# Max. 28.5V Output 2Strings(25mA/ch) $\underset{\text { Free }}{\mathrm{Pb}}$ White LED Driver 

## BD65B60GWL

## OGeneral Description

BD65B60 is a white LED driver IC that integrates PWM step-up DC/DC converter with boost-capability of up to maximum 28.5 V and current driver with drive capability of up to 25 mA (Typ.) maximum setting. Precise brightness can be controlled at wide ranges through the external PWM pulse input.
This IC features highly accurate current drivers with low differential current errors between channels, thus, reducing brightness spots on the LCD panel. Moreover, its small package is suited for saving space.

## -Features

- High efficiency PWM step-up DC/DC converter $\mathrm{f}_{\mathrm{sw} 1}=1.1 \mathrm{MHz}($ Typ. $), \mathrm{f}_{\mathrm{sw} 2}=0.60 \mathrm{MHz}($ Typ. $)$
- High accuracy \& good matching current drivers (2ch)
- Soft Start function
- Drives up to 8 LEDs in series per channel

■ Lower input voltage range requirement (2.7V to 5.5 V )

## - Applications

Backlight for smartphones, games, digital video cameras, digital single-lens reflexes, digital still cameras, digital photo frames, Portable DVD player, etc.

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OKey Specifications
    ■ Input voltage range:
    2.7V to 5.5V
    ■ Output voltage range:
    Max. 28.5V
    ■ Operational LED Channel:
    ■ Switching frequency:
    | LED Current per Channel:
            0.6MHz/1.1MHz(Typ.)
            25mA (Max.)
    - LED current accuracy:
    \pm3.0% (Max.)
    - Quiescent current
                            0\muA (Typ.)
    ■ Operating temperature range:
-40 % to +85 ' C
```



OPin Configuration (Bottom View)

## -Typical Application Circuit

| D | SW | VOUT | LED2 |
| :---: | :---: | :---: | :---: |
| C | GND | RESET | LED1 |
| B | VBAT | PWM | SCL |
|  | ISET | VIO | SDA |
|  |  |  |  |

$\begin{array}{lll}1 & 2 & 3\end{array}$

## -Pin Descriptions

| $\begin{aligned} & \text { PIN } \\ & \text { No. } \end{aligned}$ | PIN <br> Name | I/O | Function | Terminal diagram |
| :---: | :---: | :---: | :---: | :---: |
| A1 | ISET | In | Resistor Connection for LED Current setting | A |
| A2 | VIO | In | VIO voltage Terminal. Connect a 1.65 V to 3.3 V supply to VIO and bypass to GND with a $0.1 \mu \mathrm{~F}$ or greater ceramic capacitor. | B |
| A3 | SDA | In | Serial Data input for $I^{2} C$ Interface This pin is needed to connect external pull-up resistor to VIO pin. <br> Please refer to P. 37 "SDA, SCL Pull-up Resistor Selection." | B |
| B1 | VBAT | In | VBAT voltage Terminal. Connect a 2.7 V to 5.5 V supply to VBAT and bypass to GND with a $1.0 \mu \mathrm{~F}$ (Typ.) or greater ceramic capacitor. | C |
| B2 | PWM | In | Input pin for controlling the current driver. This pin has an internal pull-down resistor. Please refer to P. 35 "Brightness Control" | B |
| B3 | SCL | In | Serial Clock input for $I^{2} C$ Interface <br> This pin is needed to connect external pull-up resistor to VIO pin. <br> Please refer to P. 37 "SDA, SCL Pull-up Resistor Selection". | B |
| C1 | GND | - | Power Ground for internal switching transistor | C |
| C2 | RESET | In | Active-low reset. Pull this pin high to enable the IC. This pin is needed to connect external pull-down resistor. <br> Please refer to P. 29 "Functional Descriptions" | B |
| C3 | LED1 | In | Input terminal to Internal Current Driver. LED cathode connection. | B |
| D1 | SW | Out | Switching terminal where an external inductor is connected. Internally connects to an NMOS switch. Connect the inductor as close as possible to SW terminal to reduce parasitic inductance and capacitance. Please refer to PCB layout of P. 39 . | B |
| D2 | VOUT | In | Terminal for monitoring the output voltage of switching regulator. Also, detects SBD open and OVP. Please refer to P. 31 . <br> Connect VOUT to the positive terminal of the output capacitor (COUT). Recommended COUT value is $1.0 \mu \mathrm{~F}$ (Typ.) for DC mode or $2.2 \mu \mathrm{~F}$ (Typ.) for PWM mode. | B |
| D3 | LED2 | In | Input terminal to Internal Current Driver. LED cathode connection. | B |



A


B


C

## -Block Diagram



## -Description of Block

The lowest voltage between LED1 and LED2 pins is detected when IC is powered on. Output voltage is kept constant by controlling the switching duty through the feedback voltage which is set at 0.3 V (Typ.). The PWM Current Mode DC/DC Converter is controlled by the two inputs of the comparator: one is the differential output from the error amplifier and the other is the sum of current sensing and the ramp signal generated by the oscillator. These combined signals prevent the sub-harmonic oscillation in PWM Current Mode. The PWM output controls internal switch N-channel Transistor via the RS latch. Energy is accumulated in the external inductor when the gate of the N-channel transistor is "ON", while energy is transferred to the output capacitor via external SBD when the N -channel transistor is "OFF".

LED brightness is controlled by the current driver which can be set by: external resistor RSET, 8-bit DAC current ratio and PWM control that is selectable as DC or pulse input.

Furthermore, this IC has several protection functions such as thermal shutdown, over-current protection, under-voltage lockout, over-voltage protection, external SBD open detection, LED open and short detection. Their respective detection signals stop the switching operation instantly.

## - Absolute Maximum Ratings ( $\mathrm{Ta}=+25^{\circ} \mathrm{C}$ )

| Parameter | Symbol | Limits | Unit | Condition |
| :---: | :---: | :---: | :---: | :---: |
| Maximum Applied Voltage 1 | $V_{\text {Max }}$ | 7 | V | $\begin{aligned} & \text { VBAT, VIO, PWM, SDA, SCL, } \\ & \text { RESET, ISET } \end{aligned}$ |
| Maximum Applied Voltage 2 | $V_{\text {max }}$ | 34 | V | SW, LED1,LED2, VOUT |
| Power Dissipation | Pd1 | 650 | mW | Power dissipation derates by $5.2 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ when operating above $25^{\circ} \mathrm{C}$ (When mounted on ROHM's standard board) <br> Power dissipation is calculated by formula : <br> $\mathrm{Pd}=($ Storage temperature max $\left.25^{\circ} \mathrm{C}\right) / \theta_{\mathrm{JA}}$ <br> (ex. Pd1 $=5.2 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ ) |
| Operating Temperature Range | Topr | -40 to +85 | ${ }^{\circ} \mathrm{C}$ | - |
| Storage Temperature Range | Tstg | -55 to +150 | ${ }^{\circ} \mathrm{C}$ | - |

## -Recommended Operating Ratings $\left(\mathrm{Ta}=+25^{\circ} \mathrm{C}\right)$

| Parameter |  | Symbol | Limits |  |  | Unit |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |

-Electrical Characteristics (Unless otherwise specified, VBAT $=3.6 \mathrm{~V}, \mathrm{VIO}=3.0 \mathrm{~V}, \mathrm{Ta}=+25^{\circ} \mathrm{C}$ )

| Parameter | Symbol | Limits |  |  | Unit | Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Typ. | Max. |  |  |
| [General] |  |  |  |  |  |  |
| Quiescent Current (VBAT) | $\mathrm{l}_{\text {QVBat }}$ | - | - | 1.0 | $\mu \mathrm{A}$ | RESET=0V |
| Quiescent Current (VIO) | levio | - | - | 1.0 | $\mu \mathrm{A}$ | RESET=0V |
| Standby Current (VBAT) | $\mathrm{I}_{\text {STB }}$ | - | 2.0 | 4.0 | $\mu \mathrm{A}$ | RESET=1.8V, ad0Eh, data=00h |
| Current Consumption (VBAT) for Current Driver 1ch | Ibat1ch | - | 0.80 | - | mA | RESET $=1.8 \mathrm{~V}$, VOUT=open Fsw=1.1MHz, ad03h, data=01h <No switching> |
| Current Consumption (VBAT) for Current Driver 2ch | Ibat2ch | - | 0.85 | - | mA | RESET=1.8V, VOUT=open Fsw=1.1MHz, ad03h, data $=05 \mathrm{~h}$ <No switching> |
| Current Consumption (VIO) | IdDVio | - | - | 100 | $\mu \mathrm{A}$ | $\begin{aligned} & \text { RESET=1.8V, VOUT=open } \\ & \text { SDA=SCL=50\%@400kHz (3.0V) } \end{aligned}$ |
| [RESET, PWM Terminal] |  |  |  |  |  |  |
| Low Level Input Voltage | $\mathrm{V}_{\text {THL }}$ | - | - | 0.5 | V |  |
| High Level Input Voltage | $V_{\text {THH }}$ | 1.4 | - | - | V |  |
| RESET Input Current | IRSTin | - | - | 1 | $\mu \mathrm{A}$ |  |
| RESET Output Current | $\mathrm{I}_{\text {RSTout }}$ | -1 | - | - | $\mu \mathrm{A}$ |  |
| PWM Pull down Resistor | $\mathrm{R}_{\text {PWM }}$ | - | 300 | - | $\mathrm{k} \Omega$ |  |
| [SDA, SCL Terminal] |  |  |  |  |  |  |
| Low Level Input Voltage | $\mathrm{V}_{\text {ILI }}$ | -0.3 | - | $0.25 \times \mathrm{VIO}$ | V |  |
| High Level Input Voltage | $\mathrm{V}_{\mathrm{IHI}}$ | 0.75 xVIO | - | VIO+0.3 | V |  |
| L level Output Voltage (for SDA pin) | Vol | - | - | 0.3 | V | $1 \mathrm{OL}=3 \mathrm{~mA}$ |
| Input Current | $I_{\text {Sin }}$ | -3 | - | 3 | $\mu \mathrm{A}$ | ```Input voltage = from (0.1 x VIO) to (0.9 x VIO)``` |

