

# **TSM9634**

### A 1µA, SOT23 Precision Current-Sense Amplifier

### FEATURES

- ♦ Alternate-source for MAX9634
- Ultra-Low Supply Current: 1µA
- ♦ Wide Input Common Mode Range: +1.6V to +28V
- ♦ Low Input Offset Voltage: 250µV (max)
- ♦ Low Gain Error: <0.5% (max)
- Voltage Output
- Four Gain Options Available: TSM9634T: Gain = 25V/V TSM9634F: Gain = 50V/V TSM9634H: Gain = 100V/V TSM9634W: Gain = 200V/V
- ♦ 5-Pin SOT23 Packaging

### **APPLICATIONS**

Notebook Computers Power Management Systems Portable/Battery-Powered Systems PDAs Smart Chargers Smart Phones

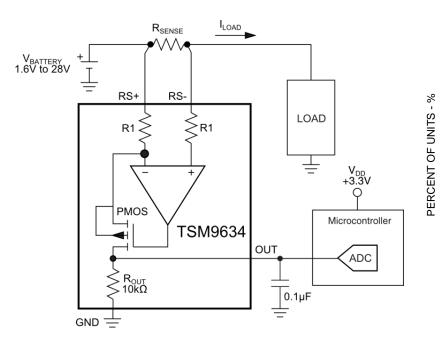
# DESCRIPTION

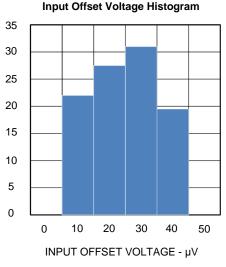
The voltage-output TSM9634 current-sense amplifiers are electrically and form-factor identical to the MAX9634 current-sense amplifiers. Consuming a very low 1µA supply current, the TSM9634 high-side current-sense amplifiers exhibit a 250-µV (max)  $V_{OS}$  and a 0.5% (max) gain error, both specifications optimized for any precision current measurement. For all high-side current-sensing applications, the TSM9634 features a wide input common-mode voltage range from 1.6V to 28V.

The SOT23 package makes the TSM9634 an ideal choice for pcb-area-critical, low-current, high-accuracy current-sense applications in all battery-powered portable instruments.

All TSM9634s are specified for operation over the -40°C to +85°C extended temperature range.

# TYPICAL APPLICATION CIRCUIT





PART	GAIN OPTION
TSM9634T	25 V/V
TSM9634F	50 V/V
TSM9634H	100 V/V
TSM9634W	200 V/V

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# **ABSOLUTE MAXIMUM RATINGS**

RS+, RS- to GND	0.3V to +30V
OUT to GND	0.3V to +6V
RS+ to RS	±30V
Short-Circuit Duration: OUT to GND	Continuous
Continuous Input Current (Any Pin)	±20mA
Continuous Power Dissipation (T <sub>A</sub> = +70°	C)
5-Pin SOT23 (Derate at 3.9mW/°C abo	ve +70°C) 312mW

Operating Temperature Range	40°C to +85°C
Junction Temperature	+150°C
Storage Temperature Range	-65°C to +150°C
Lead Temperature (Soldering, 10s)	+300°C
Soldering Temperature (Reflow)	

Electrical and thermal stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other condition beyond those indicated in the operational sections of the specifications is not implied. Exposure to any absolute maximum rating conditions for extended periods may affect device reliability and lifetime.

# **PACKAGE/ORDERING INFORMATION**

		5 RS+			
GND 2 TSM9634 OUT 3 4 RS- SOT23-5 UK Package					
ORDER NUMBER	PART MARKING	CARRIER	QUANTITY		
TSM9634TEUK+TP	TADD	Tape & Reel			
TSM9634TEUK+T	TADD	Tape & Reel	3000		
TSM9634FEUK+TP	TADB	Tape & Reel			
TSM9634FEUK+T	TADB	Tape & Reel	3000		
TSM9634HEUK+TP	TADE	Tape & Reel			
TSM9634HEUK+T	TADE	Tape & Reel	3000		
TSM9634WEUK+TP	TADG	Tape & Reel			
TSM9634WEUK+T	TADG	Tape & Reel	3000		

Lead-free Program: Touchstone Semiconductor supplies only lead-free packaging.

