## Power Factor Corrected Quasi-Resonant Primary Side Current-Mode Controller for LED Lighting with Thermal Foldback

The NCL30088 is a power factor corrected flyback controller targeting isolated and non-isolated constant current LED drivers. The controller operates in a quasi-resonant mode to provide optimal efficiency. Thanks to a novel control method, the device is able to tightly regulate a constant LED current from the primary side. This removes the need for secondary side feedback circuitry, biasing and an optocoupler.

The device is highly integrated with a minimum number of external components. A robust suite of safety protection is built in to simplify the design. This device is specifically intended for very compact, space efficient designs.

### Features

- Quasi-resonant Peak Current-mode Control Operation
- Constant Current Control with Primary Side Feedback
- Tight LED Constant Current Regulation of ±2% Typical
- Power Factor Correction
- Line Feedforward for Enhanced Regulation Accuracy
- Low Start–up Current (13 µA typ.)
- Wide V<sub>cc</sub> Range
- 300 mA / 500 mA Totem Pole Driver with 12 V Gate Clamp
- Robust Protection Features
  - ♦ OVP on V<sub>CC</sub>
  - Programmable Over Voltage / LED Open Circuit Protection
  - Cycle-by-cycle Peak Current Limit
  - Winding Short Circuit Protection
  - Secondary Diode Short Protection
  - Output Short Circuit Protection
  - Shorted Current Sense Protection
  - User Programmable NTC Based Thermal Foldback
  - Thermal Shutdown
  - ◆ V<sub>cc</sub> Undervoltage Lockout
  - Brown–out Protection
- Pb–Free, Halide–Free Product
- Four Versions: NCL30088A, B, C and D (See Table 1)

#### **Typical Applications**

- Integral LED Bulbs and Tubes
- LED Light Engines
- LED Drivers/Power Supplies
- Electronic Control Gear for LED Lighting



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8 1 SOIC-8 NB CASE 751

#### MARKING DIAGRAM



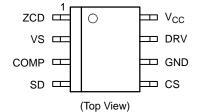
L30088x = Specific Device Code

- x = A, B, C, D
- = Assembly Location
- L = Wafer Lot
- Y = Year W = Work

Α

- W = Work Week
- = Pb-Free Package

#### PIN CONNECTIONS



#### **ORDERING INFORMATION**

See detailed ordering and shipping information in the package dimensions section on page 25 of this data sheet.

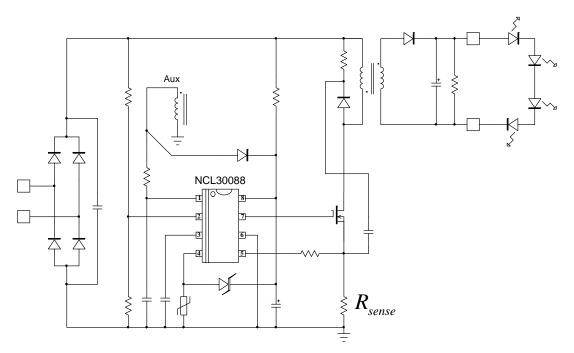


Figure 1. Typical Application Schematic in a Flyback Converter

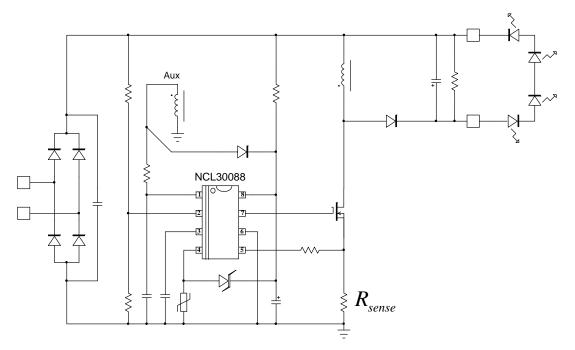


Figure 2. Typical Application Schematic in a Buck–Boost Converter

#### Table 1. FOUR NCL30088 VERSIONS

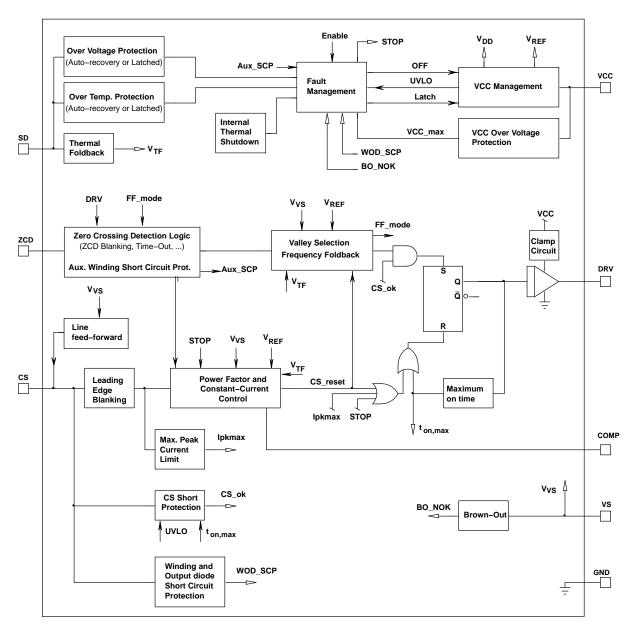
Part Number	Protection Mode	Current Regulation Reference Voltage (V <sub>REF</sub> )	Recommended for (*):
NCL30088A	Latching-off	250 mV	Isolated converters. Non–isolated converters with $V_{out} \le \sqrt{2}  \cdot  (V_{in,rms})_{LL}$
NCL30088B	Auto-recovery	250 mV	Isolated converters. Non–isolated converters with $V_{out} \le \sqrt{2}  \cdot  (V_{in,rms})_{LL}$
NCL30088C	Latching-off	200 mV	Non–isolated converters with $V_{out} > \sqrt{2}  \cdot  (V_{in,rms})_{LL}$
NCL30088D	Auto-recovery	200 mV	Non–isolated converters with $V_{out} > \sqrt{2}  \cdot  (V_{in,rms})_{LL}$

\*(V<sub>in,rms</sub>)<sub>LL</sub> designates the lowest line rms voltage. Refer to AND9200/D for more details. (<u>http://www.onsemi.com/pub\_link/Collateral/AND9200–D.PDF</u>).

#### Table 2. PIN FUNCTION DESCRIPTION

Pin No.	Pin Name	Function	Pin Description
1	ZCD	Zero Crossing Detection	Connected to the auxiliary winding, this pin detects the core reset event.
2	VS	Input Voltage Sensing	This pin observes the input voltage rail and protects the LED driver in case of too low mains conditions (brown-out). This pin also observes the input voltage rail for: – Power Factor Correction – Valley lockout
3	COMP	Filtering Capacitor	This pin receives a filtering capacitor for power factor correction. Typical values ranges from 1 – 4.70 $\mu F$
4	SD	Thermal Foldback and Shutdown	Connecting an NTC to this pin allows the user to program thermal current fold- back threshold and slope. A Zener diode can also be used to pull–up the pin and stop the controller for adjustable OVP protection.
5	CS	Current Sense	This pin monitors the primary peak current.
6	GND	-	Controller ground pin.
7	DRV	Driver Output	The driver's output to an external MOSFET
8	V <sub>CC</sub>	IC Supply Pin	This pin is the positive supply of the IC. The circuit starts to operate when $V_{CC}$ exceeds 18 V and turns off when $V_{CC}$ goes below 8.8 V (typical values). After start–up, the operating range is 9.4 V up to 25.5 V ( $V_{CC(OVP)}$ minimum level).

### **Internal Circuit Architecture**





#### Table 3. MAXIMUM RATINGS TABLE

Symbol	Rating	Value	Unit
V <sub>CC(MAX)</sub> I <sub>CC(MAX)</sub>	Maximum Power Supply voltage, $V_{CC}$ pin, continuous voltage Maximum current for $V_{CC}$ pin	-0.3 to 30 Internally limited	V mA
V <sub>DRV(MAX)</sub> I <sub>DRV(MAX)</sub>	Maximum driver pin voltage, DRV pin, continuous voltage Maximum current for DRV pin	–0.3, V <sub>DRV</sub> (Note 1) –300, +500	V mA
V <sub>MAX</sub> I <sub>MAX</sub>	Maximum voltage on low power pins (except DRV and $V_{CC}$ pins) Current range for low power pins (except DRV and $V_{CC}$ pins)	-0.3, 5.5 (Notes 2 and 5) -2, +5	V mA
$R_{\theta J-A}$	Thermal Resistance Junction-to-Air	180	°C/W
T <sub>J(MAX)</sub>	Maximum Junction Temperature	150	°C
	Operating Temperature Range	-40 to +125	°C
	Storage Temperature Range	-60 to +150	°C
	ESD Capability, HBM model (Note 3)	3.5	kV
	ESD Capability, MM model (Note 3)	250	V
	ESD Capability, CDM model (Note 3)	2	kV

Stresses exceeding those listed in the Maximum Ratings table may damage the device. If any of these limits are exceeded, device functionality should not be assumed, damage may occur and reliability may be affected.

