# 3.5 V to 40 V Input, 1 A <br> Single 2.2 MHz Buck DC/DC Converter For Automotive 

## BD9P1x5MUF-C Series

## General Description

BD9P1x5MUF-C Series are current mode synchronous buck DC/DC converter integrating POWER MOSFETs.

## Features

- Nano Pulse Control ${ }^{\text {TM }}$
- AEC-Q100 Qualified(Note 1)
- Minimum ON Pulse 50 ns (Max)
- Synchronous Buck DC/DC Converter Integrating POWER MOSFETs
- Soft Start Function
- Current Mode Control
- Reset Function

■ Quiescent Current $10 \mu \mathrm{~A}$ (Typ) with 12 V Input to 5.0 V Output

- Light Load Mode (LLM)
- Forced Pulse Wide Modulation (PWM) Mode
- Phase Compensation Included
- Selectable Spread Spectrum Switching
- External Synchronization Function
- Selectable Over Current Protection (OCP)
- Input Under Voltage Lockout (UVLO) Protection
- Thermal Shut Down (TSD) Protection
- Output Over Voltage Protection (OVP) Short Circuit Protection (SCP)
(Note 1) Grade 1


## Applications

- Automotive Powered Supplies
- Consumer Powered Supplies


## Key Specifications

- Input Voltage Range:
3.5 V to 40 V
(Initial startup is 4.0 V or more)
- Output Voltage Range

BD9P105MUF-C: $\quad 0.8 \mathrm{~V}$ to 8.5 V
BD9P135MUF-C: $\quad 3.3 \mathrm{~V}$ (Typ)
BD9P155MUF-C: $\quad 5.0 \mathrm{~V}$ (Typ)
■ Output Current:
OCP_SEL $=\mathrm{L} \quad 0.5 \mathrm{~A}($ Max $)$
OCP_SEL $=\mathrm{H} \quad 1.0 \mathrm{~A}(\mathrm{Max})$

- Switching Frequency:
2.2 MHz (Typ)
- Output Voltage Accuracy:
$\pm 1.75 \%\left(-40^{\circ} \mathrm{C}\right.$ to $\left.+125^{\circ} \mathrm{C}\right)$
■ Shutdown Current: $\quad 2.1 \mu \mathrm{~A}$ (Typ)
- Operating Temperature Range: $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$

Package
VQFN20FV4040
W (Typ) x D (Typ) x H (Max)
$4.0 \mathrm{~mm} \times 4.0 \mathrm{~mm} \times 1.0 \mathrm{~mm}$


## Typical Application Circuit



Figure 1. Application Circuit with Discharge Function (BD9P135MUF-C, BD9P155MUF-C)

Nano Pulse Control ${ }^{\text {TM }}$ is a trademark or a registered trademark of ROHM Co., Ltd.

## Typical Application Circuit - continued



Figure 2. Application Circuit without Discharge Function (BD9P135MUF-C, BD9P155MUF-C)


Figure 3. Application Circuit (BD9P105MUF-C)

Note: The difference between BD9P105MUF-C, BD9P135MUF-C and BD9P155MUF-C
The VOUT_DIS pin and discharge function are not available with BD9P105MUF-C. The FB pin is assigned on the BD9P105MUF-C and the resistors dividing the output voltage are connected. The output voltage is defined by the resistors (RFB1, R ${ }_{\text {fb2 }}$ ).
The VOUT discharge function are available with BD9P135MUF-C and BD9P155MUF-C, and connect the VOUT_DIS pin to VOUT. And connect the VOUT to the VOUT_SNS pin.


Figure 4. The difference between BD9P105MUF-C, BD9P135MUF-C and BD9P155MUF-C

## Pin Configuration



Figure 5. Pin Configuration (BD9P135MUF-C, BD9P155MUF-C)


Figure 6. Pin Configuration (BD9P105MUF-C)

Pin Description

| Pin No. | Pin Name | Function |
| :---: | :---: | :--- |
| 1,2 | PVIN | Power supply input pins that are used for the output stage of the switching <br> regulator. Connect input ceramic capacitors referring Page 33 between the <br> PGND pins and these pins. |
| 3 | N.C. | This pin is not connected to the chip. Use this as open. If this pin is used other <br> than open and adjacent pins are expected to be shorted, please confirm if there <br> is any problem with the actual application. |
| 19 | PGND | SW |
| 4,5 | EST | Vround pins for the output stage of the switching regulator. |

## Block Diagram



Figure 7. Block Diagram (BD9P105MUF-C)

## Block Diagram - continued



Figure 8. Block Diagram (BD9P135MUF-C, BD9P155MUF-C)

## Description of Blocks

- PreReg

This block is the internal power supply for TSD and VREF circuits.

- VREG

This block is the internal power supply circuit. It outputs $3.3 \mathrm{~V}(\mathrm{Typ})$ and is the power supply to the control circuit and Driver.

- TSD

This is the thermal shutdown circuit. It will shut down the device when the junction temperature ( Tj ) reaches to $175{ }^{\circ} \mathrm{C}$ (Typ) or more. When the Tj falls below the TSD threshold with hysteresis of $25^{\circ} \mathrm{C}$ (Typ), the circuits are automatically restored to normal operation.

- VREF

The VREF block generates the internal reference voltage.

- POR

The POR block is power on reset for internal logic circuit. The IC releases power on reset and starts operation with soft start when the VIN rises to 3.8 V (Typ) or more.

- UVLO REG

The UVLO block is for under voltage lockout protection. It will shut down the device when the VREG falls to 2.85 V (Typ) or less. This protection is released when VREG voltage increase to 2.95 V (Typ) or more.

- MODE

This block detects the MODE pin signal and controls switching mode. When the MODE pin is logic high level or is applied external clock, switching operation becomes forced PWM mode regardless load current. When the MODE pin is open or logic low level, switching operation changes between PWM and light load operation depending on load current.

- OSC

This block generates the clock frequency. When the clock is applied to the MODE pin, it synchronizes to external clock. Connect the SSCG pin to GND to disable Spread Spectrum function and connect the SSCG pin to the VREG pin to enable it.

- OVP

This is the output over voltage protection (OVP) circuit. When the output voltage $+7.3 \%$ (Typ) or more of the normal regulation voltage, VOUT is reduced by forced PWM switching. After output voltage falls $+4.7 \%$ (Typ) or less, the operation recovers into normal condition.

- SCP

This is the short circuit protection circuit. After soft start is completed, the switching is disabled if the output voltage falls SCP Threshold voltage or less for 0.9 ms (Typ). This short circuit protection is maintained for 30 ms (Typ) and then automatically released.

- Soft Start

This function starts up the output voltage taking 3 ms (Typ) to prevent the overshoot.

- GmAmp1

This block is an error amplifier and its inputs are the reference voltage 0.8 V (Typ) and the FB voltage.

- GmAmp2

This block sends the signal Vc which is composed of the GmAmp1 output and the current sense signal to PWM Comp.

- Clamper1

This block clamps GmAmp1 output voltage and inductor current. It works as the over current protection and LLM control current.

- Clamper2

This block clamps GmAmp2 output voltage.

- Current Sense

This block detects the amount of change in inductor current through the Low Side FET and sends a current sense signal to GmAmp2.

## Description of Blocks - continued

- PWM Comp

This block compares the output voltage of the $\mathrm{GmAmp} 2(\mathrm{Vc})$ and the saw tooth waveform $(\mathrm{Vr})$ to control the switching duty.

- Ramp

This block generates the saw tooth waveform (Vr) from the clock signal generated by OSC.

- Control Logic

This block controls switching operation and protection functions.

- Driver

This circuit drives the gates of the output FETs.

- Sleep Comp

If output/feedback voltage becomes $101.3 \%$ (Typ) or more, this block puts the device into SLEEP state. This state is released when output/feedback voltage becomes 101.0 \% (Typ) or less.

- ZX Comp

This block stops the switching by detecting reverse current of the SW current at LLM control.

- HOCP Comp

This block detects the current flowing through the High Side FET and limits the current of 2.2 A (Min) or more. This function works in abnormal situation such as the SW pin shorted to GND condition in order to prevent the High Side FET from destruction.

- Reset

When the output voltage reaches $-4.7 \%$ (Typ) or more of the normal regulation voltage, the open drain MOSFET connected to the RESET pin turns off in 3.6 ms (Typ) and the output of the RESET pin becomes high by its external pull-up resistor.
When the output voltage reaches -7.2 \% (Typ) or less, the RESET pin open drain MOSFET turns on and the RESET pin is pulled down with an impedance of $190 \Omega$ (Typ).

- Discharge

This block discharges the output voltage during EN is low and before VOUT start up. The VOUT_DIS pin is pulled down with an impedance of $75 \Omega$ (Typ).


Caution 1: Operating the IC over the absolute maximum ratings may damage the IC. The damage can either be a short circuit between pins or an open circuit between pins and the internal circuitry. Therefore, it is important to consider circuit protection measures, such as adding a fuse, in case the IC is operated over the absolute maximum ratings.
Caution 2: Should by any chance the maximum junction temperature rating be exceeded the rise in temperature of the chip may result in deterioration of the properties of the chip. In case of exceeding this absolute maximum rating, design a PCB with thermal resistance taken into consideration by increasing board size and copper area so as not to exceed the maximum junction temperature rating.
(Note 1) These voltages are guaranteed by design. Not tested.
Thermal Resistance ${ }^{\text {(Note 2) }}$

| Parameter | Symbol | Thermal Resistance (Typ) |  | Unit |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 1s ${ }^{\text {(Note 4) }}$ | $2 \mathrm{~s} 2 \mathrm{p}^{\text {(Note }}$ 5) |  |
| VQFN20FV4040 |  |  |  |  |
| Junction to Ambient | $\theta_{\text {JA }}$ | 120.0 | 38.7 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| Junction to Top Characterization Parameter ${ }^{\text {(Note 3) }}$ | $\Psi_{\text {JT }}$ | 15 | 8 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

(Note 2) Based on JESD51-2A(Still-Air).
(Note 3) The thermal characterization parameter to report the difference between junction temperature and the temperature at the top center of the outside surface of the component package.
(Note 4) Using a PCB board based on JESD51-3.
(Note 5) Using a PCB board based on JESD51-5, 7.

| Layer Number of <br> Measurement Board | Material | Board Size |
| :---: | :---: | :---: |
| Single | FR-4 | $114.3 \mathrm{~mm} \times 76.2 \mathrm{~mm} \times 1.57 \mathrm{mmt}$ |


| Top |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Copper Pattern | Thickness |  |  |  |  |
| Footprints and Traces | $70 \mu \mathrm{~m}$ |  |  |  |  |
| Layer Number of Measurement Board | Material | Board Size |  | Thermal Via ${ }^{\text {(Note 6) }}$ |  |
|  |  |  |  | Pitch | Diameter |
| 4 Layers | FR-4 | $114.3 \mathrm{~mm} \times 76.2 \mathrm{~mm} \times 1.6 \mathrm{mmt}$ |  | 1.20 mm | $\Phi 0.30 \mathrm{~mm}$ |
| Top |  | 2 Internal Layers |  | Bottom |  |
| Copper Pattern | Thickness | Copper Pattern | Thickness | Copper Pattern | Thickness |
| Footprints and Traces | $70 \mu \mathrm{~m}$ | $74.2 \mathrm{~mm} \times 74.2 \mathrm{~mm}$ | $35 \mu \mathrm{~m}$ | $74.2 \mathrm{~mm} \times 74.2 \mathrm{~mm}$ | $70 \mu \mathrm{~m}$ |

(Note 6) This thermal via connects with the copper pattern of all layers.

