Application Notes AN7514 and AN7515 $\,$





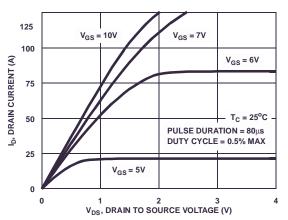
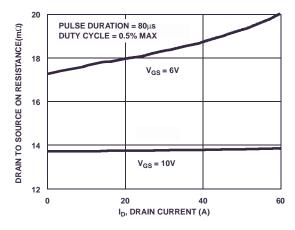


Figure 7. Transfer Characteristics

Figure 8. Saturation Characteristics



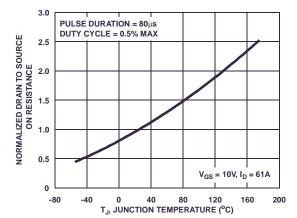


Figure 9. Drain to Source On Resistance vs Drain Current

Figure 10. Normalized Drain to Source On Resistance vs Junction Temperature

Typical Characteristics $T_C = 25$ °C unless otherwise noted

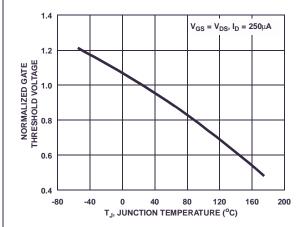
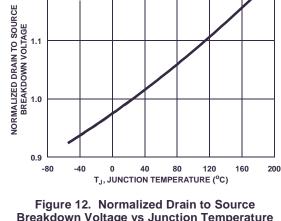


Figure 11. Normalized Gate Threshold Voltage vs **Junction Temperature**



1.2

 $I_D = 250 \mu A$

Breakdown Voltage vs Junction Temperature

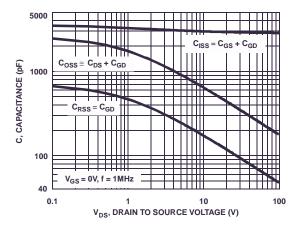


Figure 13. Capacitance vs Drain to Source Voltage

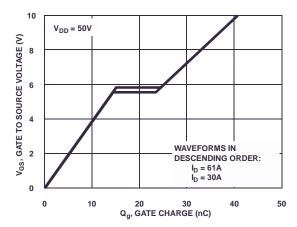


Figure 14. Gate Charge Waveforms for Constant **Gate Currents**

Test Circuits and Waveforms

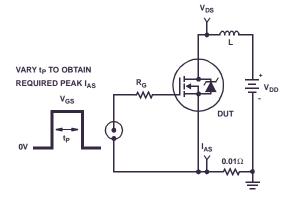


Figure 15. Unclamped Energy Test Circuit

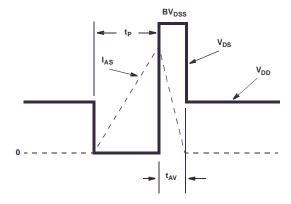


Figure 16. Unclamped Energy Waveforms

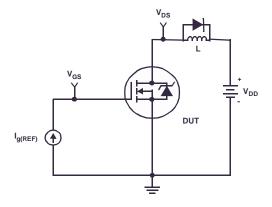


Figure 17. Gate Charge Test Circuit

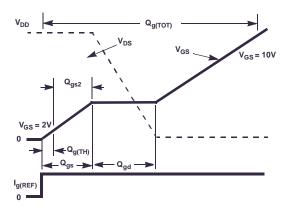


Figure 18. Gate Charge Waveforms

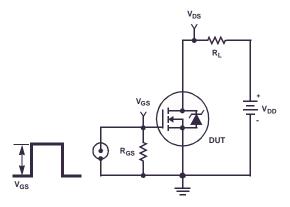


Figure 19. Switching Time Test Circuit

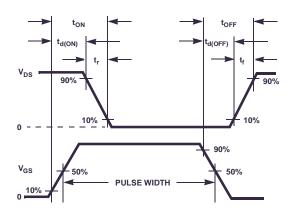


Figure 20. Switching Time Waveforms

Thermal Resistance vs. Mounting Pad Area

The maximum rated junction temperature, T_{JM} , and the thermal resistance of the heat dissipating path determines the maximum allowable device power dissipation, P_{DM} , in an application. Therefore the application's ambient temperature, T_A (°C), and thermal resistance $R_{\theta JA}$ (°C/W) must be reviewed to ensure that T_{JM} is never exceeded. Equation 1 mathematically represents the relationship and serves as the basis for establishing the rating of the part.