 V<sub>DRV</sub> is the DRV clamp voltage V<sub>DRV(high)</sub> when V<sub>CC</sub> is higher than V<sub>DRV(high)</sub>. V<sub>DRV</sub> is V<sub>CC</sub> otherwise.
This level is low enough to guarantee not to exceed the internal ESD diode and 5.5–V Zener diode. More positive and negative voltages can be applied if the pin current stays within the -2-mA / 5-mA range.

3. This device contains ESD protection and exceeds the following tests: Human Body Model 3500 V per JEDEC Standard JESD22-A114E, Machine Model Method 250 V per JEDEC Standard JESD22-A115B, Charged Device Model 2000 V per JEDEC Standard JESD22-C101E.

This device contains latch-up protection and has been tested per JEDEC Standard JESD78D, Class I and exceeds ±100 mA 4.

5. Recommended maximum V<sub>S</sub> voltage for optimal operation is 4 V. –0.3 V to +4.0 V is hence, the V<sub>S</sub> pin recommended range.

Table 4. ELECTRICAL CHARACTERISTICS (Unless otherwise noted: For typical values T<sub>J</sub> = 25°C, V<sub>CC</sub> = 12 V, V<sub>ZCD</sub> = 0 V,  $V_{CS} = 0 \text{ V}, V_{SD} = 1.5 \text{ V}$ ) For min/max values  $T_J = -40^{\circ}\text{C}$  to  $+125^{\circ}\text{C}, V_{CC} = 12 \text{ V}$ )

Description	Test Condition	Symbol	Min	Тур	Max	Unit
STARTUP AND SUPPLY CIRCUITS						
Supply Voltage Startup Threshold Minimum Operating Voltage Hysteresis V <sub>CC(on)</sub> – V <sub>CC(off)</sub> Internal logic reset	$V_{CC}$ rising $V_{CC}$ rising $V_{CC}$ falling	V <sub>CC(on)</sub> V <sub>CC(off)</sub> V <sub>CC(HYS)</sub> V <sub>CC(reset)</sub>	16.0 8.2 8 4	18.0 8.8 - 5	20.0 9.4 - 6	V
V <sub>CC</sub> Over Voltage Protection Threshold		V <sub>CC(OVP)</sub>	25.5	26.8	28.5	V
V <sub>CC(off)</sub> noise filter V <sub>CC(reset)</sub> noise filter		t <sub>VCC(off)</sub> t <sub>VCC(reset)</sub>		5 20	_	μS
Startup current		I <sub>CC(start)</sub>	-	13	30	μΑ
Startup current in fault mode		I <sub>CC(sFault)</sub>		58	75	μΑ
Supply Current Device Disabled/Fault Device Enabled/No output load on pin 7 Device Switching (F <sub>SW</sub> = 65 kHz)	$V_{CC} > V_{CC(off)}$ $F_{sw} = 65 \text{ kHz}$ $C_{DRV} = 470 \text{ pF}, F_{sw} = 65 \text{ kHz}$	I <sub>CC1</sub> I <sub>CC2</sub> I <sub>CC3</sub>	0.8 _ _	1.0 2.6 3.0	1.2 4.0 4.5	mA

CURRENT SENSE

Maximum Internal current limit	V <sub>ILIM</sub>	0.95	1.00	1.05	V
Leading Edge Blanking Duration for $V_{ILIM}$	t <sub>LEB</sub>	240	300	360	ns

6. Guaranteed by Design

 A NTC is generally placed between the SD and GND pins. Parameters R<sub>TF(start)</sub>, R<sub>TF(stop)</sub>, R<sub>OTP(off)</sub> and R<sub>OTP(on)</sub> give the resistance the NTC must exhibit to respectively, enter thermal foldback, stop thermal foldback, trigger the OTP limit and allow the circuit recovery after an OTP situation.

8. At startup, when V<sub>CC</sub> reaches V<sub>CC(on)</sub>, the controller blanks OTP for more than 250 µs to avoid detecting an OTP fault by allowing the SD pin voltage to reach its nominal value if a filtering capacitor is connected to the SD pin.

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Description	Test Condition	Symbol	Min	Тур	Max	Unit
CURRENT SENSE			-			
Propagation delay from current detection to gate off-state		tı∟ıM	-	100	150	ns
Maximum on-time		t <sub>on(MAX)</sub>	26	36	46	μs
Threshold for immediate fault protection activation		V <sub>CS(stop)</sub>	1.35	1.50	1.65	V
Leading Edge Blanking Duration for $V_{CS(stop)}$		t <sub>BCS</sub>	-	150	-	ns
Current source for CS to GND short detection		I <sub>CS(short)</sub>	400	500	600	μΑ
Current sense threshold for CS to GND short detection	V <sub>CS</sub> rising	V <sub>CS(low)</sub>	30	65	100	mV
GATE DRIVE						
Drive Resistance DRV Sink DRV Source		R <sub>SNK</sub> R <sub>SRC</sub>		13 30	-	Ω
Drive current capability DRV Sink (Note 6) DRV Source (Note 6)		I <sub>SNK</sub> I <sub>SRC</sub>		500 300	-	mA
Rise Time (10% to 90%)	C <sub>DRV</sub> = 470 pF	t <sub>r</sub>	-	40	-	ns
Fall Time (90% to 10%)	C <sub>DRV</sub> = 470 pF	t <sub>f</sub>	-	30	-	ns
DRV Low Voltage	$\label{eq:VCC} \begin{array}{l} V_{CC} = V_{CC(off)} \text{+} 0.2 \text{ V} \\ C_{DRV} = 470 \text{ pF},  R_{DRV} \text{=} 33 \text{ k} \Omega \end{array}$	V <sub>DRV(low)</sub>	8	-	-	V
DRV High Voltage	$\label{eq:V_CC} \begin{array}{l} V_{CC} = V_{CC(MAX)} \\ C_{DRV} = 470 \ \text{pF}, \ R_{DRV} {=} 33 \ \text{k}\Omega \end{array}$	$V_{DRV(high)}$	10	12	14	V
ZERO VOLTAGE DETECTION CIRCUIT						
Upper ZCD threshold voltage	V <sub>ZCD</sub> rising	V <sub>ZCD(rising)</sub>	-	90	150	mV
Lower ZCD threshold voltage	V <sub>ZCD</sub> falling	V <sub>ZCD(falling)</sub>	35	55	-	mV
ZCD hysteresis		V <sub>ZCD(HYS)</sub>	15	-	-	mV
Propagation Delay from valley detection to DRV high	V <sub>ZCD</sub> falling	T <sub>DEM</sub>	-	100	300	ns
Blanking delay after on-time		T <sub>ZCD(blank1)</sub>	1.12	1.50	1.88	μS
Timeout after last DEMAG transition		T <sub>TIMO</sub>	5.0	6.5	8.0	μs
Pulling-down resistor	$V_{ZCD} = V_{ZCD(falling)}$	R <sub>ZCD(PD)</sub>	-	200	-	kΩ
CONSTANT CURRENT AND POWER FACTOR CON	TROL					
Reference Voltage at $T_J = 25^{\circ}C$	A and B versions C and D versions	V <sub>REF</sub>	245 195	250 200	255 205	mV
Reference Voltage $T_J = 25^{\circ}C$ to $100^{\circ}C$	A and B versions C and D versions	V <sub>REF</sub>	242.5 192.5	250.0 200.0	257.5 207.5	mV
Reference Voltage $T_J = -40^{\circ}C$ to $125^{\circ}C$	A and B versions C and D versions	V <sub>REF</sub>	240 190	250 200	260 210	mV
Current sense lower threshold	V <sub>CS</sub> falling	V <sub>CS(low)</sub>	20	55	100	mV
V <sub>control</sub> to current setpoint division ratio		V <sub>ratio</sub>	-	4	-	_
Error amplifier gain	V <sub>REFX</sub> =V <sub>REF</sub>	G <sub>EA</sub>	40	50	60	μS
Error amplifier current capability	V <sub>REFX</sub> =V <sub>REF</sub>	I <sub>EA</sub>	Ī	±60		μA

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At startup, when V<sub>CC</sub> reaches V<sub>CC(on)</sub>, the controller blanks OTP for more than 250 μs to avoid detecting an OTP fault by allowing the SD pin voltage to reach its nominal value if a filtering capacitor is connected to the SD pin.