## Recommended Operating Conditions

| Parameter | Symbol | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Input Voltage | $\mathrm{V}_{\mathrm{VIN}}$, $\mathrm{V}_{\text {PVII }}$ | 3.5 | - | 40 | V |
| Operating Temperature | Ta | -40 | - | +125 | C |
| Output Voltage for BD9P105MUF-C ${ }^{\text {(Note 1) }}$ | Vout | 0.8 | - | 8.5 | V |
| Output Voltage for BD9P135MUF-C | Vout | - | 3.3 | - | V |
| Output Voltage for BD9P155MUF-C | Vout | - | 5.0 | - | V |
| SW Minimum ON Time ${ }^{\text {(Note 2) }}$ | tonmin | - | - | 50 | ns |
| SW Minimum OFF Time ( $\mathrm{V}_{\text {REG }}=3.3 \mathrm{~V}$ ) | toffmin | - | - | 130 | ns |
| SW Minimum OFF Time ( $\mathrm{V}_{\text {REG }}=5.0 \mathrm{~V}$ ) | toffmin | - | - | 100 | ns |
| Output Current | lout | - | - | 1 | A |
| Input Capacitor <br> (VIN Continuous Condition) (Note 3) | Cin | 2.3 | - | - | $\mu \mathrm{F}$ |
| VREG Capacitor ${ }^{(N o t e}$ 3) | Creg | 0.6 | 1.0 | 2.0 | $\mu \mathrm{F}$ |
| BST Capacitor ${ }^{(N o t e ~ 3)}$ | $\mathrm{CbSt}^{\text {b }}$ | 0.05 | 0.1 | 0.2 | $\mu \mathrm{F}$ |

(Note 1) Although the output voltage is configurable at 0.8 V and higher, it may be limited by the SW min ON pulse width For the same reason, although the output voltage is configurable at 8.5 V and more, it may be limited by the SW minimum OFF pulse width For the configurable range, please refer to the Output Voltage Setting in Selection of Components Externally Connected (page 30).
(Note 2) This parameter is for 0.5 A output. Not tested.
(Note 3) Ceramic capacitor is recommended. The capacitor value including temperature change, DC bias change, and aging change must be considered. If a bulk capacitor is used with Input ceramic capacitors, please select capacitors referring page 33.

Electrical Characteristics (Unless otherwise specified Ta $=-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$ )

| Parameter | Symbol | Min | Typ | Max | Unit | Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| General |  |  |  |  |  |  |
| Shutdown Current | Isown | - | 2.1 | 10.0 | $\mu \mathrm{A}$ | $\begin{aligned} & \mathrm{V}_{\text {EN }}=0 \mathrm{~V}, \\ & \mathrm{Ta}=-40^{\circ} \mathrm{C} \text { to }+105^{\circ} \mathrm{C} \end{aligned}$ |
| Quiescent Current from VIN | lQ_VIN1 | - | 2.1 | 6.0 | $\mu \mathrm{A}$ | $\begin{aligned} & \text { V MOde }=0 \mathrm{~V}, \mathrm{~V}_{\text {VCC }} \mathrm{EX}=5 \mathrm{~V} \\ & \mathrm{~V}_{\text {FB }}=\mathrm{V}_{\text {FB1 }} \times 1.04(\mathrm{SLEEP}) \end{aligned}$ |
|  | lQ_VIN2 | - | 15 | 30 | $\mu \mathrm{A}$ | $\begin{aligned} & V_{\text {MODE }}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{VCC}}=\mathrm{EX}=0 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{FB}}=\mathrm{V}_{\text {FB1 }} \times 1.04(\mathrm{SLEEP}) \end{aligned}$ |
|  | lQ_VIN3 | - | 33 | 66 | $\mu \mathrm{A}$ | $\mathrm{V}_{\text {mode }}=5 \mathrm{~V}, \mathrm{~V}_{\text {vcc_ex }}=5 \mathrm{~V}$ $\mathrm{V}_{\mathrm{FB}}=\mathrm{V}_{\mathrm{FB} 1} \times 1.04$ (No SLEEP) |
|  | lQ_VIN4 | - | 1200 | 2400 | $\mu \mathrm{A}$ | $\begin{aligned} & V_{\text {MODE }}=5 \mathrm{~V}, \mathrm{~V}_{\text {VCC Ex }}=0 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{FB}}=\mathrm{V}_{\mathrm{FB} 1} \times 1.04(\text { No SLEEP }) \end{aligned}$ |
| Quiescent Current from VCC_EX | lQ_vcc_Ex1 | - | 16 | 60 | $\mu \mathrm{A}$ | $\begin{aligned} & V_{\text {MODE }}=0 \mathrm{~V} \\ & V_{F B}=V_{F B 1} \times 1.04 \text { (SLEEP) } \end{aligned}$ |
|  | lQ_vcc_Ex2 | - | 1500 | 3000 | $\mu \mathrm{A}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{MODE}}=5 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{FB}}=\mathrm{V}_{\mathrm{FB} 1} \times 1.04 \text { (No SLEEP) } \end{aligned}$ |
| VIN Power On Reset Rising | VPOR_R | 3.6 | 3.8 | 4.0 | V | $V_{\text {IN }}$ Sweep Up |
| VREG Under Voltage Lockout Falling | Vuvlo_F | 2.70 | 2.85 | 3.00 | V | $V_{\text {Reg }}$ Sweep Down |
| VREG Under Voltage Lockout Rising | Vuvlo_R | 2.75 | 2.95 | 3.15 | V | $V_{\text {Reg }}$ Sweep Up |
| EN/MODE/OCP_SEL/SSCG |  |  |  |  |  |  |
| EN Input Voltage High | $V_{\text {ENH }}$ | 2.0 | - | 40 | V |  |
| EN Input Voltage Low | $V_{\text {ENL }}$ | 0 | - | 0.8 | V |  |
| EN Hysteresis Voltage | Venhys | 0.10 | 0.25 | 0.50 | V |  |
| EN Input Current | len | - | 0 | 1 | $\mu \mathrm{A}$ | $\mathrm{V}_{\mathrm{EN}}=5 \mathrm{~V}$ |
| MODE Input Voltage High | $\mathrm{V}_{\text {modeh }}$ | 2.0 | - | 5.5 | V |  |
| MODE Input Voltage Low | $\mathrm{V}_{\text {model }}$ | - | - | 0.8 | V |  |
| MODE Input Current | Imode $^{\text {a }}$ | - | 6 | 10 | $\mu \mathrm{A}$ | $\mathrm{V}_{\text {MODE }}=5 \mathrm{~V}$ |
| OCP_SEL Input Voltage High | $V_{\text {SELH }}$ | 2.0 | - | 5.5 | V |  |
| OCP_SEL Input Voltage Low | $\mathrm{V}_{\text {SELL }}$ | - | - | 0.8 | V |  |
| OCP_SEL Input Current | Isel | - | 0 | 1 | $\mu \mathrm{A}$ | Vocp_SEL $=5 \mathrm{~V}$ |
| SSCG Input Voltage High | Vsscgh | 2.0 | - | 5.5 | V |  |
| SSCG Input Voltage Low | Vsscgl | - | - | 0.8 | V |  |
| SSCG Input Current | Isscg | - | 0 | 1 | $\mu \mathrm{A}$ | $\mathrm{V}_{\text {sscg }}=5 \mathrm{~V}$ |


| Parameter | Symbol | Min | Typ | Max | Unit | Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| VREG |  |  |  |  |  |  |
| VREG Voltage | Vreg | 3.0 | 3.3 | 3.6 | V | Voltage Follower <br> $\mathrm{V}_{\text {Vcc_ex }}=0 \mathrm{~V}$ |
| VCC_EX Switch ON Resistance | Ronex | - | 6 | 12 | $\Omega$ | $V_{v c c}{ }_{\text {vex }}=5 \mathrm{~V}$ |
| VCC_EX Threshold Voltage High | $\mathrm{V}_{\text {TEXH }}$ | 2.90 | 3.05 | 3.20 | V | Vvcc_ex Sweep Up |
| VCC_EX Threshold Voltage Low | $\mathrm{V}_{\text {texl }}$ | 2.70 | 2.90 | 3.10 | V | Vvcc_ex Sweep Down |
| VCC_EX OVP Threshold Voltage High | VExovph | 5.85 | 6.20 | 6.55 | V |  |
| VCC_EX OVP Threshold Voltage Low | VExovpl | 5.65 | 6.00 | 6.35 | V |  |
| VOUT_DIS Discharge ON Resistance | RDIS | - | 75 | 150 | $\Omega$ | $\begin{aligned} & \mathrm{V}_{\text {EN }}=0 \mathrm{~V}, \\ & \text { Vout_DIS }=0.3 \mathrm{~V} \end{aligned}$ |
| VOUT Discharge Deactivate Voltage | VoIsL | 100 | 200 | 300 | mV | Vout_dis Sweep Down |
| Oscillator |  |  |  |  |  |  |
| Switching Frequency | fsw | 2.0 | 2.2 | 2.4 | MHz |  |
| Synchronization Frequency Range | $\mathrm{fsw}_{\text {_ }} \mathrm{Ex}$ | 1.8 | - | 2.4 | MHz | External Clock Input |
| Switching Frequency (Spread Spectrum) | fswssR | 1.90 | - | 2.52 | MHz | $V_{\text {sscg }}=5 \mathrm{~V}$ |
| Spread Spectrum Modulation Rate | $\Delta \mathrm{fsscg}$ | - | 4.5 | - | \% | $\mathrm{V}_{\text {Sscg }}=5 \mathrm{~V}$ |
| Spread Spectrum Modulation Cycle | tsscg_CYCLE | - | 466 | - | $\mu \mathrm{s}$ | $V_{\text {SscG }}=5 \mathrm{~V}$ |
| VREF/GmAmp |  |  |  |  |  |  |
| Feedback Reference Voltage (BD9P105MUF-C) | $\mathrm{V}_{\text {FB1 }}$ | 0.788 | 0.802 | 0.816 | V | $V_{F B}$ Voltage, PWM Mode |
| Enter SLEEP State Voltage (BD9P105MUF-C) | $V_{\text {fbi }}$ | 0.794 | 0.812 | 0.830 | V | $V_{\text {FB }}$ Rising, Light Load Mode |
| Exit SLEEP State Voltage (BD9P105MUF-C) | $V_{\text {fb3 }}$ | 0.792 | 0.810 | 0.828 | V | Vfb Falling, <br> Light Load Mode |
| Output Voltage (BD9P135MUF-C) | Vout_sns1 | 3.250 | 3.308 | 3.366 | V | Vout_sns Voltage, PWM Mode |
| Enter SLEEP State Voltage (BD9P135MUF-C) | Vout_SNS2 | 3.275 | 3.349 | 3.424 | V | Vout_sns Rising, Light Load Mode |
| Exit SLEEP State Voltage (BD9P135MUF-C) | Vout_Sns3 | 3.266 | 3.341 | 3.416 | V | Vout_SNs Falling, Light Load Mode |
| Output Voltage (BD9P155MUF-C) | Vout_sns1 | 4.925 | 5.013 | 5.100 | V | Vout_sns Voltage, PWM Mode |
| Enter SLEEP State Voltage (BD9P155MUF-C) | Vout_Sns2 | 4.963 | 5.076 | 5.188 | V | Vout_sns Rising, Light Load Mode |
| Exit SLEEP State Voltage (BD9P155MUF-C) | Vout_sns3 | 4.949 | 5.063 | 5.176 | V | Vout_SNs Falling, Light Load Mode |
| FB Input Current for BD9P105MUF-C | IfB | - | 0 | 1 | $\mu \mathrm{A}$ | $\mathrm{V}_{\mathrm{FB}}=5 \mathrm{~V}$ |
| VOUT_SNS Input Current | Ivout_sns | - | 0.5 | 2.0 | $\mu \mathrm{A}$ | Vout_SNS $=5 \mathrm{~V}$ |
| Start Delay Time | toly | - | 400 | 800 | $\mu \mathrm{s}$ |  |
| Soft Start Time | tss | 2.5 | 3.0 | 3.9 | ms | $\mathrm{V}_{\text {FB1 }} \times 0.1$ to $\mathrm{V}_{\text {FB1 }} \times 0.9$ |
| Driver |  |  |  |  |  |  |
| High Side FET ON Resistance | Ronh | - | 200 | 440 | $\mathrm{m} \Omega$ | $\mathrm{V}_{\text {BST }}-\mathrm{V}_{\text {SW }}=3.3 \mathrm{~V}$ |
| Low Side FET ON Resistance | Ronl | - | 130 | 290 | $m \Omega$ | Vvcc_ex $=3.3 \mathrm{~V}$ |
| High Side FET Leakage Current | ILKH | -10 | 0 | - | $\mu \mathrm{A}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=40 \mathrm{~V}, \mathrm{~V}_{\mathrm{EN}}=0 \mathrm{~V}, \\ & \mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{~V}_{\mathrm{SW}}=0 \mathrm{~V} \end{aligned}$ |
| Low Side FET Leakage Current | ILkL | - | 0 | 10 | $\mu \mathrm{A}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=40 \mathrm{~V}, \mathrm{~V}_{\text {EN }}=0 \mathrm{~V}, \\ & \mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{~V}_{\mathrm{SW}}=40^{\mathrm{V}} \end{aligned}$ |
| Over Current Protection Threshold | locp10 | 1.000 | 1.250 | 1.500 | A | Vocp_SEL $=5 \mathrm{~V}$ |
|  | locpo5 | 0.500 | 0.625 | 0.750 | A | Vocp_SEL $=0 \mathrm{~V}$ |