Consult Touchstone Semiconductor for products specified with wider operating temperature ranges.



# **ELECTRICAL CHARACTERISTICS**

 $V_{RS+} = V_{RS-} = 3.6V$ ;  $V_{SENSE} = (V_{RS+} - V_{RS-}) = 0V$ ;  $T_A = -40^{\circ}C$  to  $+85^{\circ}C$ , unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ . See Note 1

PARAMETER	SYMBOL	CONDITIONS		MIN	TYP	MAX	UNITS
	I <sub>cc</sub>	V <sub>RS+</sub> = 5V, T <sub>A</sub> = +25°C			0.5	0.85	
Supply Current (Note 2)		V <sub>RS+</sub> = 5V, -40°C < T <sub>A</sub> < +85°C				1.1	μA
Supply Current (Note 2)		V <sub>RS+</sub> = 28V, T <sub>A</sub> = +25°C			1.1	1.8	
		V <sub>RS+</sub> = 28V, -40°C < T <sub>A</sub> < +85°C				2.5	
Common-Mode Input Range	V <sub>CM</sub>	Guaranteed by CMRR , -	40°C < T <sub>A</sub> < +85°C	1.6		28	V
Common-Mode Rejection Ratio	CMRR	1.6V < V <sub>RS+</sub> < 28V, -40°C < T <sub>A</sub> < +85°C		94	130		dB
		TSM9634T/TSM9634F/	T <sub>A</sub> = +25°C	100 250			
Input Offect Veltere (Nete 2)	V	TSM9634H	-40°C < T <sub>A</sub> < +85°C			300	μV
Input Offset Voltage (Note 3)	Vos	TSM9634W	T <sub>A</sub> = +25°C		100	250	μV
		1 5101963400	-40°C < T <sub>A</sub> < +85°C			425	
		TSM9634T			25		V/V
Gain	G	TSM9634F			50		
Gain		TSM9634H			100		
		TSM9634W	TSM9634W		200		
	GE	TSM9634T/TSM9634F/	T <sub>A</sub> = +25°C		±0.1	±0.5	
Gain Error (Note 4)		TSM9634H	-40°C < T <sub>A</sub> < +85°C			±0.6	%
		TSM9634W	T <sub>A</sub> = +25°C		±0.1	±0.7	/0
			-40°C < T <sub>A</sub> < +85°C			±0.8	
Output Resistance	R <sub>OUT</sub>	(Note 5)	TSM9634T/F/H	7.0	10	13.2	kΩ
Ouput Resistance			TSM9634W	14.0	20	26.4	
	V <sub>OL</sub>	Gain = 25			1.5	7.5	mV
OUT Low Voltage		Gain = 50			3	15	
		Gain = 100			6	30	
		Gain = 200			12	85	
OUT High Voltage	V <sub>OH</sub>	$V_{OH} = V_{RS-} - V_{OUT}$ (Note 6)			0.1	0.2	V

**Note 1:** All devices are 100% production tested at  $T_A = +25$ °C. All temperature limits are guaranteed by product characterization.

Note 2: Extrapolated to  $V_{OUT} = 0$ . I<sub>CC</sub> is the total current into the RS+ and the RS- pins.

**Note 3:** Input offset voltage  $V_{OS}$  is extrapolated from  $V_{OUT}$  with  $V_{SENSE}$  set to 1mV.

Note 4: Gain error is calculated by applying two values for V<sub>SENSE</sub> and then calculating the error of the actual slope vs. the ideal transfer characteristic:

- For GAIN = 25, the applied  $V_{\text{SENSE}}$  is 20mV and 120mV.
- For GAIN = 50, the applied  $V_{SENSE}$  is 10mV and 60mV.
- For GAIN = 100, the applied  $V_{\text{SENSE}}$  is 5mV and 30mV.
- For GAIN = 200, the applied  $V_{SENSE}$  is 2.5mV and 15mV.

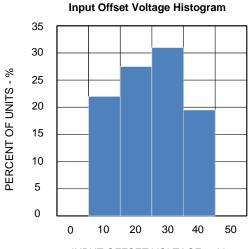
Note 5: The device is stable for any capacitive load at  $V_{\text{OUT}}$ .