-Electrical Characteristics (Unless otherwise specified, VBAT $=3.6 \mathrm{~V}, \mathrm{VIO}=3.0 \mathrm{~V}, \mathrm{Ta}=+25^{\circ} \mathrm{C}$ )

| Parameter | Symbol | Limits |  |  | Unit | Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Typ. | Max. |  |  |
| [Switching Regulator] |  |  |  |  |  |  |
| LED Control Voltage1 | $\mathrm{V}_{\text {Led1 }}$ | 0.40 | 0.50 | 0.60 | V | ad02h,data=00h |
| LED Control Voltage2 | $\mathrm{V}_{\text {Led2 }}$ | - | 0.40 | - | V | ad02h,data=01h |
| LED Control Voltage3 | $\mathrm{V}_{\text {LED }}$ | - | 0.30 | - | V | ad02h, data=02h |
| LED Control Voltage4 | $V_{\text {LED4 }}$ | - | 0.20 | - | V | ad02h,data=03h |
| Switching Frequency Accuracy | $\mathrm{F}_{\text {Sw }}$ | 0.88 | 1.10 | 1.32 | MHz | FOSC(ad02h D2)=1 |
| Duty Cycle Limit | $\mathrm{D}_{\text {MAX }}$ | 90.0 | 95.0 | 99.0 | \% | LED1-2=0.3V, Fsw=1.1MHz |
| SW Nch FET RON | Ron | - | 0.3 | - | $\Omega$ | ISW=80mA, VBAT $=3.6 \mathrm{~V}$ |
| SW Transistor Leak Current | lesw | - | 0.1 | 2.0 | $\mu \mathrm{A}$ | RESET =0V, SW=18V |
| VOUT Range | $V_{\text {RANGE }}$ | VBAT +1 V | - | OVP-1V | V | Under OVP voltage |
| [Protection] |  |  |  |  |  |  |
| Under Voltage Lock Out (fall) | Vuvlo | - | 2.1 | - | V | VBAT falling edge |
| Under Voltage Lock Out (rise) | $\mathrm{V}_{\text {UVLOH }}$ | - | 2.3 | - | V | VBAT rising edge |
| Over Current Limit 1 | locp1 | - | 1000 | - | mA | VBAT=2.7V, ad01h, data=01h *1 |
| Over Current Limit 2 | locp2 | - | 1700 | - | mA | VBAT=2.7V, ad01h,data=00h *1 |
| Over Voltage Limit Input1 | Vovp1 | 29.5 | 31 | 33 | V | VOUT rising edge, ad01h, data=10h |
| Over Voltage Limit Input2 | Vovp2 | 27 | 28 | 29.5 | V | VOUT rising edge, ad01h, data=01h |
| Over Voltage Limit Input3 | Vovp3 | 22.5 | 23.5 | 24.7 | V | VOUT rising edge, ad01h,data=00h or 11h |
| Over Voltage Limit Hysteresis | Vovphys | - | 1 | - | V |  |
| Output Short Protect | $V_{\text {OvPfault }}$ | - | 0.2 | 0.5 | V | Detect voltage of VOUT pin |
| VOUT Leak Current | love | - | 0.1 | 1.0 | $\mu \mathrm{A}$ | $\begin{aligned} & \text { RESET=0V, } \\ & \text { VOUT=18V }(\mathrm{OVP}=31 \mathrm{~V}) \end{aligned}$ |
| LED Terminal Over Voltage Protect | Vsc | 4.5 | 5.4 | 6.3 | V |  |
| [Current driver] |  |  |  |  |  |  |
| LED Maximum Current Setting Range | Ilmax | 5.0 | - | 25.0 | mA | This value is characteristics of current driver. |
| LED current Step | ILEDSTP | - | 256 | - | step | LED1, 2 |
| LED Current Accuracy 1 | laccui | - | - | $\pm 3.0$ | \% | IMAX $=15.0 \mathrm{~mA}$ |
| LED Current DAC Linearity 1 (Design target ) | Idalin1 | - | - | $\pm 2.0$ | \% | range $=10.02 \mathrm{~mA}$ to 15 mA RSET resistor $=15.0 \mathrm{~mA}$ setting *2 DAC register : <br> ad05h, data=AAh to FFh |
| LED Current DAC Linearity 2 (Design target) | Idalin2 | - | - | $\pm 3.0$ | \% | range $=5.04 \mathrm{~mA}$ to 9.96 mA RSET resistor $=15.0 \mathrm{~mA}$ setting *2 DAC register : <br> ad05h, data=55h to A9h |
| LED Current Matching | Ilmat | - | - | 2.0 | \% | (Max LED current - average current) / average current |
| LED Current Limit | ILOCP | - | 0 | 0.1 | mA | Current Limit Value at ISET Resistor $1 \mathrm{k} \Omega$ Setting |
| LED Leak Current | $\mathrm{l}_{\text {QLed }}$ | - | 0.1 | 1.0 | $\mu \mathrm{A}$ | RESET=0V, LED1\&LED2=18V |

[^0]
## OEvaluation Data

Evaluation data is measured using below parts and condition. (Unless otherwise specified)
Coil : 1277AS-H-4R7M
SBD : RB160VA-40
$\mathrm{VIO}=3.0 \mathrm{~V}$
$\mathrm{PWM}=0 \mathrm{~V}(\mathrm{GND})$


Figure 1. Quiescent Current (VBAT) vs Temperature


Figure 3. Standby Current (VBAT) vs Temperature


Figure 2. Quiescent Current (VIO) vs Temperature


Figure 4. Current Consumption (VBAT) 1CH vs Temperature <No switching>

## -Evaluation Data -continued

Evaluation data is measured using below parts and condition. (Unless otherwise specified)

> Coil : 1277AS-H-4R7M

SBD : RB160VA-40
$\mathrm{VIO}=3.0 \mathrm{~V}$
RESET=2.5V PWM=0V(GND)


Figure 5. Current Consumption (VBAT) 2CH vs Temperature <No switching>


Figure 7. Reset Threshold Voltage vs Temperature


Figure 6. Current Consumption (VIO) vs Temperature


Figure 8. PWM Threshold Voltage vs Temperature

## -Evaluation Data -continued

Evaluation data is measured using below parts and condition. (Unless otherwise specified)

> Coil : 1277AS-H-4R7M

SBD : RB160VA-40
$\mathrm{VIO}=3.0 \mathrm{~V}$
RESET=2.5V PWM=0V(GND)


Figure 9. Reset Input and Output Current vs Reset Voltage


Figure 11. SDA Threshold Voltage vs Temperature


Figure 10. PWM Pull-Down Resistance vs PWM Voltage


Figure 12. SCL Threshold Voltage vs Temperature

## -Evaluation Data -continued

Evaluation data is measured using below parts and condition. (Unless otherwise specified)
Coil : 1277AS-H-4R7M
SBD : RB160VA-40
$\mathrm{VIO}=3.0 \mathrm{~V}$
RESET=2.5V
PWM=OV(GND)


Figure 13. SDA "L" Level Output Voltage vs Temperature


Figure 15. SCL Input Current vs SCL Voltage


Figure 14. SDA Input Current vs SDA Voltage


Figure 16. LED Control Voltage 1 vs Temperature (Feedback voltage $=0.5 \mathrm{~V}$ setting)

## -Evaluation Data -continued

Evaluation data is measured using below parts and condition. (Unless otherwise specified)
Coil : 1277AS-H-4R7M
SBD : RB160VA-40
$\mathrm{VIO}=3.0 \mathrm{~V}$
RESET=2.5V
PWM=OV(GND)


Figure 17. LED Control Voltage 2 vs Temperature (Feedback voltage $=0.4 \mathrm{~V}$ setting)


Figure 19. LED Control Voltage 4 vs Temperature (Feedback voltage $=0.2 \mathrm{~V}$ setting)


Figure 18. LED Control Voltage 3 vs Temperature (Feedback voltage $=0.3 \mathrm{~V}$ setting)


Figure 20. Switching Frequency ( 1.1 MHz ) vs Temperature

## -Evaluation Data -continued

Evaluation data is measured using below parts and condition. (Unless otherwise specified)
Coil : 1277AS-H-4R7M
SBD : RB160VA-40
$\mathrm{VIO}=3.0 \mathrm{~V}$
RESET=2.5V
PWM=OV(GND)


Figure 21. Switching Frequency ( 0.6 MHz ) vs Temperature


Figure 23. Minimum Duty Cycle Limit vs Temperature


Figure 22. Maximum Duty Cycle Limit vs Temperature


Figure 24. SW Nch FET RON (at $I_{s w}=80 \mathrm{~mA}$ ) vs Temperature

## -Evaluation Data -continued

Evaluation data is measured using below parts and condition. (Unless otherwise specified)
Coil : 1277AS-H-4R7M
SBD : RB160VA-40
$\mathrm{VIO}=3.0 \mathrm{~V}$
RESET=2.5V
PWM=OV(GND)


Figure 25. SW Leak Current vs Temperature


Figure 27. Current Limit (1A) vs Temperature


Figure 26. Under Voltage Lock Out (Rise/Fall)


Figure 28. Current Limit (1.7A) vs Temperature

## -Evaluation Data -continued

Evaluation data is measured using below parts and condition. (Unless otherwise specified)
Coil : 1277AS-H-4R7M
SBD : RB160VA-40
$\mathrm{VIO}=3.0 \mathrm{~V}$
RESET=2.5V
PWM=OV(GND)


Figure 29. Over Voltage Protection 1 (23.5V) vs Temperature


Figure 31. Over Voltage Protection 3 (31V) vs Temperature


Figure 30. Over Voltage Protection 2 (28V) vs Temperature


Figure 32. Over Voltage Protection Hysteresis vs Temperature

## -Evaluation Data -continued

Evaluation data is measured using below parts and condition. (Unless otherwise specified)
Coil : 1277AS-H-4R7M
SBD : RB160VA-40
$\mathrm{VIO}=3.0 \mathrm{~V}$
RESET=2.5V
PWM=OV(GND)


Figure 33. Output Short Protect


Figure 35. LED Terminal Over Voltage Protect vs Temperature


Figure 34. VOUT Leak Current vs Temperature


Figure 36. LED1, LED2 Leak Current vs Temperature

## -Evaluation Data -continued

Evaluation data is measured using below parts and condition. (Unless otherwise specified)

> Coil : 1277AS-H-4R7M

SBD : RB160VA-40
VBAT $=3.6 \mathrm{~V}$
$\mathrm{VIO}=3.0 \mathrm{~V}$ RESET $=2.5 \mathrm{~V}$


Figure 37. LED Current vs PWM Duty (PWM output mode)


Figure 39. LED Current vs PWM Duty (DC output mode)


Figure 38. LED Current Matching vs PWM Duty (PWM output mode)


Figure 40. LED Current Matching vs PWM Duty (DC output mode)

## -Evaluation Data -continued

Evaluation data is measured using below parts and condition. (Unless otherwise specified)

> Coil : 1277AS-H-4R7M
> SBD : RB160VA-40
$\mathrm{VIO}=3.0 \mathrm{~V}$
RESET=2.5V PWM=0V(GND)


Figure 41. DNL vs LED Current Ratio


Figure 43. LED Current Matching vs LED Current Ratio

## -Evaluation Data -continued

Evaluation data is measured using below parts and conditon. (Unless otherwise specified)

> Coil : 1277AS-H-4R7M
> SBD : RB160VA-40
$\mathrm{VIO}=3.0 \mathrm{~V}$
RESET=2.5V PWM=0V(GND)


Figure 44. LED Current Limit vs ISET Current


Figure 45. LED Current vs LED Voltage


Figure 46. ISET Voltage vs Temperature

