The ISL28006 is a micropower, uni-directional high-side and low-side current sense amplifier featuring a proprietary rail-to-rail input current sensing amplifier. The ISL28006 is ideal for high-side current sense applications where the sense voltage is usually much higher than the amplifier supply voltage. The device can be used to sense voltages as high as 28 V when operating from a supply voltage as low as 2.7 V . The micropower ISL28006 consumes only $50 \mu \mathrm{~A}$ of supply current when operating from a 2.7 V to 28 V supply.

The ISL28006 features a common-mode input voltage range from OV to 28 V . The proprietary architecture extends the input voltage sensing range down to 0 V , making it an excellent choice for low-side ground sensing applications. The benefit of this architecture is that a high degree of total output accuracy is maintained over the entire 0 V to 28 V common mode input voltage range.

The ISL28006 is available in fixed ( $100 \mathrm{~V} / \mathrm{V}, 50 \mathrm{~V} / \mathrm{V}, 20 \mathrm{~V} / \mathrm{V}$ and Adjustable) gains in the space saving 5 Ld SOT-23 package and the 6 Ld SOT-23 package for the adjustable gain part. The parts operate over the extended temperature range from $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$.

## Features

- Low Power Consumption. . . . . . . . . . . . . . . . . . . . . . 50 5 A, Typ
- Supply Range . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . .2.7V to 28 V
- Wide Common Mode Input. . . . . . . . . . . . . . . . . . . . OV to 28 V
- Gain Versions
- ISL28006-100 .......................................... 100V/V
- ISL28006-50 .............................................. 50V/V
- ISL28006-20 ............................................. . 20V/V
- ISL28006-ADJ ................... ADJ (Min Gain = 20V/V)
- Operating Temperature Range . . . . . . . . . . . . $40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
- Packages. . . . . . . . . . . . . . . . . . . . . . . 5 Ld SOT-23, 6 Ld SOT-23


## Applications

- Power Management/Monitors
- Power Distribution and Safety
- DC/DC, AC/DC Converters
- Battery Management/Charging
- Automotive Power Distribution


## Related Literature

- See AN1532 for "ISL28006 Evaluation Board User's Guide"


FIGURE 1. TYPICAL APPLICATION


FIGURE 2. GAIN ACCURACY vs $\mathrm{V}_{\text {RS }}+\mathbf{=} \mathbf{O V}$ TO 28 V

## Block Diagram



FIXED GAIN PARTS


ADJUSTABLE GAIN PART

## Pin Configurations

ISL28006-100, 50, 20
(5 LD SOT-23)
TOP VIEW

ISL28006-ADJ
(6 LD SOT-23)
TOP VIEW


## Pin Descriptions

| ISL28006-100, 50, 20 ( 5 LD SOT-23) | $\begin{aligned} & \text { ISL28006-ADJ } \\ & \text { (6 LD SOT-23) } \end{aligned}$ | PIN NAME | DESCRIPTION |
| :---: | :---: | :---: | :---: |
| 1 | 6 | GND | Power Ground |
|  | 1 | FB | Input Pin for External Resistors |
| 2 | 2 | OUT | Amplifier Output |
| 3 | 3 | $\mathrm{V}_{\mathrm{CC}}$ | Positive Power Supply |
| 4 | 4 | $\mathrm{R}_{\text {+ }}$ | Sense Voltage Non-inverting Input |
| 5 | 5 | RS- | Sense Voltage Inverting Input |
|  |  |  |  |

## Ordering Information

| PART NUMBER (Notes 1, 2, 3) | GAIN | PART MARKING | PACKAGE <br> Tape \& Reel (Pb-Free) | PKG. DWG. \# |
| :---: | :---: | :---: | :---: | :---: |
| ISL28006FH100Z-T7 | 100V/V | BDJA (Note 4) | 5 Ld SOT-23 | P5.064A |
| ISL28006FH100Z-T7A | 100V/V | BDJA (Note 4) | 5 Ld SOT-23 | P5.064A |
| ISL28006FH50Z-T7 | 50V/V | BDHA (Note 4) | 5 Ld SOT-23 | P5.064A |
| ISL28006FH50Z-T7A | 50V/V | BDHA (Note 4) | 5 Ld SOT-23 | P5.064A |
| ISL28006FH2OZ-T7 | 20V/V | BDGA (Note 4) | 5 Ld SOT-23 | P5.064A |
| ISL28006FH20Z-T7A | 20V/V | BDGA (Note 4) | 5 Ld SOT-23 | P5.064A |
| ISL28006FHADJZ-T7 | ADJ | BDFA (Note 4) | 6 Ld SOT-23 | P6.064 |
| ISL28006FHADJZ-T7A | ADJ | BDFA (Note 4) | 6 Ld SOT-23 | P6.064 |
| ISL28006FH-100EVAL1Z | 100V/V Evaluation Board |  |  |  |
| ISL28006FH-50EVAL1Z | 50V/V Evaluation Board |  |  |  |
| ISL28006FH-20EVAL1Z | 20V/V Evaluation Board |  |  |  |
| ISL28006FH-ADJEVAL1Z | Adjustable Evaluation Board |  |  |  |

## NOTES:

1. Please refer to $\underline{\mathrm{TB} 347}$ for details on reel specifications.
2. These Intersil Pb-free plastic packaged products employ special Pb-free material sets, molding compounds/die attach materials, and 100\% matte tin plate plus anneal (e3 termination finish, which is RoHS compliant and compatible with both SnPb and Pb -free soldering operations). Intersil Pb-free products are MSL classified at Pb-free peak reflow temperatures that meet or exceed the Pb-free requirements of IPC/JEDEC J STD-020.
3. For Moisture Sensitivity Level (MSL), please see device information page for ISL28006. For more information on MSL please see techbrief TB363.
4. The part marking is located on the bottom of the part.

## Absolute Maximum Ratings

| Max Supply Voltage | 8 V |
| :---: | :---: |
| Max Differential Input Current | 20mA |
| Max Differential Input Voltage | $\pm 0.5 \mathrm{~V}$ |
| Max Input Voltage ( $\mathrm{R}_{\text {S+ }}, \mathrm{R}_{\mathbf{S}-,}$ FB) | ND - 0.5V to 30V |
| Max Input Current for Input Voltage <GND - 0.5V. | $\pm 20 \mathrm{~mA}$ |
| Output Short-Circuit Duration | Indefinite |
| Di-Electrically Isolated PR40 Process | Latch-up free |
| ESD Rating |  |
| Human Body Model (Tested per JESD22-A114F) | 4kV |
| Machine Model (Tested per EIA/JESD22-A115-A) | 200V |
| Charged Device Model (Tested per JESD22-C101D) | .1.5kV |

## Thermal Information

| Thermal Resistance (Typical) | $\theta_{\mathrm{JA}}\left({ }^{\circ} \mathrm{C} / \mathbf{W}\right)$ | $\theta_{\mathrm{JC}}\left({ }^{\circ} \mathrm{C} / \mathbf{W}\right)$ |
| :---: | :---: | :---: |
| 5 Ld SOT-23 (Notes 5, 6) $\ldots \ldots \ldots \ldots \ldots$ | 190 | 90 |
| 6 Ld SOT-23 (Notes 5, 6) $\ldots \ldots \ldots \ldots \ldots$. | 180 | 90 |

Maximum Storage Temperature Range . . . . . . . . . . . . . . $65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Maximum Junction Temperature (TJMAX) . . . . . . . . . . . . . . . . . . . . . $+150^{\circ} \mathrm{C}$
Pb-Free Reflow Profile . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . see link below
http://www.intersil.com/pbfree/Pb-FreeReflow.asp

## Recommended Operating Conditions

Ambient Temperature Range $\left(\mathrm{T}_{\mathrm{A}}\right) \ldots \ldots . . . . . . . . . . . .40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$

CAUTION: Do not operate at or near the maximum ratings listed for extended periods of time. Exposure to such conditions may adversely impact product reliability and result in failures not covered by warranty.