Electrical Characteristics - continued (Unless otherwise specified Ta $=-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$ )

| Parameter |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Symbol | Min | Typ | Max | Unit | Conditions |
| Reset |  |  |  |  |  |  |
| Reset Threshold Voltage Low (BD9P105MUF-C) | VRTL | 0.718 | 0.744 | 0.770 | V | $V_{\text {FB }}$ Sweep Down |
| Reset Threshold Voltage Low (BD9P135MUF-C) |  | 3.000 | 3.065 | 3.130 | V | Vout_sns Sweep Down |
| Reset Threshold Voltage Low (BD9P155MUF-C) |  | 4.550 | 4.650 | 4.750 | V |  |
| Reset Threshold Voltage High (BD9P105MUF-C) | VRth | 0.738 | 0.764 | 0.790 | V | $V_{\text {FB }}$ Sweep Up |
| Reset Threshold Voltage High (BD9P135MUF-C) |  | 3.08 | 3.16 | 3.24 | V | Vout_sns Sweep Up |
| Reset Threshold Voltage High (BD9P155MUF-C) |  | 4.66 | 4.78 | 4.90 | V |  |
| Reset Leakage Current | Irstlk | - | 0 | 1 | $\mu \mathrm{A}$ | $\begin{aligned} & V_{\text {RESET }}=5.0 \mathrm{~V}, \\ & \mathrm{~V}_{\mathrm{FB}}=0.8 \mathrm{~V} \end{aligned}$ |
| Reset ON Resistance | Rrst | - | 190 | 400 | $\Omega$ | $\begin{aligned} & V_{I N}=2 \mathrm{~V}, \mathrm{~V}_{\text {EN }}=0 \mathrm{~V} \\ & \mathrm{I}_{\text {RESET }}=1 \mathrm{~mA} \end{aligned}$ |
| Reset Active Time | trstnact | 2.0 | 3.6 | 5.0 | ms |  |
| Reset Filtering Time | trstnfilt | 1 | 5 | 10 | $\mu \mathrm{s}$ |  |
| OVP/SCP |  |  |  |  |  |  |
| FB OVP Threshold Voltage High (BD9P105MUF-C) | Vovph | 0.825 | 0.860 | 0.895 | V | $V_{\text {Fb }}$ Sweep Up |
| FB OVP Threshold Voltage Low (BD9P105MUF-C) | Vovpl | 0.805 | 0.840 | 0.875 | V | $V_{\text {fb }}$ Sweep Down |
| VOUT_SNS OVP Threshold Voltage High (BD9P105MUF-C) | Vsnsovph | 9.0 | 9.5 | 10.0 | V | Vout_sns Sweep Up |
| VOUT_SNS OVP Threshold Voltage High (BD9 $\overline{\mathrm{P}} 135 \mathrm{MUF}$-C) |  | 3.402 | 3.541 | 3.693 | V |  |
| VOUT_SNS OVP Threshold Voltage High (BD9P155MUF-C) |  | 5.156 | 5.379 | 5.595 | V |  |
| VOUT_SNS OVP Threshold Voltage Low (BD9P105MUF-C) | Vsnsovpl | 8.5 | 9.0 | 9.5 | V | Vout_sns Sweep Down |
| VOUT_SNS OVP Threshold Voltage Low (BD9P135MUF-C) |  | 3.321 | 3.455 | 3.609 | V |  |
| VOUT_SNS OVP Threshold Voltage Low (BD9P155MUF-C) |  | 5.033 | 5.249 | 5.467 | V |  |
| SCP Threshold Voltage High (BD9P105MUF-C) | VscPr | 0.68 | 0.72 | 0.76 | V | $V_{\text {Fb }}$ Sweep Up |
| SCP Threshold Voltage High <br> (BD9P135MUF-C) |  | 2.81 | 2.97 | 3.14 | V | Vout_sns Sweep Up |
| SCP Threshold Voltage High (BD9P155MUF-C) |  | 4.25 | 4.50 | 4.75 | V |  |
| SCP Threshold Voltage Low (BD9P105MUF-C) | VscPL | 0.60 | 0.64 | 0.68 | V | $V_{\text {Fb }}$ Sweep Down |
| SCP Threshold Voltage Low (BD9P135MUF-C) |  | 2.48 | 2.64 | 2.81 | V | Vout_sns Sweep Down |
| SCP Threshold Voltage Low (BD9P155MUF-C) |  | 3.75 | 4.00 | 4.25 | V |  |
| SCP Deactivate Rate of VIN/VOUT_SNS | VscP_dACT | 1.20 | 1.33 | 1.45 | V/V | SCP function is deactivated this value or less |

## Typical Performance Curves



Figure 9. Shutdown Current vs Input Voltage


Figure 11. Output Voltage vs Temperature (BD9P135MUF-C)


Figure 10. Feedback Reference Voltage vs Temperature (BD9P105MUF-C)


Figure 12. Output Voltage vs Temperature (BD9P155MUF-C)

Typical Performance Curves - continued


Figure 13. VIN Power On Reset Rising vs Temperature


Figure 15. EN Input Voltage vs Temperature


Figure 14. VREG Under Voltage Lockout vs Temperature


Figure 16. EN Input Current vs EN Voltage

Typical Performance Curves - continued


Figure 17. MODE, OCP_SEL, SSCG Input Voltage vs Temperature


Figure 19. Switching Frequency vs Temperature


Figure 18. MODE, OCP_SEL, SSCG Input Current vs MODE, OCP_SEL, SSCG Voltage


Figure 20. Over Current Protection Threshold vs Temperature

Typical Performance Curves - continued


Figure 21. High Side FET ON Resistance vs Temperature


Figure 23. Reset Threshold Voltage vs Temperature (BD9P105MUF-C)


Figure 22. Low Side FET ON Resistance vs Temperature


Figure 24. Reset Threshold Voltage vs Temperature (BD9P135MUF-C)

Typical Performance Curves - continued


Figure 25. Reset Threshold Voltage vs Temperature (BD9P155MUF-C)


Figure 27. VOUT_SNS OVP Threshold Voltage vs Temperature (BD9P105MUF-C)


Figure 26. FB OVP Threshold Voltage vs Temperature (BD9P105MUF-C)


Figure 28. VOUT_SNS OVP Threshold Voltage vs Temperature
(BD9P135MUF-C/BD9P155MUF-C)

## Function Explanation

1. Nano Pulse Control ${ }^{\text {TM }}$

Nano Pulse Control ${ }^{T M}$ is an original technology developed by ROHM Co., Ltd. It enables to control voltage stably, which is difficult in the conventional technology, even in a narrow SW ON time such as less than 50 ns at typical condition. Narrow SW ON Pulse enables direct convert of high input voltage to low output voltage. The output voltage Vout 3.3 V can be output directly from the supply voltage $\mathrm{V}_{\mathrm{in}} 24 \mathrm{~V}$ at 2.2 MHz .


Figure 29. Switching Waveform ( $\mathrm{V}_{\mathrm{IN}}=24 \mathrm{~V}$, Vout $=3.3 \mathrm{~V}$, lout $\left.=0.5 \mathrm{~A}, \mathrm{fsw}=2.2 \mathrm{MHz}\right)$
2. Light Load Mode Control and Forced PWM Mode Control

BD9P1x5MUF-C is a synchronous DC/DC converter with integrated POWER MOSFETs and realizes high transient response by using current mode Pulse Width Modulation (PWM) mode control architecture. Under a heavy load, the switching operation is performed with the PWM mode control at a fixed frequency. When the load is lighter, the operation is changed over to the Light Load Mode (LLM) control to improve the efficiency.


Figure 30. Efficiency (Light Load Mode, PWM Mode)
2. Light Load Mode control and Forced PWM Mode control - continued If the output load decreases below 200 mA (Typ) (OCP_SEL = H), the output voltage rises and power state is changed to SLEEP state when the output voltage exceeds to $\bar{V}_{\text {FB2 }}$ ( $101.3 \%$ of its setting voltage $\mathrm{V}_{\mathrm{FB} 1}$ ). During SLEEP state, switching operation is stopped and the circuit current is reduced by stopping the circuit operation except for the monitor circuit of output voltage monitor. Then, the switching operation restarts when the output voltage decreases less than $\mathrm{V}_{\text {FB3 }}$ ( 101.0 \% of its setting voltage $\mathrm{V}_{\mathrm{FB} 1}$ ) by the load current.
If the light load mode operation is not required, the IC operates in forced PWM mode by applying high voltage or an external clock to the MODE pin. In forced PWM mode, the IC operates with fixed frequency regardless of the output load and the ripple voltage of output can be reduced. Also, during soft start time, the IC operates in forced PWM mode regardless of the condition of the MODE pin. After detecting RESET high, the IC operates according to the MODE pin condition.
If OCP_SEL set low level, then the threshold current of switched between PWM mode and LLM is changed to 100 mA (Typ).
In addition, good EMI performance in AM band may not be provided by a load condition in LLM. To avoid this, use Forced PWM mode.


Figure 31. Timing Chart in Light Load Mode (OCP_SEL = H)


Figure 32. Timing Chart in Light Load Mode after Detecting RESET High (OCP_SEL = H)

## Function Explanation - continued

3. Enable Control

The device shutdown can be controlled by the EN pin. When VEN reaches VENH ( 2.0 V ) or higher, the internal circuit is activated. When the VOUT_DIS pin is connected to output voltage and the EN pin is low, the VOUT_DIS pin is pulled down by the resistance of $\bar{R}_{\text {DIS }}(75 \Omega, T y p)$ and discharges the output voltage. This discharge function is deactivated when VOUT_DIS voltage falls below VoIsL ( 200 mV , Typ) at once or 30 ms (Typ) pass after the EN pin becomes high. After being deactivated, the VOUT starts up with soft start operation. The delay time toly ( $400 \mu \mathrm{~s}$, Typ) is implemented from the EN pin becoming high to VOUT starting up regardless of VOUT_DIS voltage. The soft start time (Vout x 0.1 to Vout $x 0.9$ ) is set to tss ( 3.0 ms , Typ). When an EN voltage becomes $\mathrm{V}_{\text {ENL }}(0.8 \mathrm{~V}$ ) or less, the device is shut down. When discharge function is not required, connect the VOUT_DIS pin to GND.
The discharge function is available with only BD9P135MUF-C and BD9P155MUF-C.


Figure 33. Enable ON/OFF Timing Chart
4. Reset Function

For BD9P105MUF-C, the reset function monitors the FB pin voltage. When the output voltage reaches $\mathrm{V}_{\text {RTH }}$ (95.3 \%, Typ) or more of the normal regulation voltage, the open drain MOSFET on the RESET pin is turned off in trstnact (3.6 $\mathrm{ms}, \mathrm{Typ}$ ) and the output of the RESET pin becomes high by its pull-up resistor. In addition, when the FB voltage reaches $V_{\text {RTL }}$ ( 92.8 \%, Typ) or less, the open drain MOSFET on the RESET pin is turned on and the RESET pin is pulled down with an impedance of Rrst ( $190 \Omega$, Typ). To reject noise, the filtering time trstnfilt ( $5 \mu \mathrm{~s}, \mathrm{Typ}$ ) is implemented after FB voltage decreases below its threshold voltage ( $\mathrm{V}_{\mathrm{RTL}}$ ).
The reset function also works when output over voltage is detected. When the output voltage reaches Vovph ( $107.3 \%$, Typ) or more, the open drain MOSFET on the RESET pin is turned on. Then, when the FB voltage goes below VovpL ( $104.7 \%$, Typ) or less, the open drain MOSFET on the RESET pin is turned off. The reset active time and filtering time are activated when over voltage conditions are detected.
For BD9P135MUF-C and BD9P155MUF-C, this function monitors the VOUT_SNS pin voltage.
The RESET output voltage low level (VRESET_Low(Max)) when the open drain MOSFET is turned on is calculated by the following equation. It is recommended to use resistance of $5 \mathrm{k} \Omega$ to $100 \mathrm{k} \Omega$ and pull it up to the VREG pin or the power supply in the absolute maximum voltage ratings of the RESET pin.
During shutdown condition, the RESET pin is pulled down regardless the output voltage as far as $\mathrm{V}_{\mathrm{IN}}$ is 2 V or higher.


