## 24V/60V Boost Converter with SMBus Controlled 4-CH LED Driver

## General Description

The RT8549LV is a high efficiency Boost converter with $4-\mathrm{CH}$ LED driver supporting 60V maximum output voltage. It is designed for LCD panel applications that employs LED as lighting sources. The Boost converter generates a suitable output voltage to drive four LED strings in parallel and supports up to 18 LEDs per string.

The RT8549LV supports a wide input voltage range from 4.2 V to 24 V and provides a SMBus interface to control the LED brightness dimming mode, operating frequency and LED currents. The internal $150 \mathrm{~m} \Omega, 60 \mathrm{~V}$ power switch with current-mode control provides high efficiency operation.

The RT8549LV is available in the WDFN-16L $5 \times 5$ package to achieve optimized solution for PCB space.

## Marking Information

For marking information, contact our sales representative directly or through a Richtek distributor located in your area.

## Features

- Wide Operating Input Voltage : 4.2V to 24 V
- Max 60V Output Voltage
- 3\% LED Current Accuracy
- 2\% LED Current Matching
- Low Drop Output 120mA/0.4V Current Sink
- SMBus Programs LED Current, Switching Frequency, Dimming Mode
- LED Current : $\mathbf{2 2} \mathbf{2 8} \mathbf{5 m A}$ to $\mathbf{1 8 0 m A}$
- Switching Frequency : 200kHz to 900 kHz
- Dimming Mode : PWM, DC, Mixed-Mode
- Built-in Input UVP, Output OVP, OCP, and Soft-Start
- Support LED Hot-plug, Open/Short Detection
- Low EMI, Low Acoustic Noise
- RoHS Compliant and Halogen Free


## Applications

- UMPC and Notebook Computer Backlight


## Simplified Application Circuit



Ordering Information RT8549LVロロ

Package Type QW : WDFN-16L 5x5 (W-Type)
Lead Plating System
G: Green (Halogen Free and Pb Free)
Note :
Richtek products are :

- RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- Suitable for use in SnPb or Pb-free soldering processes.


## Pin Configurations



## Functional Pin Description

| Pin No. | Pin Name | Pin Function |
| :---: | :--- | :--- |
| 1 | CS1 | Current Sink for LED Channel 1. |
| 2 | CS2 | Current Sink for LED Channel 2. |
| 3 | CS3 | Current Sink for LED Channel 3. |
| 4 | CS4 | Current Sink for LED Channel 4. |
| 5 | GND | Ground. |
| 6 | FAULT | Fault Indicator Output. When fault condition occurs, the FAULT pin will be <br> pulled up to VIN. |
| 7 | VDC | Compensation Note for Error Amplifier. Connect a compensation network to <br> ground. |
| 8 | PWM | Output of Internal Regulator Voltage. Connect a capacitor from this pin to <br> ground. |
| 10 | EN | EnM Dimming Control Input. |
| 11 | VIN | Power Supply Input. |
| 12,13 | LX | Switch Node of Boost Converter. |
| 14 | SMBCLK | Clock of SMBus. |
| 15 | SMBDAT | Data of SMBus. |
| 16 | VOUT | Over Voltage Protection Sense Input. |
| 17 (Exposed Pad) | PGND | Ground. The exposed pad must be soldered to a large PCB and connected to <br> PGND for maximum power dissipation. |

## Function Block Diagram



## Operation

The RT8549LV integrates four LED drivers and a Boost converter. When EN is High and VIN is higher than the UVLO for a white, the RT8549LV will detect the status of the channel. Then the digital part will be reset and set all default states registers.

Once SMBus receives a "STOP" signal, the RT8549LV will start to check PWM duty and then enter soft-start mode. The RT8549LV will choose the minimum value of $V_{\text {LED }}$ as the feedback voltage of Boost converter.

During operation, when a LED string is defined as short, the driver of that channel will be turned off. When LED string is defined as open, the driver of that channel will be turned off, and auto-recovery when the "OPEN" is released.

Once "VOUT shorted to GND" or "Schottky diode shorted" are defined as the fault condition, the RT8549LV will alarm this condition through the fault flag of SMBus. The fault flag could also be cleared through the SMBus.
Absolute Maximum Ratings (Note 1)

- Supply Input Voltage, VIN to GND ..... -0.3 V to 44 V
- VDC to GND -0.3 V to 6 V
- SMBDAT, SMBCLK to GND -0.3 V to 26.5 V
- EN, PWM, COMP, FAULT to GND ..... -0.3 V to 44 V
- CS1, CS2, CS3, CS4 to GND -0.3 V to 66 V
- LX, VOUT to GND -0.3 V to 72 V
- Power Dissipation, $\mathrm{P}_{\mathrm{D}} @ \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ WDFN-16L5x5 ..... 3.47W
- Package Thermal Resistance (Note 2) WDFN-16L $5 \times 5, \theta_{\mathrm{JA}}$ ..... $28.8^{\circ} \mathrm{C} / \mathrm{W}$
WDFN-16L $5 \times 5, \theta_{\mathrm{Jc}}$ $4.4^{\circ} \mathrm{C} / \mathrm{W}$
- Lead Temperature (Soldering, 10 sec .) ..... $260^{\circ} \mathrm{C}$
- Junction Temperature ..... $150^{\circ} \mathrm{C}$
- Storage Temperature Range ..... $-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
- ESD Susceptibility (Note 3) HBM (Human Body Model) ..... 2kV
MM (Machine Model) ..... 200V
Recommended Operating Conditions- Supply Input Voltage4.2 V to 24 V
- Junction Temperature Range $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$
- Ambient Temperature Range $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$