NOTES:
5. $\theta_{\mathrm{JA}}$ is measured with the component mounted on a high effective thermal conductivity test board in free air. See Tech Brief TB379 for details.
6. For $\theta_{\mathrm{J}} \mathrm{C}$, the "case temp" location is taken at the package top center.

Electrical Specifications $\mathrm{v}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{v}_{\mathrm{RS}+}=0 \mathrm{~V}$ to $28 \mathrm{~V}, \mathrm{v}_{\text {SENSE }}=0 \mathrm{~V}, \mathrm{R}_{\mathrm{LOAD}}=1 \mathrm{M} \Omega, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ unless otherwise specified.
Boldface limits apply over the operating temperature range, $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. Temperature data established by characterization.

| PARAMETER | DESCRIPTION | CONDITIONS | MIN <br> (Note 7) | TYP | MAX <br> (Note 7) | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{OS}}$ <br> (Input Offset <br> Voltage) | $\begin{aligned} & \text { Gain = 100 } \\ & (\text { Notes 8, } 9) \end{aligned}$ | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}^{+}}=12 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=20 \mathrm{mV}$ to 100 mV | -250 | 60 | 250 | $\mu \mathrm{V}$ |
|  |  |  | -300 |  | 300 | $\mu \mathrm{V}$ |
|  |  | $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}}+=0.2 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=20 \mathrm{mV}$ to 100 mV | -2.5 | -1.2 | 2.5 | mV |
|  |  |  | -2.8 |  | 2.8 | mV |
|  | $\begin{aligned} & \text { Gain = 50, Gain = } 20 \\ & (\text { Notes 8, 9) } \end{aligned}$ | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}^{+}}=12 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=20 \mathrm{mV}$ to 100 mV | -300 | 60 | 300 | $\mu \mathrm{V}$ |
|  |  |  | -450 |  | 450 | $\mu \mathrm{V}$ |
|  |  | $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}^{+}}=0.2 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=20 \mathrm{mV}$ to 100 mV | -2.8 | -1.2 | 2.8 | mV |
|  |  |  | -3.2 |  | 3.2 | mV |
|  | $\begin{aligned} & \text { Adjustable, Gain }=21 \\ & R_{\mathrm{f}}=100 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{g}}=5 \mathrm{k} \Omega \\ & \text { (Notes 8,9) } \end{aligned}$ | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}^{+}}=12 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=20 \mathrm{mV}$ to 100 mV | -300 | 60 | 300 | $\mu \mathrm{V}$ |
|  |  |  | -450 |  | 450 | $\mu \mathrm{V}$ |
|  |  | $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}}+=0.2 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=20 \mathrm{mV}$ to 100 mV | -3.1 | -1.2 | 3.1 | mV |
|  |  |  | -3.4 |  | 3.4 | mV |
| $\mathrm{I}_{\mathrm{RS}}{ }^{+}, \mathrm{I}_{\text {RS }}{ }^{-}$ | Leakage Current | $\mathrm{V}_{\mathrm{CC}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}+}=28 \mathrm{~V}$ |  | 0.041 | 1.2 | $\mu \mathrm{A}$ |
|  |  |  |  |  | 1.5 | $\mu \mathrm{A}$ |
| $\begin{aligned} & \mathrm{I}_{\mathrm{RS}^{+}} \\ & \text {(+ Input Bias } \\ & \text { Current) } \end{aligned}$ | Gain $=100$ | $\mathrm{V}_{\mathrm{RS}^{+}}=2 \mathrm{~V}, \mathrm{~V}_{\mathrm{SENSE}}=5 \mathrm{mV}$ |  | 4.7 | 6 | $\mu \mathrm{A}$ |
|  |  |  |  |  | 7 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\mathrm{RS}^{+}}=0 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=5 \mathrm{mV}$ | -500 | -432 |  | nA |
|  |  |  | -600 |  |  | nA |
|  | Gain $=50$, Gain $=20$ | $\mathrm{V}_{\mathrm{RS}^{+}}=2 \mathrm{~V}, \mathrm{~V}_{\mathrm{SENSE}}=5 \mathrm{mV}$ |  | 4.7 | 6 | $\mu \mathrm{A}$ |
|  |  |  |  |  | 8 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\mathrm{RS}^{+}}=0 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=5 \mathrm{mV}$ | -700 | -432 |  | nA |
|  |  |  | -840 |  |  | nA |
|  | $\begin{aligned} & \text { ADJ Gain }=101 \\ & R_{f}=100 \mathrm{k} \Omega, R_{g}=1 \mathrm{k} \Omega \end{aligned}$ | $\mathrm{V}_{\mathrm{RS}^{+}}=2 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=5 \mathrm{mV}$ |  | 4.7 | 6 | $\mu \mathrm{A}$ |
|  |  |  |  |  | 7 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\mathrm{RS}^{+}}=0 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=5 \mathrm{mV}$ | -500 | -432 |  | nA |
|  |  |  | -600 |  |  | nA |

Electrical Specifications $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}+}=0 \mathrm{~V}$ to $28 \mathrm{~V}, \mathrm{v}_{\text {SENSE }}=0 \mathrm{~V}, \mathrm{R}_{\mathrm{LOAD}}=1 \mathrm{M} \Omega, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ unless otherwise specified. Boldface limits apply over the operating temperature range, $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. Temperature data established by characterization. (Continued)