Table 4. ELECTRICAL CHARACTERISTICS (Unless otherwise noted: For typical values $T_J = 25^{\circ}C$ , $V_{CC} = 12$ V, $V_{ZCD} = 0$ V,
$V_{CS} = 0 \text{ V}, V_{SD} = 1.5 \text{ V})$ For min/max values $T_J = -40^{\circ}\text{C}$ to $+125^{\circ}\text{C}, V_{CC} = 12 \text{ V})$

Description	Test Condition	Symbol	Min	Тур	Max	Unit
CONSTANT CURRENT AND POWER FACTOR CON	TROL	·		-	<u> </u>	
COMP Pin Start-up Current Source	COMP pin grounded	I <sub>EA_STUP</sub>		140		μΑ
LINE FEED FORWARD			-	-		-
V <sub>VS</sub> to I <sub>CS(offset)</sub> conversion ratio		K <sub>LFF</sub>	18	20	22	μS
Line feed-forward current on CS pin	DRV high, $V_{VS}$ = 2 V	I <sub>FF</sub>	35	40	45	μΑ
Offset current maximum value	$V_{VS} > 5 V$	I <sub>offset(MAX)</sub>	80	100	120	μΑ
VALLEY LOCKOUT SECTION			-	-		
Threshold for high-line range (HL) detection	V <sub>VS</sub> rising	V <sub>HL</sub>	2.28	2.40	2.52	V
Threshold for low-line range (LL) detection	V <sub>VS</sub> falling	V <sub>LL</sub>	2.18	2.30	2.42	V
Blanking time for line range detection		t <sub>HL(blank)</sub>	15	25	35	ms
FAULT PROTECTION			-	-		-
Thermal Shutdown (Note 6)	F <sub>SW</sub> = 65 kHz	T <sub>SHDN</sub>	130	150	170	°C
Thermal Shutdown Hysteresis		T <sub>SHDN(HYS)</sub>	-	50	-	°C
Threshold voltage for output short circuit or auxiliary winding short circuit detection		V <sub>ZCD(short)</sub>	0.8	1.0	1.2	V
Short circuit detection Timer	V <sub>ZCD</sub> < V <sub>ZCD(short)</sub>	t <sub>OVLD</sub>	70	90	110	ms
Auto-recovery timer duration		t <sub>recovery</sub>	3	4	5	S
SD pin Clamp series resistor		R <sub>SD(clamp)</sub>		1.6		kΩ
Clamped voltage	SD pin open	V <sub>SD(clamp)</sub>	1.13	1.35	1.57	V
SD pin detection level for OVP	V <sub>SD</sub> rising	V <sub>OVP</sub>	2.35	2.50	2.65	V
Delay before OVP or OTP confirmation (OVP and OTP)		T <sub>SD(delay)</sub>	22.5	30.0	37.5	μs
Reference current for direct connection of an NTC (Note 8)		I <sub>OTP(REF)</sub>	80	85	90	μΑ
Fault detection level for OTP (Note 7)	V <sub>SD</sub> falling	V <sub>OTP(off)</sub>	0.47	0.50	0.53	V
SD pin level for operation recovery after an OTP detection	V <sub>SD</sub> rising	V <sub>OTP(on)</sub>	0.66	0.70	0.74	V
OTP blanking time when circuit starts operating (Note 8)		t <sub>OTP(start)</sub>	250		370	μs
SD pin voltage at which thermal fold–back starts ( $V_{REF}$ is decreased)		V <sub>TF(start)</sub>	0.94	1.00	1.06	V
SD pin voltage at which thermal fold-back stops (V_{REF} is clamped to V_{REF50})		V <sub>TF(stop)</sub>	0.64	0.69	0.74	V
V <sub>TF(start)</sub> over I <sub>OTP(REF)</sub> ratio (Note 7)	$T_J = +25^{\circ}C \text{ to } +125^{\circ}C$	R <sub>TF(start)</sub>	10.8	11.7	12.6	kΩ
V <sub>TF(stop)</sub> over I <sub>OTP(REF)</sub> ratio (Note 7)	$T_J = +25^{\circ}C \text{ to } +125^{\circ}C$	R <sub>TF(stop)</sub>	7.4	8.1	8.8	kΩ
V <sub>OTP(off)</sub> over I <sub>OTP(REF)</sub> ratio (Note 7)	$T_J = +25^{\circ}C \text{ to } +125^{\circ}C$	R <sub>OTP(off)</sub>	5.4	5.9	6.4	kΩ
V <sub>OTP(on)</sub> over I <sub>OTP(REF)</sub> ratio (Note 7)	$T_J = +25^{\circ}C \text{ to } +125^{\circ}C$	R <sub>OTP(on)</sub>	7.5	8.1	8.7	kΩ
$V_{REF} @ V_{SD} = 600 \text{ mV}$ (SD pin falling no OTP detection) (percent of $V_{REF}$ )		V <sub>REF(50)</sub>	40	50	60	%

6. Guaranteed by Design

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At startup, when V<sub>CC</sub> reaches V<sub>CC(on)</sub>, the controller blanks OTP for more than 250 μs to avoid detecting an OTP fault by allowing the SD pin voltage to reach its nominal value if a filtering capacitor is connected to the SD pin.

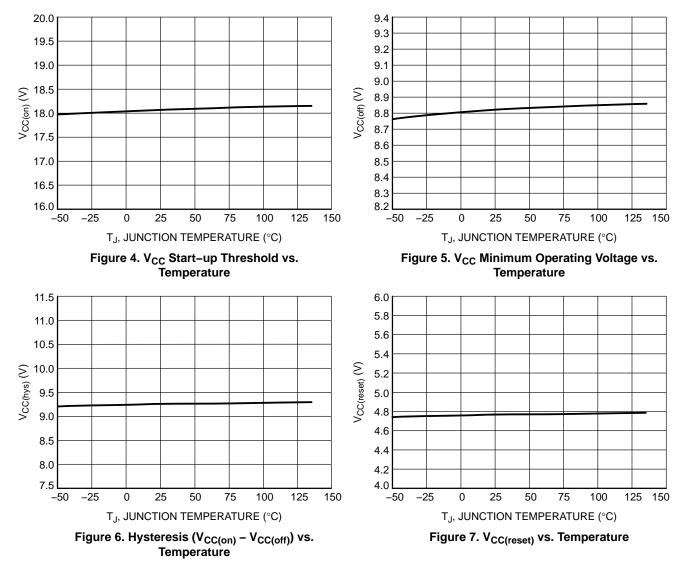
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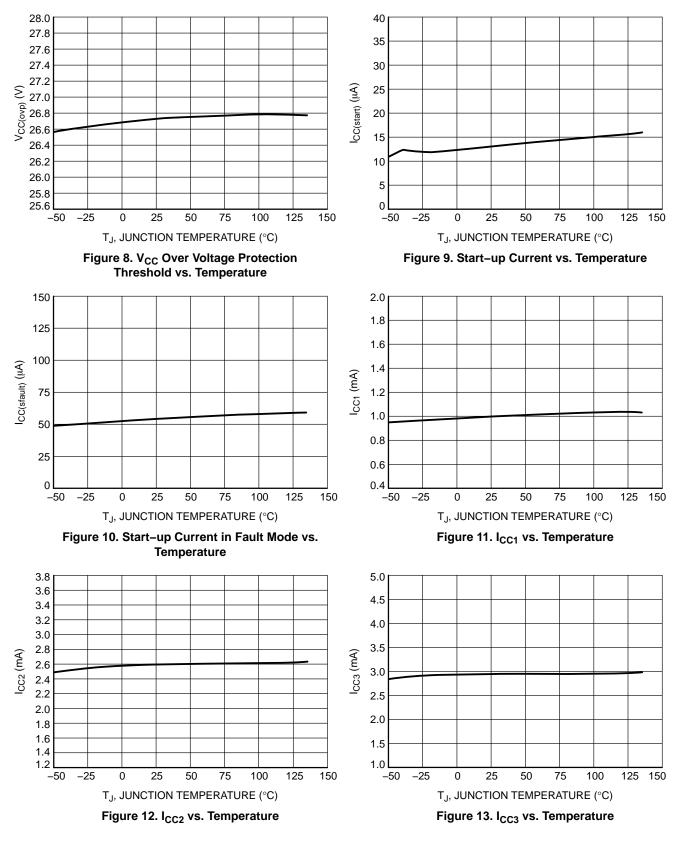
Description	Test Condition	Symbol	Min	Тур	Max	Unit
BROWN-OUT						
Brown–Out ON level (IC start pulsing)	V <sub>S</sub> rising	V <sub>BO(on)</sub>	0.95	1.00	1.05	V
Brown–Out OFF level (IC shuts down)	V <sub>S</sub> falling	V <sub>BO(off)</sub>	0.85	0.90	0.95	V
BO comparators delay		t <sub>BO(delay)</sub>		30		μs
Brown–Out blanking time		t <sub>BO(blank)</sub>	15	25	35	ms
V <sub>S</sub> pin Pulling–down Current	$V_{S} = V_{BO(on)}$	I <sub>BO(bias)</sub>	50	250	450	nA