Figure 34. Reset Timing Chart (BD9P105MUF-C)

$$
V_{R E S E T_{-} L O W(M a x)}=V_{P U L L-U P} \times \frac{R_{R S T(M a x)}}{R_{R S T(M a x)}+R_{P U L L-U P}}[\mathrm{~V}]
$$

Where:

$$
\begin{aligned}
& V_{\text {RESET_LOW(Max) }} \\
& V_{P U L L-U P}
\end{aligned}
$$

$$
\left.R_{R S T \text { (Max) }} \quad \text { is the RESET ON Resistance (Max) [ } \Omega\right]
$$

$$
R_{P U L L-U P} \quad \text { is the value of pull-up resistor to } V_{\text {PULL_UP }}[\Omega]
$$

## Function Explanation - continued

5. External Synchronization Function

By applying clock signal to the MODE pin, the switching frequency can be synchronized to the external clock signal. When clock signal is applied with the synchronization frequency range between 1.8 MHz and 2.4 MHz and the duty range between $25 \%$ and $75 \%$, the Synchronous mode is started after 4 rising edges of the clock signal. In addition, this function is enabled after $V_{\text {RESET }}$ becomes high. If the duration between each rising edge exceeds $0.9 \mu \mathrm{~s}$ (Typ) or more, the Synchronous mode is deactivated and switching operation by internal clock is activated (the Non-Synchronous mode). The Spread Spectrum function cannot be activated during the Synchronous mode.


Figure 35. External Synchronization Function

## Function Explanation - continued

6. Frequency Division Function

This device drives the High Side FET with a bootstrap and requires the ON time of the Low Side FET to charge the BST pin. Therefore, the minimum OFF time of the SW pin is specified, and the output voltage is limited by the minimum OFF time under the condition in which the voltage between input and output are close. To prevent this situation, OFF pulses are skipped when the voltage between input and output are small to keep the High Side FET turned on and increase the ON duty of the SW pin. The OFF pulse skip is done for 7 consecutive switching cycles in maximum (The switching frequency becomes a one eighth of nominal frequency). In this case, the output voltage can be calculated with the following equation.

$$
\begin{aligned}
& V_{\text {OUT }}=\text { MaxDuty } \times\left(V_{\text {IN }}-R_{\text {ONH }} \times I_{\text {OUT }}\right)-R_{D C} \times I_{\text {OUT }} \\
& =\left(1-t_{\text {OFFMIN }} \times \frac{f_{\text {SW }}}{8}\right) \times\left(V_{I N}-R_{\text {ONH }} \times I_{\text {OUT }}\right)-R_{D C} \times I_{\text {OUT }}[\mathrm{V}]
\end{aligned}
$$

Where:

| MaxDuty | is the SW pin Maximum ON Duty Cycle [\%] |  |
| :--- | :--- | :--- |
| $V_{I N}$ | is the Input Voltage [V] |  |
| $R_{\text {ONH }}$ | is the High Side FET ON Resistance $[\Omega]$ | (Refer to page 11) |
| $I_{\text {OUT }}$ | is the Output Current $[\mathrm{A}]$ |  |
| $R_{D C}$ | is the DCR of Inductor [ $\Omega$ |  |
| $t_{\text {OFFMIN }}$ | is the SW pin Minimum OFF Time [s] | (Refer to page 10) |
| $f_{S W}$ | is the Switching Frequency $[\mathrm{Hz}]$ | Refer to page 11) |



Figure 36. Frequency Division Function

## Function Explanation - continued

7. Spread Spectrum Function

Connecting the SSCG pin with the VREG pin activates the Spread Spectrum function, reducing the EMI noise level. When the Spread Spectrum function is activated, the switching frequency is varied with triangular wave of $\Delta \mathrm{fsscg}$
 tsscg_cycle ( $466 \mu \mathrm{~s}$, Typ). However, this function is masked when the RESET output is low. Connecting the SSCG pin with GND deactivates this function.


Figure 37. Spread Spectrum Function

## Function Explanation - continued

8. VCC_EX Function

This IC has the function that supplies power from VOUT to internal supply VREG to improve the efficiency. When Vvcc_ex goes above $V_{\text {texh }}\left(3.05 \mathrm{~V}\right.$, Typ) or more, $\mathrm{V}_{\text {reg }}$ is supplied from the VCC_EX pin. In case of the VCC_EX pin connected with VOUT, the output voltage is used as a power supply for the internal circuitry and driver block. To protect the internal circuit, VOUT is reduced with PWM switching when VCC_EX voltage exceeds $\mathrm{V}_{\text {Exovph }}$ ( 6.0 V , Typ). Therefore, the VCC_EX pin connection can be used when the output voltage is in the range of between $\mathrm{V}_{\text {TEXH }}(3.2 \mathrm{~V}$, Max) and VExovpl ( 5.65 V , Min). Connect the VCC_EX pin with GND when VCC_EX function is not required.
The bias current IBIAS using VCC_EX function can be calculated using the following formula.

$$
I_{B I A S}=I_{Q_{-} V I N 1}+I_{Q_{-} V C C_{-} E X 1} \times \frac{1}{\eta} \times \frac{V_{V C C_{-} E X}}{V_{I N}}[\mu \mathrm{~A}]
$$

Where:

| $I_{B I A S}$ | is total current from VIN $[\mu \mathrm{A}]$ |  |
| :--- | :--- | :--- |
| $I_{Q_{-} V I N 1}$ | is quiescent current from VIN (without current from VCC_EX) $[\mu \mathrm{A}]$ | (Refer to page 10) <br> $I_{Q_{-} V C C \_E X 1}$ |
| $\eta^{\text {is quiescent current from VCC_EX }[\mu \mathrm{A}]}$ | $\left.\begin{array}{l}\text { (Refer to page 10 }\end{array}\right)$ |  |
| $V_{V C C-E X}$ | is efficiency of Buck Converter | is the VCC_EX voltage $[\mathrm{V}]$ |
| $V_{I N}$ | is the input voltage $[\mathrm{V}]$ |  |



Figure 39. VCC_EX Timing Chart

## Protect Function

1. Over Current Protection (OCP)

The Over Current Protection (OCP) monitors the average inductor current. The OCP detection level can be selected by the OCP_SEL pin. When the OCP_SEL voltage is high, it is locP10 ( $1.250 \mathrm{~A}, \mathrm{Typ}$ ) and when the OCP_SEL voltage is low, it is locpo5 ( 0.625 A, Typ). When the average inductor current exceeds to its setting value, the duty cycle of the switching is limited and the output voltage decreases. This protection circuit is effective in preventing damage due to sudden and unexpected incidents. However, the IC should never be used in applications where the protection circuit operates continuously (e.g. when a load that significantly exceeds the output current capability of the chip is connected).


Figure 40. Over Current Protection
2. Short Circuit Protection (SCP)

For BD9P105MUF-C, the Short Circuit Protection (SCP) block compares the FB pin voltage with the internal reference voltage VREF. When the FB pin voltage has decreased to Vscpl ( 0.64 V , Typ) or less and remained there for 0.9 ms (Typ), SCP stops the operation for 30 ms (Typ) and subsequently initiates a restart. If the FB pin voltage decreases to Vscpl ( 0.64 V , Typ) or less and increases to $\mathrm{V}_{\text {scpe }}(0.72 \mathrm{~V}$, Typ) or more within 0.9 ms afterwards, SCP protection is released and output voltage recovers to normal operation. For BD9P135MUF-C and BD9P155MUF-C, the SCP block monitors the VOUT_SNS pin for the protection. SCP detection voltage VSCPL is $80 \%$ (Typ) of normal output voltage. On the other hand, SCP release voltage $\mathrm{V}_{\text {scPh }}$ is $90 \%$ (Typ) of normal output voltage.
The SCP function is deactivated during 7 ms (Typ) from VOUT starting up. In addition, when VIN decreases and VOUT also decreases, the SCP function is deactivated not to detect short circuit protection. The SCP function is likewise deactivated when VIN voltage is lower than Vscp_DACT ( $133 \%$, Typ) of the VOUT_SNS pin voltage, and then is activated after 7 ms (Typ) from VIN voltage exceeds VscP_DACT ( $133 \%$, Typ) of the VOUT_SNS pin voltage. Therefore, in the case of short circuit from VIN close to VOUT condition, SCP stops the switching operation after 7.9 ms (Typ) from short circuit. However, the device should never be used in applications characterized by continuous operation of the protection circuit (e.g. when a load that significantly exceeds the output current capability of the chip is connected).


Figure 41. Short Circuit Protection (SCP) Timing Chart (BD9P105MUF-C)

## Protect Function - continued

3. Power On Reset (POR)/Under Voltage Lockout Protection (UVLO)

The UVLO and POR are integrated to prevent the malfunction when the power supply voltage is decreased. The POR monitors the VIN pin voltage. On the other hand, UVLO monitors the VREG pin voltage.
In the sequence of VIN rising, the VREG pin voltage also rises up to 3.3 V (Typ) following VIN voltage. First, UVLO is released when VREG voltage increase above Vuvlo_r ( 2.95 V , Typ). Next, POR is released when VIN voltage increase above $\mathrm{V}_{\text {POR_R }}(3.8 \mathrm{~V}$, Typ). When both POR and UVLO are released, the IC starts up with soft start.
In the sequence of VIN falling, VREG voltage also falls. When VREG voltage decreases below Vuvlo_f ( $2.85 \mathrm{~V}, \mathrm{Typ}$ ), UVLO is detected and puts the IC goes into standby state. At the same time, POR is detected. When the VCC_EX pin is connected to VOUT, VREG voltage supplied from VCC_EX. In this case, drop voltage between VIN and VREG becomes larger than the case of VCC_EX connected to GND because VOUT voltage is restricted by maximum duty at low VIN condition. Therefore, UVLO is detected at higher VIN condition than the case when the VCC_EX pin is connected to GND.


Figure 42. POR/UVLO Timing Chart

## Protect Function - continued

4. Thermal Shutdown (TSD)

This IC has a built-in thermal shutdown circuit that prevents heat damage to the IC. If junction temperature ( Tj ) exceeds TSD detection temperature ( $175^{\circ} \mathrm{C}$, Typ), the POWER MOSFETs are turned off. When the Tj falls below the TSD temperature ( $150^{\circ} \mathrm{C}$, Typ), the IC restarts up with soft start. Where the input voltage required for the restart is the same as that for the initial startup (Input voltage 4.0 V or more). Note that the TSD circuit operates in a situation that exceeds the absolute maximum ratings and therefore, under no circumstances, should the TSD circuit be used in a set design or for any purpose other than protecting the IC from heat damage.


Figure 43. TSD Timing Chart

## Protect Function - continued

5. Over Voltage Protection (OVP)

This IC has Over Voltage Protection (OVP) monitoring FB to prevent the increase of output voltage in case of external injected current to VOUT. When FB voltage exceeds $\mathrm{V}_{\text {OVPH }}$ ( $107.3 \%$ of its setting voltage $\mathrm{V}_{\text {FB1 }}$ ), the switching regulator sinks current from VOUT by changing state to PWM. The sink current during OVP is restricted to $I_{\mathrm{NCP}}$ ( $0.625 \mathrm{~A}, \mathrm{Typ}$ ) (OCP_SEL = L). In addition, the RESET pin is pulled down to GND during OVP detection. To prevent the malfunction by noise, the internal delay trstnfilt of $5 \mu \mathrm{~s}$ (Typ) is implemented after OVP detection. When FB voltage falls below VovpL ( 104.7 \% of its setting voltage $V_{\text {FB1 }}$ ), OVP function is released. The RESET pin is kept low and PWM switching is also kept during trstnact ( 3.6 ms , Typ) after OVP function is released. When OCP_SEL is set high level, then Incp value is changed to $I_{\text {NCP }}(1.250 \mathrm{~A}$, Typ).
If the FB pin is open, this IC cannot regulate VOUT correctly. In this case, if VOUT voltage exceeds Vsnsovph or VCC_EX voltage exceed $\mathrm{V}_{\text {Exovph, }}$, the VOUT is pulled down by PWM switching to protect internal devices same as the situation that the FB pin over voltage is detected.