| PARAMETER | DESCRIPTION | CONDITIONS | MIN (Note 7) | TYP | $\begin{gathered} \text { MAX } \\ \text { (Note 7) } \end{gathered}$ | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\text {IRS }}{ }^{-}$ (- Input Bias Current) | $\mathrm{G}=100,50,20, \mathrm{ADJ}$ | $\mathrm{V}_{\mathrm{RS}^{+}}=2 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=5 \mathrm{mV}$ |  | 5 | 50 | nA |
|  |  |  |  |  | 75 | nA |
|  |  | $\mathrm{V}_{\mathrm{RS}}{ }^{+}=0 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=5 \mathrm{mV}$ | -125 | -45 |  | nA |
|  |  |  | -130 |  |  | nA |
| CMRR | Common Mode Rejection Ratio | $\mathrm{V}_{\mathrm{RS}}{ }^{+}=2 \mathrm{~V}$ to 28 V | 105 | 115 |  | dB |
| PSRR | Power Supply Rejection Ratio | $\mathrm{V}_{\mathrm{CC}}=2.7 \mathrm{~V}$ to $28 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}^{+}}=2 \mathrm{~V}$ | 90 | 105 |  | dB |
| $\mathrm{V}_{\mathrm{FS}}$ | Full-scale Sense Voltage | $\mathrm{V}_{\mathrm{CC}}=28 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}^{+}}=0.2 \mathrm{~V}, 12 \mathrm{~V}$ | 200 |  |  | mV |
| G (Gain) | (Note 8) | ISL28006-100 |  | 100 |  | V/V |
|  |  | ISL28006-50 |  | 50 |  | V/V |
|  |  | ISL28006-20 |  | 20 |  | V/V |
|  |  | ISL28006-ADJ | 20 |  |  | V/V |
| $\begin{aligned} & \mathrm{G}_{\mathrm{A}} \\ & \text { (Gain Accuracy) } \end{aligned}$ | $\begin{aligned} & \text { Gain = } 100 \\ & \text { (Note 10) } \end{aligned}$ | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}}{ }^{+}=12 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=20 \mathrm{mV}$ to 100 mV | -0.2 |  | 0.7 | \% |
|  |  |  | -1 |  | 1 | \% |
|  |  | $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}^{+}}=0.1 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=20 \mathrm{mV}$ to 100 mV |  | -0.25 |  | \% |
|  | $\begin{aligned} & \text { Gain = 50, Gain = } 20 \\ & \text { (Note 10) } \end{aligned}$ | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}^{+}}=12 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=20 \mathrm{mV}$ to 100 mV | -0.35 |  | 0.7 | \% |
|  |  |  | -1 |  | 1 | \% |
|  |  | $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}^{+}}=0.1 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=20 \mathrm{mV}$ to 100 mV | -2.2 | -0.33 | 2.2 | \% |
|  |  |  | -2.3 |  | 2.3 | \% |
|  | $\begin{aligned} & \text { ADJ Gain }=21 \\ & R_{f}=100 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{g}}=5 \mathrm{k} \Omega \\ & \text { (Note 10) } \end{aligned}$ | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}^{+}}=12 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=20 \mathrm{mV}$ to 100 mV | -0.65 |  | 1 | \% |
|  |  |  | -1 |  | 1.05 | \% |
|  |  | $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}^{+}}=0.1 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=20 \mathrm{mV}$ to 100 mV | -2.2 | -0.33 | 2.2 | \% |
|  |  |  | -2.3 |  | 2.3 |  |
| $\mathrm{V}_{\mathrm{OA}}$ (Total Output Accuracy) | $\begin{aligned} & \text { Gain = } 100 \\ & \text { (Note 11) } \end{aligned}$ | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}^{+}}=12 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}$ | -0.7 |  | 0.7 | \% |
|  |  |  | -0.9 |  | 0.9 | \% |
|  |  | $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}^{+}}=0.1 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}$ |  | -1.25 |  | \% |
|  | $\begin{aligned} & \text { Gain }=50, \text { Gain }=20 \\ & (\text { Note 11) } \end{aligned}$ | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}^{+}}=12 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}$ | -0.7 |  | 0.7 | \% |
|  |  |  | -0.9 |  | 0.9 | \% |
|  |  | $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}^{+}}=0.1 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}$ | -4.7 | -1.41 | 1.8 | \% |
|  |  |  | -5.2 |  | 2.3 | \% |
|  | $\begin{aligned} & \text { ADJ Gain }=21 \\ & R_{f}=100 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{g}}=5 \mathrm{k} \Omega \\ & (\text { Note 11) } \end{aligned}$ | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}^{+}}=12 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}$ | -0.7 |  | 1.05 | \% |
|  |  |  | -0.9 |  | 1.2 | \% |
|  |  | $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}}{ }^{+}=0.1 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}$ | -4.7 | -1.41 | 1.8 | \% |
|  |  |  | -5.2 |  | 2.3 | \% |
| $\mathrm{V}_{\mathrm{OH}}$ | Output Voltage Swing, High $\mathrm{V}_{\mathrm{CC}}-\mathrm{V}_{\mathrm{OUT}}$ | $\mathrm{I}_{\mathrm{O}}=-500 \mu \mathrm{~A}, \mathrm{~V}_{\mathrm{CC}}=2.7 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}, \mathrm{V}_{\text {RS }}+=2 \mathrm{~V}$ |  | 39 | 50 | mV |
| $\mathrm{V}_{\mathrm{OL}}$ | Output Voltage Swing, Low VOUT | $\mathrm{I}_{\mathrm{O}}=500 \mu \mathrm{~A}, \mathrm{~V}_{\mathrm{CC}}=2.7 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}^{+}}=2 \mathrm{~V}$ |  | 30 | 50 | mV |
| $\mathrm{R}_{\text {OUT }}$ | Output Resistance | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}^{+}}=12 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}, \\ & \mathrm{l}_{\mathrm{OUT}}=10 \mu \mathrm{~A} \text { to } 1 \mathrm{~mA} \end{aligned}$ |  | 6.5 |  | $\Omega$ |
| ISC+ | Short Circuit Sourcing Current | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}^{+}}=5 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=10 \Omega$ |  | 4.8 |  | mA |
| ISC- | Short Circuit Sinking Current | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}^{+}}=5 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=10 \Omega$ |  | 8.7 |  | mA |

Electrical Specifications $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}+}=0 \mathrm{~V}$ to $28 \mathrm{~V}, \mathrm{v}_{\text {SENSE }}=0 \mathrm{~V}, \mathrm{R}_{\mathrm{LOAD}}=1 \mathrm{M} \Omega, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ unless otherwise specified. Boldface limits apply over the operating temperature range, $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. Temperature data established by characterization. (Continued)