## Electrical Characteristics

$\left(\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}, \mathrm{C}_{\mathbb{I N}}=1 \mu \mathrm{~F}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\right.$, unless otherwise specified)

| Parameter | Symbol | Test Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input Power Supply |  |  |  |  |  |  |
| Input Supply Voltage | VIN |  | 4.2 | -- | 24 | V |
| Quiescent Current | $\mathrm{I}_{\mathrm{Q}}$ | $\mathrm{EN}=3.3 \mathrm{~V}, \mathrm{PWM}=0$ | -- | 3.3 | -- | mA |
| Shutdown Current | ISHDN | $\mathrm{V}_{\mathrm{IN}}=4.5 \mathrm{~V}, \mathrm{EN}=0$ | -- | -- | 10 | $\mu \mathrm{A}$ |
| Under-Voltage Lockout Threshold | VUVLO | $V_{\text {IN }}$ Rising | -- | 3.8 | -- | V |
| Under-Voltage Lockout Hysteresis | $\Delta \mathrm{V}$ UVLO |  | -- | 500 | -- | mV |
| VDC Reference Voltage | $V_{\text {DC }}$ |  | -- | 3.8 | -- | V |
| VDC Source Current | IVDC |  | -- | -- | 500 | $\mu \mathrm{A}$ |
| Interface Characteristic |  |  |  |  |  |  |
| EN, PWM, SMBCLK, SMBDAT Input High Threshold | $\mathrm{V}_{\mathrm{IH}}$ |  | 2 | -- | -- | V |
| EN, PWM, SMBCLK, SMBDAT Input Low Threshold | $V_{\text {IL }}$ |  | -- | -- | 0.8 | V |
| EN Internal Pull-Low Current | $\mathrm{IIH}_{\text {_EN }}$ | $\mathrm{V}_{\mathrm{EN}}=3.3 \mathrm{~V}$ | -- | -- | 10 | $\mu \mathrm{A}$ |


| Parameter | Symbol | Test Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SMBCLK, SMBDAT Internal Pull-Low Current | $\mathrm{IIH}_{\text {S }} \mathrm{SMB}$ | $\mathrm{V}_{\mathrm{UP}}=3.3 \mathrm{~V}$ | -- | 0.01 | 1 | $\mu \mathrm{A}$ |
| PWM Internal Pull Low Current | $\mathrm{I}_{\mathrm{H}+\mathrm{PWM}}$ | $\mathrm{V}_{\text {PWM }}=3.3 \mathrm{~V}$ | -- | -- | 15 | $\mu \mathrm{A}$ |
| SMBus Interface Timing (Note 5) |  |  |  |  |  |  |
| SMBus Operating Frequency | $\mathrm{f}_{\text {SMB }}$ |  | 10 | -- | 100 | kHz |
| Bus Free Time between Stop and Start Condition | $\mathrm{t}_{\text {BuF }}$ |  | 4.7 | -- | -- | $\mu \mathrm{S}$ |
| Hold Time after Start Condition | thd_sta | After this Period, the First Clock is Generated | 4 | -- | -- | $\mu \mathrm{s}$ |
| Repeated Start Condition Setup Time | tsu_STA |  | 4.7 | -- | -- | $\mu \mathrm{S}$ |
| Stop Condition Setup Time | tsu_Sto |  | 4 | -- | -- | $\mu \mathrm{s}$ |
| Data Hold Time | thd_dat |  | 300 | -- | -- | ns |
| Data Setup Time | tsu_dat |  | 250 | -- | -- | ns |
| Detect Clock Low Timeout | $\mathrm{t}_{\text {TIMEOUT }}$ |  | 25 | -- | 35 | ms |
| Clock Low Period | tow |  | 4.7 | -- | -- | $\mu \mathrm{s}$ |
| Clock High Period | $\mathrm{tHIGH}^{\text {l }}$ |  | 4 | -- | 50 | $\mu \mathrm{s}$ |
| Slave Device Cumulative Clock Low Extend Time_Slave | tLow_SEXT |  | -- | -- | 25 | ms |
| Mater Device Cumulative Clock Low Extend Time_Master | tLow_MEXT |  | -- | -- | 10 | ms |
| Fall Time of SMB DAT/CLK | $t_{\text {F_S }}$ SMB |  | -- | -- | 300 | ns |
| Rise Time of SMB DAT/CLK | tr_SMB |  | -- | -- | 1000 | ns |
| Power On Reset of SMB | tSMB_POR | Time in Which a Device must be Operation after Power On Reset | -- | 3 | 500 | ms |
| Boost Converter |  |  |  |  |  |  |
| Switching Frequency Accuracy | fsw_Acc | Boost Operates at PWM Mode, $\mathrm{fsw}=400 \mathrm{kHz}$ | -10 | -- | 10 | \% |
| Default Switching Frequency | fsw | Boost Operates at PWM Mode | -- | 400 | -- | kHz |
| Switching Frequency Setting Range | fsw_Rg | Boost Operates at PWM Mode | 200 | -- | 900 | kHz |
| Step-up Maximum Duty Cycle | $\mathrm{D}_{\text {max }}$ |  | -- | 93 | -- | \% |
| Boost Switch R ${ }_{\text {DS(ON) }}$ | $\mathrm{R}_{\mathrm{DS}(\mathrm{ON}) \text { _BST }}$ | $\mathrm{V}_{\mathrm{DC}}=5 \mathrm{~V}, \mathrm{ISW}_{\text {_ }} \mathrm{BST}=100 \mathrm{~mA}$ | -- | 0.18 | 0.5 | $\Omega$ |
| Switching Current Limitation | locp_bst |  | 2.8 | 3.3 | -- | A |
| Over-Voltage Protection | Vout | OVP Selection = B10 | -- | 60 | -- | V |
| LED Current |  |  |  |  |  |  |
| Leakage Current of CSx | LLK_CSx | $\mathrm{V}_{\mathrm{CSX}}=50 \mathrm{~V}, \mathrm{I}_{\mathrm{CS}}=0 \mathrm{~mA}$ | -- | -- | 10 | $\mu \mathrm{A}$ |
| Minimum CSx Regulation Voltage | VCs_MIN | $\mathrm{ICSx}=120 \mathrm{~mA}$ | -- | 0.45 | -- | V |
| Maximum LED Current Setting | Ics_max |  | -- | -- | 180 | mA |