Figure 44. FB OVP Timing Chart

5. Over Voltage Protection (OVP) - continued

If VOUT is shorted to the Battery Line as following figure, the DC/DC converter (BD9P1x5MUF-C) sinks current from VOUT to the Low Side FET. If a Reverse Polarity Protection Diode is on the Battery Line, the VIN voltage results in being boosted up and might exceed the absolute maximum ratings.


Figure 46. VOUT shorted to Battery Line

## Selection of Components Externally Connected

## Contact us if not use the recommended constant in the application circuit.

Necessary parameters in designing the power supply are as follows:
Table 1. Application Sample Specification

| Parameter | Symbol | Specification Case |
| :--- | :---: | :---: |
| Input Voltage | $\mathrm{V}_{\mathrm{IN}}$ | 3.5 V to 40 V |
| Output Voltage | $\mathrm{V}_{\text {out }}$ | 5.0 V |
| Output Ripple Voltage | $\Delta \mathrm{V}_{\mathrm{P}-\mathrm{P}}$ | 20 mV V-p |
| Output Current | Iout | $\mathrm{Typ} 0.5 \mathrm{~A} / \mathrm{Max} 1.0 \mathrm{~A}$ |
| Switching Frequency | fsw | 2.2 MHz |
| Operating Temperature Range | Ta | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |



Figure 47. Application Sample Circuit

## Selection of Components Externally Connected - continued

1. Selection of the inductor $L_{1}$ value

The inductor in the switching regulator supplies a continuous current to the load and functions as a filter to smooth the output voltage. When a large inductor is selected, the Inductor ripple current $\Delta \mathrm{I}$ L and the output voltage ripple $\Delta \mathrm{V}_{\mathrm{P}-\mathrm{P}}$ are reduced. It is the trade-off between the size and the cost of the inductor.

The inductance of the inductor is shown by the following equation:

$$
L=\frac{\left(V_{I N(\text { Max })}-V_{\text {OUT }}\right) \times V_{\text {OUT }}}{V_{\text {IN }(\text { Max })} \times f_{S W} \times \Delta I_{L}}[\mathrm{H}]
$$

Where:
$V_{\text {IN(Max) }}$ is the input voltage (Max) [V]
$V_{\text {OUT }} \quad$ is the output voltage [V]
$f_{S W} \quad$ is the switching frequency [Hz]
$\Delta I_{L} \quad$ is the peak to peak inductor current [A]
In current mode control, the sub-harmonic oscillation may happen. The slope compensation is integrated into the IC to prevent the sub-harmonic oscillation. The sub-harmonic oscillation depends on the rate of increase of output switch current. If the inductor value is too small, the sub-harmonic oscillation may happen because the inductor ripple current $\Delta L_{L}$ is increased. If the inductor value is too large, the feedback loop may not achieve stability because the inductor ripple current $\Delta_{L}$ is decreased. Therefore, the recommended inductor value range for each output current is shown below.

Table 2. Inductor range of each output current

| Output Voltage | OCP_SEL | Maximum Output Current | Inductor Range |
| :---: | :---: | :---: | :---: |
| 1.1 V to 8.5 V | H | 1.0 A | $4.7 \mu \mathrm{H}$ to $15 \mu \mathrm{H}$ |
|  | L | 0.5 A | $4.7 \mu \mathrm{H}$ to $15 \mu \mathrm{H}$ |
| 0.8 V to 1.1 V | H | 1.0 A | $10 \mu \mathrm{H}$ to $15 \mu \mathrm{H}$ |
|  | L | 0.5 A | $10 \mu \mathrm{H}$ to $15 \mu \mathrm{H}$ |

If the $\Delta \mathrm{IL}$ becomes small, the Inductor core loss (iron loss), the loss due to ESR of the output capacitor and the $\Delta \mathrm{V}_{\mathrm{p}-\mathrm{p}}$ (Output peak-to-peak ripple voltage) are also reduced. $\Delta \mathrm{V}_{\mathrm{P}-\mathrm{P}}$ is shown in the following equation.

$$
\begin{equation*}
\Delta V_{P-P}=\Delta I_{L} \times E S R+\frac{\Delta I_{L}}{8 \times C_{O U T} \times f_{S W}}[\mathrm{~V}] \tag{a}
\end{equation*}
$$

Where:
$E S R \quad$ is the equivalent series resistance of the output capacitor [ $\Omega$ ]
$C_{O U T} \quad$ is the output capacitance [F]
$\Delta I_{L} \quad$ is the peak to peak inductor current [A]
$f_{S W} \quad$ is the switching frequency $[\mathrm{Hz}]$
Even if $\Delta l_{L}$ is large, the $\Delta V_{P-P}$ target is usually satisfied by using a ceramic capacitor because it has a low ESR.
The advantage of this is that the inductance value can be set smaller. It also contributes to the miniaturization of the application board because when the inductance value is small, the inductor that has large rated current and is small can be selected.
The disadvantages are increase of core losses in the inductor.
The shielded type (closed magnetic circuit type) is the recommended type of inductor to be used. It is important not to magnetic saturate the core in any situation, so please make sure that the definition of rated current is different according to the manufactures. Please check the rated current at maximum ambient temperature of application to inductor manufacturer.

## Selection of Components Externally Connected - continued

2. Selection of Output Capacitor Cout

The output capacitor is selected based on the ESR that is required from the previous page equation (a). $\Delta \mathrm{V}_{\mathrm{p}-\mathrm{p}}$ can be reduced by using a capacitor with a small ESR.

The ceramic capacitor is the best option that meets this requirement. It is because not only it has a small ESR but the ceramic capacitor also contributes to the size reduction of the application circuit. Please confirm the frequency characteristics of ESR from the datasheet of the capacitor manufacturer, and consider a low ESR value for the switching frequency being used. It is necessary to consider that the capacitance of the ceramic capacitor changes obviously according to DC biasing characteristic. For the voltage rating of the ceramic capacitor, twice or more the maximum output voltage is usually required. By selecting a high voltage rating, it is possible to reduce the influence of DC bias characteristics. Moreover, in order to maintain good temperature characteristics, the one with the characteristics of X7R or better is recommended. Because the voltage rating of a large ceramic capacitor is low, the selection becomes difficult for an application with high output voltage. In that case, please connect multiple ceramic capacitors.

These capacitors are rated in ripple current. The RMS values of the ripple current that can be obtained in the following equation and must not exceed the ripple current rating.

$$
I_{\text {COUT }(R M S)}=\frac{\Delta I_{L}}{\sqrt{12}}[\mathrm{~A}]
$$

Where:

$$
\begin{array}{ll}
I_{\text {COUT (RMS) }} & \text { is the value of the ripple electric current }[\mathrm{A}] \\
\Delta I_{L} & \text { is the peak to peak inductor current }[\mathrm{A}]
\end{array}
$$

Next, when the output setting voltage is 3.3 V or more, the output ceramic capacitor Cout is recommended for $22 \mu \mathrm{~F}$ (Typ) or more. When the output setting voltage less than 3.3 V , the output ceramic capacitor Cout is recommended to the following equation.

$$
C_{\text {OUT }} \geq \frac{72.6}{V_{\text {OUT }}}[\mu \mathrm{F}]
$$

Where:

$$
V_{\text {OUT }} \quad \text { is the output voltage }[\mathrm{V}]
$$

When selecting the capacitor ensure that the capacitance Cout_worst of the following equation is maintained at the characteristics of DC Bias, AC Voltage, temperature and tolerance. The approximate value can be calculated by this formula.

$$
C_{\text {OUT_WORST }} \geq \frac{54.5}{V_{\text {OUT }}}[\mu \mathrm{F}]
$$

Where:

$$
V_{\text {OUT }} \quad \text { is the output voltage [V] }
$$

If the capacitance falls below this value, the oscillation may happen. When using the electrolytic capacitor and the conductive polymer hybrid aluminum electrolytic capacitor, please place it in addition to the ceramic capacitors with the capacity described above. Actually, the changes in the frequency characteristic are greatly affected by the type and the condition (temperature, etc.) of parts that are used, the wire routing and layout of the PCB. Please confirm stability and responsiveness in actual application.

In addition, for the total value of capacitance in the output line Cout(Max), please choose a capacitance value less than the value obtained by the following equation:

$$
C_{\text {OUT }(\text { Max })}<\frac{t_{\text {SS(Min })} \times 1.25 \times\left(I_{\text {OCP }(\text { Min })}-I_{\text {OUT_START }(\text { Max })}\right)}{}[\mathrm{F}]
$$

## Where:

$$
\begin{array}{ll}
I_{\text {OCP(Min) }} & \text { is the OCP operation current (Min) }[\mathrm{A}] \\
t_{\text {SS(Min) }} & \text { is the Soft Start Time }(\mathrm{Min})[\mathrm{s}] \\
I_{\text {OUT_START }} \text { (Max) } & \text { is the maximum load current during startup [A] } \\
V_{\text {OUT }} & \text { is the output voltage }[\mathrm{V}]
\end{array}
$$

If the limits from the above-mentioned are exceeded, Startup failure may happen in 7.9 ms after VOUT starts up. If the capacitance value is extremely large, over-current protection may be activated by the inrush current at startup preventing the output to turn on. Please confirm this on the actual application.
Also, in case of large changing input voltage and load current, select the capacitance by verifying that the actual application setup meets the required specification.

## Selection of Components Externally Connected - continued

3. Selection of Input Capacitor $\mathrm{C}_{\mathrm{IN}}, \mathrm{C}_{\text {вLк }}$

For input capacitors, there are two types of capacitor: decoupling capacitors $\mathrm{C}_{\mathrm{In}}$ and bulk capacitors Cblк.
Ceramic capacitors with total values $2.3 \mu \mathrm{~F}$ or more are necessary for the decoupling capacitors $\mathrm{C}_{\mathrm{IN}}$ for ripple noise reduction. If a low ESR electrolytic capacitor with large capacitance is connected parallel to the decoupling capacitors as a bulk capacitor, ceramic capacitors with $0.5 \mu \mathrm{~F}$ or more are necessary for the decoupling capacitors. (However, to reduce EMI noise level, $2.3 \mu \mathrm{~F}$ or more are recommended for ceramic capacitors.) These capacitor values including device variation, temperature characteristics, DC bias characteristics, and aging change must be larger than minimum value. It is effective for switching noise reduction to place one of ceramic capacitor close to the PVIN and the VIN pins. The voltage rating of the capacitors is recommended to be 1.2 times or more the maximum input voltage, or twice the normal input voltage. Also, the IC might not operate properly when the PCB layout or the position of the capacitor is not good. Please check "PCB Layout Design" on page 48.

The bulk capacitor is optional. The bulk capacitor prevents the decrease in the line voltage and serves as a backup power supply to keep the input voltage constant. A low ESR electrolytic capacitor with large capacitance is suitable for the bulk capacitor. It is necessary to select the best capacitance value for each of application. In that case, please take note not to exceed the rated ripple current of the capacitor.

The RMS value of the input ripple current $\operatorname{ICIN(RMS)}$ is obtained in the following equation:

$$
I_{C I N(R M S)}=\sqrt{\frac{V_{\text {OUT }}}{V_{I N}}\left\{I_{\text {OUT }(\text { Max }}{ }^{2}\left(1-\frac{V_{\text {OUT }}}{V_{I N}}\right)+\frac{1}{12} \Delta I_{L}^{2}\right\}}
$$

Where:
$I_{\text {OUT (Max) }} \quad$ is the output current (Max) [A]
In addition, in automotive and other applications requiring high reliability, it is recommended to connect the capacitors in parallel to accommodate multiple electrolytic capacitors and minimize the chances of drying up. For ceramic capacitors, it is recommended to make two series + two parallel structures to decrease the risk of capacitor destruction due to short circuit conditions.

When the impedance on the input side is high for some reason (because the wiring from the power supply to the VIN pin is long, etc.), then high capacitance is required. In actual conditions, it is necessary to verify that there are no problems like IC is turned off, or the output overshoots due to the change in ViN at transient response.

