## General Description

The F1423 is a 600 MHz to 3000 MHz TX differential input / single-ended output RF amplifier used in transmitter applications.
The F1423 TX Amp provides 13.1 dB gain with +41.8 dBm OIP3 and 5.1 dB noise figure at 2000 MHz . This device uses a single 5 V supply and 120 mA of $\mathrm{I}_{\mathrm{C}}$.

This device is packaged in a $4 \mathrm{~mm} \times 4 \mathrm{~mm}$, 24 -pin Thin QFN with 50 ohm differential RF input and 50 ohm single ended RF output impedances for ease of integration into the signal-path.

## Competitive Advantage

In typical Base Stations, RF Amplifiers are used in the TX traffic paths to drive the transmit power amplifier. The F1423 TX Amplifier offers very high reliability due to its construction using silicon die in a QFN package. The F1423 includes a broadband differential input to accept AC-coupled signals directly from a balanced modulator or RF DAC architecture.

## Applications

- Multi-mode, Multi-carrier Transmitters
- GSM850/900 Base Stations
- PCS1900 Base Stations
- DCS1800 Base Stations
- WiMAX and LTE Base Stations
- UMTS/WCDMA 3G Base Stations
- PHS/PAS Base Stations
- Public Safety Infrastructure


## Features

- Broadband $600 \mathrm{MHz}-3000 \mathrm{MHz}$
- 13.1 dB typical gain @ 2000 MHz
- $\quad 5.1 \mathrm{~dB}$ NF @ 2000 MHz
- +41.8 dBm OIP3 @ 2000 MHz
- +21.5 dBm output P1dB @ 2000 MHz
- Single 5 V supply voltage
- $\mathrm{I}_{\mathrm{CC}}=120 \mathrm{~mA}$
- Up to $+105^{\circ} \mathrm{C} \mathrm{T}_{\text {CASE }}$ operating temperature
- $50 \Omega$ differential input impedance
- $50 \Omega$ single ended output impedance
- Positive gain slope for board loss compensation
- Standby mode for power savings
- $4 \mathrm{~mm} \times 4 \mathrm{~mm}, 24$-pin TQFN package


## Functional Block Diagram



## Ordering Information



## Renesns

## Absolute Maximum Ratings

| Parameter | Symbol | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {cc }}$ to GND | $\mathrm{V}_{\mathrm{cc}}$ | -0.3 | +5.5 | V |
| STBY, Band_Sel | $\mathrm{V}_{\text {Cnt }}$ | -0.3 | $\mathrm{V}_{\text {CC }}+0.25$ | V |
| RBIAS1 | $\mathrm{I}_{\text {RB1 }}$ |  | +1.5 | mA |
| RBIAS2 | $\mathrm{I}_{\text {RB2 }}$ |  | +0.8 | mA |
| RFIN+, RFIN-, Voltage ${ }^{1}$ | $V_{\text {RFin }}$ | -0.02 | +0.02 | V |
| RFIN+, RFIN-, Current ${ }^{1}$ | $\mathrm{I}_{\text {RFin }}$ | -5 | +5 | mA |
| RFOUT externally applied DC voltage | $\mathrm{V}_{\text {RFout }}$ | $\mathrm{V}_{\text {CC }}-0.15$ | $\mathrm{V}_{\mathrm{CC}}+0.15$ | V |
| RF Differential Input Power (applied for 24 hours maximum) | $\mathrm{P}_{\text {in }}$ |  | +22 | dBm |
| Continuous Power Dissipation | $\mathrm{P}_{\text {diss }}$ |  | 1.5 | W |
| Junction Temperature | $\mathrm{T}_{\mathrm{j}}$ |  | 150 | ${ }^{\circ} \mathrm{C}$ |
| Storage Temperature Range | $\mathrm{T}_{\text {st }}$ | -65 | 150 | ${ }^{\circ} \mathrm{C}$ |
| Lead Temperature (soldering, 10s) |  |  | 260 | ${ }^{\circ} \mathrm{C}$ |
| ElectroStatic Discharge - HBM (JEDEC/ESDA JS-001-2014) |  |  | $\begin{gathered} \text { Class } 2 \\ (2000 \mathrm{~V}) \end{gathered}$ |  |
| ElectroStatic Discharge - CDM <br> (JESD 22-C101F) |  |  | $\begin{aligned} & \hline \text { Class C3 } \\ & (1000 \mathrm{~V}) \end{aligned}$ |  |

Note 1: The RFIN+ and RFIN- pins connect to an internal balun that presents a very low impedance to ground.