**Note 6:**  $V_{OH}$  is the voltage from  $V_{RS}$  to  $V_{OUT}$  with  $V_{SENSE} = 3.6V/GAIN$ .

# **TSM9634**

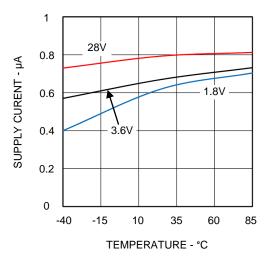
# **TYPICAL PERFORMANCE CHARACTERISTICS**

 $V_{RS+} = V_{RS-} = 3.6V$ ;  $T_A = +25^{\circ}C$ , unless otherwise noted.

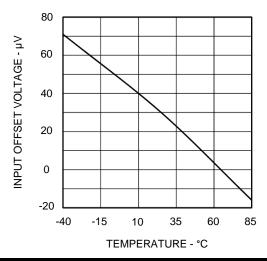


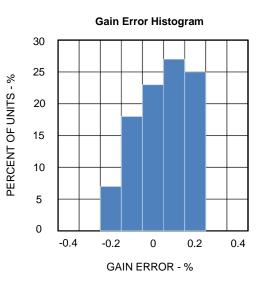
INPUT OFFSET VOLTAGE -  $\mu V$ 

Supply Current vs Temperature

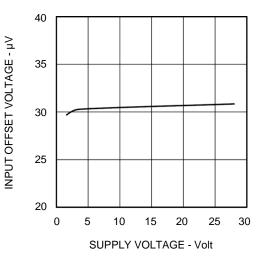


Input Offset Voltage vs Temperature

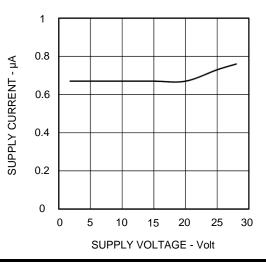




Input Offset Voltage vs Common-Mode Voltage



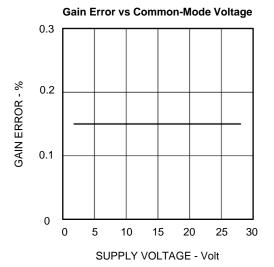
Supply Current vs Common-Mode Voltage

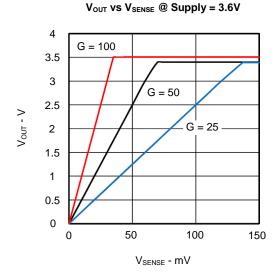




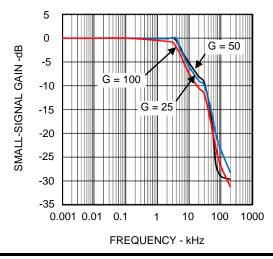
TSM9634DS r1p0 RTFDS

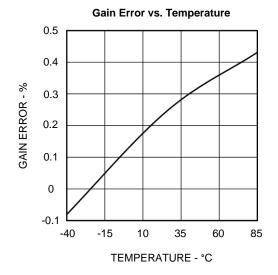
# **TSM9634** YPICAL PERFORMANCE CHARACTERISTICS $V_{RS+} = V_{RS-} = 3.6V$ ; $T_A = +25^{\circ}C$ , unless otherwise noted.



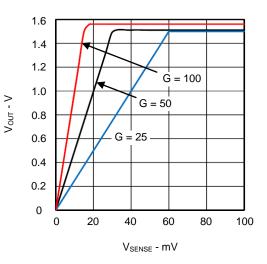


Small-Signal Gain vs Frequency

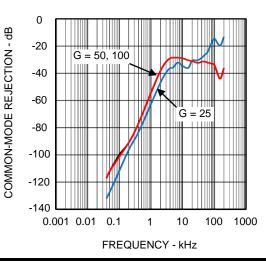




V<sub>OUT</sub> vs V<sub>SENSE</sub> @ Supply = 1.6V



**Common-Mode Rejection vs Frequency** 





# **TYPICAL PERFORMANCE CHARACTERISTICS**

 $V_{RS+} = V_{RS-} = 3.6V$ ;  $T_A = +25^{\circ}C$ , unless otherwise noted.