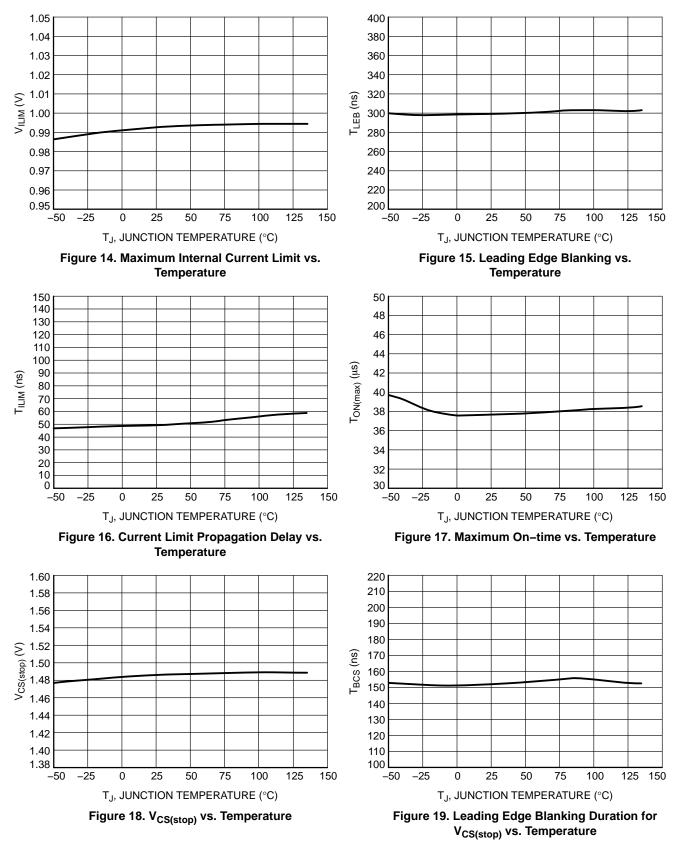
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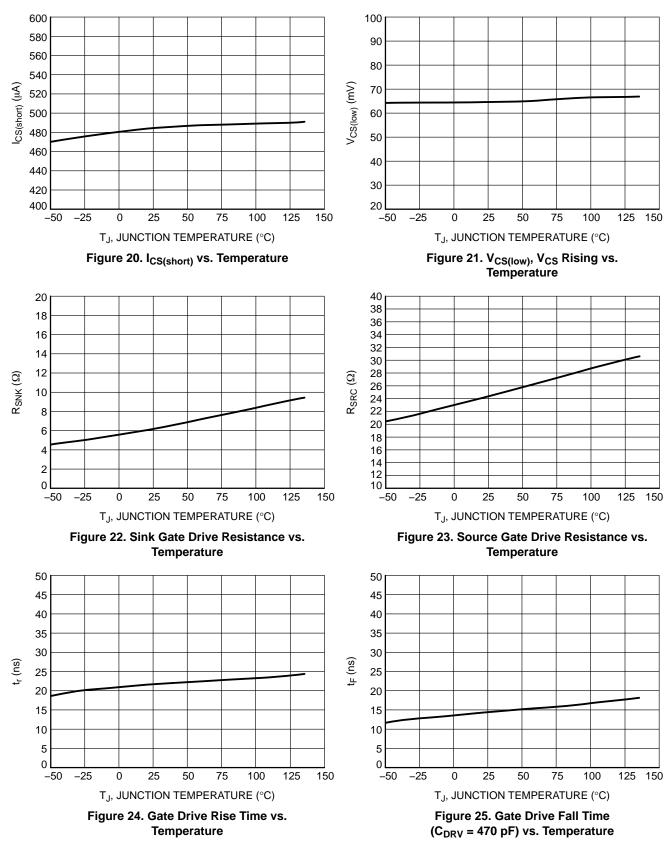
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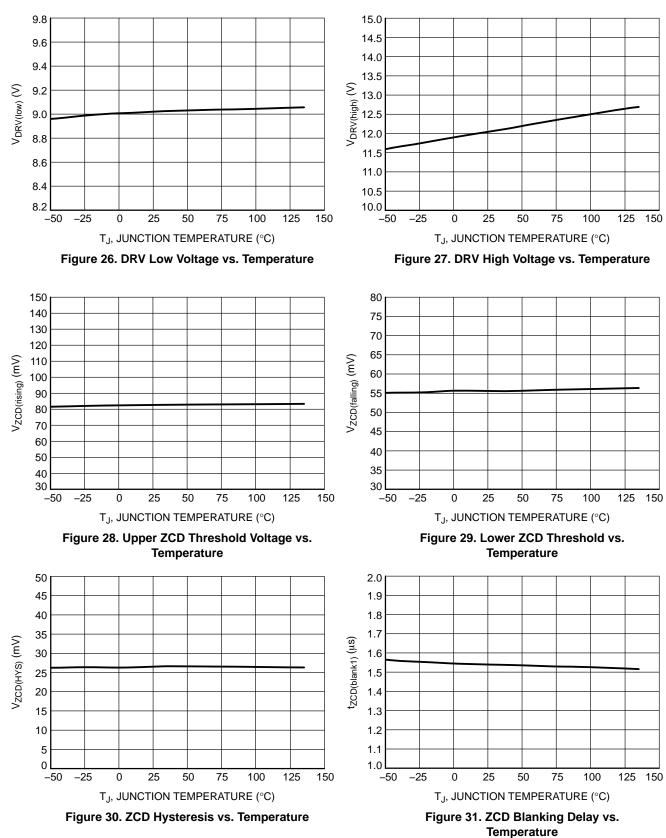