Stresses above those listed above may cause permanent damage to the device. Functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## Package Thermal and Moisture Characteristics

| $\theta_{\mathrm{JA}}$ (Junction - Ambient) | $40^{\circ} \mathrm{C} / \mathrm{W}$ |
| :--- | :--- |
| $\theta_{\mathrm{JC}}$ (Junction - Case) [The Case is defined as the exposed paddle] | $4^{\circ} \mathrm{C} / \mathrm{W}$ |
| Moisture Sensitivity Rating (Per J-STD-020) | MSL1 |

## F1423 Recommended Operating Conditions

| Parameter | Symbol | Conditions | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supply Voltage(s) | $\mathrm{V}_{\text {c }}$ | All $\mathrm{V}_{\text {cc }}$ pins | 4.75 |  | 5.25 | V |
| Operating Temperature Range | $\mathrm{T}_{\text {CASE }}$ | Case Temperature | -40 |  | +105 | ${ }^{\circ} \mathrm{C}$ |
| RF Frequency Range | $\mathrm{F}_{\text {RF }}$ | Operating Range | 600 |  | $3000^{1}$ | MHz |
| RF Source Impedance | $\mathrm{Z}_{\text {RII }}$ | Differential |  | 50 |  | $\Omega$ |
| RF Load Impedance | $\mathrm{Z}_{\text {RFO }}$ | Single Ended |  | 50 |  | $\Omega$ |
| RF Band Designation ${ }^{2}$ |  |  |  |  |  |  |
| RF Frequency Range | $\mathrm{F}_{\text {RF_LB }}$ | Low-band | 600 |  | 1100 | MHz |
|  | $\mathrm{F}_{\text {RF_MB }}$ | Mid-band | 1400 |  | 2100 |  |
|  | $\mathrm{F}_{\text {RF_HB }}$ | High-band | 2100 |  | $3000^{1}$ |  |
|  | $\mathrm{F}_{\text {R__BB }}$ | Broad-band | 600 |  | $3000^{1}$ |  |

Note 1: Though device linearity is specified over the range from 700 MHz to 2700 MHz , gain flatness up to 3000 MHz is specified in the high-band and broadband tables to account for extended DPD bandwidth requirements.
Note 2: To optimize RF performance, a different output match will be used for each of the 4 RF bands listed (see Table 2). In addition, different value amplifier bias resistors will be used to optimize performance in each of the 4 bands.

## renesas

## F1423 Specification - General

See F1423 Typical Application Circuit. Unless otherwise stated, specifications apply when operated as a TX RF Amplifier, $\mathrm{V}_{\mathrm{CC}}=+5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{C}}=+25^{\circ} \mathrm{C}$.

| Parameter | Symbol | Condition | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Logic Input High | $\mathrm{V}_{\text {IH }}$ |  | 1.1 |  |  | v |
| Logic Input Low | $\mathrm{V}_{\text {IL }}$ |  |  |  | 0.63 |  |
| Logic Current | $\mathrm{I}_{\text {STBY }}$ | STBY pin | -10 |  | +10 | $\mu \mathrm{A}$ |
|  | $\mathrm{I}_{\text {band }}$ | Band_Sel pin | -10 |  | +10 |  |
| Supply Current ${ }^{3}$ | $\mathrm{I}_{\text {CC_LB }}$ | Low-band bias setting |  | 103 |  | mA |
|  | $\mathrm{I}_{\text {CC_M }}$ | Mid-band bias setting |  | 120 |  |  |
|  | $\mathrm{I}_{\text {CC_ } \_ \text {B }}$ | High-band bias setting |  | 120 |  |  |
|  | $\mathrm{ICC}_{\text {C_B }}$ | Broad-band bias setting |  | 120 | $135{ }^{1}$ |  |
| Standby Current | $\mathrm{ICC} \mathrm{\_STBY}$ | STBY = 5V |  | 0.8 | 1.0 | mA |
| Power ON switching time | Ton | 50\% STBY to RF output settled to within $\pm 0.5 \mathrm{~dB}$ |  | 1 |  | $\mu \mathrm{s}$ |
| Power OFF switching time | Toff | 50\% STBY to DC standby current settled to within $\pm 2 \mathrm{~mA}$ of final $\mathrm{I}_{\mathrm{CC}}$ value |  | 1 |  | $\mu \mathrm{S}$ |

Note 1: Items in min/max columns in bold italics are Guaranteed by Test.
Note 2: Items in $\mathrm{min} / \mathrm{max}$ columns that are not bold/italics are Guaranteed by Design Characterization. Note 3: Use external resistors to set amplifier bias currents to optimize device linearity. See Table 2.

## RENESAS

## F1423 SPECIFICATION - LOW-BAND

See F1423 Typical Application Circuit. Unless otherwise stated, specifications apply when operated as a TX RF Amplifier, $\mathrm{V}_{\mathrm{CC}}=+5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{C}}=+25^{\circ} \mathrm{C}, \mathrm{F}_{\mathrm{RF}}=700 \mathrm{MHz}$, Pout $=+7 \mathrm{dBm}, \mathrm{R} 8=2.1 \mathrm{k} \Omega, \mathrm{R} 9=9.1 \mathrm{k} \Omega, \mathrm{C} 1=9 \mathrm{pF}$, Rsource $=50 \Omega$ differential, Rload $=50 \Omega$ single-ended, Band_Sel $=$ open, EVKit trace connector and transformer losses are de-embedded.