## -Evaluation Data -continued

LED current is measured using below parts. (Unless otherwise specified)
Coil : 1277AS-H-4R7M
SBD : RB160VA-40
$\mathrm{VIO}=1.8 \mathrm{~V}$
RESET=2.5V PWM=0V(GND)


Figure 47. LED Current 5mA (RSET=120k $\Omega$ ) vs Temperature


Figure 49. LED Current 15mA (RSET=39k $\Omega$ ) vs Temperature


Figure 48. LED Current 10mA (RSET=62k $\Omega$ ) vs Temperature


Figure 50. LED Current Matching 15mA (RSET=39k $\Omega$ ) vs Temperature

## - Typical Performance Curves

Conditions:
VBAT $=3.6 \mathrm{~V}, \mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{Fsw}=0.6 \mathrm{MHz}$, LED 6series $\times 1$ string and 2strings
(1) $\mathrm{FB}=0.3 \mathrm{~V}$ setting

Efficiency is calculated using the following equation:
Efficiency $=($ VOUT $\times$ LED current $) /($ VBAT $\times$ Input current $)$
LED current is calculated using the following equation:
LED current $=$ max current $\times$ ratio $\times P W M$ duty
Where:
max current is 12 mA set by RSET, which is the resistor connected to ISET terminal. ratio is controlled by register (ad05h D[7:0])
PWM duty is equal to $100 \%$
6series 1string Efficiency ( $\mathrm{FB}=0.3 \mathrm{~V}$ )

(2) $\mathrm{FB}=0.5 \mathrm{~V}$ setting

Efficiency is calculated using the following equation:
Efficiency $=($ VOUT $\times($ LED1 + LED2 current $)$ ) $/($ VBAT $\times$ Input current $)$
LED current is calculated using the following equation:
LED current $=$ max current $\times$ ratio $\times$ PWM duty
Where:
max current is 25 mA set by RSET, which is the resistor connected to ISET terminal. ratio is controlled by register (ad05h D[7:0])
PWM duty is equal to100\%
6series 2strings Efficiency ( $\mathrm{FB}=0.5 \mathrm{~V}$ )



## -Control Signal Input Timing

Timing sequence (VBAT, VIO, RESET, $I^{2} \mathrm{C}$ (SDA, SCL)) VBAT voltage > VIO voltage


Figure 51. Timing Diagram

Table 1. Input Timing

| Symbol | Name | Unit | Min. | Typ. | Max. |
| :---: | :--- | :---: | :---: | :---: | :---: |
| t 1 | Power Supply(IC) - Power supply (IO) time | $\mu \mathrm{s}$ | 100 | - | - |
| t 2 | Power Supply(IO) - RESET wait time | $\mu \mathrm{s}$ | 0 | - | - |
| t 3 | RESET - ${ }^{2} \mathrm{C}$ wait time | $\mu \mathrm{s}$ | 100 | - | - |
| t4 | RESET low width | $\mu \mathrm{s}$ | 50 | - | - |
| t5 | RESET - Power Supply(IO) time | $\mu \mathrm{s}$ | 0 | - | - |
| t6 | Power Supply(IO) - Power Supply(IC) | $\mu \mathrm{s}$ | 0 | - | - |

## -Serial Interface

It can interface with $I^{2} C$ BUS format compatible.
(1) Slave address

| A7 | A6 | A5 | A4 | A3 | A2 | A1 | R/W |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 0 | 0 | 1 | 0 | 0 | $1 / 0$ |

Figure 52. Slave Address
(2) Bit Transfer

SCL transfers 1-bit data during each clock pulse and data is sampled at " H " state. SDA cannot be changed at the time of bit transfer. Any changes on the SDA while SCL is in H state, a START condition or a STOP condition will occur and it will be interpreted as a control signal.


Figure 53. Bit transfer ( $l^{2} \mathrm{C}$ format)
(3) START and STOP condition

When SDA changes state while SCL is H , data is not transferred on the $I^{2} \mathrm{C}$ bus. Two conditions might occur if this happens. If SDA changes from H to L while $\operatorname{SCL}$ is H , it will become START $(\mathrm{S})$ condition which signals the beginning of a new command. If SDA changes from $L$ to $H$ while $S C L$ is $H$, it will become STOP ( $P$ ) condition which signals the end of the previous command.


Figure 54. START/STOP condition ( $\mathrm{I}^{2} \mathrm{C}$ format)

## (4) Acknowledge

Transfer of 8 -bit data occurs after each START condition. After eight bits had been sent, the transmitter opens SDA while the receiver returns the acknowledge signal by setting SDA to L .
Acknowledge is returned between address 00h and 0Eh.


Figure 55. Acknowledge ( ${ }^{2} \mathrm{C}$ format)
(5) Write protocol

A register address is transferred by the next 1 byte that transferred the slave address and the write-in command. The 3rd byte writes data in the internal register written in by the 2nd byte, and after the 4th byte or, the increment of register address is carried out automatically. However, when a register address turns into the last address 0Eh, it is set to 00h by the next transmission. After the transmission ends, the increment of the address is carried out.


Figure 56. Writing protocol
(6) Read protocol

It reads from the next byte after writing a slave address and R/W bit. The register to read is consider as the following address accessed at the end, and the data of the address that carried out the increment is read after it. If an address turns into the last address OEh, the next byte will read out 00h. After the transmission end, the increment of the address is carried out.


Figure 57. Reading protocol
(7) Multiple Read protocol

After specifying an internal address, it reads by repeated START condition and changing the data transfer direction. The data of the address that carried out the increment is read after it. If an address turns into the last address OEh, the next byte will read out 00 h . After the transmission end, the increment of the address is carried out.


Figure 58. Multiple reading protocols
As for read protocol and multiple read protocol, please do $\bar{A}$ (not acknowledge) after doing the final reading operation. It stops with read when ending by A(acknowledge), and SDA stops in the state of Low when the reading data of that time is 0 . However, this state returns usually when SCL is moved, data is read, and $\bar{A}($ not acknowledge) is done.
(8) Timing diagram


Figure 59. Timing Diagram ( $\mathrm{I}^{2} \mathrm{C}$ format)
(9) Electrical Characteristics (Unless otherwise specified, $\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{VBAT}=3.6 \mathrm{~V}, \mathrm{VIO}=1.8 \mathrm{~V}$ )

Table 2. Electrical Characteristics

| Parameter | Symbol | Standard-mode |  |  | Fast-mode |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Typ. | Max. | Min. | Typ. | Max. |  |
| 【 $1^{2} \mathrm{C}$ BUS format】 |  |  |  |  |  |  |  |  |
| SCL clock frequency | fscl | 0 | - | 100 | 0 | - | 400 | kHz |
| LOW period of the SCL clock | tlow | 4.7 | - | - | 1.3 | - | - | $\mu \mathrm{s}$ |
| HIGH period of the SCL clock | thigh | 4.0 | - | - | 0.6 | - | - | $\mu \mathrm{s}$ |
| Hold time (repeated) START condition After this period, the first clock is generated | thD; STA | 4.0 | - | - | 0.6 | - | - | $\mu \mathrm{S}$ |
| Set-up time for a repeated START condition | tSU;STA | 4.7 | - | - | 0.6 | - | - | $\mu \mathrm{s}$ |
| Data hold time | tHD;DAT | 0 | - | 3.45 | 0 | - | 0.9 | $\mu \mathrm{s}$ |
| Data set-up time | tSU;DAT | 250 | - | - | 100 | - | - | ns |
| Set-up time for STOP condition | tsu;STO | 4.0 | - | - | 0.6 | - | - | $\mu \mathrm{S}$ |
| Bus free time between a STOP and START condition | tBUF | 4.7 | - | - | 1.3 | - | - | $\mu \mathrm{S}$ |

## - Register List

Table 3. Register List

| Add ress | R/W | Initial | Register Data |  |  |  |  |  |  |  | Function |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 |  |
| 00h | W | 00h | - | - | - | - | - | - | - | SFRST | Software <br> Reset |
| 01h | R/W | 01h | - | - | - | OVP(1) | OVP(0) | - | - | ROCP | Common <br> Setting1 |
| 02h | R/W | 02h | SKIPEN <br> (1) | SKIPEN <br> (0) | SWSRT <br> (1) | SWSRT <br> (0) | - | FOSC | FB(1) | FB(0) | Common <br> Setting2 |
| 03h | R/W | 05h | - | - | - | - | - | $\begin{aligned} & \text { LED2 } \\ & \text { SEL } \end{aligned}$ | - | $\begin{aligned} & \text { LED1 } \\ & \text { SEL } \end{aligned}$ | LED channel select |
| 04h | R/W | 00h | - | - | - | - | - | - | - | - | dummy1 |
| 05h | R/W | FFh | ILED(7) | ILED(6) | ILED(5) | ILED(4) | ILED(3) | ILED(2) | ILED(1) | ILED(0) | Current ratio Setting |
| 06h | R/W | 00h | - | - | - | - | - | - | - | - | dummy2 |
| 07h | R/W | 06h | - | - | PWMEN | - | - | LPFEN | SHORT | - | Control Setting |
| 08h | R/W | 00h | - | - | - | - | - | SRCHG <br> (2) | SRCHG <br> (1) | SRCHG <br> (0) | Slew Rate changing Setting |
| 09h | R/W | 00h | - | - | - | - | - | - | - | - | dummy3 |
| OAh | R/W | 00h | - | - | - | - | - | - | - | - | dummy 4 |
| OBh | R/W | 00h | - | - | - | - | - | - | - | - | dummy5 |
| OCh | R/W | 00h | - | - | - | - | - | - | - | - | dummy6 |
| ODh | R/W | 00h | - | - | - | - | - | - | - | - | dummy 7 |
| OEh | R/W | 00h | - | - | - | - | - | - | - | PON | Enable Setting |

Input "0" for "-".
A free address has the possibility to assign it to the register for the test.
Access to the register for the test and the undefined register is prohibited.