## Selection of Components Externally Connected - continued

4. Selection of Output Voltage Setting Resistor RFB1, R $\mathrm{R}_{\mathrm{FB} 2}$ (BD9P105MUF-C)

For the BD9P105MUF-C, the output voltage is set with external resistors $R_{\text {FB1 }}$ and RFB2 $^{2}$. The reference voltage of GmAmp1 is set to 0.8 V and the IC operates to regulate FB voltage to 0.8 V . The output voltage is defined by the formula (1). $\mathrm{R}_{\mathrm{FB} 1}$ and $\mathrm{R}_{\mathrm{FB} 2}$ should be adjusted to set the required output voltage. If $\mathrm{R}_{\mathrm{FB} 1}$ and $\mathrm{R}_{\mathrm{FB} 2}$ are large, the current flowing through on these resistors is small and the circuit current at no load can be reduced. However, the phase shift is likely to happen because of the parasitic capacitance of IC and PCB on the FB pin. Therefore, the combined resistance $R_{\text {FB } 1 / / R_{F B 2} \text { should be set to } 100 \mathrm{k} \Omega \text { or less. If the combined resistance } \mathrm{R}_{\text {FB1 }} 1 / \mathrm{R}_{\text {FB2 }} \text { is } 100 \mathrm{k} \Omega \text { or more, } \mathrm{C}_{\text {FB1 }} \text { and } \mathrm{C}_{\text {FB2 }} \text { should }}$ be chosen to satisfy the formula (2). In this case, the value of $\mathrm{C}_{\text {FB1 }}$ and $\mathrm{C}_{\text {FB2 }}$ should be chose the capacitor of 47 pF or more that is much larger than $\mathrm{C}_{\mathrm{p}}$.

$$
\begin{align*}
& V_{O U T}=\frac{R_{F B 1}+R_{F B 2}}{R_{F B 2}} \times 0.8[\mathrm{~V}]  \tag{1}\\
& \frac{R_{F B 1} \times C_{F B 1}}{R_{F B 2} \times C_{F B 2}} \approx 1 \tag{2}
\end{align*}
$$



Figure 48. Setting for Output Setting Resistor
If the voltage between input and output increases and the ON time of the SW decreases to under tonmin, the switching frequency is decreased. To ensure stable switching frequency, the output voltage must satisfy the following equation. If this equation is not satisfied, the SW pulse is skipped. In this case, the switching frequency decreases and the output voltage ripple increases.

$$
V_{\text {OUT }} \geq V_{\text {IN }(\text { Max })} \times f_{\text {SW (Max) }} \times t_{\text {ONMIN }(\text { Max })}[\mathrm{V}]
$$

Where:

$$
\begin{array}{lll}
V_{I N(\operatorname{Max})} & \text { is the Input Voltage (Max) [V] } & \\
f_{S W(\text { Max })} & \text { is the Switching Frequency (Max) [Hz] } & \text { (Refer to page 11) } \\
t_{\text {ONMIN }(\operatorname{Max})} & \text { is the SW Minimum ON time (Max) [s] } & \text { (Refer to page 10) }
\end{array}
$$

If the voltage between input and output decreases, the ON time of the SW increases by skipping the off time and the switching frequency is decreased. To keep switching frequency stably, the following equation must be satisfied.

$$
V_{\text {OUT }} \leq V_{I N(\text { Min })} \times\left(1-f_{S W(\operatorname{Max})} \times t_{\text {OFFMIN }(\text { Max })}\right)[\mathrm{V}]
$$

Where:
$t_{\text {OFFMIN(Max) }}$ is the SW Minimum OFF Time (Max) [s] (Refer to page 10)
5. Selection of the Bootstrap Capacitor

For Bootstrap capacitor $\mathrm{C}_{\mathrm{BST}}$, please connect a $0.1 \mu \mathrm{~F}$ (Typ) ceramic capacitor as close as possible between the BST pin and the SW pin.
6. Selection of the VREG Capacitor.

For VREG capacitor $\mathrm{C}_{\text {REG }}$, please connect a $1.0 \mu \mathrm{~F}$ (Typ) ceramic capacitor between the VREG pin and GND.

## Application Examples 1

Table 3. Specification Example 1

| Parameter | Symbol | Specification Case |
| :--- | :---: | :---: |
| Product Name | IC | BD9P105MUF-C |
| Input Voltage | VIN | 8 V to 18 V |
| Output Voltage | Vout | 6.0 V |
| Output Current | lout | Typ $0.5 \mathrm{~A} / \mathrm{Max} 1.0 \mathrm{~A}$ |
| Operating Temperature Range | Ta | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |



Figure 49. Reference Circuit 1

Table 4. Application Example 1 Parts List with $\pi$-type filter

| No. | Package | Parameters | Part Name (Series) | Type | Manufacturer |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{C}_{\mathrm{F} 1}$ (Note 1) | 3216 | $1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCJ31MR71H105K | Ceramic | MURATA |
| $\mathrm{L}_{\text {F }}$ | W6.0 $\times$ H4.5 $\times$ L6.3 mm ${ }^{3}$ | $2.2 \mu \mathrm{H}$ | CLF6045NIT-2R2N-D | Inductor | TDK |
| $\mathrm{C}_{\text {F2 }}$ | 1005 | $0.1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCM155R71H104K | Ceramic | MURATA |
| Свцк | $\varphi 10 \mathrm{~mm} \times \mathrm{L} 10 \mathrm{~mm}$ | $220 \mu \mathrm{~F}, 35 \mathrm{~V}$ | UWD1V221MCL1GS | Electrolytic capacitor | NICHICON |
| $\mathrm{Clin2}^{(\text {Note 1) }}$ | 3216 | $1 \mu \mathrm{~F}, \mathrm{X7R}, 50 \mathrm{~V}$ | GCJ31MR71H105K | Ceramic | MURATA |
| $\mathrm{ClN1}^{\text {a }}$ | 1005 | $0.1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCM155R71H104K | Ceramic | MURATA |
| Creg | 2012 | $1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 16 \mathrm{~V}$ | GCM21BR71C105K | Ceramic | MURATA |
| $\mathrm{CbSt}^{\text {b }}$ | 1005 | $0.1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCM155R71H104K | Ceramic | MURATA |
| RRST | 1005 | $10 \mathrm{k} \Omega, 1$ \%, 1/16 W | MCR01MZPF1002 | Chip resistor | ROHM |
| $\mathrm{L}_{1}$ | W6.0 $\times$ H4.5 $\times$ L6.3 mm ${ }^{3}$ | $4.7 \mu \mathrm{H}$ | CLF6045NIT-4R7N-D | Inductor | TDK |
| Cout1 | 3225 | $22 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 10 \mathrm{~V}$ | GCM32ER71A226K | Ceramic | MURATA |
| Cout2 | - | Open | - | - | - |
| RFB1 | 1005 | $130 \mathrm{k} \Omega, 1$ \%, 1/16 W | MCR01MZPF1303 | Chip resistor | ROHM |
| $\mathrm{R}_{\text {fB2 }}$ | 1005 | $20 \mathrm{k} \Omega, 1$ \%, 1/16 W | MCR01MZPF2002 | Chip resistor | ROHM |

(Note 1) To reduce EMI noise level, $4.7 \mu \mathrm{~F},(3225, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}, \mathrm{GCM} 32 \mathrm{ER} 71 \mathrm{H} 475 \mathrm{~K})$ is recommended for $\mathrm{C}_{\mathrm{F} 1}$ and $\mathrm{C}_{\text {IN2 }}$.
Table 5. Application Example 1 Parts List without m-type filter

| No. | Package | Parameters | Part Name (Series) | Type | Manufacturer |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{C}_{\mathrm{F} 1}$ | - | Open | - | - | - |
| $\mathrm{L}_{\mathrm{F} 1}$ | - | Open | - | - | - |
| $\mathrm{C}_{\mathrm{F} 2}$ | - | Open | - | - | - |
| $\mathrm{C}_{\mathrm{BLK}}$ | - | Open | - | - | - |
| $\mathrm{C}_{\mathrm{IN} 2}$ | 3225 | $4.7 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCM32ER71H475K | Ceramic | MURATA |
| $\mathrm{C}_{\mathrm{IN} 1}$ | 1005 | $0.1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCM155R71H104K | Ceramic | MURATA |

## Application Examples 1 - continued

( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ )


Figure 50. Efficiency vs Output Current $\left(\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}\right)$


Figure 52. Frequency Characteristic $\left(\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}\right.$, lout $\left.=0.5 \mathrm{~A}\right)$


Figure 51. Input Current vs Output Current ( $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$ )


Figure 53. MODE ON/OFF Response $\left(\mathrm{V}_{\text {IN }}=12 \mathrm{~V}\right.$, lout $\left.=50 \mathrm{~mA}\right)$

## Application Examples 1 - continued

( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ )


Figure 54. Load Response 1

$$
\left(\mathrm{V}_{\text {IN }}=12 \mathrm{~V}, \mathrm{~V}_{\text {MODE }}=5 \mathrm{~V} \text {, Iout }=0 \mathrm{~A} \text { to } 1 \mathrm{~A}\right)
$$



Figure 56. Line Response 1
$\left(\mathrm{V}_{\text {IN }}=16 \mathrm{~V}\right.$ to 8 V , lout $\left.=1 \mathrm{~A}\right)$


Figure 55. Load Response 2 $\left(\mathrm{V}_{\text {In }}=12 \mathrm{~V}, \mathrm{~V}_{\text {mode }}=0 \mathrm{~V}\right.$, lout $=0 \mathrm{~A}$ to 1 A$)$


Figure 57. Line Response 2
$\left(\mathrm{V}_{\text {IN }}=16 \mathrm{~V}\right.$ to 5 V , lout $\left.=1 \mathrm{~A}\right)$

## Application Examples 1 - continued

( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ )


Figure 58. Output Voltage vs Input Voltage 1 $($ RLOAD $=600 \Omega$ )


Figure 60. Line Regulation

$$
\text { (lout = } 1 \text { A) }
$$



Figure 59. Output Voltage vs Input Voltage 2 ( RLOAD $=6 \Omega$ )


Figure 61. Load Regulation
( $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$ )

## Application Examples 2

Table 6. Specification Example 2

| Parameter | Symbol | Specification Case |
| :--- | :---: | :---: |
| Product Name | IC | BD9P135MUF-C |
| Input Voltage | V IN | 8 V to 18 V |
| Output Voltage | Vout | 3.3 V |
| Output Current | lout | Typ $0.5 \mathrm{~A} / \mathrm{Max} 1.0 \mathrm{~A}$ |
| Operating Temperature Range | Ta | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |



Figure 62. Reference Circuit 2

Table 7. Application Example 2 Parts List with $\pi$-type filter

| No. | Package | Parameters | Part Name (Series) | Type | Manufacturer |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{C}_{\text {F1 }}$ (Note 1) | 3216 | $1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCJ31MR71H105K | Ceramic | MURATA |
| LF1 | $\mathrm{W} 6.0 \times \mathrm{H} 4.5 \times \mathrm{L} 6.3 \mathrm{~mm}^{3}$ | $2.2 \mu \mathrm{H}$ | CLF6045NIT-2R2N-D | Inductor | TDK |
| $\mathrm{C}_{\text {F2 }}$ | 1005 | $0.1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCM155R71H104K | Ceramic | MURATA |
| Свцк | $\varphi 10 \mathrm{~mm} \times \mathrm{L} 10 \mathrm{~mm}$ | $220 \mu \mathrm{~F}, 35 \mathrm{~V}$ | UWD1V221MCL1GS | Electrolytic capacitor | NICHICON |
| $\mathrm{Cl}_{12}$ (Note 1) | 3216 | $1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCJ31MR71H105K | Ceramic | MURATA |
| $\mathrm{Cl}_{\text {IN1 }}$ | 1005 | $0.1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCM155R71H104K | Ceramic | MURATA |
| Creg | 2012 | $1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 16 \mathrm{~V}$ | GCM21BR71C105K | Ceramic | MURATA |
| $\mathrm{C}_{\text {bSt }}$ | 1005 | $0.1 \mu \mathrm{~F}, \mathrm{X7R}, 50 \mathrm{~V}$ | GCM155R71H104K | Ceramic | MURATA |
| RRST | 1005 | $10 \mathrm{k} \Omega, 1$ \%, 1/16 W | MCR01MZPF1002 | Chip resistor | ROHM |
| $\mathrm{L}_{1}$ | W6.0 $\times$ H4.5 $\times 6.3 \mathrm{~mm}^{3}$ | $4.7 \mu \mathrm{H}$ | CLF6045NIT-4R7N-D | Inductor | TDK |
| Cout1 | 3225 | 22 FF, X7R, 10 V | GCM32ER71A226K | Ceramic | MURATA |
| Cout2 | - | Open | - | - | - |