| Parameter | Symbol | Condition | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RF Input Return Loss | RFIN $_{\text {RL_LB }}$ |  |  | 17 |  | dB |
| RF Output Return Loss | $\mathrm{RFOUT}_{\text {RL_LB }}$ |  |  | 12.8 |  | dB |
| Common Mode Rejection | $\mathrm{CMRR}_{\text {LB }}$ | 700 MHz to 1100 MHz |  | 20.7 |  | dB |
| Gain | $\mathrm{G}_{\mathrm{LB}}$ |  | $12.0{ }^{1}$ | 12.6 | 13.2 | dB |
| Gain Flatness | $\mathrm{G}_{\text {FLAT_LB }}$ | Any 400 MHz BW from 700 MHz to 1100 MHz |  | 0.4 |  | dB |
| Gain Ripple | $\mathrm{G}_{\text {RIPPLE_LB }}$ | In any 20 MHz range over RF Band |  | $\pm 0.04$ |  | dB |
| Noise Figure ${ }^{3}$ | $\mathrm{NF}_{\text {LB }}$ |  |  | 4.5 |  | dB |
|  |  | $\mathrm{T}_{\text {case }}=+105{ }^{\circ} \mathrm{C}$ |  | 5.4 |  |  |
| Output Third Order Intercept Point ${ }^{3}$ | OIP3 ${ }_{\text {LB }}$ | Pout $=+4 \mathrm{dBm} /$ tone 5 MHz tone separation | $39^{2}$ | 42.5 |  | dBm |
| Output 1dB Compression ${ }^{3}$ | OP1dB ${ }_{\text {LB }}$ |  | 20 | 21.1 |  | dBm |

## F1423 Specification - Mid-Band

See F1423 Typical Application Circuit Unless otherwise stated, specifications apply when operated as a TX RF Amplifier, $\mathrm{V}_{\mathrm{CC}}=+5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{C}}=+25^{\circ} \mathrm{C}, \mathrm{F}_{\mathrm{RF}}=2000 \mathrm{MHz}$, Pout $=+7 \mathrm{dBm}, \mathrm{R} 8=2.4 \mathrm{k} \Omega, \mathrm{R} 9=60.4 \mathrm{k} \Omega, \mathrm{C} 1=9 \mathrm{pF}$, Rsource $=50 \Omega$ differential, Rload = $50 \Omega$ single-ended, Band_Sel = GND, EVKit trace connector and transformer losses are de-embedded.

| Parameter | Symbol | Condition | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RF Input Return loss | $\mathrm{RFIN}_{\text {RL_MB }}$ |  |  | 15 |  | dB |
| RF Output Return Loss | $\mathrm{RFOUT}_{\text {RL_MB }}$ |  |  | 16.5 |  | dB |
| Common Mode Rejection | $\mathrm{CMRR}_{\text {мв }}$ | 1400 MHz to 2100 MHz |  | 19.0 |  | dB |
| Gain | $\mathrm{G}_{\text {мв }}$ |  | $12.5{ }^{1}$ | 13.1 | 13.7 | dB |
| Gain Flatness | $\mathrm{G}_{\text {flat_mb }}$ | Any 400MHz BW from 1400 MHz to 2100 MHz |  | 0.17 |  | dB |
| Gain Ripple | $\mathrm{G}_{\text {RIPPLE_MB }}$ | In any 20 MHz range over RF Band |  | $\pm 0.01$ |  | dB |
| Noise Figure ${ }^{3}$ | $N F_{\text {MB }}$ |  |  | 5.1 |  | dB |
|  |  | $\mathrm{T}_{\text {case }}=+105^{\circ} \mathrm{C}$ |  | 5.8 |  |  |
| Output Third Order Intercept Point ${ }^{3}$ | OIP3 $_{\text {мв }}$ | Pout $=+4 \mathrm{dBm} /$ tone 5 MHz tone separation | $38.8{ }^{2}$ | 41.8 |  | dBm |
| Output 1dB Compression ${ }^{3}$ | OP1dB ${ }_{\text {M }}$ |  | 20.3 | 21.5 |  | dBm |

Note 1: Items in min/max columns in bold italics are Guaranteed by Test.
Note 2: Items in $\mathrm{min} / \mathrm{max}$ columns that are not bold/italics are Guaranteed by Design Characterization.
Note 3: Measured using external 1:1 transformer at the RF input.

## F1423 Specification - High-Band

See F1423 Typical Application Circuit. Unless otherwise stated, specifications apply when operated as a TX RF Amplifier, $\mathrm{V}_{\mathrm{CC}}=+5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{C}}=+25^{\circ} \mathrm{C}, \mathrm{F}_{\mathrm{RF}}=2700 \mathrm{MHz}$, Pout $=+7 \mathrm{dBm}, \mathrm{R} 8=2.4 \mathrm{k} \Omega, \mathrm{R} 9=60.4 \mathrm{k} \Omega, \mathrm{C} 1=6 \mathrm{pF}$, Rsource $=50 \Omega$ differential, Rload $=50 \Omega$ single-ended, Band_Sel $=$ GND, EVKit trace connector and transformer losses are de-embedded.