| Parameter | Symbol | Test Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dimming Frequency | fPWM |  | 200 | -- | 1000 | Hz |
| LED Current Accuracy | ICS_ACC | PWM Duty $=100 \%$, $\mathrm{I}_{\text {LED }}=120 \mathrm{~mA}$ | -3 | -- | 3 | \% |
| LED Current Matching | lLED_MAT | PWM Duty $=100 \%$, $\mathrm{L}_{\text {LED }}=120 \mathrm{~mA}$ | -2 | -- | 2 | \% |
| CSx Channel Unused Threshold | VCS_UNUSE |  | -- | 0.2 | -- | V |
| Light Bar Open Threshold | VCs_OPEN |  | -- | 0.1 | -- | V |
| Light Bar Short Threshold | VCS_SHORT |  | -- | 5.6 | -- | V |
| Thermal Shutdown Temperature | Totp |  | -- | 150 | -- | ${ }^{\circ} \mathrm{C}$ |
| Thermal Shutdown Hysteresis | TotP_hys |  | -- | 20 | -- | ${ }^{\circ} \mathrm{C}$ |
| Mixed Mode Dimming Frequency | fPWM_LED | When Dimming Duty < 25\% | -- | 26 | -- | kHz |

Note 1. Stresses beyond those listed "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions may affect device reliability.
Note 2. $\theta_{\mathrm{JA}}$ is measured at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ on a high effective thermal conductivity four-layer test board per JEDEC 51-7. $\theta_{\mathrm{Jc}}$ is measured at the exposed pad of the package.

Note 3. Devices are ESD sensitive. Handling precaution is recommended.
Note 4. The device is not guaranteed to function outside its operating conditions.
Note 5. Guaranteed by design; not subject to production testing.

## Typical Application Circuit



Figure 1. General Application


Figure 2. External P-MOSFET Isolation Application


Figure 3. Wide Input Voltage Step Application


Figure 4. High Power Application

## Timing Diagram

## SMBus Common AC Specification



SMBus Timeout


## Power-On Sequence



## Power-Off Sequence



## Typical Operating Characteristics



LED Current vs. Input Voltage



LED Current vs. Temperature




Quiescent Current vs. Temperature



Quiescent Current vs. Input Voltage


LED Current vs. SMBus Command



Power On from SMBus Command


Power On from PWM


Line Transient Response


Power Off from EN


Power Off from PWM


## Application Information

The RT8549LV is a general purpose 4-CH LED driver and is capable of delivering a maximum 180 mA LED current. The IC is a current-mode Boost converter integrated with a 60V/3.3A power switch and can cover a wide VIN range from 4.2 V to 24 V . The part integrates both built-in softstart and with PWM dimming control; moreover, it provides over voltage, over-temperature and current limit protections. It also integrates PWM and mixed mode dimming function for accurate LED current control. The PWM dimming frequency can operate form 200 Hz to 1 kHz without inducing any inrush current in LED and inductor.

## Dimming Control

The RT8549LV provides three dimming modes for controlling the LED brightness. The three dimming modes include PWM mode, DC mode and Mixed mode, and the dimming mode could be set by register 00h. If the 00h[1:0] is set 11, the dimming mode is still in Mixed mode which is shown in Table 2 below.

## PWM Mode

The ON/OFF of the current source is synchronized to the PWM signal. The frequency of LED current is equal to the PWM input signal.

## DC Mode

The PWM signal will be monitored and calculate its duty. The magnitude of $I_{\text {LED }}$ will be proportional to the duty.
$I_{\text {LED }}=I_{\text {MAX }} x$ duty

## Mixed Mode

When $25 \% \leq$ PWM duty $\leq 100 \%$, the PWM duty modulated the amplitude of the current. (same as DC mode) PWM duty $<25 \%$, the DC dimming will translate to PWM dimming, controlling the PWM duty instead by amplitude.