| PARAMETER | DESCRIPTION | CONDITIONS | $\begin{gathered} \text { MIN } \\ \text { (Note 7) } \end{gathered}$ | TYP | $\begin{gathered} \text { MAX } \\ \text { (Note 7) } \end{gathered}$ | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\text {ICC }}$ | Gain $=100$ | $\mathrm{V}_{\mathrm{RS}}{ }^{+}>2 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=5 \mathrm{mV}$ |  | 50 | 59 | $\mu \mathrm{A}$ |
|  |  |  |  |  | 62 | $\mu \mathrm{A}$ |
|  | Gain $=50,20$, | $\mathrm{V}_{\mathrm{RS}}{ }^{+} \mathbf{~ 2 ~} \mathrm{V}, \mathrm{V}_{\text {SENSE }}=5 \mathrm{mV}$ |  | 50 | 62 | $\mu \mathrm{A}$ |
|  |  |  |  |  | 63 | $\mu \mathrm{A}$ |
|  | $\begin{aligned} & \text { ADJ Gain }=21 \\ & R_{f}=100 \mathrm{k} \Omega, R_{g}=5 \mathrm{k} \Omega \end{aligned}$ | $\mathrm{V}_{\text {RS }}{ }^{+} \mathbf{2} \mathrm{V}, \mathrm{V}_{\text {SENSE }}=5 \mathrm{mV}$ |  | 50 | 62 | $\mu \mathrm{A}$ |
|  |  |  |  |  | 63 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {cc }}$ | Supply Voltage | Guaranteed by PSRR | 2.7 |  | 28 | v |
| Slew Rate | Gain $=100$ | Puise on $\mathrm{R}_{\text {S }+}$ pin, $\mathrm{V}_{\text {OUT }}=8 \mathrm{~V}_{\text {P-P }}$ (Figure 75) | 0.58 | 0.76 |  | V/ $\mu \mathrm{s}$ |
|  | Gain $=50$ | Pulse on $\mathrm{R}_{\text {S }+}$ pin, $\mathrm{V}_{\text {OUT }}=8 \mathrm{~V}_{\mathrm{P}-\mathrm{P}}$ (Figure 75) | 0.58 | 0.67 |  | V/ $\mu \mathrm{s}$ |
|  | Gain $=20$ | Pulse on $\mathrm{R}_{\text {S }}$ pin, $\mathrm{V}_{\text {OUT }}=3.5 \mathrm{~V}_{\text {P-P }}$ (Figure 75) | 0.50 | 0.67 |  | V/ $\mu \mathrm{s}$ |
|  | $\begin{aligned} & \text { ADJ Gain }=21 \\ & R_{f}=100 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{g}}=5 \mathrm{k} \Omega \end{aligned}$ | Pulse on $\mathrm{R}_{\mathbf{S}+} \mathrm{pin}, \mathrm{V}_{\text {OUT }}=3.5 \mathrm{~V}_{\text {P-P }}($ Figure 75) | 0.50 | 0.67 |  | V/ $\mu \mathrm{s}$ |
| BW-3dB | Gain $=100$ | $\mathrm{V}_{\mathrm{RS}^{+}}=12 \mathrm{~V}, 0.1 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}$ |  | 110 |  | kHz |
|  | Gain $=50$ | $\mathrm{V}_{\text {RS }}{ }^{+}=12 \mathrm{~V}, 0.1 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}$ |  | 160 |  | kHz |
|  | Gain $=20$ | $\mathrm{V}_{\text {RS }}{ }^{+}=12 \mathrm{~V}, 0.1 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}$ |  | 180 |  | kHz |
|  | ADJ, Gain = 101 (Figure 65) | $\begin{aligned} & \mathrm{V}_{\mathrm{RS}^{+}=12 \mathrm{~V}, 0.1 \mathrm{~V},} \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}, \mathrm{R}_{\mathrm{f}}=100 \mathrm{k} \Omega, \\ & \mathrm{R}_{\mathrm{g}}=1 \mathrm{k} \Omega \end{aligned}$ |  | 40 |  | kHz |
|  | ADJ, Gain = 51 (Figure 65) | $\mathrm{V}_{\text {S }^{+}}=12 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}, \mathrm{R}_{\mathrm{f}}=100 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{g}}=2 \mathrm{k} \Omega$ |  | 78 |  | kHz |
|  |  | $\mathrm{V}_{\mathrm{RS}^{+}}=0.1 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}, \mathrm{R}_{\mathrm{f}}=100 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{g}}=2 \mathrm{k} \Omega$ |  | 122 |  | kHz |
|  | ADJ, Gain = 21 (Figure 65) | $\mathrm{V}_{\mathrm{RS}^{+}}=12 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}, \mathrm{R}_{\mathrm{f}}=100 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{g}}=5 \mathrm{k} \Omega$ |  | 131 |  | kHz |
|  |  | $\mathrm{V}_{\mathrm{RS}^{+}}=0.1 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}, \mathrm{R}_{\mathrm{f}}=100 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{g}}=5 \mathrm{k} \Omega$ |  | 237 |  | kHz |
| $\mathrm{t}_{5}$ | Output Settling Time to $1 \%$ of Final Value | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}^{+}}=12 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=10 \mathrm{~V}$ step, $\mathrm{V}_{\text {SENSE }}>7 \mathrm{mV}$ |  | 15 |  | us |
|  |  | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\text {RS }}{ }^{+}=0.2 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=10 \mathrm{~V}$ step, $\mathrm{V}_{\text {SENSE }}>7 \mathrm{mV}$ |  | 20 |  | $\mu \mathrm{s}$ |
|  | Capacitive-Load Stability | No sustained oscillations |  | 300 |  | pF |
| $\mathrm{t}_{\text {S Power-up }}$ | Power-Up Time to 1\% of Final Value | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}^{+}}=12 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}$ |  | 15 |  | $\mu \mathrm{s}$ |
|  |  | $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{~V}_{\mathrm{RS}}{ }^{+}=0.2 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}$ |  | 50 |  | $\mu \mathrm{s}$ |
|  | Saturation Recovery Time | $\mathrm{V}_{\mathrm{CC}}=\mathrm{V}_{\mathrm{RS}^{+}}=12 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=100 \mathrm{mV}$, overdrive |  | 10 |  | $\mu \mathrm{s}$ |

## NOTES:

7. Compliance to datasheet limits is assured by one or more methods: production test, characterization and/or design.
8. DEFINITION OF TERMS:

- $V_{\text {SENSE }} A=V_{\text {SENSE }} @ 100 \mathrm{mV}$
- $\mathrm{V}_{\text {SENSE }} \mathrm{B}=\mathrm{V}_{\text {SENSE }} @ 20 \mathrm{mV}$
- $\mathrm{V}_{\text {OUT }} A=\mathrm{V}_{\text {OUT }} @ \mathrm{~V}_{\text {SENSE }} A=100 \mathrm{mV}$
- $V_{\text {OUT }} B=V_{\text {OUT }} @ V_{\text {SENSE }} B=20 \mathrm{mV}$
$\cdot G=$ GAIN $=\left(\frac{v_{\text {OUT }} A-V_{\text {OUT }}{ }^{B}}{V_{\text {SENSE }}{ }^{A}-V_{\text {SENSE }}{ }^{B}}\right)$

9. $V_{O S}$ is extrapolated from the gain measurement. $v_{\text {OS }}=V_{\text {SENSE }} A-\frac{V_{\text {OUT }} A}{G}$
10. $\%$ Gain Accuracy $=G_{A}=\left(\frac{G_{\text {MEASURED }}-G_{\text {EXPECTED }}}{G_{\text {EXPECTED }}}\right) \times 100$
11. Output Accuracy \% VOA $=\left(\frac{\text { VOUT }_{\text {MEASURED }}-\text { VOUT }_{\text {EXPECTED }}}{\text { VOUT }_{\text {EXPECTED }}}\right) \times 100$, where $V_{\text {OUT }}=V_{\text {SENSE }} X$ GAIN and $V_{\text {SENSE }}=100 \mathrm{mV}$

Typical Performance Curves $\mathrm{v}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{MR}$, unless othemisise specified.


FIGURE 3. HIGH-SIDE and LOW-SIDE THRESHOLD VOLTAGE
$\mathbf{V}_{\mathbf{R S}+(\mathrm{L}-\mathrm{H})}$ and $\mathbf{V}_{\text {RS+(H-L) }}, \mathbf{V}_{\text {SENSE }}=10 \mathrm{mV}$


FIGURE 5. LARGE SIGNAL TRANSIENT RESPONSE $\mathrm{V}_{\mathrm{RS}}+\mathbf{}=\mathbf{0} \mathbf{2} \mathrm{V}$,
$V_{\text {SENSE }}=100 \mathrm{mV}$


FIGURE 7. $\mathrm{V}_{\mathrm{OS}}(\mu \mathrm{V})$ DISTRIBUTION AT $+25^{\circ} \mathrm{C}, \mathrm{V}_{\text {RS }+}=12 \mathrm{~V}$, QUANTITY: 100


FIGURE 4. $\mathbf{V}_{\text {OUT }}$ vs $\mathbf{V}_{\text {RS }}, \mathbf{V}_{\text {SENSE }}=\mathbf{2 0 m V}$ TRANSIENT RESPONSE


FIGURE 6. LARGE SIGNAL TRANSIENT RESPONSE $\mathrm{V}_{\text {RS }}{ }^{+}=\mathbf{1 2 V}$, $V_{\text {SENSE }}=100 \mathrm{mV}$


FIGURE 8. $\mathbf{V}_{\mathbf{O S}}$ vs $\mathbf{V}_{\mathbf{R S}}+$

Typical Performance Curves $\mathrm{V}_{\mathrm{Cc}}-12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}-1 \mathrm{~m} 2$, untess othemises specfifed. (Continued)