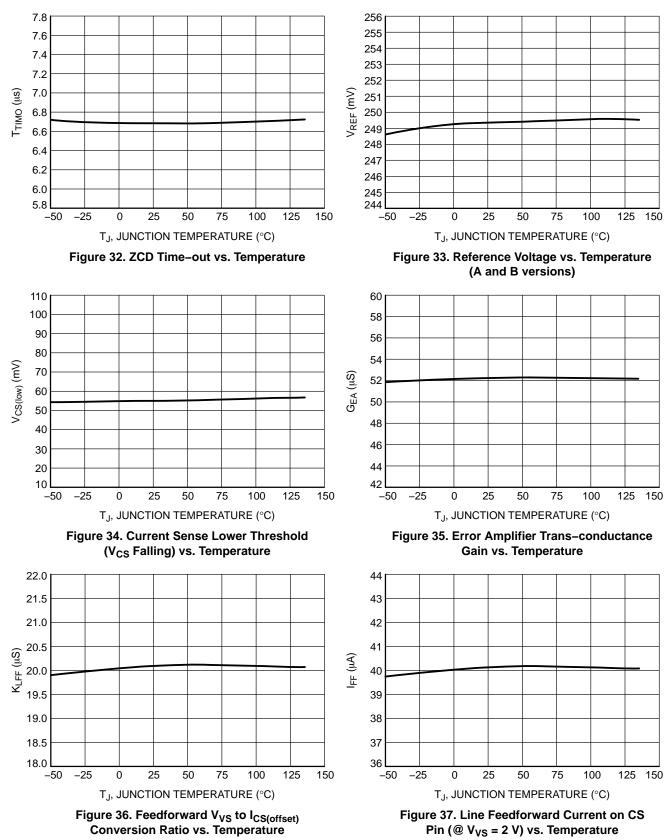




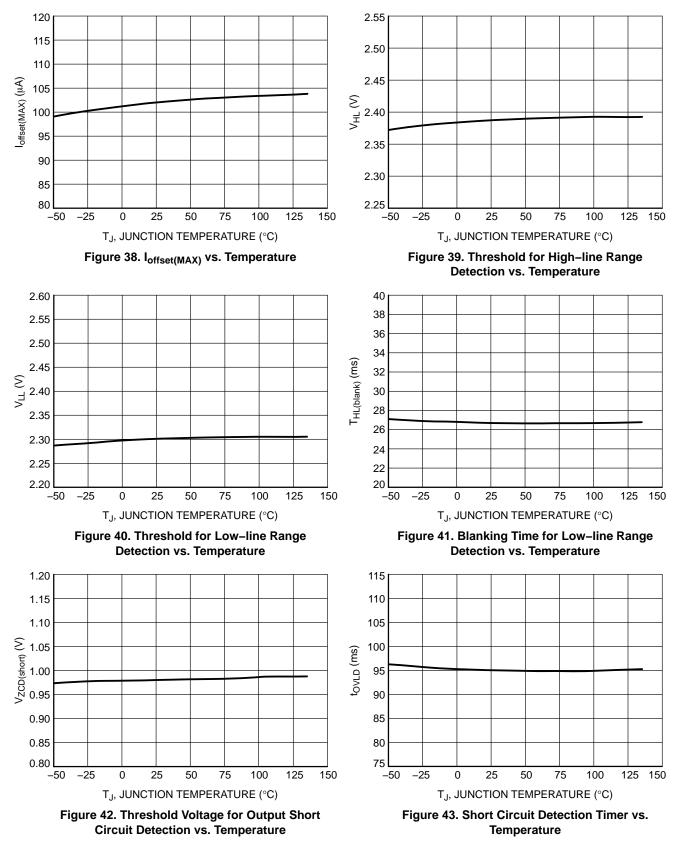




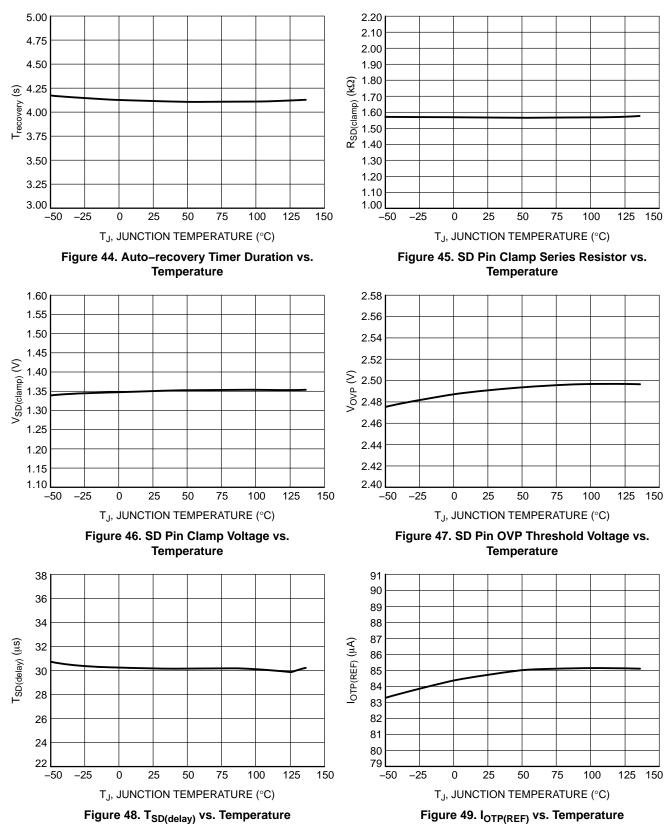




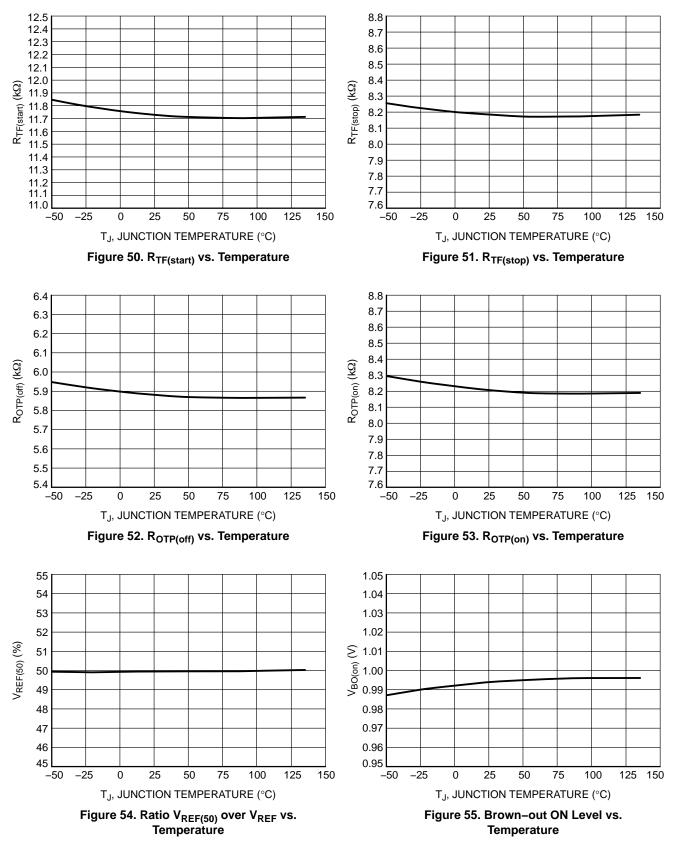


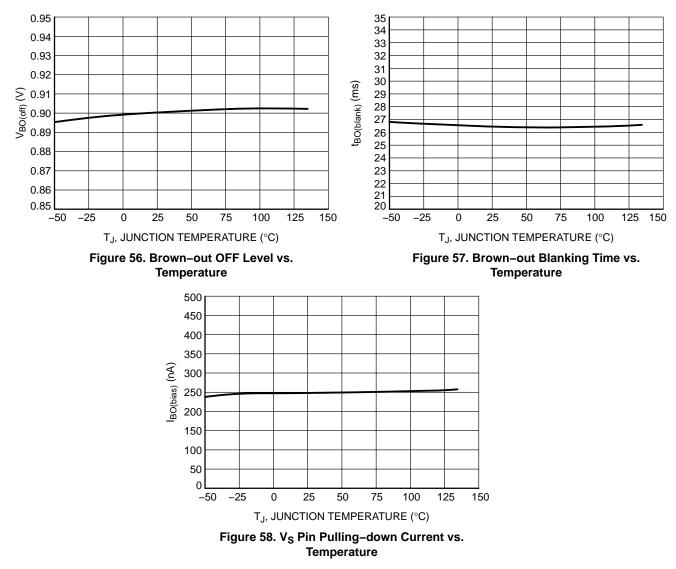












#### **Application Information**

The NCL30088 is a driver for power-factor corrected flyback and non-isolated buck-boost and SEPIC converters. Its current-mode, quasi-resonant architecture optimizes the efficiency by turning on the MOSFET when its drain-source voltage is minimal (valley). At high line, the circuit delays the MOSFET turn on until the second valley is detected to reduce the switching losses. A proprietary circuitry ensures both accurate regulation of the output current (without the need for a secondary-side feedback) and near-unity power factor correction. The circuit contains a suite of powerful protections to ensure a robust LED driver design without the need for extra components or overdesign.

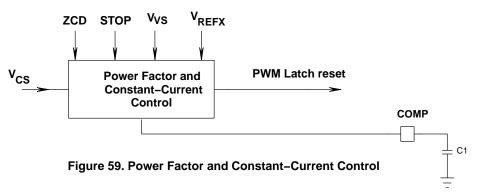
- Quasi-Resonance Current-Mode Operation: implementing quasi-resonance operation in peak current-mode control, the NCL30088 optimizes the efficiency by turning on the MOSFET when its drain-source voltage is minimal (valley). In light-load conditions, the circuit changes valleys to reduce the switching losses. For stable operation, the valley at which the MOSFET switches on remains locked until the input voltage or the output current set-point significantly changes.
- **Primary–Side Constant–Current Control with Power Factor Correction:** a proprietary circuitry allows the LED driver to achieve both near–unity power factor correction and accurate regulation of the output current without requiring any secondary–side feedback (no optocoupler needed). A power factor as high as 0.99 and an output current deviation below ±2% are typically obtained.
- Main protection features:
  - Over Temperature Thermal Fold–back / Shutdown/ Over Voltage Protection: the NCL30088 features a gradual current foldback to protect the driver from excessive temperature down to 50% of the programmed current. This represents a power reduction of the LED by more than 50%. If the temperature continues to rise after this point to a second level, the controller stops operating. This mode would only be expected to be reached if there is a severe fault. The first and second temperature thresholds depend on the value of the NTC

connected to the SD pin. Note, the SD pin can also be used to shutdown the device by pulling this pin below the  $V_{OTP(off)}$  min level. A Zener diode can also be used to pull–up the pin and stop the controller for adjustable OVP protection. Both protections are latching–off (A and C versions) or auto–recovery (the circuit can recover operation after 4–s delay has elapsed – B and D versions).

- Cycle-by-cycle peak current limit: when the current sense voltage exceeds the internal threshold V<sub>ILIM</sub>, the MOSFET is immediately turned off (cycle-by-cycle current limitation).
- Winding or Output Diode Short–Circuit Protection: an additional comparator senses the CS signal and stops the controller if it exceeds 150% x VILIM for 4 consecutive cycles. This feature can protect the converter if a winding is shorted or if the output diode is shorted or simply if the transformer saturates. This protection is latching–off (A and C versions) or auto–recovery (B and D versions).
- Output Short-circuit protection: if the ZCD pin voltage remains low for a 90-ms time interval, the controller detects that the output or the ZCD pin is grounded and hence, stops operation. This protection is latching-off (A and C versions) or auto-recovery (B and D versions).
- **Open LED protection:** if the V<sub>CC</sub> pin voltage exceeds the OVP threshold, the controller shuts down and waits 4 seconds before restarting switching operation.
- Floating or Short Pin Detection: the circuit can detect most of these situations which helps pass safety tests.

#### **Power Factor and Constant Current Control**

The NCL30088 embeds an analog/digital block to control the power factor and regulate the output current by monitoring the ZCD,  $V_S$  and CS pin voltages (signals ZCD,  $V_S$  and  $V_{CS}$  of Figure 59). This circuitry generates the current setpoint ( $V_{CONTROL}/4$ ) and compares it to the current sense signal ( $V_{CS}$ ) to dictate the MOSFET turning off event when  $V_{CS}$  exceeds  $V_{CONTROL}/4$ .



As illustrated in Figure 59, the V<sub>S</sub> pin provides the sinusoidal reference necessary for shaping the input current. The obtained current reference is further modulated so that when averaged over a half–line period, it is equal to the output current reference (V<sub>REFX</sub>). This averaging process is made by an internal Operational Trans–conductance Amplifier (OTA) and the capacitor connected to the COMP pin (C1 of Figure 59). Typical COMP capacitance is 1  $\mu$ F and should not be less than 470 nF to ensure stability. The COMP ripple does not affect the power factor performance as the circuit digitally eliminates it when generating the current setpoint.