Table 1. Register Map
Slave Address : b0110001

| Register Address | bit7 | bit6 | bit5 | bit4 | bit3 | bit2 | bit1 | bit0 | Default Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0 \times 00$ | OVP <br> Reset [7] |  |  | $\begin{aligned} & \text { OCP } \\ & \text { Fault [4] } \end{aligned}$ |  | $\begin{gathered} \text { DIM_sig_ } \\ \text { Sel [2] } \end{gathered}$ | Dimming Control [1:0] |  | $0 \times 01$ |
| $0 \times 01$ |  | OVP [6:5] |  | Current <br> Limit [4] | Switching_frequency [3:0] |  |  |  | 0x54 |
| $0 \times 02$ | LED Current Setting [7:0] |  |  |  |  |  |  |  | $0 \times 00$ |
| $0 \times 03$ | Fault Enable [7] |  |  |  | Fault Flag Clear [3] | $\overline{S L P}$ [2] | SLP Latch [1] | Fault Flag [0] | 0x80 |
| 0x04 | SMBus Dimming Control [7:0] |  |  |  |  |  |  |  | 0x00 |
| 0x06 | Written <br> Check [7] |  |  |  |  |  |  |  | 0x80 |

Table 2. Dimming Control Mode Selection

| Address | Bit | Name | Default Value | Description | R/W |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 00h | [1:0] | Dimming mode selection | DC mode (01) | 00 : PWM mode | R/W |
|  |  |  |  | 01 : DC mode |  |
|  |  |  |  | 10 : Mixed mode |  |

## Dimming Control Signal Selection

The RT8549LV integrates a dimming control signal selection. The dimming control signal source could be set by the second bit of register 00 h . If the bit equals to 0 , it means the dimming control signal source just depends
on the input signal of the PWM pin. Otherwise, if the bit equals to 1 , the dimming control signal is controlled by the command of register 04h. The dimming control signal of register 04h supports the DC mode and Mixed mode. The option is shown in Table 3 below.

Table 3. Dimming Control Signal Selection

| Address | Bit | Name | Default Value | Description | R/W |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 00h | [2] | Dimming Control <br> Signal Selection | PWM pin (0) | 0 : Dimming control signal is depend on PWM pin. | R/W |
|  |  | 1 Dimming control signal supply by register 04h. |  |  |  |

Note : There is no two cycle delay when the bit set to 1 .

## OCP Fault

There is an over-current protection function cycle-by-cycle to turn off the power MOSFET of the Boost converter. We could have a further protection if the OCP Fault function is enabled (addr 0x00h, bit 4). Once this register is set high, internal counter is started to check OCP status. if OCP occurs 128 times continuously, the fault pin will be pulled high to turned off the external P-MOSFET.

The OCP Fault Could be Selection as the Table 4.

## Switching Frequency

The LED driver switching frequency is adjusted by the SMBus, The switching frequency setting range and resolutions are shown in the Table 6 below.

If the switching frequency command is below to $0 \times 02 \mathrm{~h}$ ( $0 \times 01 \mathrm{~h}$ to $0 \times 00 \mathrm{~h}$ ), the switching frequency would be clamped at 200 kHz . The command is above the 0x09h ( $0 x 0 \mathrm{~A}$ to $0 \times 0 \mathrm{~F}$ ), the switching frequency would be clamped at 900 kHz .

## OVP Reset

The RT8549LV integrates an OVP Reset mechanism. User could choose to let the IC Reset or output voltage clamped on a voltage of OVP. The OVP Reset mechanism is setting by SMBus interface, and set the bit [7] of register 00h.

Table 4. OCP Fault Setting

| Address | Bit | Name | Default Value | Description | R/W |
| :---: | :---: | :---: | :---: | :--- | :---: |
| 00 h | $[4]$ | OCP Fault | Disable (0) | 0 : Disable |  |
|  |  |  | R/W : Enable |  |  |

Table 5. OVP Reset Setting

| Address | Bit | Name | Default Value | Description | R/W |
| :---: | :---: | :---: | :---: | :--- | :---: |
| 00 h | [7]{} | OVP Reset | Disable (0) | 0 : Disable | R/W |
|  |  |  |  |  |  |

Table 6. Switching Frequency Setting

| Address | Bit | Name | Default Value | Description | Resolution | R/W |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 01h | [3:0] | Boost switching frequency | 400kHz (0x04h) | 0x04h : 400 kHz | $\begin{gathered} \sim 100 \mathrm{kHz} \\ (0 \times 02 \mathrm{~h} \text { to } \\ 0 \times 09 \mathrm{~h}) \end{gathered}$ | R/W |
|  |  |  |  | Between the code 0x00h and $0 x 02 \mathrm{~h}$ are equal to 200 kHz . |  |  |
|  |  |  |  | Between the code 0x09h and $0 x 0 F h$ are equal to 900 kHz . |  |  |

## Current Limit Protection

The RT8549LV integrates current limit protection, and the current of current limit protection could be set by SMBus, which is shown in the Table 7 below.

The RT8549LV can limit the peak current to achieve overcurrent protection. The RT8549LV senses the inductor current during the "ON" period that flows through the LX pin. The duty cycle depends on the current signal and internal slope compensation in comparison with the error signal. The internal switch of Boost converter will be turned off when the peak current value of inductor current is larger than the over-current protection setting. In the "OFF" period, the inductor current will be decreased until the internal switch is turned on by the oscillator.

## Over-Voltage Protection

The RT8549LV integrates over-voltage protection. The overvoltage protection could be set by the SMBus, the voltage of over-voltage protection ( $\mathrm{V}_{\mathrm{Ovp}}$ ) could be selected as the Table 8 below.

When the Boost output voltage rises above the $\mathrm{V}_{\text {ovp }}$, the internal switch will be turned off. Once the Boost output voltage drop below the Vovp, the internal switch will be turned on again. The Boost output voltage can be clamped at the $\mathrm{V}_{\mathrm{OvP}}$.