| Parameter | Symbol | Condition | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RF Input Return loss | RFIN $_{\text {RL_HB }}$ |  |  | 15.5 |  | dB |
| RF Output Return Loss | RFOUT ${ }_{\text {RL_Hв }}$ |  |  | 20 |  | dB |
| Common Mode Rejection | $\mathrm{CMRR}_{\text {нв }}$ | 2100 MHz to 3000 MHz |  | 18.5 |  | dB |
| Gain | $\mathrm{G}_{\text {нв }}$ |  | $12.4{ }^{1}$ | 13.1 | 13.9 | dB |
| Gain Flatness | $\mathrm{G}_{\text {flat_hb }}$ | Any 400 MHz BW from 2100 MHz to 3000 MHz |  | 0.23 |  | dB |
| Gain Ripple | $\mathrm{G}_{\text {RIPPLE_HB }}$ | In any 20 MHz range over RF Band |  | $\pm 0.015$ |  | dB |
| Noise Figure ${ }^{3}$ | $\mathrm{NF}_{\text {нв }}$ |  |  | 6.0 |  | dB |
|  |  | $\mathrm{T}_{\text {case }}=+105^{\circ} \mathrm{C}$ |  | 6.6 |  |  |
| Output Third Order Intercept Point ${ }^{3}$ | OIP3 $_{\text {нв }}$ | Pout $=+4 \mathrm{dBm} /$ tone <br> 5 MHz tone separation |  | 37.3 |  | dBm |
| Output 1dB Compression ${ }^{3}$ | OP1dB ${ }_{\text {Hв }}$ |  | $20.0^{2}$ | 20.6 |  | dBm |

## F1423 Specification - Broad-Band

See F1423 Typical Application Circuit. Unless otherwise stated, specifications apply when operated as a TX RF Amplifier, $\mathrm{V}_{\mathrm{CC}}=+5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{C}}=+25^{\circ} \mathrm{C}, \mathrm{F}_{\mathrm{RF}}=2200 \mathrm{MHz}$, Pout $=+7 \mathrm{dBm}, \mathrm{R} 8=2.4 \mathrm{k} \Omega, \mathrm{R} 9=60.4 \mathrm{k} \Omega, \mathrm{C} 1=9 \mathrm{pF}$, Rsource $=50 \Omega$ differential, Rload $=50 \Omega$ single-ended, Band_Sel = GND, EVKIT trace connector and transformer losses are de-embedded.

| Parameter | Symbol | Condition | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RF Input Return loss | RFIN RL_BB |  |  | 15.0 |  | dB |
| RF Output Return Loss | RFOUT $_{\text {RL_ BB }}$ |  |  | 18.5 |  | dB |
| Common Mode Rejection | $\mathrm{CMRR}_{\text {BB }}$ | 700 MHz to 3000 MHz |  | 18.5 |  | dB |
| Gain | $\mathrm{G}_{\text {BB }}$ |  | $12.6{ }^{1}$ | 13.2 | 13.8 | dB |
| Gain Flatness | $\mathrm{G}_{\text {flat_bb }}$ | Any 400 MHz BW from 700 MHz to 3000 MHz |  | 0.4 |  | dB |
| Gain Ripple | $\mathrm{G}_{\text {RIPPLE_BB }}$ | In any 20 MHz range over 400 MHz BW |  | $\pm 0.04$ |  | dB |
| Gain Slope | $\mathrm{G}_{\text {sLOPE_BB }}$ |  |  | $\pm 0.002$ |  | dB/MHz |
| Noise Figure ${ }^{3}$ | $\mathrm{NF}_{\text {BB }}$ |  |  | 5.2 |  | dB |
|  |  | $\mathrm{T}_{\text {case }}=+105^{\circ} \mathrm{C}$ |  | 5.8 |  |  |
| Output Third Order Intercept Point ${ }^{3}$ | OIP3 $_{\text {BB }}$ | Pout $=+4 \mathrm{dBm} /$ tone 5 MHz tone separation |  | 41.4 |  | dBm |
| Output 1dB Compression ${ }^{3}$ | OP1dB ${ }_{\text {BB }}$ |  | $20.5^{2}$ | 21.4 |  | dBm |

Note 1: Items in min/max columns in bold italics are Guaranteed by Test.
Note 2: Items in $\mathrm{min} / \mathrm{max}$ columns that are not bold/italics are Guaranteed by Design Characterization.
Note 3: Measured using external 1:1 transformer at the RF input.

Table1: STBY Truth Table

| Parameter | Level | Function |
| :---: | :---: | :---: |
| STBY | Logic Low or Open Circuit | Powered On |
|  | Logic High | Powered Off |

Table2: Component Settings for Optimized Linearity Performance per RF band

| Band | Frequency Range <br> $(\mathbf{M H z})$ | Band_Sel <br> $(\mathbf{P i n} \mathbf{1 1})$ | Pin 14 to GND <br> $(\mathbf{k} \Omega)$ | Pin 15 to GND <br> $(\mathbf{k} \Omega)$ | C1 <br> $(\mathbf{p F})$ | $\mathbf{I}_{\mathbf{c c}}$ <br> $(\mathbf{m A})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Low - Band | $600-1100$ | Open | 2.1 | 9.1 | 9 | 104 |
| Mid - Band | $1400-2100$ | GND | 2.4 | 60.4 | 9 | 120 |
| High - Band | $2100-3000$ | GND | 2.4 | 60.4 | 6 | 120 |
| Broad - Band | $700-3000$ | GND | 2.4 | 60.4 | 9 | 120 |

## Typical Operating Conditions (TOC)

Unless otherwise noted for the TOC graphs on the following pages, the following conditions apply.