## - Register Map

Address 00h < Software Reset >

| Address | R/W | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 00h | W | - | - | - | - | - | - | - | SFRST |
| Initial Value | 00h | - | - | - | - | - | - | - | 0 |


| D0: | SFTRST | Software Reset |
| :--- | :--- | :--- |
|  | $0:$ | Reset cancel |
|  | $1:$ | Reset (Initializes all registers) |

Address 01h < Common Setting1>
Address 01h < Common Setting1>

| Address | R/W | D7 | D6 | D5 | D4 | D3 | D2 | D1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 01h | R/W | - | - | - | OVP(1) | OVP(0) | - | - |
| Initial Value | 01h | 0 | 0 | 0 | 0 | 0 | 0 | 0 |


| $D[4: 3]$ : | OVP(1:0) | Over Voltage Protection Detect Voltage |
| :---: | :---: | :---: |
|  | 00b: | 23.5 V (Typ.) this setting is suitable for the (initial value) |
|  | 01b: | 28.0 V (Typ.) this setting is suitable for the |
|  | 10b: | 31.0 V (Typ.) this setting is suitable for the |
|  |  | Ratings |
|  | 11b: | 23.5 V (Typ.) this setting is suitable for the |
| DO: | ROCP | Over Current Protection Level Setting |
|  | 0 : | 1.7A (Typ.) |
|  | 1: | 1A (Typ.) (initial value) |

Address 02 h < Slew Rate, Fosc, Feedback voltage >

| Address | R/W | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 02h | R/W | SKIPEN <br> $(1)$ | SKIPEN <br> $(0)$ | SWSRT <br> $(1)$ | SWSRT <br> $(0)$ | - | FOSC | FB(1) | FB(0) |
| Initial Value | 02h | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |

D[7:6]:
SKIPEN(1:0)
00b:
01b:
10b:
11b:

Pulse skip Setting pulse skip all mode active (initial value) pulse skip mode1 disable (Minimum duty fix mode) pulse skip mode2 disable (pulse stop mode) pulse skip all mode disable

Pulse skip all mode is Min duty fix mode and pulse stop mode.
Pulse skip mode1 is Min duty fix mode.
Pulse skip mode2 is pulse stop mode.

| D[5:4]: | SWSRT(1:0) | Control the rise and fall time of slew rate for SW terminal |
| :---: | :---: | :---: |
|  | 00b: | $x 1$ (initial value) |
|  | 01b: | x0.8 (design concept) |
|  | 10b: | x0.6 (design concept) |
|  | 11b: | x0.4 (design concept) |
| D2: | FOSC | Switching Frequency Value Setting |
|  | 0 : | 0.6 MHz (initial value) |
|  | 1 : | 1.1 MHz |
| $\mathrm{D}[1: 0]$ : | FB(1:0) | Feedback voltage Setting |
|  | 00b: | 0.5 V |
|  | 01b: | 0.4 V |
|  | 10b: | 0.3 V (initial value) |
|  | 11b: | 0.2 V |

Address 03h < LED channel select >

| Address | R/W | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 03h | R/W | - | - | - | - | - | LED2 | - | LED1 |
| Initial Value | 05h | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |

D2: LED2SEL $0: \quad$ unused LED2 1: used LED2 (initial value)

D0: LED1SEL
0 :
1: unused LED1 used LED1 (initial value)

Selection of the current driver and the protection for LED1

When this address is selected to 00h, the selected current driver and protection turn off.
(Note:) Set this address before setting address 0Eh to 01h (Power on).
Once setting adOEh to 01h, this address (LED channel select) is non-functional.

|  | Setting | LED1 channel | LED2 channel | Comment |
| :---: | :---: | :---: | :---: | :---: |
| Reset | RESET terminal " H " to " L " Software Reset (adOOh data=01h) | $\bigcirc$ | $\bigcirc$ |  |
| $\begin{aligned} & \text { Initial } \\ & \text { LED1 = used } \\ & \text { LED2 = used } \end{aligned}$ | ad03h data=05h | $\bigcirc$ | $\bigcirc$ |  |
| $\begin{aligned} & \text { LED1 }=\text { used } \\ & \text { LED2 }=\text { unused } \end{aligned}$ | ad03h data=01h | $\bigcirc$ | $\times$ |  |
| Power on | ad0Eh data=01h | $\bigcirc$ | $\times$ |  |
| $\begin{aligned} & \text { LED1 }=\text { used } \\ & \text { LED2 }=\text { unused } \end{aligned}$ | ad03h data=04h | $\bigcirc$ | $\times$ | LED channel select is not changed |
| Power off | ad0Eh data=00h | $\bigcirc$ | $\times$ |  |
| $\begin{aligned} & \text { LED1 }=\text { unused } \\ & \text { LED2 }=\text { used } \end{aligned}$ | ad03h data=04h | $\times$ | $\bigcirc$ | LED channel select is changed. |
| Power on | ad0Eh data=01h | $\times$ | $\bigcirc$ |  |

O: select
$\times$ : unselect

Address 05h < LED Current Ratio Setting >

| Address | R/W | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 05h | R/W | ILED(7) | ILED(6) | ILED(5) | $\operatorname{ILED}(4)$ | $\operatorname{ILED}(3)$ | $\operatorname{ILED}(2)$ | $\operatorname{ILED}(1)$ | $\operatorname{ILED}(0)$ |
| Initial Value | FFh | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |

$D[7: 0]: \quad$ ILEDx(7:0) LED Current Setting
This address determines the ratio of the operating LED current with respect to the maximum LED current set by RSET. The ratio can be varied from $1 / 256$ to $256 / 256$.

| data 00h $\rightarrow$ | ratio $=(0+1) / 256=$ | 1/256 $=$ | 0.39\% |
| :---: | :---: | :---: | :---: |
| , | $(32+1) / 256$ | 33/256 | 12.89\% |
| ata C7h | (199+1)/256 | 200/256 = | 78.13\% |
| ata FFh $\rightarrow$ | ratio $=(255+1) / 256$ | 256/25 | 100 |
| $\begin{aligned} \text { LED current } & =\text { max current } \times \text { ratio } \times \text { PWM duty (from PWM terminal) } \\ & =\operatorname{IMAX} \times(\text { ILED }+1) / 256 \times \text { PWM duty } \end{aligned}$ |  |  |  |

Where:
IMAX is set by RSET, which is the resistor connected to ISET terminal (see LED Current Setting at P.34).

Address 07h <Control Setting>

| Address | R/W | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 07h | R/W | - | - | PWMEN | - | - | LPFEN | SHORT | - |
| Initial Value | 06h | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 |

D5:

PWMEN
0:
1 :

PWM Enable Control (Valid/Invalid) PWM input is invalid, " H " fixed (initial value)
PWM input is valid

PWMEN="1", LPFEN="0"


PWMEN="0", LPFEN="0"


Figure 60. PWMEN setting

D2:

## LPFEN

0 :
Low pass filter is used (initial value)
PWM dimming condition on PWMEN and LPFEN setting

| PWMEN | LPFEN | LED Current |
| :---: | :---: | :---: |
| 0 | 0 | DC ( 8bit DAC ) |
| 0 | 1 | DC ( 8bit DAC ) |
| 1 | 0 | PWM ( 8bit DAC and PWM duty ) |
| 1 | 1 | DC ( 8bit DAC and PWM duty $)$ |

D1: SHORT
LED Short Protection Setting Short Protection is Invalid
5.4V (Initial value)

Address 08h <Slew Rate Change Setting>

| Address | R/W | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 08h | R/W | - | - | - | - | - | SRCHG <br> $(2)$ | SRCHG <br> $(1)$ | SRCHG <br> $(0)$ |
| Initial Value | 00h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

$\mathrm{D}[2: 0]$ :

| SRCHG(2:0) | Sl |
| :--- | :--- |
| 000b: | Ke |
| 001b: | $R e$ |
| 010b: | $R e$ |
| 011b: | $R e$ |
| 100b: | $R e$ |
| 101b,110b,111b: | $R e$ |

Slew Rate Change Setting
Keep the slew rate selected at ad02h $D[5: 4]$ (initial value)
Repeat $\mathrm{x} 0.4 \rightarrow \mathrm{x} 0.6 \rightarrow \mathrm{x} 0.8 \rightarrow \mathrm{x} 1.0 \rightarrow \mathrm{x} 0.8 \rightarrow \mathrm{x} 0.6 \rightarrow \cdots$
Repeat $\mathrm{x} 0.4 \rightarrow \mathrm{x} 0.6 \rightarrow \mathrm{x} 0.8 \rightarrow \mathrm{x} 0.6 \rightarrow \cdots$
Repeat $x 0.4 \rightarrow x 0.6 \rightarrow \cdots$
Repeat $\times 0.8 \rightarrow x 1.0 \rightarrow \cdots$
Repeat $\mathrm{x} 0.6 \rightarrow \mathrm{x0} .8 \rightarrow \cdots$


SWCHG(2:0)=001b
sw


SWSRT |  | $\times 0.4$ | $\times 0.6$ | $\times 0.8$ | $\times 1.0$ | $\times 0.8$ | $\times 0.6$ | $\times 0.4$ | $\times 0.6$ | $\times 0.8$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |



SWCHG(2:0)=011b


SWCHG(2:0)=101b, 110b, 111b

| SWSRT | $\times 0.6$ | $\times 0.8$ | $\times 0.6$ | $\times 0.8$ | $\times 0.6$ | $\times 0.8$ | $\times 0.6$ | $\times 0.8$ | $\times 0.6$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

Address 0Eh <Enable Setting>

| Address | R/W | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0Eh | R/W | - | - | - | - | - | - | - | PON |
| Initial Value | 00h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |


| DO: | PON | Power control for all blocks |
| :--- | :--- | :--- |
|  | $0:$ | Power off (initial value) |
|  | $1:$ | Power on |

## -Functional Descriptions

## 1) Reset

There are two kinds of reset, software reset and hardware reset.

- Software reset

All the registers are initialized by SFTRST = " 1 ".
SFTRST is an automatically returned to "0". (Auto Return 0)

- Hardware reset

It shifts to hardware reset by changing RESET pin "H" $\rightarrow$ "L".
The condition of all the registers under hardware reset pin is returned to the initial value, and it stops accepting all address.
To release from a state of hardware reset, change RESET pin " L " $\rightarrow$ " H ".

- Reset Sequence

When hardware reset was done during software reset, software reset is canceled when hardware reset is canceled.
(Because the initial value of software reset is " 0 ")

## 2) Pulse skip control

This IC regulates the output voltage using an improved pulse-skip. In "pulse-skip" mode, the error amplifier disables the oscillator causing the "switching" of the power stages to stop when low output voltage and high input voltage are detected. The said switching cycle will be reactivated when the IC detects low input voltage.
At light loads, a conventional "pulse-skip" regulation mode is used. The "pulse-skip" regulation minimizes the operating current because this IC does not switch continuously and hence the losses of the switching are reduced. When the error amplifier disables "switching", the load is also isolated from the input. This improved "pulse-skip" control is also referred to as active-cycle control.