Table 7. Current Limit Protection Setting

| Address | Bit | Name | Default Value | Description | R/W |
| :---: | :---: | :--- | :--- | :--- | :--- |
| 01 h | $[4]$ | Switching current limitation <br> selection | $3.3 \mathrm{~A}(1)$ | Boost switch current limitation. |  |
|  |  |  |  | R/W |  |
|  |  |  |  |  |  |

Table 8. OVP Voltage Setting

| Address | Bit | Name | Default Value | Description | R/W |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 01h | [6:5] | Over voltage protection selection | 65 V (11) | Boost output over voltage protection. | R/W |
|  |  |  |  | 11 : 65V |  |
|  |  |  |  | 10:60V |  |
|  |  |  |  | 01:50V |  |
|  |  |  |  | 00:35V |  |

## LED Current Setting

The LED current of each channel could be set by SMBus command, it is shown in the Table 9.

When the LED current setting command is below 0x20h to $0 \times 01 \mathrm{~h}$, the LED current will be kept at 22.58 mA . When the command is $0 x 00 \mathrm{~h}$, the LED current will be set to 0 mA . The maximum LED current setting is 180 mA . The one step of LED current is approximately 0.706 mA .

## Fault Protection

The fault protection function can protect the system once there is an abnormal state at switching pin. (eg. too low during turn off and too high during turn on) the FAULT pin will output a voltage level same with VIN, forcing the PMOSFET to be turned off, to prevent the short current to damage IC or components. When under normal operation, the FAULT pin output voltage will be clamp at 6V making sure the P-MOSFET can be fully turn on.

In addition, this function could be chosen enable or disable by SMBus command, setting the bit [7] of register 03 h . If the bit data is written 1 , it means enable fault protection, and vice versa.

When the protection enable, and the one of two fault condition is happened. To read fault flag bit [0] of register 03 h , it would be from 0 changed to 1 . After the fault condition is cleared, user could set fault flag clear bit [3] of register 03h to 1 and write it.

Table 9. LED Current Setting

| Address | Bit | Name | Default Value | Description | Resolution | R/W |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 02h | [7:0] | LED current setting | OmA (0x00h) | control the max current | $\begin{gathered} \sim 0.706 \mathrm{~mA} \\ (0 \times F F h \text { to } 0 \times 20 \mathrm{~h}) \end{gathered}$ | R/W |
|  |  |  |  | 0xFFh : 180mA |  |  |
|  |  |  |  | 0x20h: 22.58 mA |  |  |
|  |  |  |  | 0x00h: 0mA |  |  |
|  |  |  |  | Between the code 0x01h and $0 \times 20 \mathrm{~h}$ are equal to 22.58 mA |  |  |

Table 10. Fault Protection Setting

| Address | Bit | Name | Default Value | Description | R/W |
| :---: | :---: | :--- | :---: | :--- | :---: |
| 03 h | $[0]$ | Monitor fault condition | -- | Detect fault condition happen or not (Read only). | R |
|  | $[3]$ | Fault flag could be <br> cleared by SMBus. | Original State <br> (0) | 0 : keep the original state <br> $1:$ clear fault flag | R/W |
|  | $[7]$ | Fault function enable. | Enable (1) | $0:$ disable <br> $1:$ enable | R/W |

## Short LED Protection

The RT8549LV integrates Short LED Protection (SLP). If CSx pin voltages exceeds the threshold of approximately 5.6 V during normal operation, the channels will be turned off. And the channel will keep rechecking in the rest mode.
User could turn on or turn off the SLP function by SMBus interface. If the bit [2] of register 03h write 1, its means the SLP function is turn off. On the contrary, the bit is written 0 means turn it on. The register setting is shown in Table 11 below.
User could choose latch mode of SLP by setting. Once the SLP occurs, the particular channel will be off.

## SMBus Dimming

The RT8549LV integrates an SMBus dimming control signal by register 04h. The dimming duty is adjusted from $0 \%(0 \times 00)$ to $100 \%(0 x F F)$, and one step is about $0.392 \%$. Users just need to write the register 04h. ex. Register 04 h write into $0 \times 7 \mathrm{~F}$, the register code is corresponds to $50 \%$ dimming duty. The setting method is shown Table 12 below.

The internal SMBus signal supports only DC mode and Mixed mode. The dimming frequency is about 26 kHz when the dimming duty below to $25 \%$ of Mixed mode.

## LED Current Written Check

The RT8549LV provides a check bit, it is for users to check LED current greater than zero. If LED current setting is greater than zero, the check bit would be changed to 0 . Otherwise, LED current setting equals to zero, and the check bit would be changed to 1 . The check bit is shown in Table 13 below.

Table 11. Short LED Protection Setting

| Address | Bit | Name | Default Value | Description | R/W |
| :---: | :---: | :--- | :---: | :--- | :--- |
| 03 h | $[1]$ | Short LED protection latch | Reset Mode(0) | $0:$ Reset Mode <br> $1:$ Latch Mode | R/W |
|  | $[2]$ | Short LED protection | Enable (0) | $0:$ Enable <br> $1:$ Disable | R/W |

Table 12. SMBus Dimming Control Setting

| Address | Bit | Name | Default Value | Description | Resolution | R/W |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 04 h | $[7: 0]$ | SMBus Dimming Control | $0 \%(0 \times 00)$ | $0 \times 00: 0 \%$ <br> $0 \times F F: 100 \%$ | $0.392 \%$ | R/W |

Table 13. LED Current Check Bit

| Address | Bit | Name | Default Value | Description | R/W |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 06 h | $[7]$ | Written Check | LED Current $=0(1)$ | $0:$ LED Current Setting $>0$ <br> $1:$ LED Current Setting $=0$ | R |

## SMBus Write Timing Sequence

## Write 1 byte

(Command byte is sent after the address and determines which register receives the data that follows the command byte.)