- Vcc= 5.0 V
- Tcase $=25^{\circ} \mathrm{C}$ (All temperatures are referenced to the exposed paddle).
- $Z_{s}=\mathbf{5 0} 0 \mathrm{Ohms}$ Differential
- $Z_{L}=50$ Ohms Single Ended
- Board configured as defined in Table 2 for each band.
- Pout $=4 \mathrm{dBm}$ / Tone
- 5 MHz Tone Spacing
- EVKIT traces, connectors, and transformer losses are de-embedded.
- S-parameters (S11, S21, S12, and S22) measured using a de-embedded Differential Board EVKit and the inputs are mathematically combined using an ideal 1:1 (50 $\Omega: 50 \Omega$ ) transformer to produce the $\mathbf{2}$ port S-parameters.
- Amplitude and phase imbalances measures RFIN+ to RFOUT and compares to RFIN- to RFOUT. Phase imbalance is the deviation from an ideal $\mathbf{1 8 0}$ degrees.
- OIP3, Output P1dB and Noise Figure measured using a Transformer Board EVKit.

Note: The use of the external transformer T1 is included for simple 2 port evaluation purposes.
At some frequencies the external transformer interacts with the on-chip balun affecting the gain and noise figure flatness responses. These interactions have been removed from the noise figure TOCs.

## TOCs [Differential Board S-Pars, Amplitude and Phase Imbalance, Broad-Band Bias](-1-)

## RF Gain vs. Vcc and $\mathrm{T}_{\text {case }}$



Output Match vs. Vcc and $\mathrm{T}_{\text {Case }}$


## Amplitude Imbalance vs. TCASE



Input Match vs. Vcc and $\mathbf{T}_{\text {CASE }}$


Reverse Gain vs. Vcc and $\mathrm{T}_{\text {Case }}$


Phase Imbalance vs. $T_{\text {CASE }}$


## TOCs [Transformer Board, OIP3, P1dB, Noise Figure, Icc, Broad-Band Bias](-2-)

OIP3 vs. Vcc and TCASE


Output P1dB vs. Vcc and $\mathrm{T}_{\text {CASE }}$


OIP3 vs. Pout Level


## Noise Figure vs. Vcc and Tcase



## Icc vs. Vcc and TCASE



## TOCs [Differential Board S-Pars, Amplitude and Phase Imbalance, Low-Band Bias](-3-)

## RF Gain vs. Vcc and $\mathrm{T}_{\text {case }}$



Output Match vs. Vcc and $\mathrm{T}_{\text {CASE }}$


Amplitude Imbalance vs. $\mathrm{T}_{\text {CASE }}$


## Input Match vs. Vcc and $\mathbf{T}_{\text {CASE }}$



## Reverse Gain vs. Vcc and $\mathbf{T}_{\text {CASE }}$



Phase Imbalance vs. $\mathrm{T}_{\text {CASE }}$


## TOCs [Transformer Board, OIP3, P1dB, Noise Figure, Icc, Low-Band Bias](-4-)

## OIP3 vs. Vcc and Tcase



Noise Figure vs. Vcc and $\mathrm{T}_{\text {CASE }}$


Output P1dB vs. Vcc and $\mathrm{T}_{\text {CASE }}$


Icc vs. Vcc and $\mathbf{T}_{\text {CASE }}$


## TOCs [Differential Board S-Pars, Amplitude and Phase Imbalance, Mid-Band Bias](-5-)

## RF Gain vs. Vcc and $\mathrm{T}_{\text {case }}$



Output Match vs. Vcc and $\mathrm{T}_{\text {Case }}$


Amplitude Imbalance vs. TCASE


Input Match vs. Vcc and $\mathbf{T}_{\text {CASE }}$


## Reverse Gain vs. Vcc and $\mathbf{T}_{\text {CASE }}$



Phase Imbalance vs. $\mathbf{T}_{\text {CASE }}$


## TOCs [Transformer Board, OIP3, P1dB, Noise Figure, Icc, Mid-Band Bias](-6-)

## OIP3 vs. Vcc and TCASE



## Noise Figure vs. Vcc and $\mathrm{T}_{\text {CASE }}$



Output P1dB vs. Vcc and $\mathrm{T}_{\text {CASE }}$


Icc vs. Vcc and $\mathbf{T}_{\text {CASE }}$


## TOCs [Differential Board S-Pars, Amplitude and Phase Imbalance, High-Band Bias](-7-)

## RF Gain vs. Vcc and $\mathrm{T}_{\text {case }}$



Output Match vs. Vcc and TCASE


Amplitude Imbalance vs. TCASE


Input Match vs. Vcc and $\mathbf{T}_{\text {CASE }}$


## Reverse Gain vs. Vcc and TCASE



## Phase Imbalance vs. Tcase



## TOCs [Transformer Board, OIP3, P1dB, Noise Figure, Icc, ACLR, High-Band Bias](-8-)

## OIP3 vs. Vcc and Tcase



## Noise Figure vs. Vcc and TCASE



WCDMA ACLR vs. Pout ( $\mathrm{PAR}=4.3 \mathrm{~dB}$ )