$$P_{DM} = \frac{(T_{JM} - T_A)}{R_{\theta JA}} \tag{EQ. 1}$$

In using surface mount devices such as the TO-263 package, the environment in which it is applied will have a significant influence on the part's current and maximum power dissipation ratings. Precise determination of P_{DM} is complex and influenced by many factors:

- Mounting pad area onto which the device is attached and whether there is copper on one side or both sides of the board.
- The number of copper layers and the thickness of the board.
- 3. The use of external heat sinks.
- 4. The use of thermal vias.
- 5. Air flow and board orientation.
- 6. For non steady state applications, the pulse width, the duty cycle and the transient thermal response of the part, the board and the environment they are in.

ON Semiconductor provides thermal information to assist the designer's preliminary application evaluation. Figure 21 defines the R0JA for the device as a function of the top copper (component side) area. This is for a horizontally positioned FR-4 board with 1oz copper after 1000 seconds of steady state power with no air flow. This graph provides the necessary information for calculation of the steady state junction temperature or power dissipation. Pulse applications can be evaluated using the ON Semiconductor device Spice thermal model or manually utilizing the normalized maximum transient thermal impedance curve.

Thermal resistances corresponding to other copper areas can be obtained from Figure 21 or by calculation using Equation 2 or 3. Equation 2 is used for copper area defined in inches square and equation 3 is for area in centimeter square. The area, in square inches or square centimeters is the top copper area including the gate and source pads.

$$R_{\theta JA} = 26.51 + \frac{19.84}{(0.262 + Area)}$$
 (EQ. 2)

Area in Iches Squared

$$R_{\theta JA} = 26.51 + \frac{128}{(1.69 + Area)}$$
 (EQ. 3)

Area in Centimeter Squared

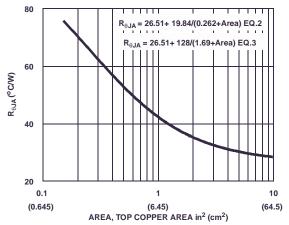
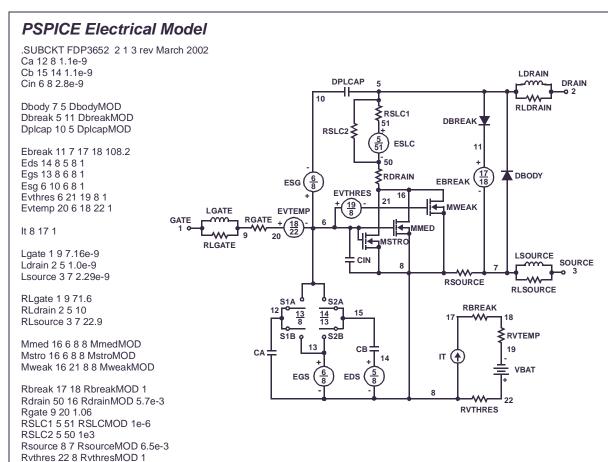


Figure 21. Thermal Resistance vs Mounting
Pad Area



Vbat 22 19 DC 1

Rvtemp 18 19 RvtempMOD 1 S1a 6 12 13 8 S1AMOD S1b 13 12 13 8 S1BMOD S2a 6 15 14 13 S2AMOD S2b 13 15 14 13 S2BMOD