## Write N bytes

(Command byte is sent after the address and determines which register receives the data that follows the command byte.)


## SMBus Read Timing Sequence

## Read 1 byte

(Command byte is sent after the address and determines which register is accessed. After a start, the device address is sent again and LSB is set to logic 1. Data defined by command byte then is sent by RT8549LV.)

| Slave Address |  |  |  |  |  |  | $\mathrm{R} / \overline{\mathrm{W}}$ |  |  | Register Address |  |  |  | R/W |  | Register Data 1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | A | Command Byte | A | S | Slave Address | 1 | A | Data Byte 1 | $\overline{\mathrm{A}}$ | P |

## Read N bytes

(Command byte is sent after the address and determines which register is accessed. After a start, the device address is sent again and LSB is set to logic 1. Data defined by command byte then is sent by RT8549LV.)


## LED Connection

The RT8549LV equips 4-CH LED drivers and each channel supports up to 17 LEDs $\left(V_{f}=3 V\right)$. The LED strings are connected from the output of the Boost converter to the $\operatorname{CSx}$ ( $x=1$ to 4 ) pins respectively. If one of the current sink channels is not used, the CSx pin should be connected to GND. If the un-used channel is not connected to GND, it will be considered that the LED string is opened, the channel will turn light when the LED string is recovering connected.

## Compensation

The regulator loop can be compensated by adjusting the external components connected to the COMP pin. The COMP pin is the output of the internal error amplifier. The compensation capacitor will adjust the integrator zero to maintain stability and the resistor value will adjust the frequency integrator gain for fast transient response. Typical values of the compensation components are $\mathrm{R}_{\text {COMP }}=0 \Omega, \mathrm{C}_{\text {COMP }}=100 \mathrm{nF}$.

## Line Transient Response

The line transient response relates to the bandwidth of loop compensation. The bandwidth and stability need to trade off. If bandwidth is large, the line transient response is better. On the contrary, the stability would be worse. Moreover, if the variation of input voltage is larger or the slew rate of input voltage variation is steeper, the bandwidth needs to become larger to fit the application. The loop compensation is designed as below, the first step determine the dominate pole and right hand plane zero.
$\mathrm{f}_{\text {DP }}=\frac{2 \times \mathrm{I}_{\text {OUT }}}{2 \pi \times \mathrm{V}_{\text {OUT }} \times \mathrm{C}_{\text {OUT }}}$
$\mathrm{f}_{\text {RHPZ }}=\frac{(1-\mathrm{D})^{2} \times \mathrm{V}_{\text {OUT }}}{2 \pi \times \mathrm{I}_{\text {OUT }} \times \mathrm{L}}$
Then the second step determines the compensation components ( $\mathrm{R}_{\text {Cомр }}, \mathrm{C}_{\text {сомр }}, \mathrm{C}_{\text {сомр2 }}$ ). After consideration the loops gain. The $\mathrm{R}_{\text {сомр }}$ can be suggested form 1 k to $33 k \Omega$,
$R_{\text {COMP }}=10^{\frac{\mathrm{G}_{\mathrm{A}}}{20}} \times \frac{1}{\mathrm{G}_{\mathrm{m}}}$
$\mathrm{C}_{\mathrm{COMP}}=\frac{1}{2 \times \pi \times \mathrm{R}_{\mathrm{COMP}} \times \mathrm{f}_{\mathrm{DP}}}$

## $\mathrm{C}_{\mathrm{COMP2}}=\frac{1}{2 \times \pi \times \mathrm{R}_{\mathrm{COMP}} \times \mathrm{f}_{\mathrm{RHPZ}}}$

Where $f_{D P}$ is the dominate pole, $f_{R H P Z}$ is the right-halfplane zero.

The overshoot voltage will be induced on output voltage ( $\mathrm{V}_{\text {OUT }}$ ) when the input voltage is changed from low to high. The overshoot voltage will direct reflect on $V_{\text {LED_max }}$ ( $V_{\text {Led_max }}$ is the voltage between the CSx pin and ground). The overshoot voltage ( $\mathrm{V}_{\text {OS }}$ ) of $\mathrm{V}_{\text {LED_max }}$ could be measured and ensure it away from the SLP threshold, such as below waveform.

Line Transient Response


In general notebook application, the compensator components is recommended as $\mathrm{R}_{\text {CoMP }}=33 \mathrm{k}, \mathrm{C}_{\text {comp }}=$ $22 \mathrm{nF}, \mathrm{C}_{\text {Comp2 }}=1 \mathrm{nF}$ and the value of output capacitor should be $68 \mu \mathrm{~F}$ at least.

## Over Temperature Protection

The RT8549LV has over temperature protection function to prevent the IC from overheating due to excessive power dissipation. The OTP function will shutdown the IC when junction temperature exceeds $150^{\circ} \mathrm{C}$ (typ.). When junction temperature cools down to $130^{\circ} \mathrm{C}$ (TOTP_hys $=20^{\circ} \mathrm{C}$ ), the LED driver will return to normal work.

## Series Resistor Selection On PWM Pin

The calculation of series resistor should consider the Input high threshold $\left(\mathrm{V}_{\mathrm{IH}}\right)$ and the internal pull-low current ( $I_{\mathrm{IH}_{2}}$ PWM) of PWM. The minimum value of $\mathrm{V}_{\mathrm{IH}}$ is 2 V , and the maximum of $\mathrm{I}_{\mathrm{IH}_{-} \mathrm{PWM}}$ is $15 \mu \mathrm{~A}$. The resistor could be calculated by the equation below. $\mathrm{Ex} . \mathrm{V}_{\mathrm{PWM}}=3.3 \mathrm{~V}$, the $R_{\text {PWM }}$ must be smaller than $86.67 \mathrm{k} \Omega$.
$\mathrm{R}_{\mathrm{PWM}}<\frac{\mathrm{V}_{\mathrm{PWM}}-2 \mathrm{~V}}{15 \mu \mathrm{~A}}$
Where $\mathrm{V}_{\mathrm{PWM}}$ is the high level of PWM dimming signal.