Pulse skip setting can be controlled in four (4) different modes by register (SKIPEN:(ad02h D[7:6])).


Figure 61. Pulse-skip
3) Soft start

BD65B60 has a soft start function which prevents large coil current from flowing to the IC. During start-up, in-rush current is prevented. The "soft start" of this IC controls the over-current setting hence peak current is controlled.
After changing Enable register (PON:(ad0Eh D0)) from "L" to "H", Soft start takes place within the period of 1.8 ms (Typ.) Once "soft start" is finished, boost condition change to normal state.

<The case of PWM dimming>


Soft Start Time=T1 + T2 $=1.8 \mathrm{~ms}$

Figure 62. Soft start

## -Protection

PROTECTION TABLE

| No | Failure Mode | Detection Mode | LED current | DC/DC <br> Feedback | DC/DC <br> Action | After release Failure |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | LED1 is used LED2 is used LED Short ( LED1 is Short) | $\begin{aligned} & \text { LED1 > } 5.4 \mathrm{~V} \text { (Typ.) } \\ & \text { LED2 }<0.9 \mathrm{~V} \text { (Typ.) } \\ & \text { VSC }=5.4 \mathrm{~V} \text { (Typ.) } \end{aligned}$ | ```<short LED> stop <other LED> Active``` | <short LED> <br> Feedback cut <other LED> Feedback Active | Normal Output | Latch |
| 2 | LED1 is used LED2 is used LED Short ( Both LED1 and LED2 are Short ) | $\begin{aligned} & \text { LED1 > } 5.4 \mathrm{~V} \text { (Typ.) } \\ & \text { LED2 }>5.4 \mathrm{~V} \text { (Typ.) } \\ & \text { VSC }=5.4 \mathrm{~V} \text { (Typ.) } \end{aligned}$ | <short LED> Active | <short LED> Feedback Active | Normal Output | Auto return |
| 3 | LED1 is used LED2 is used LED Short ( Both LED1 and LED2 are Short ) | $\begin{aligned} & \text { LED1 < } 5.4 \mathrm{~V} \text { (Typ.) } \\ & \text { LED2 < } 5.4 \mathrm{~V} \text { (Typ.) } \\ & \text { VSC }=5.4 \mathrm{~V} \text { (Typ.) } \end{aligned}$ | <short LED> Active | <short LED> Feedback Active | Normal Output | Auto return |
| 4 | LED1 is used LED2 is unused LED Short ( LED1 is Short ) | $\begin{gathered} \text { LED1 }>5.4 \mathrm{~V} \text { (Typ.) } \\ \text { VSC }=5.4 \mathrm{~V} \text { (Typ.) } \end{gathered}$ | <short LED> Active | <short LED> Feedback Active | Normal Output | Auto return |
| 5 | LED1 is used LED2 is unused LED Short ( LED1 is Short ) | $\begin{gathered} \text { LED1 < } 5.4 \mathrm{~V} \text { (Typ.) } \\ \text { VSC }=5.4 \mathrm{~V} \text { (Typ.) } \end{gathered}$ | <short LED> Active | <short LED> Feedback Active | Normal Output | Auto return |
| 6 | LED OPEN ( LED1 is Open ) | $\begin{gathered} \text { VOUT > OVP setting } \\ \text { LED2 }<5.4 \mathrm{~V} \text { (Typ.) } \\ \text { VSC }=5.4 \mathrm{~V} \text { (Typ.) } \end{gathered}$ | $\begin{aligned} & \text { <open LED> } \\ & \text { Don't flow } \\ & \text { <other LED> } \\ & \text { Active } \end{aligned}$ | <open LED> <br> Feedback Active <other LED> Feedback Active | OVP action | Auto return |
| 7 | LED OPEN ( LED1 is Open ) | $\begin{gathered} \text { VOUT > OVP setting } \\ \text { LED2 }>5.4 \mathrm{~V} \text { (Typ.) } \\ \text { VSC }=5.4 \mathrm{~V} \text { (Typ.) } \end{gathered}$ | ```<open LED> Don't flow <other LED> Don't flow``` | <open LED> <br> Feedback Active <other LED> Feedback Active | LED Short action | Latch |
| 8 | LED OPEN ( Both LED1 and LED2 are Open ) | VOUT >OVP setting | Don't flow | Active | OVP action | Auto return |
| 9 | VOUT/SW short to GND | VOUT < 0.2V | Don't flow | Active | Stop | Auto return |
| 10 | LED VF more than OVP setting | VOUT > OVP setting | Stop | Active | OVP action | Auto return |
| 11 | too high | SW current > OCP | Active | Active | $\begin{aligned} & \text { OCP } \\ & \text { action } \end{aligned}$ | Auto return |
| 12 | too high | Temperature > $\operatorname{TSD}\left(175^{\circ} \mathrm{C}\right)$ | Stop | Active | Stop | Auto return |

Condition: normal state (This state isn't "soft start")
The Latch is released by
(1) Input hardware reset signal to RESET terminal
(2) Input the register of software reset by I2C
(3) detect UVLO

Please refer to "Application Deficiency Operation" regarding these functions.

## - Over voltage protection (OVP)

When LED is disconnected, it will result to open DC/DC output causing it to over step-up. When VOUT pin exceeds the absolute maximum rating, the switch N -channel Transistor and IC will break down. To prevent this, the over-voltage limit is activated when VOUT pin becomes equal or more than the detect voltage thus turning off the switching and stopping the operation of the DC/DC.

After over voltage protection, as shown in Figure 63, the IC changes from active into non-active, and the output voltage goes down slowly.


Figure 63. OVP operating description

## - Over Current Protection

Over current flows in current detect resistor that is connected between internal switching $\operatorname{Tr}$ source and GND. When it increases beyond the detect voltage, over current protect operates. Over current protect prevents the increase of more than the detect voltage by reducing the "ON" Duty of switching $\operatorname{Tr}$ without stopping boosting operation.
Since the over current detector of this IC detects peak current, over current does not flow more than the set value.

- External SBD open detect / Output Short protection

If in case external SBD and DC/DC output (VOUT) connections are opened or VOUT is shorted to GND, there is a risk that the coil and the internal Tr may be destroyed. External SBD open and output short protection activate when VOUT becomes 200 mV (Typ.) or below causing the output Tr to turn off and preventing the destruction of the coil and the IC. No current will flow ( 0 mA ) since the IC changes from active into non-active.

## - Thermal shut down

This IC has thermal shut down function.
The thermal shut down works at $175^{\circ} \mathrm{C}$ (Typ.) or higher, and the IC changes from active into non-active.

## - Low voltage detect protection (UVLO)

When supply voltage (VBAT) becomes lower than the detect voltage 2.1 V (Typ.), DC/DC converter and constant current driver are disabled. Moreover, this function can be turned off by boosting supply voltage up to more than hysteresis voltage.


Figure 64. UVLO protection

## - Application Deficiency Operation

(1) When 1 LED or 1string is OPEN during the operation

The LED string, which become OPEN will not light (e.g. LED1) but the other LED string will continue its operation. As shown in Figure 65, LED1 voltage becomes 0 V when channel LED1 is opened. This voltage which is below 0.3 V (Typ.) will then be detected as its lowest feedback voltage causing the output voltage to boost up to its over voltage protection limits.


Figure 65. LED open protect
(2) When LED short-circuited in multiple

All LED strings are lighted unless LED1 and LED2 terminal voltage is more than 5.4 V (Typ.)(SHORT:(ad02h D0)=1). Only the string that is short-circuited becomes more than 5.4 V (Typ.) will be turned off while the other LED string continues to turn on normally.
As shown in Figure 66, LED1 current (Shorted line) is changed from 25 mA (Typ.) to 0 mA (Typ.), so LED1 terminal doesn't generate heat.


Figure 66. LED short protect
(3) When Schottky diode (SBD) remove

In the situation where the SBD connection is opened while DC/DC is still activated, SW terminal voltage becomes more than the rated voltage due to lack of parts that can accept the current accumulated inside the coil. Consequently, IC might be destroyed. To prevent the IC destruction, SBD open protection is operated. The SW terminal will not be damaged because boost operation will be stopped when VOUT terminal detects less than 0.2 V .

## -Selecting the Number of Operational LED Channels

The number of operational LED channels is chosen by modifying D2 and D0 of the register address 03h. In the example as shown in Figure67, only LED1 channel is active (ad03h, data=01h).


Figure 67. LED selection register is set for open strings

## -LED Current Setting

LED current is set by register (ad05h D[7:0]) and RSET resistor which is computed in the following equation:
LED current $=$ max current $\times$ ratio $\times$ PWM duty (from PWM terminal)

$$
=\operatorname{IMAX} \times(\text { ILED }+1) / 256 \times \text { PWM duty }
$$

Where:
IMAX = this is set by the resistor (RSET) connected to ISET terminal and computed in the following equation:
$\operatorname{IMAX}$ current $=600 /$ RSET $(\mathrm{A})$
IMAX setting example

| RSET | IMAX |
| :---: | :---: |
| $24 \mathrm{k} \Omega$ | 25.0 mA |
| $30 \mathrm{k} \Omega$ | 20.0 mA |
| $56 \mathrm{k} \Omega$ | 10.7 mA |
| $120 \mathrm{k} \Omega$ | 5.0 mA |

ratio $=$ this is given by varying ad05h $D[7: 0]$

| $\rightarrow$ | ratio $=$ | (0 | 1/256 = | 0.39\% |
| :---: | :---: | :---: | :---: | :---: |
| ata 20h $\rightarrow$ | ratio $=$ | $(32+1) / 256=$ | 33/256 = | 12.89\% |
| data C7h | ratio $=$ | $(199+1) / 256=$ | 200/256 = | 78.13\% |
| data FFh | ratio $=$ | $(255+1) / 256=$ | 256/256 | 100.00\% |

PWM duty = PWM "H" duty of PWM pulse. PWM pulse is inputted from PWM terminal.

## -Feedback Voltage Setting

Feedback voltage is set by register (ad02h D[1:0]). To improve the efficiency, low feedback voltage which is determined by the LED current and output voltage (VOUT) ripple should be set.

To maintain a VOUT ripple below 50mV, the recommended feedback voltages for each LED current range are shown below:
Feedback voltage

| Feedback voltage | IMAX |
| :---: | :---: |
| 0.5 V | All range |
| 0.4 V | Under 23.0 mA |
| 0.3 V | Under 15.3 mA |
| 0.2 V | Under 7.6 mA |

## -Brightness Control

This IC has several methods of brightness controls such as: maximum current set by RSET resistor connected at ISET terminal; current ratio set by 8bit DAC and PWM control which can be set as DC or pulse input.