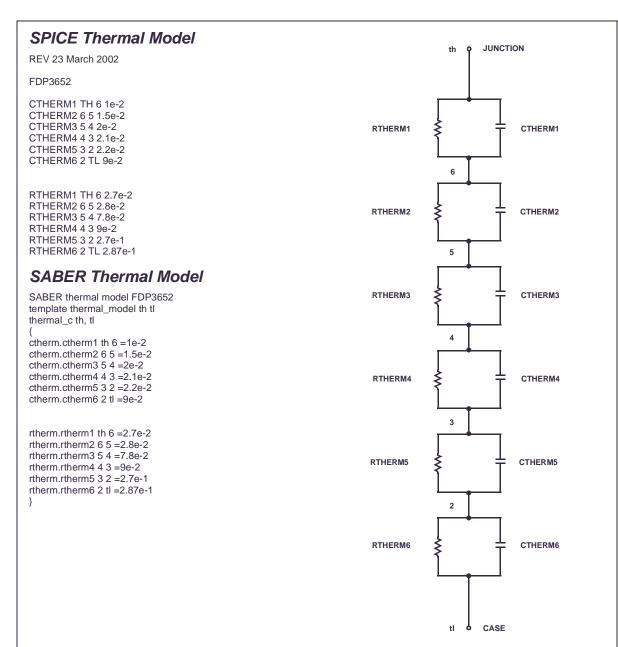
ESLC 51 50 VALUE={(V(5,51)/ABS(V(5,51)))*(PWR(V(5,51)/(1e-6*150),7))}

```
.MODEL DbodyMOD D (IS=1.5E-11 N=1.06 RS=2.5e-3 TRS1=2.4e-3 TRS2=1.1e-6
+ CJO=1.9e-9 M=5.8e-1 TT=2.5e-8 XTI=3.9)
.MODEL DbreakMOD D (RS=2.7e-1 TRS1=1e-3 TRS2=-8.9e-6)
.MODEL DplcapMOD D (CJO=7e-10 IS=1e-30 N=10 M=0.58)
.MODEL MmedMOD NMOS (VTO=3.6 KP=5.5 IS=1e-30 N=10 TOX=1 L=1u W=1u RG=1.06)
.MODEL MstroMOD NMOS (VTO=4.3 KP=110 IS=1e-30 N=10 TOX=1 L=1u W=1u)
.MODEL MweakMOD NMOS (VTO=3 KP=0.03 IS=1e-30 N=10 TOX=1 L=1u W=1u RG=1.06e1 RS=.1)
.MODEL RbreakMOD RES (TC1=1.05e-3 TC2=1e-6)
.MODEL RdrainMOD RES (TC1=1.7e-2 TC2=3.2e-5)
.MODEL RSLCMOD RES (TC1=1e-3 TC2=1e-7)
.MODEL RsourceMOD RES (TC1=1e-3 TC2=1e-6)
.MODEL RvthresMOD RES (TC1=-5.3e-3 TC2=-1.2e-5)
.MODEL RytempMOD RES (TC1=-3.3e-3 TC2=1.3e-6)
.MODEL S1AMOD VSWITCH (RON=1e-5 ROFF=0.1 VON=-8 VOFF=-5)
.MODEL S1BMOD VSWITCH (RON=1e-5 ROFF=0.1 VON=-5 VOFF=-8)
.MODEL S2AMOD VSWITCH (RON=1e-5 ROFF=0.1 VON=-1 VOFF=0.5)
.MODEL S2BMOD VSWITCH (RON=1e-5 ROFF=0.1 VON=0.5 VOFF=-1)
```

.ENDS

Note: For further discussion of the PSPICE model, consult **A New PSPICE Sub-Circuit for the Power MOSFET Featuring Global Temperature Options**; IEEE Power Electronics Specialist Conference Records, 1991, written by William J. Hepp and C. Frank Wheatley.