## Series Resistor Selection On EN Pin

The calculation of series resistor should consider the Input high threshold $\left(\mathrm{V}_{\mathbb{H}}\right)$ and the internal pull-low current ( $\left.\mathrm{I}_{\mathrm{H}_{-}} \mathrm{EN}\right)$ of $E N$. The minimum value of $V_{I H}$ is 2 V , and the maximum of $\mathrm{I}_{\mathrm{H}_{-} \mathrm{EN}}$ is $10 \mu \mathrm{~A}$. The resistor could be calculated by the equation below. $\mathrm{Ex} . \mathrm{V}_{\mathrm{EN}}=3.3 \mathrm{~V}$, the $\mathrm{R}_{\mathrm{EN}}$ must be smaller than $130 \mathrm{k} \Omega$.
$R_{E N}<\frac{V_{E N}-2 V}{10 \mu A}$
Where $\mathrm{V}_{\mathrm{EN}}$ is the high level of EN signal.

## Inductor Selection

The value of the inductance, $L$, can be approximated by the following equation, where the transition is from Discontinuous Conduction Mode (DCM) to Continuous Conduction Mode (CCM) :
$\mathrm{L}=\frac{\mathrm{D} \times(1-\mathrm{D})^{2} \times \mathrm{V}_{\text {OUT }}}{2 \times \mathrm{f}_{\text {OSC }} \times l_{\text {OUT }}}$
The duty cycle, D, can be calculated as the following equation:
$D=\frac{V_{\text {OUT }}-V_{\text {IN }}}{V_{\text {OUT }}}$
where $\mathrm{V}_{\text {OUt }}$ is the maximum output voltage, $\mathrm{V}_{\text {IN }}$ is the minimum input voltage, fosc is the operating frequency, and Iout is the sum of current from all LED strings. The Boost converter operates in DCM over the entire input voltage range when the inductor value is less than this value, L . With an inductance greater than L , the converter operates in CCM at the minimum input voltage and may be discontinuous at higher voltages.

The inductor must be selected with a saturated current rating that is greater than the peak current and the peak current must be below the Current Limit Threshold (3.3A typ) as provided by the following equation:
$\mathrm{I}_{\text {PEAK }}=\frac{\mathrm{V}_{\text {OUT }} \times \mathrm{I}_{\text {OUT }}}{\eta \times \mathrm{V}_{\text {IN }}}+\frac{\mathrm{V}_{\text {IN }} \times \mathrm{D} \times \mathrm{T}_{\text {OSC }}}{2 \times \mathrm{L}}$
where $\eta$ is the efficiency of the power converter.
Moreover, the slope of inductor current also be considered as the following question.
$L>\frac{V_{\text {OUT }}-V_{I N}}{1.68 \times 10^{6}}$
Please pay attention for it, the inductance minimum value does not smaller than the criteria.

## Diode Selection

Schottky diodes are recommended for most applications because of their fast recovery time and low forward voltage. Power dissipation, reverse voltage rating, and pulsating peak current are important parameters for consideration when making a Schottky diode selection. Make sure that the diode's peak current rating exceeds I IPEAK and reverse voltage rating exceeds the maximum output voltage.

## Supply Voltage Capacitor Selection

The RT8549LV equips a built-in LDO linear regulator to provide the internal logic of IC power. The output of LDO is the pin out of VDC. The VDC pin is recommended to connect at least a $1 \mu \mathrm{~F} / 25 \mathrm{~V}$ bypass capacitor. The bypass capacitor should be X5R or X7R type to assure the bypass capacitance remains stable in over-voltage or overtemperature.

## Input Capacitor Selection

The ceramic capacitors are recommended for input capacitor applications. Low ESR will effectively reduce the input voltage ripple caused by switching operation. Two $10 \mu \mathrm{~F} / 25 \mathrm{~V}$ capacitors are sufficient for most applications. Nevertheless, this value can be decreased for lower output current requirement. Another consideration is the voltage rating of the input capacitor must be greater than the maximum input voltage.

## Output Capacitor Selection

Output ripple voltage is an important index for estimating the performance. This portion consists of two parts, one is the ESR voltage of output capacitor, another part is formed by charging and discharging process of output capacitor. Refer to Figure 3, evaluate $\Delta V_{\text {out1 }}$ by ideal energy equalization. According to the definition of $Q$, the $Q$ value can be calculated as the following equation :

$$
\begin{aligned}
\mathrm{Q}= & \frac{1}{2} \times\left[\left(\mathrm{I}_{\mathrm{IN}}+\frac{1}{2} \Delta \mathrm{I}_{\mathrm{L}}-\mathrm{l}_{\text {OUT }}\right)+\left(\mathrm{I}_{\mathrm{I}}-\frac{1}{2} \Delta \mathrm{I}_{\mathrm{L}}-\mathrm{I}_{\text {OUT }}\right)\right] \\
& \times \frac{\mathrm{V}_{\text {IN }}}{\mathrm{V}_{\text {OUT }}} \times \frac{1}{f_{\text {OSC }}}=\mathrm{C}_{\text {OUT }} \times \Delta \mathrm{V}_{\text {OUT } 1}
\end{aligned}
$$

where fosc is the switching frequency, and $\Delta \mathrm{I}_{\mathrm{L}}$ is the inductor ripple current. Move Cout to the left side to estimate the value of $\Delta \mathrm{V}_{\text {OUT1 }}$ as the following equation :

$$
\Delta \mathrm{V}_{\mathrm{OUT} 1}=\frac{\mathrm{D} \times \mathrm{I}_{\mathrm{OUT}}}{\eta \times \mathrm{C}_{\mathrm{OUT}} \times \mathrm{f}_{\mathrm{OSC}}}
$$