| No. | PWMEN | LPFEN | LED Current |
| :---: | :---: | :---: | :---: |
| $(1)$ | 0 | 0 | DC ( 8bit DAC ) |
|  | 0 | 1 | DC ( 8bit DAC ) |
| $(2)$ | 1 | 0 | PWM ( 8bit DAC and PWM duty ) |
| $(3)$ | 1 | 1 | DC (8bit DAC and PWM duty ) |

Figure 68. Brightness control
When PWMEN="1" by (ad07h D5), PWM pulse can be inputted and vice versa when PWMEN = " 0 ".
When LPFEN=" 0 " by (ad07h D2), the capacitor of LPF is disconnected. LED current is as same as PWM pulse.
When LPFEN=" 1 ", the capacitor of LPF is connected. LED current becomes DC.
(1)DC Dimming controlled by 8bit current DAC, as shown in Figure 68.

This dimming is controlled by 8bit current DAC controlled by current ratio register (ad05h).
The LED current becomes DC, because PWM input is not accepted by PWMEN=" 0 ".
Setting current is shown as below.
LED current $=$ max. current x ratio

$$
=\text { IMAX } \times(\text { ILED +1) / } 256
$$

(2)PWM Dimming controlled by 8bit current DAC and PWM duty for CABC, as shown in Figure 70.

This dimming is controlled by 8bit current DAC and PWM pulse inputted to PWM terminal. Main brightness is controlled by 8bit current DAC and the dimming according to contents like movie and picture is controlled by PWM.
LED current flows with the H section of PWM, and does not flow with the L section. Therefore, the average LED current increases in proportion to duty cycle of PWM signal. Because it becomes to switch the driver, the current tolerance is low when the PWM brightness is adjusted making it possible to control the brightness until $5 \mu \mathrm{~s}$ (Min. $10 \%$ at 20 kHz ). And, do not use for the brightness control, because effect of ISET changeover is big under $5 \mu \mathrm{~s}$ ON time and under $5 \mu \mathrm{~s}$ OFF time.
Setting current is shown as below.
LED current $=$ max. current $\times$ ratio $\times$ PWM duty (from PWM terminal)

$$
=\operatorname{IMAX} \times(\text { ILED }+1) / 256 \times \text { PWM duty }
$$

(3)DC Dimming controlled by 8bit current DAC and PWM duty for CABC, as shown in Figure 69.

This dimming is controlled by 8bit current DAC and PWM pulse inputted to PWM terminal.
Main brightness is controlled by 8bit current DAC and the dimming according to contents like movie and picture is controlled by PWM. By LPF, PWM pulse becomes average into BD65B60, according to the duty of PWM pulse. Therefore, the average LED current increases in proportion to duty cycle of PWM signal. Because LED current becomes DC, coil current also becomes DC. The noise of this dimming is smaller than that of PWM dimming, but the current tolerance is worse than PWM dimming. PWM dimming range is from $10 \%$ to $100 \%$. If duty changes under $10 \%$, LED current tolerance become big. Typical PWM frequency is 20 kHz to 100 kHz .
Setting current is shown as below.
LED current $=$ max. current $\times$ ratio $\times$ PWM duty (from PWM terminal)
$=$ IMAX $\times($ ILED +1$) / 256 \times$ PWM duty


Figure 69. DC dimming


Figure 70. PWM dimming

## -Coil Selection

The DC/DC is designed using a coil value equal or greater than $4.7 \mu \mathrm{H}$. Sub-harmonic oscillation of current mode DC / DC might happen if the coil "L" value used is equal or lower than $2.2 \mu \mathrm{H}$.
When the coil "L" value increases, the phase margin of DC / DC becomes zero therefore, output capacitor value should also be increased. Make the resistor component smaller in order to increase the efficiency of DCR Inductor. Estimation of Coil Peak Current is shown at the examples below.

Peak Current calculation
<Estimate of the current value which is needed for the normal operation>
As over current detector of this IC is detected the peak current, it have to estimate peak current to flow to the coil by operating condition.
$\begin{array}{lll}\text { In case of, } & - \text { Supply voltage of coil }=\text { VIN } & - \text { Inductance value of coil }=\mathrm{L} \\ & - \text { Switching frequency }=\mathrm{fsw} & - \text { Output voltage }=\text { VouT } \\ & - \text { Total LED current }=\text { ILED } & \\ & - \text { Average current of coil }=\text { lave } & - \text { Peak current of coil }=\text { Ipeak } \\ & - \text { Cycle of Switching }=T & - \text { Efficiency }=\text { eff } \quad \text { (Please set up having margin) } \\ & - \text { ON time of switching transistor }=\text { Ton } & - \text { ON Duty }=D\end{array}$
The relation is shown below:
CCM: Ipeak $=($ VIN $/ \mathrm{L}) \times(1 /$ fsw $) \times(1-($ Vin $/$ Vout $))$, DCM: Ipeak $=($ Vin $/ \mathrm{L}) \times$ Ton
lave $=($ Vout $\times$ IOUT $/ \mathrm{VIN}) /$ eff
Ton $=(\text { lave } \times(1-\mathrm{VIN} / \text { Vout }) \times(1 / \mathrm{fsw}) \times(\mathrm{L} / \mathrm{VIN}) \times 2)^{1 / 2}$
Each current is calculated.
As peak current varies according to whether there is the direct current superposed, the next is decided.
CCM: $(1-$ VIN $/$ Vout $) \times(1 / \mathrm{fsw})<$ Ton $\rightarrow$ peak current $=$ Ipeak $/ 2+$ lave
DCM: $\quad(1-\mathrm{VIN} /$ Vout $) \times(1 / \mathrm{fsw})>$ Ton $\rightarrow$ peak current $=$ VIN $/ \mathrm{L} \times$ Ton
(Example 1)
In case of, V IN $=3.6 \mathrm{~V}$, L=10 H , fsw=0.6MHz, Vout=26.4V, Iled=50mA, Efficiency=88\%
lave $=(26.4 \mathrm{~V} \times 50 \mathrm{~mA} / 3.6 \mathrm{~V}) / 88 \%=0.4167 \mathrm{~A}$
Ton $=(0.4167 \mathrm{~A} \times(1-3.6 \mathrm{~V} / 26.4 \mathrm{~V}) \times(1 / 0.6 \mathrm{MHz}) \times(10 \mu \mathrm{H} / 3.6 \mathrm{~V}) \times 2)^{1 / 2}=1.825 \mu \mathrm{~s}$
( $1-\mathrm{VIN} /$ Vout $) \times(1 / \mathrm{fsw})=1.439 \mu \mathrm{~s}<\operatorname{Ton}(1.825 \mu \mathrm{~s}) \quad$ CCM
Ipeak $=(3.6 \mathrm{~V} / 10 \mu \mathrm{H}) \times(1 / 0.6 \mathrm{MHz}) \times(1-(3.6 \mathrm{~V} / 26.4 \mathrm{~V}))=0.5182 \mathrm{~A}$
Peak current $=0.5182 \mathrm{~A} / 2+0.4167 \mathrm{~A}=0.6758 \mathrm{~A}$
(Example 2)
In case of, $\mathrm{VIN}=3.6 \mathrm{~V}, \mathrm{~L}=10 \mu \mathrm{H}, \mathrm{fsw}=0.6 \mathrm{MHz}$, Vout=19.8V, ILed=11.3mA, Efficiency=88\% lave $=(19.8 \mathrm{~V} \times 11.3 \mathrm{~mA} / 3.6 \mathrm{~V}) / 88 \%=0.0706 \mathrm{~A}$
Ton $=(0.0706 \mathrm{~A} \times(1-3.6 \mathrm{~V} / 19.8 \mathrm{~V}) \times(1 / 0.6 \mathrm{MHz}) \times(10 \mu \mathrm{H} / 3.6 \mathrm{~V}) \times 2)^{1 / 2}=0.731 \mu \mathrm{~s}$
( $1-\mathrm{VIN} / \mathrm{VOUT}$ ) $\times(1 / \mathrm{fsw})=1.364 \mu \mathrm{~s}>\operatorname{Ton}(0.731 \mu \mathrm{~s}) \quad$ DCM
Ipeak $=\mathrm{VIN} / \mathrm{L} \times$ Ton $=3.6 \mathrm{~V} / 10 \mu \mathrm{H} \times 0.731 \mu \mathrm{~s}=0.2633 \mathrm{~A}$
Peak current $=0.2633 \mathrm{~A}$

## DCM/CCM calculation

Discontinuous Condition Mode (DCM) and Continuous Condition Mode (CCM) are calculated as following.
CCM: $\quad \mathrm{L}>$ VOUT $\times \mathrm{D} \times(1-\mathrm{D})^{2} \times \mathrm{T} /(2 \times$ ILED $)$
DCM: $\quad \mathrm{L}<$ Vout $\times \mathrm{D} \times(1-\mathrm{D})^{2} \times \mathrm{T} /(2 \times$ ILED $)$
*D = 1- Vin / Vout
(Example 1)
In case of, $\mathrm{Vin}=3.6 \mathrm{~V}, \mathrm{~L}=10 \mu \mathrm{H}$, fsw=0.6MHz, Vout=26.4V, ILED=50mA
VOUT $\times \mathrm{D} \times(1-\mathrm{D})^{2} \times \mathrm{T} /(2 \times$ ILED $)$
$=26.4 \mathrm{~V} \times(1-3.6 \mathrm{~V} / 26.4 \mathrm{~V}) \times(3.6 \mathrm{~V} / 26.4 \mathrm{~V})^{2} \times 1 /\left(0.6 \times 10^{6} \mathrm{~Hz}\right) /(2 \times 0.05 \mathrm{~A})=7.066 \mu \mathrm{H}<\mathrm{L}(10 \mu \mathrm{H})$
$\rightarrow$ CCM
(Example 2)
In case of, V In $=3.6 \mathrm{~V}, \mathrm{~L}=10 \mu \mathrm{H}$, fsw=0.6MHz, Vout=19.8V, ILED=11.3mA
VOUT $\times \mathrm{D} \times(1-\mathrm{D})^{2} \times \mathrm{T} /(2 \times$ ILED $)$
$=19.8 \mathrm{~V} \times(1-3.6 \mathrm{~V} / 19.8 \mathrm{~V}) \times(3.6 \mathrm{~V} / 19.8 \mathrm{~V})^{2} \times 1 /\left(0.6 \times 10^{6} \mathrm{~Hz}\right) /(2 \times 0.0113 \mathrm{~A})=39.494 \mu \mathrm{H}>\mathrm{L}(10 \mu \mathrm{H})$
$\rightarrow$ DCM

## -OUTPUT Capacitor Selection

Output Capacitor smoothly keeps output voltage and supplies LED current. Output Voltage consists of Charge (FET ON) and Discharge (LED current). So Output voltage has Output ripple Voltage in every FET switching.
Select a capacitor value which allows the output ripple voltage to settle within 50 mV .