If the  $V_S$  pin properly conveys the sinusoidal shape, power factor will be close to unity and the Total Harmonic Distortion (THD) will be low. In any case, the output current will be well regulated following the equation below:

$$I_{out} = \frac{V_{REFX}}{2N_{PS}R_{sense}}$$
 (eq. 1)

Where:

- N<sub>PS</sub> is the secondary to primary transformer turns N<sub>PS</sub> = N<sub>S</sub>/N<sub>P</sub>. N<sub>PS</sub> is 1 in the case of non–isolated buck–boost or SEPIC converter.
- R<sub>sense</sub> is the current sense resistor (see Figure 1).
- $V_{REFX}$  is the output current internal reference.  $V_{REFX} = V_{REF}$  (250 mV in A and B versions and 200 mV in C and D versions, typically) at full load.

The output current reference  $(V_{REFX})$  is  $V_{REF}$  unless the temperature is high enough to activate the thermal fold–back (see "protections" section).

If a major fault is detected, the circuit enters the latched–off or auto–recovery mode and the COMP pin is grounded (except in an UVLO condition). This ensures a clean start–up when the circuit resumes operation.

#### Start-up Sequence

Generally an LED lamp is expected to emit light in < 1 sec and typically within 300 ms. The start–up phase consists of the time to charge the V<sub>CC</sub> capacitor, begin switching and the time to charge the output capacitor until sufficient current flows into the LED string. To speed–up this phase, the following defines the start–up sequence:

- The COMP pin is grounded when the circuit is off. The average COMP voltage needs to exceed the V<sub>S</sub> pin peak value to have the LED current properly regulated (whatever the current target is). To speed–up the COMP capacitance charge and shorten the start–up phase, an internal 80–μA current source adds to the OTA sourced current (60 μA max typically) to charge up the COMP capacitance. The 80–μA current source remains on until the OTA starts to sink current as a result of the COMP pin voltage sufficient rise. At that moment, the COMP pin being near its steady–state value, it is only driven by the OTA.
- If V<sub>CC</sub> drops below the V<sub>CC(off)</sub> threshold because the circuit fails to start–up properly on the first attempt, a new try takes place as soon as V<sub>CC</sub> is recharged to V<sub>CC(on)</sub>. The COMP voltage is not reset at that moment. Instead, the new attempt starts with the COMP level obtained at the end of the previous operating phase.
- If the load is shorted, the circuit will operate in hiccup mode with V<sub>CC</sub> oscillating between V<sub>CC(off)</sub> and V<sub>CC(on)</sub> until the AUX\_SCP protection trips (AUX\_SCP is triggered if the ZCD pin voltage does not exceed 1 V within a 90-ms operation period of time thus indicating a short to ground of the ZCD pin or an excessive load preventing the output voltage from rising). The NCL30088A and NCL30088C latch off in this case. With the B and D versions, the AUX\_SCP protection forces the 4-s auto-recovery delay to reduce the operation duty-ratio. Figure 60 illustrates a start-up sequence with the output shorted to ground, in this second case.

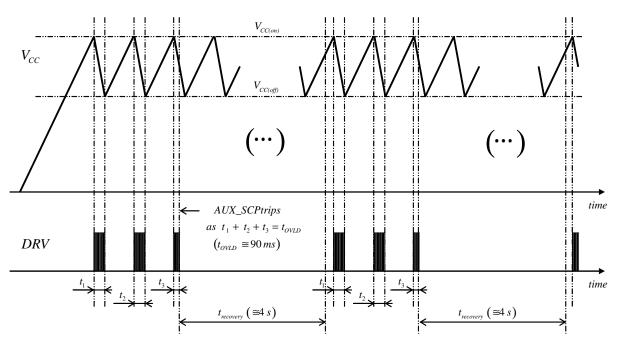


Figure 60. Start-up Sequence in a Load Short-circuit Situation (auto-recovery versions)

#### Zero Crossing Detection Block

The ZCD pin detects when the drain–source voltage of the power MOSFET reaches a valley by crossing below the 55–mV internal threshold. At startup or in case of extremely damped free oscillations, the ZCD comparator may not be able to detect the valleys. To avoid such a situation, the

NCL30088 features a time–out circuit that generates pulses if the voltage on ZCD pin stays below the 55–mV threshold for 6.5 µs. The time–out also acts as a substitute clock for the valley detection and simulates a missing valley in case the free oscillations are too damped.

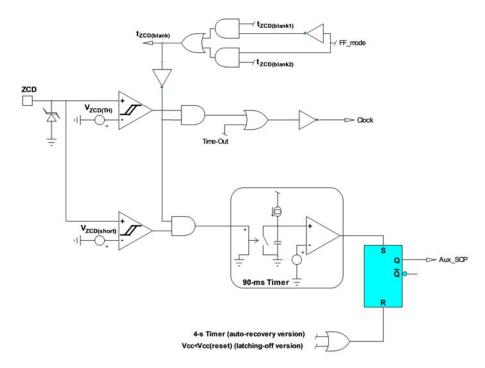


Figure 61. Zero Current Detection Block

If the ZCD pin or the auxiliary winding happen to be shorted, the time–out function would normally make the controller keep switching and hence lead to improper LED current value. The "AUX\_SCP" protection prevents such a stressful operation: a secondary timer starts counting that is only reset when the ZCD voltage exceeds the V<sub>ZCD(short)</sub> threshold (1 V typically). If this timer reaches 90 ms (no ZCD voltage pulse having exceeded V<sub>ZCD(short)</sub> for this time period), the controller detects a fault and stops operation for 4 seconds (B and D versions) or latches off (A and C versions).

The "clock" shown in Figure 61 is used by the "valley selection frequency foldback" circuitry of the block diagram (Figure 3), to generate the next DRV pulse (if no fault prevents it):

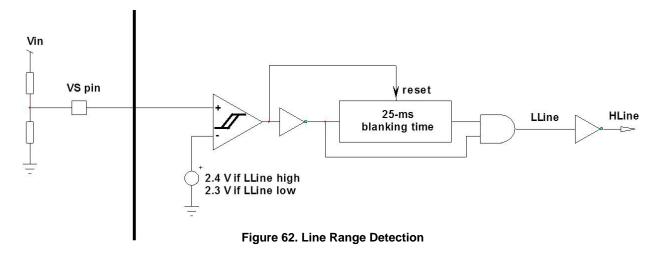
• Immediately when the clock occurs in QR mode at low line or valley 2 at high line (full load)

• After the appropriate number of "clock" pulses in thermal foldback mode

For an optimal operation, the maximum ZCD level should be maintained below 5 V to stay safely below the built in clamping voltage of the pin.

#### Line Range Detection

As sketched in Figure 62, this circuit detects the low–line range if the V<sub>S</sub> pin remains below the V<sub>LL</sub> threshold (2.3 V typical) for more than the 25–ms blanking time. High–line is detected as soon as the V<sub>S</sub> pin voltage exceeds V<sub>HL</sub> (2.4 V typical). These levels roughly correspond to 184–V rms and 192–V rms line voltages if the external resistors divider applied to the V<sub>S</sub> pin is designed to provide a 1–V peak value at 80 V rms.



In the low-line range, conduction losses are generally dominant. Adding a dead-time would further increase these losses. Hence, only a short dead-time is necessary to reach the MOSFET valley. In high-line conditions, switching losses generally are the most critical. It is thus efficient to skip one valley to lower the switching frequency. Hence, under normal operation, the NCL30088 optimizes the efficiency over the line range by turning on the MOSFET at the first valley in low-line conditions and at the second valley in the high-line case. This is illustrated by Figure 63 that sketches the MOSFET Drain-source voltage in both cases. In the event that thermal foldback is activated, additional valleys can be skipped as the power is reduced.

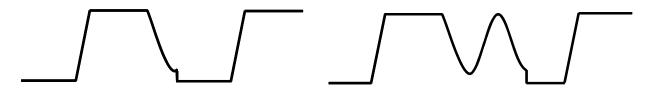


Figure 63. Full-load Operation - Quasi-resonant Mode in low line (left), turn on at valley 2 when in high line (right)

#### Line Feedforward

As illustrated by Figure 64, the input voltage is sensed by the  $V_S$  pin and converted into a current. By adding an

external resistor in series between the sense resistor and the CS pin, a voltage offset proportional to the input voltage is added to the CS signal for the MOSFET on-time.

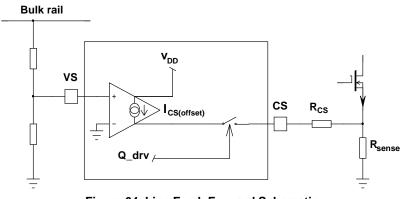


Figure 64. Line Feed–Forward Schematic

In Figure 64, Q\_drv designates the output of the PWM latch which is high for the on-time and low otherwise.