Then, take the ESR into consideration, the ESR voltage can be determined as the following equation :
$\Delta \mathrm{V}_{\mathrm{ESR}}=\left(\frac{\mathrm{l}_{\mathrm{OUT}}}{1-\mathrm{D}}+\frac{\mathrm{V}_{\mathrm{IN}} \times \mathrm{D} \times \mathrm{T}_{\mathrm{OSC}}}{2 \mathrm{~L}}\right) \times \mathrm{R}_{\mathrm{ESR}}$
Finally, the total output ripple $\Delta \mathrm{V}_{\text {OUT }}$ is combined from the $\Delta \mathrm{V}_{\text {OUT1 }}$ and $\Delta \mathrm{V}_{\text {ESR }}$. In the general application, the output capacitor is recommended to use a $47 \mu \mathrm{~F} / 63 \mathrm{~V}$ electrolytic capacitor.


Figure 3. The Output Ripple Voltage Without the Contribution of ESR

## Thermal Considerations

For continuous operation, do not exceed absolute maximum junction temperature. The maximum power dissipation depends on the thermal resistance of the IC package, PCB layout, rate of surrounding airflow, and difference between junction and ambient temperature. The maximum power dissipation can be calculated by the following formula:
$P_{D(M A X)}=\left(T_{J(M A X)}-T_{A}\right) / \theta_{J A}$
where $T_{J(M A X)}$ is the maximum junction temperature, $T_{A}$ is the ambient temperature, and $\theta_{\mathrm{JA}}$ is the junction to ambient thermal resistance.

For recommended operating condition specifications, the maximum junction temperature is $125^{\circ} \mathrm{C}$. The junction to ambient thermal resistance, $\theta_{\mathrm{JA}}$, is layout dependent. For WDFN-16L $5 \times 5$ package, the thermal resistance, $\theta_{\mathrm{JA}}$, is $28.8^{\circ} \mathrm{C} / \mathrm{W}$ on a standard JEDEC 51-7 four-layer thermal test board. The maximum power dissipation at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ can be calculated by the following formula :
$P_{D(\text { max })}=\left(125^{\circ} \mathrm{C}-25^{\circ} \mathrm{C}\right) /\left(28.8^{\circ} \mathrm{C} / \mathrm{W}\right)=3.47 \mathrm{~W}$ for WDFN-16L $5 \times 5$ package

The maximum power dissipation depends on the operating ambient temperature for fixed $\mathrm{T}_{\mathrm{J} \text { (MAX) }}$ and thermal resistance, $\theta_{\mathrm{JA}}$. The derating curve in Figure 5 allows the designer to see the effect of rising ambient temperature on the maximum power dissipation.


Figure 5. Derating Curve of Maximum Power Dissipation

## Layout Consideration

PCB layout is very important for designing switching power converter circuits. The following layout guides should be strictly followed for best performance of the RT8549LV.

- The power components, L1, D1, $\mathrm{C}_{\mathrm{IN} 1}$ and Cout must be placed as close as possible to reduce power loop. The PCB trace between power components must be as short and wide as possible.
- Place L1 and D1 as close as possible to LX pin. The trace should be as short and wide as possible. Keep the LX node away from the COMP, VDC, SMBDAT and SMBCLK ground.
- The compensation circuit (Rcomp, CсомP) should be kept away from the power loops and should be shielded with a ground trace to prevent any noise coupling. Place the compensation components as close as possible to the COMP pin.
- The exposed pad of the chip should be connected to a large ground plane for thermal consideration.


Figure 6. PCB Layout Guide

## Outline Dimension



Note : The configuration of the Pin \#1 identifier is optional, but must be located within the zone indicated.

| Symbol | Dimensions In Millimeters |  | Dimensions In Inches |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Max. | Min. | Max. |  |  |  |
| A | 0.700 | 0.800 | 0.028 | 0.031 |  |  |  |
| A1 | 0.000 | 0.050 | 0.000 | 0.002 |  |  |  |
| A3 | 0.175 | 0.250 | 0.007 | 0.010 |  |  |  |
| b | 0.200 | 0.300 | 0.008 | 0.012 |  |  |  |
| D | 4.900 | 5.100 | 0.193 | 0.201 |  |  |  |
| D2 | 4.350 | 4.450 | 0.171 | 0.175 |  |  |  |
| E | 4.900 | 5.100 | 0.193 | 0.201 |  |  |  |
| E2 | 3.650 | 3.750 | 0.144 | 0.148 |  |  |  |
| e | 0.500 |  |  |  |  |  | 0.020 |
| L | 0.350 | 0.450 | 0.014 | 0.018 |  |  |  |

W-Type 16L DFN 5x5 Package

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| Version | Date | Item | Description |
| :---: | :---: | :---: | :---: |
| P00_LNO | $2013 / 12 / 24$ |  | First Edition |

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