Output ripple voltage is calculated as follows.
Output ripple Voltage

| - Switching cycle = T | - Total LED current = ILED |
| :--- | :--- |
| - Switching ON duty = D | - Output ripple Voltage = Vripple |
| - Output Capacitor = Cout | - Output Capacitor (real value) $=$ Creal |
| - Decreasing ratio of Capacitor $=$ Cerror | - Supply voltage of coil $=$ VIN |

Creal $=$ Cout $\times$ Cerror $\quad$ (Capacitor value is decreased by Bias)
Creal $=\operatorname{ILED} \times(1-\mathrm{D}) \times \mathrm{T} /$ Vripple
Cout $=\operatorname{ILED} \times(1-\mathrm{D}) \times \mathrm{T} /$ Vripple $/$ Cerror
(Example 1)
In case of, Vin=3.6V, fsw=0.6MHz, Vout=19.8V, ILEd=15mA, Cout=1.0 $\mu$ F, Cerror=50\%
$\mathrm{T}=1 / 0.6 \mathrm{MHz}$
$\mathrm{D}=1-\mathrm{VIN} /$ Vout $=1-3.6 \mathrm{~V} / 19.8 \mathrm{~V}=0.818$
Vripple $=\operatorname{ILED} \times(1-\mathrm{D}) \times \mathrm{T} /($ CouT $\times$ Cerror $)$
$=15 \mathrm{~mA} \times(3.6 \mathrm{~V} / 19.8 \mathrm{~V}) \times(1 / 0.6 \mathrm{MHz}) /(1.0 \mu \mathrm{~F} \times 0.5)$
$=9.1 \mathrm{mV}$


Figure 71. Bias Characteristics of Capacitor

## OINPUT Capacitor Selection

$1 \mu \mathrm{~F}$ ceramic capacitor with 10 V (greater than coil voltage) is recommended for the Inductor.

## -Schottky Diode Selection

Shottky diode should be used for boost. Maximum peak current should be greater than inductor peak current (1A(Typ.) or 1.7A(Typ.)) to ensure reliable operation. Average current should be greater than the maximum output current. Schottky diodes with a low forward drop and fast switching speeds are ideal for increasing efficiency in portable applications. Choose a reverse break down voltage of the Schottky diode significantly larger than the output voltage.

## OLED Selection

Please select LED VF that input voltage is smaller than output voltage (VOUT).
And also select LED VF that output voltage is smaller than OVP voltage - 1 V .

## -SDA, SCL Pull-up Resistor Selection

Please select the most suitable Pull-up resistor value to input I2C frequency. The case Pull-up resistor value is too big, SCL and SDA pulse are rounded. Therefore high speed transfer is impossible.

## OIC and Coil Power Supply Separation

BD65B60 can operate in a separate power source for the IC and coil. With this application, IC power consumption is decreased and the applied voltage can be exceeded the IC rating of 5.5 V .

Figure 72 shows the separate power sources for coil and IC wherein the coil power supply is connected to a high voltage source applied from adapters.


Figure 72. Separate Power Supply Application

## - PCB Layout

PCB layout is very important to achieve the best performance of the IC. Layout pattern can greatly affect some characteristics of the IC, such as efficiency and ripple.


Figure 73. Schematic
<Input bypass capacitor CVBAT (1.0 FF(Typ.))>
Connect input bypass capacitor CVBAT (1.0رF(Typ.)) as close as possible to coil and GND pin.
<Input bypass capacitor CVIO ( $0.1 \mu \mathrm{~F}$ (Typ.))>
Connect input bypass capacitor CVIO ( $0.1 \mu \mathrm{~F}(\mathrm{Typ}$.$) ) as close as possible to \mathrm{VIO}$ pin and GND pin.
<Coil>
Connect coil as close as possible to SW pin. When the distance between coil and SW pin is long, the efficiency becomes incorrect due to the effect of PCB parasitic capacitance.
<Schottky barrier diode SBD>
Connect Schottky barrier diode SBD as close as possible between coil and SW pin.
<Output capacitor COUT>
Connect output capacitor COUT between cathode of SBD and GND.
Make both GND sides of CVBAT and COUT as close as possible.

## <Others>

Connect the current setting resistor RSET near the ISET and GND pins. When these pins are not directly connected near the chip, the performance of BD65B60 may be affected and it may limit the current drive. As for the wire of the inductor, make sure that its resistance is small enough to reduce the electric power consumption and to increase the entire efficiency.
Do not connect capacitor between ISET and GND pin.

## - Recommended Layout Pattern



Figure 74. Top Copper trace layer


Figure 75. Bottom Copper trace layer

## -Selection of External Parts

Recommended external parts are shown below.
If there are parts that will be used and not listed below, make sure to choose the equivalent parts.

| Value | Manufacturer | Product number | Size (mm) |  |  |  | DCR <br> ( $\Omega$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Vertical | Horizontal | $\begin{aligned} & \text { Height } \\ & \text { (MAX) } \end{aligned}$ |  |  |
| $10 \mu \mathrm{H}$ | TDK | VLF302512MT-100M | 3.0 | 2.5 | 1.2 | 690 | 0.25 |
| $10 \mu \mathrm{H}$ | TDK | VLF403212MT-100M | 4.0 | 3.2 | 1.2 | 1000 | 0.23 |
| $10 \mu \mathrm{H}$ | TDK | VLF302510MT-100M | 3.0 | 2.5 | 1.0 | 650 | 0.31 |
| $10 \mu \mathrm{H}$ | TDK | VLF403210MT-100M | 4.0 | 3.2 | 1.0 | 780 | 0.26 |
| $10 \mu \mathrm{H}$ | TOKO | DEM3532C series <br> 1229AS-H-100M | 3.5 | 3.7 | 1.2 | 750 | 0.24 |
| $4.7 \mu \mathrm{H}$ | TOKO | DFE322512C series 1277AS-H-4R7M | 3.2 | 2.5 | 1.2 | 1800 | 0.17 |
| $4.7 \mu \mathrm{H}$ | TOKO | DFE252012C series 1239AS-H-4R7M | 2.5 | 2.0 | 1.2 | 1500 | 0.24 |
| $10 \mu \mathrm{H}$ | TOKO | $\begin{gathered} \text { DFE252012C series } \\ \text { 1239AS-H-100M } \end{gathered}$ | 2.5 | 2.0 | 1.2 | 1000 | 0.46 |
| $4.7 \mu \mathrm{H}$ | TOKO | DFE322510C series 1276AS-H-4R7M | 3.2 | 2.5 | 1.0 | 1400 | 0.22 |
| $10 \mu \mathrm{H}$ | TOKO | $\begin{aligned} & \text { DFE322510C series } \\ & \text { 1276AS-H-100M } \end{aligned}$ | 3.2 | 2.5 | 1.0 | 900 | 0.49 |

-Capacitor

| Value | Pressure | Manufacturer | Product number | Size (mm) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Horizontal | Height |  |
| $2.2 \mu \mathrm{~F}$ | 50 V | MURATA | GRM31CB31H225K | 3.2 | 1.6 | 1.6 |
| $1.0 \mu \mathrm{~F}$ | 50 V | MURATA | GRM31MB31H105K | 3.2 | 1.6 | 1.15 |
| $1.0 \mu \mathrm{~F}$ | 50 V | MURATA | GRM188B31H105K | 1.6 | 0.8 | 0.8 |
| $4.7 \mu \mathrm{~F}$ | 25 V | MURATA | GRM319R61E475K | 3.2 | 1.6 | 0.85 |
| $2.2 \mu \mathrm{~F}$ | 25 V | MURATA | GRM219B31E225K | 2.0 | 1.25 | 0.85 |
| $1.0 \mu \mathrm{~F}$ | 25 V | MURATA | GRM188B31E105K | 1.6 | 0.8 | 0.8 |
| $4.7 \mu \mathrm{~F}$ | 10 V | MURATA | GRM219B31A475K | 2.0 | 1.25 | 0.85 |
| $2.2 \mu \mathrm{~F}$ | 10 V | MURATA | GRM188B31A225K | 1.6 | 0.8 | 0.8 |
| $1.0 \mu \mathrm{~F}$ | 10 V | MURATA | GRM188B11A105K | 1.6 | 0.8 | 0.8 |


| Pressure | Manufacturer | Product number | Size (mm) |  |  | Io | recommended the number of LEDs |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Vertical | Horizontal | Height |  |  |
| 30 V | ROHM | RB521SM-30 | 1.6 | 0.8 | 0.6 | 0.2A | 7series 1string |
| 30 V | ROHM | RB550SS-30 | 1.6 | 0.8 | 0.6 | 0.5A | 7series 2strings |
| 30 V | ROHM | RB550VA-30 | 2.5 | 1.3 | 0.6 | 1.0A | 7series 2strings |
| 40 V | ROHM | RB521SM-40 | 1.6 | 0.8 | 0.6 | 0.2A | 8series 1string |
| 40 V | ROHM | RB160SS-40 | 1.6 | 0.8 | 0.6 | 1.0A | 8series 2strings |
| 40V | ROHM | RB160VA-40 | 2.5 | 1.3 | 0.6 | 1.0A | 8series 2strings |

The coil is the most influential part to efficiency. Select a coil which has an excellent direct current resistor (DCR) and current-inductance characteristic. BD65B60 IC is designed for an inductance value of $4.7 \mu \mathrm{H}$ to $10 \mu \mathrm{H}$. Do not use inductance values less than $2.2 \mu \mathrm{H}$. Select a ceramic capacitor type with excellent frequency and temperature characteristics.
Furthermore, select a capacitor with small direct current resistance and pay sufficient attention to the layout pattern.

## - Application Example

Figure 76 and Figure 77 are Application examples.


Figure 76. Application example (6 series $\times 1$ string)


Figure 77. Application example (8 series $\times 2$ strings)

## - Attention Point of Board Layout

In board pattern design, power supply line should be low Impedance, especially around DC/DC converter. Insert a bypass capacitor if necessary.

## - About Heat Loss

In heat design, operate the DC/DC converter in the following condition.
(The following temperature is a guarantee temperature, so consider the margin.)

1. Ambient temperature Ta must be less than $85^{\circ} \mathrm{C}$.
2. The loss of IC must be less than dissipation Pd.

## -Cautions on use

(1) Absolute Maximum Ratings

An excess in the absolute maximum ratings, such as supply voltage (VBAT), temperature range of operating conditions (Topr), etc., can break down devices, thus making impossible to identify breaking mode such as a short circuit or an open circuit. If any special mode exceeding the absolute maximum ratings is assumed, consideration should be given to take physical safety measures including the use of fuses, etc.
(2) Operating conditions

These conditions represent a range within which characteristics can be provided approximately as expected. The electrical characteristics are guaranteed under the conditions of each parameter.