Small-Signal Pulse Response, Gain = 50

Large-Signal Pulse Response, Gain = 50

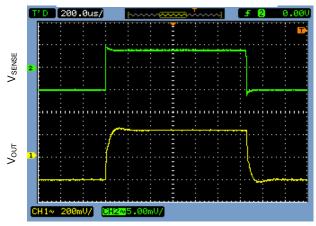
**F 2** 

0.0

<sup>2</sup> D 200.0us/

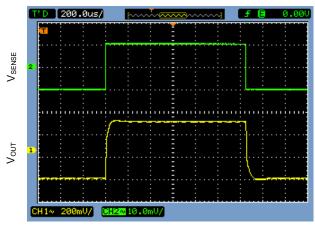
V<sub>SENSE</sub>

Vour

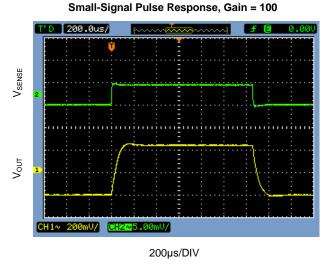


#### 200µs/DIV

Small-Signal Pulse Response, Gain = 25



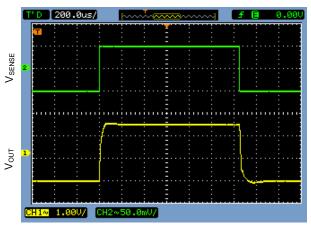
200µs/DIV



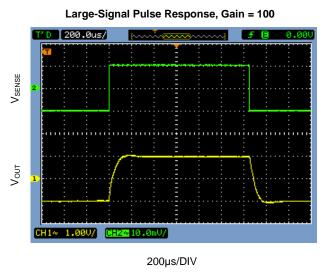


#### 200µs/DIV





200µs/DIV



#### TSM9634DS r1p0 RTFDS

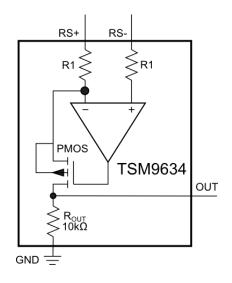




# **PIN FUNCTIONS**

PIN	LABEL	FUNCTION	
SOT23	LADEL	FUNCTION	
5	RS+	External Sense Resistor Power-Side Connection	
4	RS-	External Sense Resistor Load-Side Connection	
1, 2	GND	Ground. Connect these pins to analog ground.	
3	OUT	Output Voltage. $V_{OUT}$ is proportional to $V_{SENSE} = V_{RS+} - V_{RS-}$	

# **BLOCK DIAGRAMS**



# **DESCRIPTION OF OPERATION**

The internal configuration of the TSM9634 - a unidirectional high-side, current-sense amplifier - is based on a commonly-used operational amplifier (op amp) circuit for measuring load currents (in one direction) in the presence of high-common-mode voltages. In the general case, a current-sense amplifier monitors the voltage caused by a load current through an external sense resistor and generates an output voltage as a function of that load current. Referring to the typical application circuit on Page 1, the inputs of the op-amp-based circuit are connected across an external RSENSE resistor that is used to measure load current. At the non-inverting input of the TSM9634 (the RS+ terminal), the applied voltage is ILOAD x RSENSE. Since the RS- terminal is the non-inverting input of the internal op amp, op-amp feedback action forces the inverting input of the internal op amp to the same potential (ILOAD x RSENSE). Therefore, the voltage drop across

RSENSE ( $V_{SENSE}$ ) and the voltage drop across R1 (at the RS+ terminal) are equal. To minimize any additional error because of op-amp input bias current mismatch, both R1s are the same value.