SABER Electrical Model REV March 2002 template FDP3652 n2,n1,n3 electrical n2,n1,n3 var i iscl dp..model dbodymod = (isl=1.5e-11,nl=1.06,rs=2.5e-3,trs1=2.4e-3,trs2=1.1e-6,cjo=1.9e-9,m=5.8e-1,tt=2.5e-8,xti=3.9) dp..model dbreakmod = (rs=2.7e-1.trs1=1e-3.trs2=-8.9e-6) dp..model dplcapmod = (cjo=7e-10,isl=10e-30,nl=10,m=0.58) $m..model mmedmod = (type=_n,vto=3.6,kp=5.5,is=1e-30,tox=1)$ m..model mstrongmod = (type=_n,vto=4.3,kp=110,is=1e-30, tox=1) m..model mweakmod = (type=_n,vto=3,kp=0.03,is=1e-30, tox=1,rs=.1) sw_vcsp..model s1amod = (ron=1e-5,roff=0.1,von=-8,voff=-5) LDRAIN sw_vcsp..model s1bmod = (ron=1e-5,roff=0.1,von=-5,voff=-8) **DPLCAP** DRAIN sw_vcsp..model s2amod = (ron=1e-5,roff=0.1,von=-1,voff=0.5) 10 sw_vcsp..model s2bmod = (ron=1e-5,roff=0.1,von=0.5,voff=-1) **RLDRAIN** €RSLC1 c.ca n12 n8 = 1.1e-9c.cb n15 n14 = 1.1e-951 RSLC2 ≥ c.cin n6 n8 = 2.8e-9ISCL dp.dbody n7 n5 = model=dbodymod 50 DBREAK _ dp.dbreak n5 n11 = model=dbreakmod ≨rdrain 8 ESG dp.dplcap n10 n5 = model=dplcapmod 11 **DBODY EVTHRES** spe.ebreak n11 n7 n17 n18 = 108.2 **LGATE EVTEMP** spe.eds n14 n8 n5 n8 = 1 RGATE spe.egs n13 n8 n6 n8 = 1 **EBREAK** 20 spe.esg n6 n10 n6 n8 = 1 **←**MSTRC RLGATE spe.evthres n6 n21 n19 n8 = 1 **LSOURCE** CIN SOURCE spe.evtemp n20 n6 n18 n22 = 1 RSOURCE i.it n8 n17 = 1 RLSOURCE I.lgate n1 n9 = 7.16e-9**RBREAK** <u>14</u> 13 <u>13</u> 8 17 I.ldrain n2 n5 = 1.0e-9I.Isource n3 n7 = 2.29e-9**≷**RVTEMP CB 19 res.rlgate n1 n9 = 71.6 CA IT res.rldrain n2 n5 = 10VBAT res.rlsource n3 n7 = 22.9 EGS **EDS** m.mmed n16 n6 n8 n8 = model=mmedmod, l=1u, w=1u m.mstrong n16 n6 n8 n8 = model=mstrongmod, l=1u, w=1u **RVTHRES** m.mweak n16 n21 n8 n8 = model=mweakmod, l=1u, w=1u res.rbreak n17 n18 = 1, tc1=1.05e-3,tc2=1e-6 res.rdrain n50 n16 = 5.7e-3, tc1=1.7e-2,tc2=3.2e-5 res.rgate n9 n20 = 1.06 res.rslc1 n5 n51 = 1e-6, tc1=1e-3,tc2=1e-7 res.rslc2 n5 n50 = 1e3res.rsource n8 n7 = 6.5e-3, tc1=1e-3,tc2=1e-6 res.rvthres n22 n8 = 1, tc1=-5.3e-3,tc2=-1.2e-5 res.rvtemp n18 n19 = 1, tc1=-3.3e-3,tc2=1.3e-6 sw vcsp.s1a n6 n12 n13 n8 = model=s1amod sw_vcsp.s1b n13 n12 n13 n8 = model=s1bmod sw_vcsp.s2a n6 n15 n14 n13 = model=s2amod sw_vcsp.s2b n13 n15 n14 n13 = model=s2bmod v.vbat n22 n19 = dc=1 equations { i (n51->n50) +=iscl (v(n51,n50) = ((v(n5,n51)/(1e-9+abs(v(n5,n51))))*((abs(v(n5,n51)*1e6/150))**7))



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