(3) Reverse connection of power supply connector

The reverse connection of power supply connector can break down ICs. Take protective measures against the breakdown due to the reverse connection, such as mounting an external diode between the power supply and the IC's power supply terminal.
(4) Power supply line

Design PCB pattern to provide low impedance for the wiring between the power supply and the GND lines. Furthermore, for all power supply terminals to ICs, mount a capacitor between the power supply and the GND terminal. At the same time, in order to use an electrolytic capacitor, thoroughly check to be sure the characteristics of the capacitor to be used present no problem including the occurrence of capacity dropout at a low temperature, thus determining the constant.
(5) GND voltage

Make setting of the potential of the GND terminal so that it will be maintained at the minimum in any operating state. Furthermore, check to be sure no terminals are at a potential lower than the GND voltage including an actual electric transient.
(6) Short circuit between terminals and erroneous mounting

In order to mount ICs on a set PCB, pay thorough attention to the direction and offset of the ICs. Erroneous mounting can break down the ICs. Furthermore, if a short circuit occurs due to foreign matters entering between terminals or between the terminal and the power supply or the GND terminal, the ICs can break down.
(7) Operation in strong electromagnetic field Be noted that using ICs in the strong electromagnetic field can malfunction them.
(8) Inspection with set PCB

On the inspection with the set PCB, if a capacitor is connected to a low-impedance IC terminal, the IC can suffer stress. Therefore, be sure to discharge from the set PCB by each process. Furthermore, in order to mount or dismount the set PCB to/from the jig for the inspection process, be sure to turn OFF the power supply and then mount the set PCB to the jig. After the completion of the inspection, be sure to turn OFF the power supply and then dismount it from the jig. In addition, for protection against static electricity, establish a ground for the assembly process and pay thorough attention to the transportation and the storage of the set PCB.
(9) Input terminals

In terms of the construction of IC, parasitic elements are inevitably formed in relation to potential. The operation of the parasitic element can cause interference with circuit operation, thus resulting in a malfunction and then breakdown of the input terminal. Therefore, pay thorough attention not to handle the input terminals, such as to apply to the input terminals a voltage lower than the GND respectively, so that any parasitic element will operate. Furthermore, do not apply a voltage to the input terminals when no power supply voltage is applied to the IC. In addition, even if the power supply voltage is applied, apply to the input terminals a voltage lower than the power supply voltage or within the guaranteed value of electrical characteristics.
(10) Ground wiring pattern

If small-signal GND and large-current GND are provided, It will be recommended to separate the large-current GND pattern from the small-signal GND pattern and establish a single ground at the reference point of the set PCB so that resistance to the wiring pattern and voltage fluctuations due to a large current will cause no fluctuations in voltages of the small-signal GND. Pay attention not to cause fluctuations in the GND wiring pattern of external parts as well.
(11) External capacitor

In order to use a ceramic capacitor as the external capacitor, determine the constant with consideration given to a degradation in the nominal capacitance due to DC bias and changes in the capacitance due to temperature, etc.
(12) Thermal shutdown circuit (TSD)

When junction temperatures become $175^{\circ} \mathrm{C}$ (Typ.) or higher, the thermal shutdown circuit operates and turns a switch OFF. The thermal shutdown circuit, which is aimed at isolating the LSI from thermal runaway as much as possible, is not aimed at the protection or guarantee of the LSI. Therefore, do not continuously use the LSI with this circuit operating or use the LSI assuming its operation.
(13) Thermal design

Perform thermal design in which there are adequate margins by taking into account the permissible dissipation ( Pd ) in actual states of use.
(14) Selection of coil

Select the low DCR inductors to decrease power loss for DC/DC converter.
-Ordering Information


## - Marking Diagram



## OPhysical Dimension Tape and Reel Information

| Package Name | UCSP50L1(BD65B60GWL) |
| :--- | :--- |



Drawing No: EX926-5021
(UNIT:mm)
< Tape and Reel Information >

| Tape | Embossed carrier tape |
| :--- | :--- |
| Quantity | $3000 p c s / R e e l$ |
| Direction of feed | E2 <br> (The direction is the 1pin of product is at the upper left when you hold <br> reel on the left hand and you pull out the tape on the right hand |



Revision History

| Date | Revision |  |
| :---: | :---: | :--- |
| 3.Jun.2013 | 001 | New Release |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |

## Notice

## Precaution on using ROHM Products

1. Our Products are designed and manufactured for application in ordinary electronic equipments (such as AV equipment, OA equipment, telecommunication equipment, home electronic appliances, amusement equipment, etc.). If you intend to use our Products in devices requiring extremely high reliability (such as medical equipment ${ }^{(N o t e}{ }^{1}$ ), transport equipment, traffic equipment, aircraft/spacecraft, nuclear power controllers, fuel controllers, car equipment including car accessories, safety devices, etc.) and whose malfunction or failure may cause loss of human life, bodily injury or serious damage to property ("Specific Applications"), please consult with the ROHM sales representative in advance. Unless otherwise agreed in writing by ROHM in advance, ROHM shall not be in any way responsible or liable for any damages, expenses or losses incurred by you or third parties arising from the use of any ROHM's Products for Specific Applications.
(Note1) Medical Equipment Classification of the Specific Applications

| JAPAN | USA | EU | CHINA |
| :---: | :---: | :---: | :---: |
| CLASSIII | CLASSIII | CLASS II b | CLASSIII |
|  |  | CLASSIII |  |

2. ROHM designs and manufactures its Products subject to strict quality control system. However, semiconductor products can fail or malfunction at a certain rate. Please be sure to implement, at your own responsibilities, adequate safety measures including but not limited to fail-safe design against the physical injury, damage to any property, which a failure or malfunction of our Products may cause. The following are examples of safety measures:
[a] Installation of protection circuits or other protective devices to improve system safety
[b] Installation of redundant circuits to reduce the impact of single or multiple circuit failure
3. Our Products are designed and manufactured for use under standard conditions and not under any special or extraordinary environments or conditions, as exemplified below. Accordingly, ROHM shall not be in any way responsible or liable for any damages, expenses or losses arising from the use of any ROHM's Products under any special or extraordinary environments or conditions. If you intend to use our Products under any special or extraordinary environments or conditions (as exemplified below), your independent verification and confirmation of product performance, reliability, etc, prior to use, must be necessary:
[a] Use of our Products in any types of liquid, including water, oils, chemicals, and organic solvents
[b] Use of our Products outdoors or in places where the Products are exposed to direct sunlight or dust
[c] Use of our Products in places where the Products are exposed to sea wind or corrosive gases, including Cl 2 , $\mathrm{H}_{2} \mathrm{~S}, \mathrm{NH}_{3}, \mathrm{SO}_{2}$, and $\mathrm{NO}_{2}$
[d] Use of our Products in places where the Products are exposed to static electricity or electromagnetic waves
[e] Use of our Products in proximity to heat-producing components, plastic cords, or other flammable items
[f] Sealing or coating our Products with resin or other coating materials
[g] Use of our Products without cleaning residue of flux (even if you use no-clean type fluxes, cleaning residue of flux is recommended); or Washing our Products by using water or water-soluble cleaning agents for cleaning residue after soldering
[h] Use of the Products in places subject to dew condensation
4. The Products are not subject to radiation-proof design.
5. Please verify and confirm characteristics of the final or mounted products in using the Products.
6. In particular, if a transient load (a large amount of load applied in a short period of time, such as pulse. is applied, confirmation of performance characteristics after on-board mounting is strongly recommended. Avoid applying power exceeding normal rated power; exceeding the power rating under steady-state loading condition may negatively affect product performance and reliability.
7. De-rate Power Dissipation (Pd) depending on Ambient temperature (Ta). When used in sealed area, confirm the actual ambient temperature.
8. Confirm that operation temperature is within the specified range described in the product specification.
9. ROHM shall not be in any way responsible or liable for failure induced under deviant condition from what is defined in this document.

## Precaution for Mounting / Circuit board design

1. When a highly active halogenous (chlorine, bromine, etc.) flux is used, the residue of flux may negatively affect product performance and reliability.
2. In principle, the reflow soldering method must be used; if flow soldering method is preferred, please consult with the ROHM representative in advance.

For details, please refer to ROHM Mounting specification

## Precautions Regarding Application Examples and External Circuits

1. If change is made to the constant of an external circuit, please allow a sufficient margin considering variations of the characteristics of the Products and external components, including transient characteristics, as well as static characteristics.
2. You agree that application notes, reference designs, and associated data and information contained in this document are presented only as guidance for Products use. Therefore, in case you use such information, you are solely responsible for it and you must exercise your own independent verification and judgment in the use of such information contained in this document. ROHM shall not be in any way responsible or liable for any damages, expenses or losses incurred by you or third parties arising from the use of such information.

## Precaution for Electrostatic

This Product is electrostatic sensitive product, which may be damaged due to electrostatic discharge. Please take proper caution in your manufacturing process and storage so that voltage exceeding the Products maximum rating will not be applied to Products. Please take special care under dry condition (e.g. Grounding of human body / equipment / solder iron, isolation from charged objects, setting of lonizer, friction prevention and temperature / humidity control).

## Precaution for Storage / Transportation

1. Product performance and soldered connections may deteriorate if the Products are stored in the places where:
[a] the Products are exposed to sea winds or corrosive gases, including $\mathrm{Cl} 2, \mathrm{H} 2 \mathrm{~S}, \mathrm{NH} 3, \mathrm{SO} 2$, and NO 2
[b] the temperature or humidity exceeds those recommended by ROHM
[c] the Products are exposed to direct sunshine or condensation
[d] the Products are exposed to high Electrostatic
2. Even under ROHM recommended storage condition, solderability of products out of recommended storage time period may be degraded. It is strongly recommended to confirm solderability before using Products of which storage time is exceeding the recommended storage time period.
3. Store / transport cartons in the correct direction, which is indicated on a carton with a symbol. Otherwise bent leads may occur due to excessive stress applied when dropping of a carton.
4. Use Products within the specified time after opening a humidity barrier bag. Baking is required before using Products of which storage time is exceeding the recommended storage time period.

## Precaution for Product Label

QR code printed on ROHM Products label is for ROHM's internal use only.

## Precaution for Disposition

When disposing Products please dispose them properly using an authorized industry waste company.

## Precaution for Foreign Exchange and Foreign Trade act

Since our Products might fall under controlled goods prescribed by the applicable foreign exchange and foreign trade act, please consult with ROHM representative in case of export.

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[^0]:    *1 This parameter is tested with DC measurement
    *2 condition: RSET resistor $=40 \mathrm{k} \Omega$, ILED $=15.0 \mathrm{~mA}$ setting calculation: IDALIN1=(ILED(XXh)/ILED(FFh) x 256/(XXh+1)) - 1