FIGURE 9. $\mathbf{V}_{\mathbf{O S}}$ vs $\mathrm{V}_{\mathrm{RS}}+$


FIGURE 11. $\mathrm{V}_{\mathrm{OS}}$ vs $\mathrm{V}_{\mathrm{CC}}, \mathrm{V}_{\text {RS }+}=\mathbf{0 . 1 V}$


FIGURE 13. GAIN ACCURACY vs $\mathbf{V}_{R S}+=0 \mathrm{~V}$ TO 2V


FIGURE 10. $\mathrm{V}_{\mathbf{O S}}$ vs $\mathrm{V}_{\mathbf{C C}}, \mathrm{V}_{\mathrm{RS}+}=\mathbf{1 2 \mathrm { V }}$


FIGURE 12. GAIN ACCURACY vs $\mathbf{V}_{\text {RS }+}=0 \mathrm{~V}$ TO 28V


FIGURE 14. GAIN ACCURACY vs $\mathrm{V}_{\mathbf{C C}}, \mathrm{V}_{\mathrm{RS}+}=\mathbf{1 2 V}$

## Typical Performance Curves $\mathrm{V}_{\mathrm{cc}}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{Mn2}$, uness othemises specified. (Continued)



FIGURE 15. GAIN ACCURACY vs $\mathrm{V}_{\mathbf{C c}}, \mathrm{V}_{\mathrm{RS}+}=\mathbf{0 . 1 V}$


FIGURE 17. GAIN vs FREQUENCY $\mathrm{V}_{\text {RS }+}=100 \mathrm{mV} / 12 \mathrm{~V}$, $v_{\text {SENSE }}=100 \mathrm{mV}, \mathrm{V}_{\text {OUT }}=50 \mathrm{~m} \mathrm{~V}_{\text {P-P }}$


FIGURE 19. CAPACITIVE LOAD DRIVE GAIN vs FREQUENCY


FIGURE 16. NORMALIZED $V_{O A}$ vs IOUT


FIGURE 18. $\mathrm{V}_{\mathbf{0 S}}(\boldsymbol{\mu} \mathrm{V})$ vs TEMPERATURE


FIGURE 20. CAPACITIVE LOAD DRIVE PHASE vs FREQUENCY

Typical Performance Curves $\mathrm{V}_{\mathrm{cc}}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{~m} 2$, untess othemise specfifed. (Continued)


FIGURE 21. GAIN ACCURACY (\%) vs TEMPERATURE


FIGURE 23. $\mathrm{V}_{\text {OS }}(\mu \mathrm{V})$ DISTRIBUTION AT $+25^{\circ} \mathrm{C}, \mathrm{V}_{\text {RS }+}=12 \mathrm{~V}$, QUANTITY: 100


FIGURE 25. $\mathbf{V}_{\text {OS }}$ vs $\mathbf{V}_{\mathbf{R S}}+$


FIGURE 22. $\mathrm{V}_{\text {OUT }}$ ERROR (\%) vs TEMPERATURE


FIGURE 24. $\mathbf{V}_{\mathbf{O S}}$ vs $\mathbf{V}_{\text {RS }+}$


FIGURE 26. $\mathbf{V}_{\mathbf{O S}} \mathbf{v s} \mathbf{V}_{\mathbf{C C}}, \mathbf{V}_{\mathbf{R S}+}=\mathbf{1 2 V}$

Typical Performance Curves $\mathrm{V}_{\mathrm{Cc}}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{~m} 2$, untess othemise specfifed. (Continued)


FIGURE 27. $\mathbf{V}_{\mathbf{O S}}$ vs $\mathbf{V}_{\mathbf{C C}}, \mathbf{V}_{\mathbf{R S}+}=\mathbf{V}_{\mathbf{R S}+}=0.1 \mathrm{~V}$


FIGURE 29. GAIN ACCURACY vs $\mathrm{V}_{\mathrm{RS}+}=0 \mathrm{~V}$ TO 2 V


FIGURE 31. GAIN ACCURACY vs $\mathbf{V}_{\mathbf{C c}}$, LOW-SIDE


FIGURE 28. GAIN ACCURACY vs $\mathrm{V}_{\text {RS }+}=0 \mathrm{~V}$ TO 28V


FIGURE 30. GAIN ACCURACY vs $\mathbf{V}_{\mathbf{C C}}$, HIGH-SIDE


FIGURE 32. NORMALIZED $V_{O A}$ vs IOUT

## Typical Performance Curves $\mathrm{V}_{\mathrm{Cc}}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{M2}$, untess otherwis s specfifed. (Continued)



FIGURE 33. GAIN vs FREQUENCY $\mathrm{V}_{\text {RS }+}=100 \mathrm{mV} / 12 \mathrm{~V}$, $V_{\text {SENSE }}=100 \mathrm{mV}, \mathrm{V}_{\text {OUT }}=50 \mathrm{mV} \mathrm{V}_{\text {P-P }}$


FIGURE 35. CAPACITIVE LOAD DRIVE GAIN vs FREQUENCY


FIGURE 37. GAIN ACCURACY (\%) vs TEMPERATURE


FIGURE 34. $\mathrm{V}_{\mathbf{O S}}(\mu \mathrm{V})$ vs TEMPERATURE


FIGURE 36. CAPACITIVE LOAD DRIVE PHASE vs FREQUENCY


FIGURE 38. $V_{\text {OUT }}$ ERROR (\%) vs TEMPERATURE

Typical Performance Curves $\mathrm{VCC}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{Mn}$, unless ofterwise specified. (Continued)


FIGURE 39. $\mathrm{V}_{\mathrm{OS}}(\mu \mathrm{V})$ DISTRIBUTION AT $+25^{\circ} \mathrm{C}, \mathrm{V}_{\text {RS }+}=12 \mathrm{~V}$, QUANTITY: 100


FIGURE 41. $\mathbf{V}_{\mathbf{O S}}$ vs $\mathbf{V}_{\text {RS }}+$


FIGURE 43. $\mathrm{V}_{\mathbf{O S}}$ vs $\mathrm{V}_{\mathbf{C C}}, \mathrm{V}_{\mathrm{RS}+}=0.1 \mathrm{~V}$


FIGURE 40. $\mathbf{V}_{\mathbf{O S}}$ vs $\mathbf{V}_{\text {RS }+}$


FIGURE 42. $\mathrm{V}_{\mathbf{O S}}$ vs $\mathrm{V}_{\mathrm{CC}}, \mathrm{V}_{\text {RS+ }}=12 \mathrm{~V}$


FIGURE 44. GAIN ACCURACY vs $\mathrm{V}_{\text {RS }+}=0 \mathrm{~V}$ TO 28V

## Typical Performance Curves $\mathrm{V}_{\mathrm{VC}}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{M2}$, untess otherwis s specfifed. (Continued)



FIGURE 45. GAIN ACCURACY vs $\mathrm{V}_{\mathrm{RS}+}=0 \mathrm{~V}$ TO 2V


FIGURE 47. GAIN ACCURACY vs $\mathbf{V}_{\mathbf{C C}}$, LOW-SIDE


FIGURE 49. GAIN vs FREQUENCY $\mathrm{V}_{\text {RS }+}=100 \mathrm{mV} / 12 \mathrm{~V}$,
$V_{\text {SENSE }}=100 \mathrm{mV}, \mathrm{V}_{\text {OUT }}=50 \mathrm{mV} \mathrm{V}_{\text {P-P }}$