#### Protections

The circuit incorporates a large variety of protections to make the LED driver very rugged. Among them, we can list:

#### **Output Short Circuit Situation**

An overload fault is detected if the ZCD pin voltage remains below  $V_{ZCD(short)}$  for 90 ms. In such a situation, the circuit stops generating pulses until the 4–s delay auto–recovery time has elapsed (B and D versions) or latches off (A and C versions).

#### Winding or Output Diode Short Circuit Protection

If a transformer winding happens to be shorted, the primary inductance will collapse leading the current to ramp up in a very abrupt manner. The  $V_{ILIM}$  comparator (current limitation threshold) will trip to open the MOSFET and eventually stop the current rise. However, because of the

abnormally steep slope of the current, internal propagation delays and the MOSFET turn–off time will make possible the current rise up to 50% or more of the nominal maximum value set by  $V_{ILIM}$ . As illustrated in Figure 65, the circuit uses this current overshoot to detect a winding short circuit. The leading edge blanking (LEB) time for short circuit protection (LEB2) is significantly faster than the LEB time for cycle–by–cycle protection (LEB1). Practically, if four consecutive switching periods lead the CS pin voltage to exceed ( $V_{CS(stop)}=150\% *V_{ILIM}$ ), the controller enters auto–recovery mode in B and D versions (4–s operation interruption between active bursts) and latches off in A and C versions. Similarly, this function can also protect the power supply if the output diode is shorted or if the transformer simply saturates.

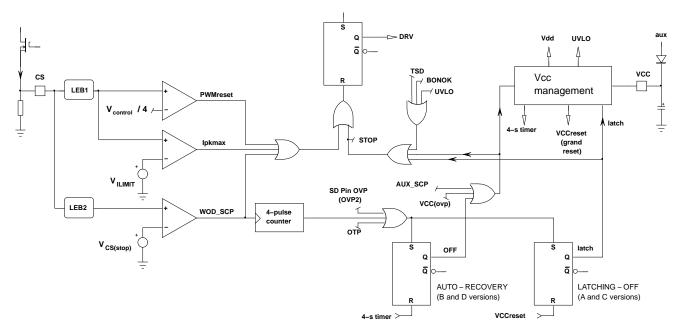


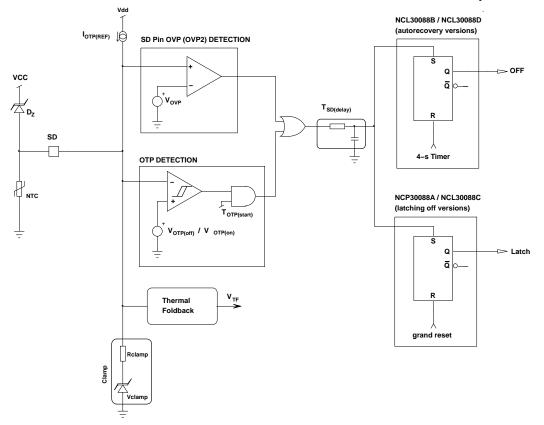
Figure 65. Winding Short Circuit Protection, Max. Peak Current Limit Circuits

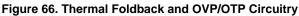
#### V<sub>CC</sub> Over Voltage Protection

The circuit stops generating pulses if  $V_{CC}$  exceeds  $V_{CC(OVP)}$  and enters auto-recovery mode. This feature protects the circuit if the output LED string happens to open or is disconnected.

#### Programmable Over Voltage Protection (OVP2)

Connect a Zener diode between  $V_{CC}$  and the SD pin to set a programmable  $V_{CC}$  OVP (D<sub>Z</sub> of Figure 66). The triggering level is ( $V_Z+V_{OVP}$ ) where  $V_{OVP}$  is the 2.5–V internal threshold. If this protection trips, the NCL30088A and NCL30088C latch off while the NCL30088B and NCL30088D enter the auto–recovery mode.





The SD pin is clamped to about 1.35 V ( $V_{clamp}$ ) through a 1.6–k $\Omega$  resistor ( $R_{clamp}$ ). It is then necessary to inject about

$$\left( \frac{V_{OVP} - V_{clamp}}{R_{clamp}} \right)$$

that is

$$\left(\frac{2.50\,-\,1.35}{1.6\,k}\cong\,700\,\mu A\right)$$

typically, to trigger the OVP protection. This current helps ensure an accurate detection by using the Zener diode far from its knee region.

# Programmable Over Temperature Foldback Protection (OTP)

Connect an NTC between the SD pin and ground to detect an over-temperature condition. In response to a high temperature (detected if  $V_{SD}$  drops below  $V_{TF(start)}$ ), the circuit gradually reduces the LED current down 50% of its nominal value when  $V_{SD}$  reaches  $V_{TF(stop)}$ , in accordance with the characteristic of Figure 67.

If this thermal foldback cannot prevent the temperature from rising (testified by  $V_{SD}$  drop below  $V_{OTP}$ ), the circuit latches off (A and C versions) or enters auto–recovery mode (B and D versions) and cannot resume operation until  $V_{SD}$  exceeds  $V_{OTP(on)}$  to provide some temperature hysteresis (around 10°C typically). The OTP thresholds nearly correspond to the following resistances of the NTC:

- Thermal foldback starts when  $R_{NTC} \le R_{TF(start)}$ (11.7 k $\Omega$ , typically)
- Thermal foldback stops when  $R_{NTC} \le R_{TF(stop)}$  (8.0 k $\Omega$ , typically)
- OTP triggers when  $R_{NTC} \leq R_{OTP(off)}$  (5.9 k $\Omega$ , typically)
- OTP is removed when R<sub>NTC</sub> ≥ R<sub>OTP(on)</sub> (8.0 kΩ, typically) (Note 9)
- This condition is sufficient for operation recovery of the B and D versions. For the A and C versions which latch off when OTP triggers, the circuit further needs to be reset by a V<sub>CC</sub> drop below V<sub>CC(reset)</sub>. An online EXCEL<sup>®</sup>-based design tool is available to aid in selecting the appropriate NTC value.

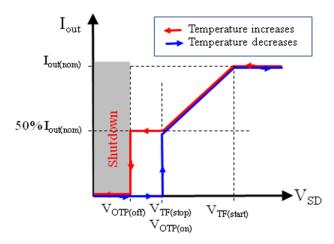
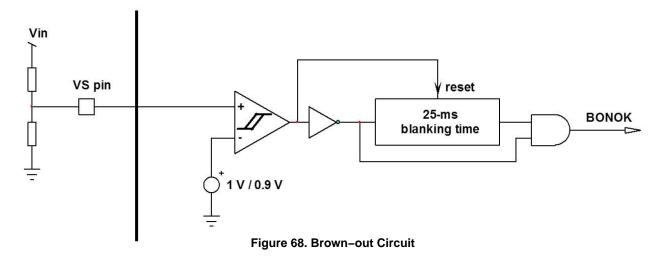


Figure 67. Output Current Reduction versus SD Pin Voltage

At startup, when  $V_{CC}$  reaches  $V_{CC(on)}$ , the OTP comparator is blanked for at least 250 µs in order to allow the SD pin voltage to reach its nominal value if a filtering capacitor is connected to the SD pin. This avoids flickering of the LED light during turn on.

#### **Brown–Out Protection**

The NCL30088 prevents operation when the line voltage is too low for proper operation. As illustrated in Figure 68, the circuit detects a brown–out situation if the V<sub>S</sub> pin remains below the V<sub>BO(off)</sub> threshold (0.9 V typical) for more than the 25–ms blanking time. In this case, the controller stops operating. Operation resumes as soon as the V<sub>S</sub> pin voltage exceeds V<sub>BO(on)</sub> (1.0 V typical) and V<sub>CC</sub> is higher than V<sub>CC(on)</sub>. To ease recovery, the circuit overrides the V<sub>CC</sub> normal sequence (no need for V<sub>CC</sub> cycling down below V<sub>CC(off)</sub>). Instead, its consumption immediately reduces to I<sub>CC(start)</sub> so that V<sub>CC</sub> rapidly charges up to V<sub>CC(on)</sub>. Once done, the circuit re–starts operating.



#### **Die Over Temperature (TSD)**

The circuit stops operating if the junction temperature  $(T_J)$  exceeds 150°C typically. The controller remains off until  $T_J$  goes below nearly 100°C.

#### **Pin Connection Faults**

The circuit addresses most pin connection fault cases:

#### • CS pin short to ground

The circuit senses the CS pin impedance every time it starts–up and after DRV pulses terminated by the  $36-\mu s$  maximum on–time. If the measured impedance does not exceed 120 ohm typically, the circuit stops operating. In practice, it is recommended to place a minimum of 250–ohm in series between the CS pin and the current sense resistor to take into account possible parametric deviations.