(Note 1) To reduce EMI noise level, $4.7 \mu \mathrm{~F},\left(3225, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}\right.$, GCM32ER71H475K) is recommended for $\mathrm{C}_{\mathrm{F} 1}$ and $\mathrm{C}_{\text {IN2 }}$.
Table 8. Application Example 2 Parts List without $\pi$-type filter

| No. | Package | Parameters | Part Name (Series) | Type | Manufacturer |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{C}_{\mathrm{F} 1}$ | - | Open | - | - | - |
| $\mathrm{L}_{\mathrm{F} 1}$ | - | Open | - | - | - |
| $\mathrm{C}_{\mathrm{F} 2}$ | - | Open | - | - | - |
| $\mathrm{C}_{\mathrm{BLK}}$ | - | Open | - | - | - |
| $\mathrm{C}_{\mathrm{IN} 2}$ | 3225 | $4.7 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCM32ER71H475K | Ceramic | MURATA |
| $\mathrm{C}_{\mathrm{IN} 1}$ | 1005 | $0.1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCM155R71H104K | Ceramic | MURATA |

## Application Examples 2 - continued

( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ )


Figure 63. Efficiency vs Output Current $\left(\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}\right)$


Figure 65. Frequency Characteristic $\left(\mathrm{V}_{\text {IN }}=12 \mathrm{~V}\right.$, lout $\left.=0.5 \mathrm{~A}\right)$


Figure 64. Input Current vs Output Current $\left(\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}\right)$


Figure 66. MODE ON/OFF Response $\left(\mathrm{V}_{\text {IN }}=12 \mathrm{~V}\right.$, lout $\left.=50 \mathrm{~mA}\right)$

## Application Examples 2 - continued

( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ )


Figure 67. Load Response 1 $\left(\mathrm{V}_{\text {IN }}=12 \mathrm{~V}, \mathrm{~V}_{\text {MODE }}=5 \mathrm{~V}\right.$, lout $=0 \mathrm{~A}$ to 1 A$)$


Figure 69. Line Response 1
$\left(\mathrm{V}_{\text {IN }}=16 \mathrm{~V}\right.$ to 8 V , lout $\left.=1 \mathrm{~A}\right)$


Figure 68. Load Response 2
$\left(\mathrm{V}_{\text {IN }}=12 \mathrm{~V}, \mathrm{~V}_{\text {MODE }}=0 \mathrm{~V}\right.$, Iout $=0 \mathrm{~A}$ to 1 A$)$


Figure 70. Line Response 2
$\left(\mathrm{V}_{\text {IN }}=16 \mathrm{~V}\right.$ to 3.5 V , lout $\left.=1 \mathrm{~A}\right)$

## Application Examples 2-continued

( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ )


Figure 71. Output Voltage vs Input Voltage 1 (Rload $=330 \Omega$ )


Figure 73. Line Regulation (lout $=1 \mathrm{~A}$ )


Figure 72. Output Voltage vs Input Voltage 2 ( Rload $=3.3 \Omega$ )


Figure 74. Load Regulation $\left(\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}\right)$

## Application Examples 3

Table 9. Specification Example 3

| Parameter | Symbol | Specification Case |
| :--- | :---: | :---: |
| Product Name | IC | BD9P155MUF-C |
| Input Voltage | V IN | 8 V to 18 V |
| Output Voltage | Vout | 5.0 V |
| Output Current | lout | Typ $0.5 \mathrm{~A} / \mathrm{Max} 1.0 \mathrm{~A}$ |
| Operating Temperature Range | Ta | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |



Figure 75. Reference Circuit 3

Table 10. Application Example 3 Parts List with $\pi$-type filter

| No. | Package | Parameters | Part Name (Series) | Type | Manufacturer |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{C}_{\mathrm{F} 1}$ (Note 1) | 3216 | $1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCJ31MR71H105K | Ceramic | MURATA |
| LF1 | $\mathrm{W} 6.0 \times \mathrm{H} 4.5 \times \mathrm{L} 6.3 \mathrm{~mm}^{3}$ | $2.2 \mu \mathrm{H}$ | CLF6045NIT-2R2N-D | Inductor | TDK |
| $\mathrm{C}_{\text {F2 }}$ | 1005 | 0.1 FF, X7R, 50 V | GCM155R71H104K | Ceramic | MURATA |
| Свцк | $\varphi 10 \mathrm{~mm} \times \mathrm{L} 10 \mathrm{~mm}$ | $220 \mu \mathrm{~F}, 35 \mathrm{~V}$ | UWD1V221MCL1GS | Electrolytic capacitor | NICHICON |
| $\mathrm{Cl}_{12}{ }^{\text {(Note 1) }}$ | 3216 | $1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCJ31MR71H105K | Ceramic | MURATA |
| $\mathrm{ClN1}^{\text {a }}$ | 1005 | $0.1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCM155R71H104K | Ceramic | MURATA |
| Creg | 2012 | $1 \mu \mathrm{~F}, \mathrm{X7R}, 16 \mathrm{~V}$ | GCM21BR71C105K | Ceramic | MURATA |
| $\mathrm{CbSt}^{\text {b }}$ | 1005 | $0.1 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCM155R71H104K | Ceramic | MURATA |
| RRST | 1005 | $10 \mathrm{k} \Omega, 1$ \%, 1/16 W | MCR01MZPF1002 | Chip resistor | ROHM |
| $\mathrm{L}_{1}$ | $\mathrm{W} 6.0 \times \mathrm{H} 4.5 \times \mathrm{L} 6.3 \mathrm{~mm}^{3}$ | $4.7 \mu \mathrm{H}$ | CLF6045NIT-4R7N-D | Inductor | TDK |
| Cout1 | 3225 | $22 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 10 \mathrm{~V}$ | GCM32ER71A226K | Ceramic | MURATA |
| Cout2 | - | Open | - | - | - |

(Note 1) To reduce EMI noise level, $4.7 \mu \mathrm{~F},(3225, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}, \mathrm{GCM} 32 \mathrm{ER} 71 \mathrm{H} 475 \mathrm{~K})$ is recommended for $\mathrm{C}_{\mathrm{F} 1}$ and $\mathrm{C}_{\mathrm{IN} 2}$.
Table 11. Application Example 3 Parts List without m-type filter

| No. | Package | Parameters | Part Name (Series) | Type | Manufacturer |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{C}_{\mathrm{F} 1}$ | - | Open | - | - | - |
| $\mathrm{L}_{\mathrm{F} 1}$ | - | Open | - | - | - |
| $\mathrm{C}_{\mathrm{F} 2}$ | - | Open | - | - | - |
| $\mathrm{C}_{\mathrm{BLK}}$ | - | Open | - | - | - |
| $\mathrm{C}_{\text {IN } 2}$ | 3225 | $4.7 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 50 \mathrm{~V}$ | GCM32ER71H475K | Ceramic | MURATA |
| $\mathrm{C}_{\text {IN } 1}$ | 1005 | $0.1 \mu \mathrm{~F}, \mathrm{X7R}, 50 \mathrm{~V}$ | GCM155R71H104K | Ceramic | MURATA |

## Application Examples 3-continued

( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ )


Figure 76. Efficiency vs Output Current $\left(\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}\right)$


Figure 78. Frequency Characteristic $\left(\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}\right.$, lout $\left.=0.5 \mathrm{~A}\right)$


Figure 77. Input Current vs Output Current $\left(\mathrm{V}_{\text {IN }}=12 \mathrm{~V}\right)$


Figure 79. MODE ON/OFF Response $\left(\mathrm{V}_{\text {IN }}=12 \mathrm{~V}\right.$, lout $\left.=50 \mathrm{~mA}\right)$

## Application Examples 3 - continued

( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ )


Figure 80. Load Response 1 $\left(\mathrm{V}_{\text {IN }}=12 \mathrm{~V}, \mathrm{~V}_{\text {MODE }}=5 \mathrm{~V}\right.$, Iout $=0 \mathrm{~A}$ to 1 A$)$


Figure 81. Load Response 2 $\left(\mathrm{V}_{\text {IN }}=12 \mathrm{~V}, \mathrm{~V}_{\text {MODE }}=0 \mathrm{~V}\right.$, Iout $=0 \mathrm{~A}$ to 1 A$)$

Figure 83. Line Response 2
$\left(\mathrm{V}_{\text {IN }}=16 \mathrm{~V}\right.$ to 4 V , lout $=1 \mathrm{~A}$ )


Figure 82. Line Response 1 $\left(\mathrm{V}_{\text {IN }}=16 \mathrm{~V}\right.$ to 8 V , lout $=1 \mathrm{~A}$ )

## Application Examples 3-continued

( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ )


Figure 84. Output Voltage vs Input Voltage 1 (RLOAD $=500 \Omega$ )


Figure 86. Line Regulation
(lout $=1$ A)


Figure 85. Output Voltage vs Input Voltage 2 (RLOAD $=5 \Omega$ )


Figure 87. Load Regulation (Vin = 12 V )

## Automotive Power Supply Line Circuit



Figure 88. Automotive Power Supply Line Circuit
As a reference, the automotive power supply line circuit example is given in figure above.
The $\pi$-type filter is a third-order LC filter. In general, it is used in combination with decoupling capacitors for high frequency. Since large attenuation characteristics can be obtained, excellent characteristic is also obtained as an EMI filter. Devices used for $\pi$-type filters should be placed close to each other.
TVS (Transient Voltage Suppressors) is used for primary protection of the automotive power supply line. Since it is necessary to withstand high energy of load dump surge, a general zener diode is insufficient. Recommended device is shown in the following table.
In addition, a reverse polarity protection diode is needed considering if a power supply such as Battery is accidentally connected in the opposite direction.

Table 12. Reference Parts of Automotive Power Supply Line Circuit

| Device | Part name (series) | Manufacturer | Device | Part name (series) | Manufacturer |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L | CLF series | TDK | TVS | SMB series | Vishay |  |
| L | XAL series | Coilcraft | D | S3A to S3M series | Vishay |  |
| C | CJ series /CZ series | NICHICON |  |  |  |  |

## Recommended Parts Manufacturer List

Shown below is the list of the recommended parts manufacturers for reference.

| Type | Manufacturer | URL |
| :---: | :---: | :---: |
| Electrolytic Capacitor | NICHICON | $\underline{\text { www.nichicon-us.com }}$ |
| Ceramic Capacitor | Murata | $\underline{\text { www.murata.com }}$ |
| Hybrid Capacitor | Suncon | $\underline{\text { www.sunelec.co.jp }}$ |
| Inductor | TDK | $\underline{\text { product.tdk.com }}$ |
| Inductor | Coilcraft | $\underline{\text { www.coilcraft.com }}$ |
| Inductor | SUMIDA | $\underline{\text { www.sumida.com }}$ |
| Diode | Vishay | $\underline{\text { www.vishay.com }}$ |
| Diode/Resistor | ROHM | $\underline{\text { www.rohm.com }}$ |

## PCB Layout Design

PCB layout design for DC/DC converter power supply IC is as important as the circuit design. Appropriate layout can avoid various problems caused by power supply circuit. Figure 89 (a) to Figure 89 (c) figure the current path in a buck converter circuit. The Loop1 in Figure 89 (a) is a current path when High Side Switch is ON and Low Side Switch is OFF, the Loop2 in Figure 89 (b) is when High Side Switch is OFF and Low Side Switch is ON. The thick line in Figure 89 (c) shows the difference between Loop1 and Loop2. The current in thick line changes sharply each time the switching element High Side Switch and Low Side Switch change from OFF to ON, and vice versa. These sharp changes induce several harmonics in the waveform. Therefore, the loop area of thick line that is consisted by input capacitor and IC should be as small as possible to minimize noise. For more detail, refer to application note of switching regulator series "PCB Layout Techniques of Buck Converter".


Figure 89 (a). Current Path when High Side Switch $=$ ON, Low Side Switch $=$ OFF


Figure 89 (b). Current Path when High Side Switch $=$ OFF, Low Side Switch $=$ ON


Figure 89 (c). Difference of Current and Critical Area in Layout

## PCB Layout Design - continued

When designing the PCB layout, please pay extra attention to the following points.