FIGURE 46. GAIN ACCURACY vs $\mathbf{V}_{\mathbf{C C}}$, HIGH-SIDE


FIGURE 48. NORMALIZED $V_{O A}$ vs IOUT


FIGURE 50. $\mathrm{V}_{\mathbf{O S}}(\mu \mathrm{V})$ vs TEMPERATURE

## Typical Performance Curves $\mathrm{V}_{\mathrm{VC}}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{M2}$, unless otherwis s specfifed. (Continued)



FIGURE 51. CAPACITIVE LOAD DRIVE GAIN VS FREQUENCY


FIGURE 53. GAIN ACCURACY (\%) vs TEMPERATURE


FIGURE 55. $\mathrm{V}_{\mathrm{OS}}(\mu \mathrm{V})$ DISTRIBUTION AT $+25^{\circ} \mathrm{C}, \mathrm{V}_{\text {RS }+}=\mathbf{1 2 V}$, QUANTITY: 100


FIGURE 52. CAPACITIVE LOAD DRIVE PHASE VS FREQUENCY


FIGURE 54. $\mathrm{V}_{\text {OUT }}$ ERROR (\%) vs TEMPERATURE


FIGURE 56. $\mathbf{V}_{\mathbf{O S}}$ vs $\mathbf{V R S}^{+}$

Typical Performance Curves $\mathrm{V}_{\mathrm{Cc}}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{~m} 2$, untess otherwise specfifed. (Continued)


FIGURE 57. $\mathrm{V}_{\mathbf{O S}}$ vs $\mathrm{V}_{\text {RS }+}$


FIGURE 59. $\mathrm{V}_{\text {OS }}$ vs $\mathrm{V}_{\mathbf{C C}}$, LOW-SIDE


FIGURE 61. GAIN ACCURACY vs $\mathbf{V}_{R S+}=0 \mathrm{~V}$ TO 2 V


FIGURE 58. $\mathbf{V}_{\mathbf{O S}}$ vs $\mathbf{V}_{\mathbf{C C}}$, HIGH-SIDE


FIGURE 60. GAIN ACCURACY vs $\mathrm{V}_{\text {RS }+}=0 \mathrm{~V}$ TO 28V


FIGURE 62. GAIN ACCURACY vs $\mathbf{V}_{\mathbf{C C}}, \mathrm{V}_{\mathbf{R S}+}=12 \mathrm{~V}$

## Typical Performance Curves $\mathrm{V}_{\mathrm{VC}}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{M2}$, unless otherwis s specified. (Continued)



FIGURE 63. GAIN ACCURACY vs $\mathrm{V}_{\mathbf{C C}}, \mathrm{V}_{\mathbf{R S}+}=\mathbf{0} .1 \mathrm{~V}$


FIGURE 65. GAIN vs FREQUENCY $\mathrm{V}_{\text {RS }+}=100 \mathrm{mV} / \mathbf{1 2 V}$,
$V_{\text {SENSE }}=100 \mathrm{mV}, \mathrm{V}_{\text {OUT }}=50 \mathrm{mV} \mathrm{V}_{\text {P-P }}$


FIGURE 67. GAIN ACCURACY (\%) vs TEMPERATURE


FIGURE 64. NORMALIZED $V_{O A}$ vs IOUT


FIGURE 66. $\mathbf{V}_{\mathbf{O S}}(\boldsymbol{\mu} \mathrm{V})$ vs TEMPERATURE


FIGURE 68. $\mathrm{V}_{\text {OUT }}$ ERROR (\%) vs TEMPERATURE

Typical Performance Curves $\mathrm{V}_{\mathrm{Cc}}=12 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \mathrm{man}$, untess othemise specfifed. (Continued)


FIGURE 69. LOW SIDE CURRENT SENSING INPUT BIAS CURRENTS


FIGURE 70. HIGH SIDE CURRENT SENSING INPUT BIAS CURRENTS

## Test Circuits and Waveforms



FIGURE 71. $\mathbf{I}_{\mathbf{C C}}, \mathbf{V}_{\mathbf{O S}}, \mathbf{V}_{\mathbf{O A}}$, CMRR, PSRR, GAIN ACCURACY


FIGURE 73. $\mathbf{t}_{\mathbf{s}}$, SATURATION RECOVERY TIME


FIGURE 72. INPUT BIAS CURRENT, LEAKAGE CURRENT


FIGURE 74. GAIN vs FREQUENCY


FIGURE 75. SLEW RATE

## Applications Information

## Functional Description

The ISL28006-20, ISL28006-50 and ISL28006-100 are single supply, uni-directional current sense amplifiers with fixed gains of $20 \mathrm{~V} / \mathrm{V}, 50 \mathrm{~V} / \mathrm{V}$ and 100V/V respectively. The ISL28006-ADJ is single supply, uni-directional current sense amplifier with an adjustable gain via external resistors (see Figure 80). The ISL28006-ADJ is stable for gains of 20 and higher.

The ISL28006 is a 2-stage amplifier. Figure 76 shows the active circuitry for high-side current sense applications where the sense voltage is between 1.35 V to 28 V . Figure 77 shows the active circuitry for ground sense applications where the sense voltage is between OV to 1.35 V .

The first stage is a bi-level trans-conductance amp and level translator. The gm stage converts the low voltage drop (VENSE) sensed across an external milli-ohm sense resistor, to a current ( $@ g m=21.3 \mu \mathrm{~A} / \mathrm{V}$ ). The trans-conductance amplifier forces a current through $\mathrm{R}_{1}$ resulting to a voltage drop across $\mathrm{R}_{1}$ that is equal to the sense voltage ( $V_{\text {SENSE }}$ ). The current through $R_{1}$ is mirrored across $\mathrm{R}_{5}$ creating a ground-referenced voltage at the input of the second amplifier equal to $\mathrm{V}_{\text {SENSE }}$.

The second stage is responsible for the overall gain and frequency response performance of the device. The fixed gains $(20,50,100)$ are set with internal resistors $R_{f}$ and $R_{g}$. The variable gain (ADJ) has an additional FB pin and uses external
gain resistors to set the gain of the output. For the fixed gain amps the only external component needed is a current sense resistor (typically $0.001 \Omega$ to $0.01 \Omega, 1 \mathrm{~W}$ to 2 W ).

The transfer function for the fixed gain parts is given in Equation 1.
$\mathrm{V}_{\text {OUT }}=\mathrm{GAIN} \times\left(\mathrm{I}_{\mathbf{S}} \mathrm{R}_{\mathbf{S}}+\mathrm{V}_{\text {OS }}\right)$
The transfer function for the adjustable gain part is given in Equation 2.
$v_{\text {OUT }}=\left(1+\frac{R_{F}}{R_{G}}\right)\left(I_{S} R_{S}+v_{O S}\right)$
Where $I_{\mathbf{S}} \mathbf{R}_{\mathbf{S}}$ is the product of the load current and the sense resistor and is equal to VSENSE.