#### • Fault of the GND connection

If the GND pin is properly connected, the supply current drawn from the positive terminal of the  $V_{CC}$  capacitor, flows out of the GND pin to return to the negative terminal of the  $V_{CC}$  capacitor. If the GND pin is not connected, the circuit ESD diodes offer another return path. The accidental non–connection of the GND pin is monitored by detecting that one of the ESD diode is conducting. Practically, the ESD diode of CS pin is monitored. If such a fault is detected for 200 µs, the circuit stops generating DRV pulses.

More generally, incorrect pin connection situations (open, grounded, shorted to adjacent pin) are covered by <u>AND9204/D</u>.

#### Fault Modes

The circuit turns off whenever a major faulty condition prevents it from operating:

- Severe OTP (V<sub>SD</sub> level below V<sub>OTP(off)</sub>)
- V<sub>CC</sub> OVP
- OVP2 (additional OVP provided by SD pin)
- Output diode short circuit protection: "WOD\_SCP high"
- Output / Auxiliary winding Short circuit protection: "Aux\_SCP high"
- Die over temperature (TSD)

In this mode, the DRV pulses generation is interrupted.

In the case of a latching–off fault, the circuit stops pulsing until the LED driver is unplugged and  $V_{CC}$  drops below  $V_{CC(reset)}$ . At that moment, the fault is cleared and the circuit could resume operation.

In the auto-recovery case, the circuit cannot generate DRV pulses for the auto-recovery 4–s delay. When this time has elapsed, the circuit recovers operation as soon as the  $V_{CC}$  voltage has exceeded  $V_{CC(on)}$ .

In the B and D versions, all these protections are auto-recovery. The SD pin OTP and OVP, WOD\_SCP and AUX\_SCP are latching off in the A and C versions (see Table 5).

	AUX_SCP	WOD_SCP	SD Pin OTP	SD Pin OVP
NCL30088A*	Latching off	Latching off	Latching off	Latching off
NCL30088B	Auto-recovery	Auto-recovery	Auto-recovery	Auto-recovery
NCL30088C*	Latching off	Latching off	Latching off	Latching off
NCL30088D	Auto-recovery	Auto-recovery	Auto-recovery	Auto-recovery

## Table 5. PROTECTION MODES

### ORDERING INFORMATION

Device	Package Type	Shipping	
NCL30088ADR2G*			
NCL30088BDR2G	SOIC-8	2500 / Tape & Reel	
NCL30088CDR2G*	(Pb-Free/Halide Free)		
NCL30088DDR2G			

\*Please contact local sales representative for availability.

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\*For additional information on our Pb–Free strategy and soldering details, please download the ON Semiconductor Soldering and Mounting Techniques Reference Manual, SOLDERRM/D.

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#### SOIC-8 NB CASE 751-07 **ISSUE AK**

STYLE 1: PIN 1. EMITTER COLLECTOR 2. COLLECTOR З. 4. EMITTER EMITTER 5. BASE 6. 7 BASE 8. EMITTER STYLE 5: PIN 1. DRAIN 2. DRAIN З. DRAIN DRAIN 4. 5. GATE 6. GATE SOURCE 7. 8. SOURCE STYLE 9: PIN 1. EMITTER, COMMON COLLECTOR, DIE #1 COLLECTOR, DIE #2 2. З. EMITTER, COMMON 4. 5. EMITTER, COMMON 6. BASE, DIE #2 BASE, DIE #1 7. 8. EMITTER, COMMON STYLE 13: PIN 1. N.C. 2. SOURCE 3. SOURCE GATE 4. 5. DRAIN 6. DRAIN DRAIN 7. 8. DRAIN STYLE 17: PIN 1. VCC 2. V2OUT V10UT З. 4. TXE 5. RXE 6. VFF GND 7. 8. ACC STYLE 21: PIN 1. CATHODE 1 2. CATHODE 2 З. CATHODE 3 CATHODE 4 4. 5. CATHODE 5 6. COMMON ANODE COMMON ANODE 7. 8. CATHODE 6 STYLE 25: PIN 1. VIN 2 N/C З. REXT 4. GND 5. IOUT 6. IOUT 7. IOUT 8. IOUT STYLE 29: BASE, DIE #1 PIN 1. EMITTER, #1 BASE, #2 2. З. EMITTER, #2 4. 5 COLLECTOR, #2 COLLECTOR, #2 6.

STYLE 2: PIN 1. COLLECTOR, DIE, #1 2. COLLECTOR, #1 COLLECTOR, #2 З. 4 COLLECTOR, #2 BASE, #2 5. EMITTER, #2 6. 7 BASE #1 EMITTER, #1 8. STYLE 6: PIN 1. SOURCE 2. DRAIN 3. DRAIN SOURCE 4. SOURCE 5. 6. GATE GATE 7. 8. SOURCE STYLE 10: PIN 1. GROUND BIAS 1 OUTPUT 2. З. GROUND 4. 5. GROUND BIAS 2 INPUT 6. 7. 8. GROUND STYLE 14: PIN 1. N-SOURCE 2. N-GATE P-SOURCE 3 P-GATE 4. 5. P-DRAIN 6. P-DRAIN N-DRAIN 7. 8. N-DRAIN STYLE 18: PIN 1. ANODE 2. ANODE SOURCE 3. GATE 4. 5. DRAIN 6 DRAIN CATHODE 7. 8. CATHODE STYLE 22: PIN 1. I/O LINE 1 2. COMMON CATHODE/VCC 3 COMMON CATHODE/VCC I/O LINE 3 4. 5. COMMON ANODE/GND 6. I/O LINE 4 7. I/O LINE 5 8. COMMON ANODE/GND STYLE 26: PIN 1. GND 2 dv/dt ENABLE З. 4. ILIMIT 5. SOURCE SOURCE 6. SOURCE 7. 8. VCC STYLE 30: PIN 1. DRAIN 1 DRAIN 1 2 GATE 2 З. SOURCE 2 4. SOURCE 1/DRAIN 2 SOURCE 1/DRAIN 2 5. 6.

STYLE 3: PIN 1. DRAIN, DIE #1 2. DRAIN, #1 3. DRAIN, #2 4. DRAIN, #2 5. GATE, #2 6. SOURCE, #2 7. GATE, #1 8. SOURCE, #1
STYLE 7: PIN 1. INPUT 2. EXTERNAL BYPASS 3. THIRD STAGE SOURCE 4. GROUND 5. DRAIN 6. GATE 3 7. SECOND STAGE Vd 8. FIRST STAGE Vd
STYLE 11: PIN 1. SOURCE 1 2. GATE 1 3. SOURCE 2 4. GATE 2 5. DRAIN 2 7. DRAIN 1 8. DRAIN 1
STYLE 15: PIN 1. ANODE 1 2. ANODE 1 3. ANODE 1 4. ANODE 1 5. CATHODE, COMMON 6. CATHODE, COMMON 7. CATHODE, COMMON 8. CATHODE, COMMON
STYLE 19: PIN 1. SOURCE 1 2. GATE 1 3. SOURCE 2 4. GATE 2 5. DRAIN 2 6. MIRROR 2 7. DRAIN 1 8. MIRROR 1
STYLE 23: PIN 1. LINE 1 IN 2. COMMON ANODE/GND 3. COMMON ANODE/GND 4. LINE 2 IN 5. LINE 2 OUT 6. COMMON ANODE/GND 7. COMMON ANODE/GND 8. LINE 1 OUT
STYLE 27: PIN 1. ILIMIT 2. OVLO 3. UVLO 4. INPUT+ 5. SOURCE 6. SOURCE 7. SOURCE 8. DRAIN

#### DATE 16 FEB 2011

STYLE 4: ANODE ANODE PIN 1. 2. ANODE З. 4. ANODE ANODE 5. 6. ANODE 7 ANODE COMMON CATHODE 8. STYLE 8: PIN 1. COLLECTOR, DIE #1 2. BASE, #1 BASE, #2 З. COLLECTOR, #2 4. COLLECTOR, #2 5. 6. EMITTER, #2 EMITTER, #1 7. 8. COLLECTOR, #1 STYLE 12: PIN 1. SOURCE SOURCE SOURCE 2. 3. 4. GATE 5. DRAIN 6. DRAIN DRAIN 7. 8. DRAIN STYLE 16: PIN 1. EMITTER, DIE #1 2. BASE, DIE #1 EMITTER, DIE #2 3 BASE, DIE #2 4. 5. COLLECTOR, DIE #2 6. COLLECTOR, DIE #2 COLLECTOR, DIE #1 7. COLLECTOR, DIE #1 8. STYLE 20: PIN 1. SOURCE (N) GATE (N) SOURCE (P) 2. 3. 4. GATE (P) 5. DRAIN 6. DRAIN DRAIN 7. 8. DRAIN STYLE 24: PIN 1. BASE 2. EMITTER З. COLLECTOR/ANODE COLLECTOR/ANODE 4. 5. CATHODE CATHODE COLLECTOR/ANODE 6. 7. COLLECTOR/ANODE 8. STYLE 28: PIN 1. SW\_TO\_GND 2. DASIC OFF DASIC\_SW\_DET 3. 4. GND 5. 6. V MON VBULK 7. VBULK 8. VIN

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