1. The decoupling capacitors $\left(\mathrm{C}_{\mathbb{N} 1}\right)$ for the VIN pin (pin 20) and the PVIN pins (pin 1, 2) should be placed closest to the PVIN pins and the PGND pins (pin 4,5). In addition, placing a capacitor $0.1 \mu \mathrm{~F}$ close to the PVIN pin results in minimizing the high-frequency noise.
2. The device, the input capacitor, the output inductor and the output capacitor should be placed on the same side of the board and the connection of each part should be made on the same layer.
3. Place the ground plane in a layer closest to the surface layer where the device is mounted.
4. The GND pin (pin 13) is the reference ground and the PGND pins are the power ground. These pins should be connected through the back side of the device. The power systems ground should be connected to the ground plane using as many vias as possible.
5. The capacitor for VREG should be placed closest to the VREG pin (pin 17), the GND pin and the PGND pin. As shown in the Recommended Board Layout Example, it can be realized that connecting with the shortest distance for the GND pin and the PGND pins by placing the capacitor for VREG on the closest to the VREG pin and wiring at the back side of the IC.
6. Place Bootstrap capacitor Cbst close to the device with short traces to the SW pins (pin 6, 7) and the BST pin (pin 8).
7. To minimize the emission noise from switching node, the distance between the SW pins to inductor should be as short as possible and not to expand the copper area more than necessary.
8. Place the output capacitor close to the inductor and power ground area.
9. Make the feedback line from the output away from the inductor and the switching node. If this line is affected by external noise, an error may be occurred in the output voltage or the control may become unstable. Therefore, move the feedback line to back side layer of the board through via and connect it to the VOUT_SNS pin (pin 14 [BD9P105MUF-C], pin 15 [BD9P135MUF-C, BD9P155MUF-C]). When the VCC_EX function and the output discharge function are used, connect it to the VCC_EX (pin 16) and the VOUT_DIS pin (pin 14 [BD9P135MUF-C, BD9P155MUF-C]) as well, respectively.
10. $R_{F B 1}$ and $R_{F B 2}$ Feedback resistors are needed for BD9P105MUF-C. Place $R_{F B 1}, R_{F B 2}$ close to the $F B$ pin (pin 15).
11. R Rbo is for measuring the frequency characteristic of the feedback. By inserting a resistor in R Rbo, the frequency characteristics (phase margin) of the feedback can be measured. R frbo should be short-circuited for the normal use.


Figure 90. Recommended Board Layout Example (for BD9P1x5MUF-C)


Figure 91. The resistor for measuring the frequency charācteristic of the feedback

## Power Dissipation

For thermal design, be sure to operate the IC within the following conditions.
(Since the temperatures described hereunder are all guaranteed temperatures, take margin into account.)

1. The ambient temperature Ta is to be $125^{\circ} \mathrm{C}$ or less.
2. The chip junction temperature Tj is to be $150^{\circ} \mathrm{C}$ or less.

The chip junction temperature Tj can be considered in the following two patterns:

1. To obtain Tj from the package surface center temperature Tt in actual use

$$
T j=T t+\psi_{J T} \times W\left[{ }^{\circ} \mathrm{C}\right]
$$

2. To obtain Tj from the ambient temperature Ta

$$
T j=T a+\theta_{J A} \times W\left[{ }^{\circ} \mathrm{C}\right]
$$

Where:

| $\psi_{J T}$ | is junction to top characterization parameter | (Refer to page 9) |
| :--- | :--- | :--- |
| $\theta_{J A}$ | is junction to ambient | (Refer to page 9) |

The heat loss W of the IC can be obtained by the formula shown below.
This formula is approximation, please confirm this on the actual application circuit.

$$
\begin{aligned}
W= & R_{\text {ONH }} \times I_{\text {OUT }}^{2} \times \frac{V_{\text {OUT }}}{V_{I N}}+R_{O N L L} \times I_{\text {OUT }}^{2}\left(1-\frac{V_{\text {OUT }}}{V_{I N}}\right) \\
& +V_{I N} \times I_{Q_{-} V I N 4}+V_{\text {OUT }} \times I_{Q_{-} V C C_{-} E X 2}+\frac{1}{2} \times(t r+t f) \times V_{I N} \times I_{O U T} \times f_{S W} \quad[\mathrm{~W}]
\end{aligned}
$$

Where:

| $R_{O N H}$ | is the High Side FET ON Resistance $[\Omega]$ | (Refer to page 11) |
| :--- | :--- | :--- |
| $R_{O N L}$ | is the Low Side FET ON Resistance [ $\Omega]$ | (Refer to page 11) |

$I_{\text {OUT }} \quad$ is the Load Current [A]
$V_{\text {OUT }} \quad$ is the Output Voltage [V]
$V_{I N} \quad$ is the Input Voltage [V]
$I_{Q_{-} \text {VIN4 }} \quad$ is the Quiescent Current from VIN [A] (Refer to page 10)
$I_{Q_{-} V C C_{-} E X 2}$ is the Quiescent Current from VCC_EX [A]
(Refer to page 10)
$t r \quad$ is the Switching Rise Time [s] (5 ns, Typ)
$t f \quad$ is the Switching Fall Time [s] (5 ns, Typ)
$f_{S W} \quad$ is the Switching Frequency [Hz] (Refer to page 11)


1. $R_{O N H} \times I_{O U T}{ }^{2}$
2. $R_{\text {ONL }} \times I_{\text {OUT }}{ }^{2}$
3. $\frac{1}{2} \times(t r+t f) \times V_{I N} \times I_{O U T} \times f_{S W}$

Figure 92. SW Waveform

## I/O Equivalence Circuits

| 19. EN | 10. MODE |
| :---: | :---: |
|  |  |
| 6,7. SW, 8.BST | 12. RESET |
|  |  |
| 9. OCP_SEL, 11. SSCG | 14. VOUT_DIS (BD9P135MUF-C, BD9P155MUF-C) |
|  | VOUT_DIS |

*Resistance value is Typ.

I/O Equivalence Circuits - continued

| 14. VOUT_SNS, 15. FB (BD9P105MUF-C) | 15. VOUT_SNS (BD9P155MUF-C) |
| :---: | :---: |
|  | vout_SNS $\square$ |
| 15. VOUT_SNS (BD9P135MUF-C) | 16. VCC_EX, 17. VREG |
|  |  |

## Operational Notes

1. Reverse Connection of Power Supply

Connecting the power supply in reverse polarity can damage the IC. Take precautions against reverse polarity when connecting the power supply, such as mounting an external diode between the power supply and the IC's power supply pins.
2. Power Supply Lines

Design the PCB layout pattern to provide low impedance supply lines. Furthermore, connect a capacitor to ground at all power supply pins. Consider the effect of temperature and aging on the capacitance value when using electrolytic capacitors.
3. Ground Voltage

Ensure that no pins are at a voltage below that of the ground pin at any time, even during transient condition. However, pins that drive inductive loads (e.g. motor driver outputs, DC-DC converter outputs) may inevitably go below ground due to back EMF or electromotive force. In such cases, the user should make sure that such voltages going below ground will not cause the IC and the system to malfunction by examining carefully all relevant factors and conditions such as motor characteristics, supply voltage, operating frequency and PCB wiring to name a few.

## 4. Ground Wiring Pattern

When using both small-signal and large-current ground traces, the two ground traces should be routed separately but connected to a single ground at the reference point of the application board to avoid fluctuations in the small-signal ground caused by large currents. Also ensure that the ground traces of external components do not cause variations on the ground voltage. The ground lines must be as short and thick as possible to reduce line impedance.

## 5. Recommended Operating Conditions

The function and operation of the IC are guaranteed within the range specified by the recommended operating conditions. The characteristic values are guaranteed only under the conditions of each item specified by the electrical characteristics.
6. Inrush Current

When power is first supplied to the IC, it is possible that the internal logic may be unstable and inrush current may flow instantaneously due to the internal powering sequence and delays, especially if the IC has more than one power supply. Therefore, give special consideration to power coupling capacitance, power wiring, width of ground wiring, and routing of connections.
7. Testing on Application Boards

When testing the IC on an application board, connecting a capacitor directly to a low-impedance output pin may subject the IC to stress. Always discharge capacitors completely after each process or step. The IC's power supply should always be turned off completely before connecting or removing it from the test setup during the inspection process. To prevent damage from static discharge, ground the IC during assembly and use similar precautions during transport and storage.

## 8. Inter-pin Short and Mounting Errors

Ensure that the direction and position are correct when mounting the IC on the PCB. Incorrect mounting may result in damaging the IC. Avoid nearby pins being shorted to each other especially to ground, power supply and output pin. Inter-pin shorts could be due to many reasons such as metal particles, water droplets (in very humid environment) and unintentional solder bridge deposited in between pins during assembly to name a few.
9. Unused Input Pins

Input pins of an IC are often connected to the gate of a MOS transistor. The gate has extremely high impedance and extremely low capacitance. If left unconnected, the electric field from the outside can easily charge it. The small charge acquired in this way is enough to produce a significant effect on the conduction through the transistor and cause unexpected operation of the IC. So unless otherwise specified, unused input pins should be connected to the power supply or ground line.

## Operational Notes - continued

## 10. Regarding the Input Pin of the IC

This monolithic IC contains $\mathrm{P}+$ isolation and P substrate layers between adjacent elements in order to keep them isolated. $\mathrm{P}-\mathrm{N}$ junctions are formed at the intersection of the P layers with the N layers of other elements, creating a parasitic diode or transistor. For example (refer to figure below):

When GND > Pin A and GND > Pin B, the P-N junction operates as a parasitic diode.
When GND > Pin B, the P-N junction operates as a parasitic transistor.
Parasitic diodes inevitably occur in the structure of the IC. The operation of parasitic diodes can result in mutual interference among circuits, operational faults, or physical damage. Therefore, conditions that cause these diodes to operate, such as applying a voltage lower than the GND voltage to an input pin (and thus to the $P$ substrate) should be avoided.


Figure 93. Example of Monolithic IC Structure

## 11. Ceramic Capacitor

When using a ceramic capacitor, determine a capacitance value considering the change of capacitance with temperature and the decrease in nominal capacitance due to DC bias and others.

## 12. Thermal Shutdown Circuit(TSD)

This IC has a built-in thermal shutdown circuit that prevents heat damage to the IC. Normal operation should always be within the IC's maximum junction temperature rating. If however the rating is exceeded for a continued period, the junction temperature ( Tj ) will rise which will activate the TSD circuit that will turn OFF power output pins. When the Tj falls below the TSD threshold, the circuits are automatically restored to normal operation.
Note that the TSD circuit operates in a situation that exceeds the absolute maximum ratings and therefore, under no circumstances, should the TSD circuit be used in a set design or for any purpose other than protecting the IC from heat damage.

## 13. Over Current Protection Circuit (OCP)

This IC incorporates an integrated overcurrent protection circuit that is activated when the load is shorted. This protection circuit is effective in preventing damage due to sudden and unexpected incidents. However, the IC should not be used in applications characterized by continuous operation or transitioning of the protection circuit.

## Ordering Information



## Marking Diagram

VQFN20FV4040 (TOP VIEW)


| Orderable Part Number | Output Voltage | Part Number Making |
| :---: | :---: | :---: |
| BD9P105MUF-CE2 | Adjustable | 9P105 |
| BD9P135MUF-CE2 | 3.3 V | 9P135 |
| BD9P155MUF-CE2 | 5.0 V | 9P155 |

Physical Dimension and Packing Information


## Revision History

| Date | Revision |  | Changes |
| :---: | :---: | :--- | :--- |
| 28.Apr.2020 | 001 | New Release |  |

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| JAPAN | USA | EU | CHINA |
| :---: | :---: | :---: | :---: |
| CLASSIII | CLASSIII | CLASS II b | CLASSIII |
|  |  | CLASSIII |  |

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[h] Use of the Products in places subject to dew condensation
4. The Products are not subject to radiation-proof design.
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7. De-rate Power Dissipation depending on ambient temperature. When used in sealed area, confirm that it is the use in the range that does not exceed the maximum junction temperature.
8. Confirm that operation temperature is within the specified range described in the product specification.
9. ROHM shall not be in any way responsible or liable for failure induced under deviant condition from what is defined in this document.

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For details, please refer to ROHM Mounting specification

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[c] the Products are exposed to direct sunshine or condensation
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