Output P1dB vs. Vcc and $\mathrm{T}_{\text {CASE }}$


Icc vs. Vcc and $\mathbf{T}_{\text {Case }}$


WCDMA ACLR vs. Pout ( $\operatorname{PAR}=\mathbf{1 1 . 4} \mathbf{~ d B}$ )


## Package Drawing

( $4 \mathrm{~mm} \times 4 \mathrm{~mm}$ 24-pin TQFN), NBG24

Note: The F1423 uses the P2 exposed paddle dimensions noted below


|  | DIMENSION |  |  |
| :---: | :---: | :---: | :---: |
|  | MIN | NOM | MAX |
| 02 | SEE EPAD OPTION |  |  |
| E2 | SEE EPAD OPTION |  |  |
| L | 0.30 | 0.40 | 0.50 |
| D | 4.00 BSC |  |  |
| E | 4.00 BSC |  |  |
| e | 0.50 BSC |  |  |
| A | 0.70 | 0.75 | 0.80 |
| A1 | 0.00 | 0.02 | 0.05 |
| b | . 20 | . 25 | . 30 |
| ada | 0.15 |  |  |
| bbb | 0.10 |  |  |
| ccc | 0.10 |  |  |
| ddd | 0.05 |  |  |
| eee | 0.08 |  |  |
| fff | 0.10 |  |  |



EPAD OPTIONS:

|  | P2 |  |  |
| :---: | :---: | :---: | :---: |
|  | MIN | NOM | MAX |
| 02 | 2.50 | 2.60 | 2.70 |
| E2 | 2.50 | 2.60 | 2.70 |

NOTES:

1. ALL DIMENSIONING AND TOLERANCING CONFORM TO ANSI Y14.5M-1982
2. ALL DIMENSIONS ARE IN MILLIMEIERS.

## ReNESAS

## Land Pattern Dimension



Land Pattern to Support $2.6 \mathrm{~mm} \times 2.6 \mathrm{~mm}$ Exposed Paddle Version (See Version P2 of Package Drawing)

## RECOMMENDED LAND PATTERN DIMENSION

NOTES:

1. ALL DIMENSION ARE IN mm . ANGLES IN DEGREES.
2. TOP DOWN VIEW. AS VIEWED ON PCB.
3. COMPONENT OUTLINE SHOW FOR REFERENCE IN GREEN.
4. LAND PATTERN IN BLUE. NSMD PATTERN ASSUMED.
5. LAND PATTERN RECOMMENDATION PER IPC-7351B GENERIC REQUIREMENT FOR SURFACE MOUNT DESIGN AND LAND PATTERN.

## Renesns

## Pin Diagram



## Pin Description

| Pin | Name | Function |
| :---: | :---: | :--- |
| 1 | RFIN+ | Differential Input +. Pin looks like a DC short to ground. Must use <br> external DC block if DC is present on RF line. |
| $2,4,9,12,16$, <br> 18,23 | GND | Ground these pins. These pins are internally connected to the <br> exposed paddle. |
| 3 | RFIN- | Differential Input -. Pin looks like a DC short to ground. Must use <br> external DC block if DC is present on RF line. |
| $5,6,7,8,19$, <br> $20,21,22,24$ | NC | No internal connection. OK to connect to GND, OK to connect to <br> VCC. Application circuit ties these pins to ground. |
| 10 | VCC | 5 V Power Supply. Connect to VCC and use bypass capacitors as <br> close to the pin as possible. |
| 11 | Band_Sel | Leave pin open circuited for low-band select and connect 0 $\Omega$ resistor <br> to GND for high-band select. Internally this pin has a 1.5 M $\Omega$ pull-up <br> resistor that connects to VCC. |
| 13 | STBY | Standby (High= device power OFF, Low/Open = device power ON). <br> Internally this pin has a 1 M $\Omega$ pull-down resistor that is connected to <br> GND. |
| 14 | RBIAS1 | Connect external resistor to GND. Use value in Table 2. |
| 15 | RBIAS2 | Connect external resistor to GND. Use value in Table 2. |
| 17 | RFOUT | RF output. Must use external DC block as close to the pin as <br> possible. |
|  | Exposed Pad. Internally connected to GND. Solder this exposed pad <br> to a PCB pad that uses multiple ground vias to provide heat transfer <br> out of the device into the PCB ground planes. These multiple ground <br> vias are also required to achieve the noted RF performance. |  |

## Renesns

## APPLICATIONS Information

The F1423 has been optimized for use in high performance RF applications from 600 MHz to 3000 MHz .