When the sensed input voltage is $>1.35 \mathrm{~V}$, the $\mathrm{gm}_{\mathrm{HI}}$ amplifier path is selected and the input gm stage derives its $\sim 2.86 \mu \mathrm{~A}$ supply current from the input source through the RS+ terminal. When the sense voltage at $\mathrm{R}_{\mathrm{S}^{+}}$drops below the 1.35 V threshold, the $\mathrm{gm}_{\mathrm{LO}}$ amplifier is enabled for Low Side current sensing. The gm ${ }_{\text {LO }}$ input bias current reverses, flowing out of the RS- pin. Since the $\mathrm{gm}_{\text {LO }}$ amplifier is sensing voltage around ground, it cannot source current to R5. A current mirror referenced off Vcc supplies the current to the second stage for generating a ground referenced output voltage. See Figures 69 and 70 for typical input bias currents for High and Low side current sensing.



FIGURE 77. LOW-SIDE CURRENT DETECTION

## Hysteretic Comparator

The input trans-conductance amps are under control of a hysteretic comparator operating from the incoming source voltage on the $\mathrm{R}_{\mathrm{S}+}$ pin (Figure 78). The comparator monitors the voltage on $\mathrm{R}_{\mathrm{S}+}$ and switches the sense amplifier from the low-side gm amp to the high-side gm amplifier whenever the input voltage at $\mathrm{R}_{\mathrm{S}_{+}}$increases above the 1.35 V threshold. Conversely, a decreasing voltage on the $\mathrm{R}_{\mathrm{S}+}$ pin, causes the hysteric comparator to switch from the high-side gm amp to the low-side gm amp as the voltage decreases below 1.35V. It is that low-side sense gm amplifier that gives the ISL28006 the proprietary ability to sense current all the way to OV. Negative voltages on the $\mathrm{R}_{\mathrm{S}_{+}}$or $\mathrm{R}_{\mathrm{S}_{-}}$are beyond the sensing voltage range of this amplifier.


FIGURE 78. GAIN ACCURACY vs $\mathrm{V}_{\mathrm{RS}+}=0 \mathrm{~V}$ TO 2V

## Typical Application Circuit

Figure 80 shows the basic application circuit and optional protection components for switched-load applications. For applications where the load and the power source is permanently connected, only an external sense resistor is needed. For applications where fast transients are caused by hot plugging the source or load, external protection components may be needed. The external current limiting resistor ( $R_{P}$ ) in Figure 80 may be required to limit the peak current through the internal ESD diodes to <20mA. This condition can occur in applications that experience high levels of in-rush current causing high peak voltages that can damage the internal ESD diodes. An Rp resistor
value of $100 \Omega$ will provide protection for a 2 V transient with the maximum of 20 mA flowing through the input while adding only an additional $13 \mu \mathrm{~V}$ (worse case over-temperature) of $\mathrm{V}_{\mathrm{OS}}$. Refer to Equation 3:
$\left(\left(\mathrm{R}_{\mathrm{P}} \times \mathrm{I}_{\mathrm{RS}}\right)=(100 \Omega \times 130 \mathrm{nA})=13 \mu \mathrm{~V}\right)$
Switching applications can generate voltage spikes that can overdrive the amplifier input and drive the output of the amplifier into the rails, resulting in a long overload recover time. Capacitors $C_{M}$ and $C_{D}$ filter the common mode and differential voltage spikes.

## Error Sources

There are 3 dominant error sources: gain error, input offset voltage error and Kelvin voltage error (see Figure 79). The gain error is dominated by the internal resistance matching tolerances. The remaining errors appear as sense voltage errors at the input to the amplifier. They are $\mathrm{V}_{\mathrm{OS}}$ of the amplifier and Kelvin voltage errors. If the transient protection resistor is added, an additional $\mathrm{V}_{\mathrm{OS}}$ error can result from the IxR voltage due to input bias current. The limiting resistor should only be added to the $\mathrm{R}_{\mathrm{S}}$ input, due to the high-side gm amplifier ( $\mathrm{gm}_{\mathrm{HI}}$ ) sinking several micro amps of current through the $\mathrm{R}_{\mathbf{S}+}$ pin.

## Layout Guidelines

## The Kelvin Connected Sense Resistor

The source of Kelvin voltage errors is illustrated in Figure 79. The resistance of $1 / 2 \mathrm{Oz}$ copper is $\sim 1 \mathrm{~m} \Omega$ per square with a TC of $\sim 3900 \mathrm{ppm} /{ }^{\circ} \mathrm{C}\left(0.39 \% /{ }^{\circ} \mathrm{C}\right)$. When you compare this unwanted parasitic resistance with the total $1 \mathrm{~m} \Omega$ to $10 \mathrm{~m} \Omega$ resistance of the sense resistor, it is easy to see why the sense connection must be chosen very carefully. For example, consider a maximum current of 20A through a $0.005 \Omega$ sense resistor, generating a $\mathrm{V}_{\text {SENSE }}=0.1$ and a full scale output voltage of 10 V ( $G=100$ ). Two side contacts of only 0.25 square per contact puts the $V_{\text {SENSE }}$ input about $0.5 \times 1 \mathrm{~m} \Omega$ away from the resistor end capacitor. If only 10 A the 20 A total current flows through the kelvin path to the resistor, you get an error voltage of 10 mV ( $10 \mathrm{~A} \times 0.5 \mathrm{sq} \times 0.001 \Omega / \mathrm{sq} .=10 \mathrm{mV}$ ) added to the 100 mV sense voltage for a sense voltage error of $10 \%(0.110 \mathrm{~V}-0.1) / 0.1 \mathrm{~V}) \times 100$.


FIGURE 79. PC BOARD CURRENT SENSE KELVIN CONNECTION


FIGURE 80. TYPICAL APPLICATION CIRCUIT

## Overall Accuracy ( $\mathbf{V O A}_{\mathbf{O A}}$ \%)

$V_{O A}$ is defined as the total output accuracy Referred-to-Output (RTO). The output accuracy contains all offset and gain errors, at a single output voltage. Equation 4 is used to calculate the \% total output accuracy.
$v_{O A}=100 \times\left(\frac{v_{\text {OUT }} \text { actual }-v_{\text {OUT }} \text { expected }}{v_{\text {OUT }} \text { expected }}\right)$
where
$\mathrm{V}_{\text {OUT }}$ Actual $=\mathrm{V}_{\text {SENSE }} \times$ GAIN
Example: Gain $=100$, For 100 mV V SENSE
10.1V. The overall accuracy $\left(\mathrm{V}_{\mathrm{OA}}\right)$ is $1 \%$ as shown in Equation 5.
$V_{O A}=100 \times\left(\frac{10.1-10}{10}\right)=1 \%$

## Power Dissipation

It is possible to exceed the $+150^{\circ} \mathrm{C}$ maximum junction temperatures under certain load and power supply conditions. It is therefore important to calculate the maximum junction temperature ( $\mathrm{T}_{\text {JMAX }}$ ) for all applications to determine if power supply voltages, load conditions, or package type need to be modified to remain in the safe operating area. These parameters are related using Equation 6:

$$
\begin{equation*}
\mathrm{T}_{\text {JMAX }}=\mathrm{T}_{\text {MAX }}+\theta_{\text {JA }} \times \text { PPD }_{\text {MAXTOTAL }} \tag{EQ.6}
\end{equation*}
$$

where:

- PDMAXTOTAL is the sum of the maximum power dissipation of each amplifier in the package ( $\mathrm{PD}_{\text {MAX }}$ )
- $\mathrm{PD}_{\text {MAX }}$ for each amplifier can be calculated using Equation 7:

$$
\begin{equation*}
\mathrm{PD}_{\mathrm{MAX}}=\mathrm{v}_{\mathbf{s}} \times \mathrm{I}_{\mathrm{qMAX}}+\left(\mathrm{v}_{\mathrm{S}}-\mathrm{v}_{\text {OUTMAX }}\right) \times \frac{\mathrm{v}_{\text {OUTMAX }}}{R_{\mathrm{L}}} \tag{EQ.7}
\end{equation*}
$$

where:

- $\mathrm{T}_{\text {MAX }}=$ Maximum ambient temperature
- $\theta_{\mathrm{JA}}=$ Thermal resistance of the package
- $\mathrm{PD}_{\text {MAX }}=$ Maximum power dissipation of 1 amplifier
- $\mathrm{V}_{\mathrm{CC}}=$ Total supply voltage
- $I_{\text {qMAX }}=$ Maximum quiescent supply current of 1 amplifier
- $\mathrm{V}_{\text {OUTMAX }}=$ Maximum output voltage swing of the application
- $\mathrm{R}_{\mathrm{L}}=$ Load resistance


## Revision History

The revision history provided is for informational purposes only and is believed to be accurate, but not warranted. Please go to web to make sure you have the latest Rev.

| DATE | REVISION | CHANGE |
| :---: | :---: | :---: |
| November 22, 2013 | FN6548.6 | Added eight new Typical Performance Curves <br> 1. Av=100 Capacitive Load Drive Gain vs Freq <br> 2. $A v=100$ Capacitive Load Drive Phase vs Freq <br> 3. $A v=50$ Capacitive Load Drive Gain vs Freq <br> 4. $A v=50$ Capacitive Load Drive Phase vs Freq <br> 5. $A v=20$ Capacitive Load Drive Gain vs Freq <br> 6. $\mathrm{Av}=20$ Capacitive Load Drive Phase vs Freq <br> 7. High Side Operation Input Bias Currents <br> 8. Low Side Operation Input Bias Currents <br> Under Electrical Specifications Table: <br> Changed parameter from Is to Icc to clarify supply current <br> Ordering information table on page 3: Changed Note 4 location in the table. |
| April 12, 2011 | FN6548.5 | Converted to new template <br> Page 1 - Changed headings for "Typical Application" and "Gain Accuracy vs VRS+ = 0 V to $\mathbf{2 8 V}$ " to Figure titles <br> (Figures 1 and 2). <br> Page 1 - Updated Intersil Trademark statement at bottom of page 1 per directive from Legal. <br> Page 7 - Updated over temp note in Min Max column of spec tables from "Parameters with MIN and/or MAX limits are $100 \%$ tested at $+25^{\circ} \mathrm{C}$, unless otherwise specified. Temperature limits established by characterization and are not production tested." to new standard "Compliance to datasheet limits is assured by one or more methods: production test, characterization and/or design." <br> Page 19 - Figure 69, Low side current detection schematic: Moved the LOAD from the ground side of the power side circuit to the high side. |
| September 2, 2010 | FN6548.4 | Added -T7A tape and reel options to Ordering Information Table for all packages. |
| May 12, 2010 | FN6548.3 | Added Note 4 to Part Marking Column in "Ordering Information" on page 3. Corrected hyperlinks in Notes 1 and 3 in "Ordering Information" on page 3. |
| April 8, 2010 |  | Removed "Coming Soon" from evaluation boards in "Ordering Information" on page 3. |
| April 7, 2010 |  | Added "Related Literature" on page 1 <br> Updated Package Drawing Number in the "Ordering Information" on page 3 for the 20V, 50 V and 100V options from MDP0038 to P50.64A. <br> Revised package outline drawing from MDP0038 to P5.064A on page 24. MDP0038 package contained 2 packages for both the 5 and 6 Ld SOT-23. MDP0038 was obsoleted and the packages were separated and made into 2 separate package outline drawings; P5.064A and P6.064A. Changes to the 5 Ld SOT-23 were to move dimensions from table onto drawing, add land pattern and add JEDEC reference number. |
| March 10, 2010 | FN6548.2 | Releasing adjustable gain option. <br> Added adjustable block diagram (Page 2), Added adjustable gain limits to electrical spec table, added Figures 47 through 60, Added $+85^{\circ} \mathrm{C}$ curves to Figures 6 thru 14, 20 thru 28, 34 thru 42, and Figures 48 thru 56. Modified Figure 70. |
| February 4, 2010 | FN6548.1 | -Page 1: <br> Edited last sentence of paragraph 2. <br> Moved order of GAIN listings from 20, 50, 100 to 100, 50, 20 in the 3rd paragraph. <br> Under Features ....removed "Low Input Offset Voltage $250 \mu \mathrm{~V}$, max" <br> Under Features .... moved order of parts listing from 20, 50, 100 (from top to bottom) to 100, 50, 20. <br> -Page 3: Removed coming soon on ISL28006FH50Z and ISL28006FH2OZ and changes the order or listing them to 100, 50, 20. <br> -Page 5: VOA test. Under conditions column ...deleted 20 mV to. It now reads ... Vsense $=100 \mathrm{mV}$ <br> SR test. Under conditions column ..deleted what was there. It now reads ... Pulse on RS+pin, See Figure 51 <br> -Page 6: ts test. Removed Gain = 100 and Gain $=100 \mathrm{~V} / \mathrm{V}$ in both description and conditions columns respectively. <br> -Page 9: Added VRS+= 12V to Figures 16, 17, 18. <br> -Page 11: Added VRS+= 12V to Figures 30, 31, 32. <br> -Page 13 \& 14: Added VRS+= 12V to Figures 44, 45, 46. <br> -Page 14 Added Figure 51 and adjusted figure numbers to account for the added figure. <br> -Figs 8,26 , and 40 change "HIGH SIDE" to "VRS $=12 \mathrm{~V}$ ", where RS is subscript. <br> -Figs 9,27 , and 41 change "LOW SIDE" to "VRS $=0.1 \mathrm{~V}$ ", where RS is subscript. |
| December 14, 2009 | FN6548.0 | Initial Release |

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## Package Outline Drawing

## P5.064A

5 LEAD SMALL OUTLINE TRANSISTOR PLASTIC PACKAGE Rev 0, 2/10


TOP VIEW



DETAIL "X"


TYPICAL RECOMMENDED LAND PATTERN

NOTES:

1. Dimensions are in millimeters. Dimensions in ( ) for Reference Only.
2. Dimensioning and tolerancing conform to ASME Y14.5M-1994.
3. Dimension is exclusive of mold flash, protrusions or gate burrs.
4. Foot length is measured at reference to guage plane.
5. This dimension is measured at Datum " H ",
6. Package conforms to JEDEC MO-178AA.

Package Outline Drawing

## P6.064

6 LEAD SMALL OUTLINE TRANSISTOR PLASTIC PACKAGE Rev 4, 2/10


see detail $X$
END VIEW


NOTES:

1. Dimensions are in millimeters.

Dimensions in ( ) for Reference Only.
2. Dimensioning and tolerancing conform to ASME Y14.5M-1994.
3. Dimension is exclusive of mold flash, protrusions or gate burrs.
4. Foot length is measured at reference to guage plane.
5. Package conforms to JEDEC MO-178AB.

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LMP8481AHQDGKRQ1 INA211CIRSWT LT6108AHMS8-1\#PBF INA214CIRSWR LT1620CMS8\#PBF INA215CIDCKR
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AD8214ARMZ AD8214ARMZ-R7 AD8290ACPZ-R2 AD8290ACPZ-R7 AD22057RZ AD8215YRZ AD8417WHRZ AD8210YRZ
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