## STBY

The STBY control pin allows for power saving when the device is not in use. Setting the STBY pin to a logic low, or leaving the pin open, will put the device in normal operation mode. The STBY pin has an internal 1 Meg ohm resistor to ground. Applying a logic high to this pin will put the part in standby mode. Voltage should not be applied to the STBY pin without VCC present.

## Band_Sel

The Band_Sel control pin can be used to adjust the current in the device for Mid Band, High Band, and Wide Band frequency applications. This is done by grounding the Band_Sel pin. Internally there is a 1.5 Meg ohm pull-up resistor. Voltage should not be applied to the Band_Sel pin without VCC present.

## RBias1 and RBias2

RBIAS1 (pin 14) and RBIAS2 (pin 15) use a single external resistor to ground on each pin to set the DC current in the device and to optimize the linearity performance of the amplifier stage. The resistor values in Table 2 can be used as a guide for the RF band of interest. By decreasing the resistor value to ground on the RBIAS1 pin will increase the DC current in the amplifier stage. The resistor to ground on RBIAS2 is used to optimize the linearity performance in conjunction with the resistor on RBIAS1.

## Amplifier Stability

To ensure unconditional stability the value of R1 should be set to 510 Ohms. This will reduce the RF Gain, OIP3, and OP1dB by approx 0.4 dB . Additionally, shunt resistors to ground of approximately 1 k ohm should be connected from pin 1 to ground and pin 3 to ground. This will stabilize the circuit due to common mode source impedances. The installed 1 k resistor will add 0.1 dB degradation to the Gain and Noise Figure. The 1 k ohm will also dampen any common mode amplitude and phase interactions from the differential source impedance and the F1423 differential input impedance.

## Power Supplies

A common VCC power supply should be used for all pins requiring DC power. All supply pins should be bypassed with external capacitors to minimize noise and fast transients. Supply noise can degrade noise figure and fast transients can trigger ESD clamps and cause them to fail. Supply voltage change or transients should have a slew rate smaller than $1 \mathrm{~V} / 20 \mu \mathrm{~s}$. In addition, all control pins should remain at $0 \mathrm{~V}(+/-0.3 \mathrm{~V})$ while the supply voltage ramps or while it returns to zero.

## Control Pin Interface

If control signal integrity is a concern and clean signals cannot be guaranteed due to overshoot, undershoot, ringing, etc., the following circuit at the input of each control pin is recommended. This applies to all control pins 11 and 13. Note the recommended resistor and capacitor values do not necessarily match the EV kit BOM for the case of poor control signal integrity.


## Renesns

## EVKit Picture (Differential Board)



## EVKit Picture (Transformer Board)



## Renesns

## EVKit / Applications Circuit (Differential Board)



## EVKit / Applications Circuit (Transformer Board)



## EVKit BOM (Differential Board)

| Part Ref | QTY | DESCRIPTION | Mfr. Part \# | Mfr. |
| :---: | :---: | :---: | :---: | :---: |
| C1 | 1 | 9.0 pF $\pm 0.25$ pF, $50 \mathrm{~V}, \mathrm{COG}$, Ceramic Capacitor (0402) | GRM1555C1H9R0C | Murata |
| C2 | 1 | $1000 \mathrm{pF} \pm 5 \%, 50 \mathrm{~V}, \mathrm{C} 0 \mathrm{G}$, Ceramic Capacitor (0402) | GRM1555C1H102J | Murata |
| C3 | 1 | $0.1 \mu \mathrm{~F} \pm 10 \%$, $16 \mathrm{~V}, \mathrm{X} 7 \mathrm{R}$, Ceramic Capacitor (0402) | GRM155R71C104K | Murata |
| C4 | 1 | $10 \mu \mathrm{~F} \pm 20 \%$, $6.3 \mathrm{~V}, \mathrm{X} 5 \mathrm{R}$, Ceramic Capacitor (0603) | GRM188R60J106M | Murata |
| R1 | 1 | Not installed (0402) |  |  |
| R2, R3, R4 | 3 | $0 \Omega$ Resistor, 1/10W, (0402) | ERJ-2GE0R00X | Panasonic |
| R5, R6 | 0 | Not installed |  |  |
| R7 | 1 | 2.1k $\Omega \pm 1 \%$, Resistor, 1/10W, (0402) | ERJ-2RKF2101X | Panasonic |
| R8 | 1 | $2.4 \mathrm{k} \Omega \pm 1 \%$, Resistor, 1/10W, (0402) | ERJ-2RKF2401X | Panasonic |
| R9 | 1 | $60.4 \mathrm{k} \Omega \pm 1 \%$, Resistor, 1/10W, (0402) | ERJ-2RKF6042X | Panasonic |
| R10 | 1 | 9.1k $\Omega \pm 1 \%$, Resistor, $1 / 10 \mathrm{~W},(0402)$ | ERJ-2RKF9101X | Panasonic |
| R11 | 1 | Not installed |  |  |
| R12 | 1 | Not installed |  |  |
| J1, J2, J3, J9 | 4 | SMA_END_LAUNCH (small) | 142-0711-821 | Emerson Johnson |
| J4, J5, J8 | 3 | CONN HEADER VERT $2 \times 1$ Gold | 961102-6404-AR | 3M |
| J6, J7 | 2 | CONN HEADER VERT $2 \times 4$ Gold | 67997-108HLF | FCI |
| U1 | 1 | RF Amplifier | F1423NBGI | IDT |
|  | 1 | Printed Circuit Board (3 port) | F1423 EVKIT (3 port) |  |

## EVKit BOM (Transformer Board)

| Part Ref | QTY | DESCRIPTION | Mfr. Part \# | Mfr. |
| :---: | :---: | :---: | :---: | :---: |
| C1 | 1 | 9.0 pF $\pm 0.25$ pF, $50 \mathrm{~V}, \mathrm{COG}, \mathrm{Ceramic}$ Capacitor (0402) | GRM1555C1H9R0C | Murata |
| C2 | 1 | 1000 pF $\pm 5 \%$, 50 V, C0G, Ceramic Capacitor (0402) | GRM1555C1H102J | Murata |
| C3 | 1 | $0.1 \mu \mathrm{~F} \pm 10 \%$, $16 \mathrm{~V}, \mathrm{X} 7 \mathrm{R}$, Ceramic Capacitor (0402) | GRM155R71C104K | Murata |
| C4 | 1 | $10 \mu \mathrm{~F} \pm 20 \%$, $6.3 \mathrm{~V}, \mathrm{X} 5 \mathrm{R}$, Ceramic Capacitor (0603) | GRM188R60J106M | Murata |
| R1 | 1 | Not installed (0402) |  |  |
| R2, R3, R4 | 3 | $0 \Omega$ Resistor, 1/10W, (0402) | ERJ-2GE0R00X | Panasonic |
| R5, R6 | 0 | Not installed |  |  |
| R7 | 1 | 2.1k $\Omega \pm 1 \%$, Resistor, $1 / 10 \mathrm{~W},(0402)$ | ERJ-2RKF2101X | Panasonic |
| R8 | 1 | $2.4 \mathrm{k} \Omega \pm 1 \%$, Resistor, 1/10W, (0402) | ERJ-2RKF2401X | Panasonic |
| R9 | 1 | $60.4 \mathrm{k} \Omega \pm 1 \%$, Resistor, 1/10W, (0402) | ERJ-2RKF6042X | Panasonic |
| R10 | 1 | $9.1 \mathrm{k} \Omega \pm 1 \%$, Resistor, $1 / 10 \mathrm{~W},(0402)$ | ERJ-2RKF9101X | Panasonic |
| R11 | 1 | Not installed |  |  |
| R12 | 1 | Not installed |  |  |
| R13, R14 | 2 | $510 \Omega \pm 1 \%$, Resistor, 1/10W, (0402) (Note 1) | ERJ-2RKF5100X | Panasonic |
| T1 | 1 | 1:1 wideband transformer | TC1-1-43+ | Mini Circuits |
| J1, J3, J9 | 3 | SMA_END_LAUNCH (small) | 142-0711-821 | Emerson Johnson |
| J4, J5, J8 | 3 | CONN HEADER VERT $2 \times 1$ Gold | 961102-6404-AR | 3M |
| J6, J7 | 2 | CONN HEADER VERT $2 \times 4$ Gold | 67997-108HLF | FCI |
| U1 | 1 | RF Amplifier | F1423NBGI | IDT |
|  | 1 | Printed Circuit Board (Transformer) | F1423 EVKIT XFMR |  |

Note 1: When using an external transformer for evaluation, a common mode resonance interaction can occur with the on-chip balun. Resistors R13 and R14 will dampen the resonance but affects the Gain and NF by approx 0.2 dB .

## Top Markings



## EVkit Operation

The F1423 EVkits (single ended and differential) have a number of control features available.

## STBY (2 pin Header J5)

Two-pin header $\mathrm{J5}$ can be used to set the part for operational or standby mode. Leaving the two $\mathrm{J5}$ pins unconnected will place it in the operational mode. Connecting the two J 5 pins together will pull up the STBY pin to Vcc through R4 and place the part into the standby mode.

## Band_Sel (2 pin Header J4)

Two-pin header $\mathrm{J4}$ can be used to set the part for best operational performance in different RF bands. Based on Table 2 above the Low-Band performance is best with these two J 4 pins left open while the other bands typically have these two pins shorted together.

## RF Band Biasing (RBIAS1, RBIAS2, Band_Sel)

Below are 4 settings showing the recommended J4, J7, and 78 jumper connections for best linearity performance in the different RF bands. The jumpers (shown in red below) select the RBIAS1 and RBIAS2 resistor values along with the Band_Sel setting (see Table 2 above). Never have two shunts installed at the same time on header J7 since this may produce excessive bias current and damage the part.


Broad-Band


Mid-Band


Low-Band


High-Band

Renesas

## Revision History Sheet

| Rev | Date | Page | Description of Change |
| :---: | :---: | :---: | :--- | :--- |
| O | $2015-$ Nov-6 |  | Initial Release |

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