Since the internal p-channel FET's source is connected to the inverting input of the internal op amp and since the voltage drop across R1 is the same as the external  $V_{\text{SENSE}}$ , op amp feedback action drives the gate of the FET such that the FET's drain-source current is equal to:

$$I_{DS} = \frac{V_{SENSE}}{R1}$$



or

$$I_{DS} = \frac{I_{LOAD} \times R_{SENSE}}{R1}$$

Since the FET's drain terminal is connected to ROUT, the output voltage of the TSM9634 at the OUT terminal is, therefore;

$$V_{OUT} = I_{LOAD} \times R_{SENSE} \times \frac{R_{OUT}}{R1}$$

The current-sense amplifier's gain accuracy is therefore the ratio match of ROUT to R1. For each of the four gain options available, Table 1 lists the values for ROUT and R1. The TSM9634's output

# **APPLICATIONS INFORMATION**

### **Choosing the Sense Resistor**

Selecting the optimal value for the external RSENSE is based on the following criteria and for each commentary follows:

- 1) RSENSE Voltage Loss
- 2)  $V_{\text{OUT}}$  Swing vs. Applied Input Voltage at  $V_{\text{RS+}}$  and Desired  $V_{\text{SENSE}}$
- 3) Total ILOAD Accuracy
- 4) Circuit Efficiency and Power Dissipation
- 5) RSENSE Kelvin Connections

### 1) RSENSE Voltage Loss

For lowest IR voltage loss in RSENSE, the smallest usable value for RSENSE should be selected.

# 2) $V_{\text{OUT}}$ Swing vs. Applied Input Voltage at $V_{\text{RS+}}$ and Desired $V_{\text{SENSE}}$

As there is no separate power supply pin for the TSM9634, the circuit draws its power from the applied voltage at both its RS+ and RS- terminals. Therefore, the signal voltage at the OUT terminal is bounded by the minimum supply voltage applied to the TSM9634.

Therefore,

$$V_{OUT(max)} = V_{RS+(min)} - V_{SENSE(max)} - V_{OH(max)}$$

stage is protected against input overdrive by use of an output current-limiting circuit of 3mA (typical) and a 7V internal clamp protection circuit.

# Table 1: Internal Gain Setting Resistors (Typical Values)

GAIN (V/V)	<b>R1 (</b> Ω)	<b>ROUT (</b> Ω)	Part Number
25	400	10k	TSM9634T
50	200	10k	TSM9634F
100	100	10k	TSM9634H
200	100	20k	TSM9634W

and

$$R_{SENSE} = \frac{V_{OUT} (max)}{GAIN \times I_{LOAD} (max)}$$

where the full-scale V<sub>SENSE</sub> should be less than V<sub>OUT(MAX)</sub>/GAIN at the application's minimum RS+ terminal voltage. For best performance with a 3.6V power supply, RSENSE should be chosen to generate a V<sub>SENSE</sub> of: a) 120mV (for the 25V/V GAIN option), b) 60mV (for the 50V/V GAIN option), c) 30mV (for the 100V/V GAIN option), or d) 15mV (for the 200V/V GAIN option) at the full-scale I<sub>LOAD(MAX)</sub> current in each application. For the case where the minimum power supply voltage is higher than 3.6V, each of the four full-scale V<sub>SENSE</sub>s above can be increased.

### 3) Total ILOAD Accuracy

In the TSM9634's linear region where  $V_{OUT} < V_{OUT(max)}$ , there are two specifications related to the circuit's accuracy: a) the TSM9634's input offset voltage ( $V_{OS} = 250\mu V$ , max) and b) its gain error (GE(max) = 0.5%). An expression for the TSM9634's total output voltage (+ error) is given by:

 $V_{OUT} = [GAIN x (1 \pm GE) x V_{SENSE}] \pm (GAIN x V_{OS})$ 

A large value for RSENSE permits the use of smaller load currents to be measured more accurately because the effects of offset voltages are less significant when compared to larger  $V_{\text{SENSE}}$  voltages. Due care though should be exercised as



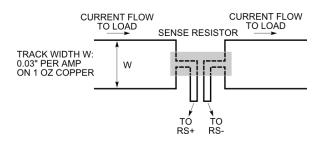
previously mentioned with large values of RSENSE.

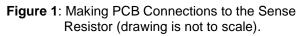
### 4) Circuit Efficiency and Power Dissipation

IR losses in RSENSE can be large especially at high load currents. It is important to select the smallest, usable RSENSE value to minimize power dissipation and to keep the physical size of RSENSE small. If the external RSENSE is allowed to dissipate significant power, then its inherent temperature coefficient may alter its design center value, thereby reducing load current measurement accuracy. Precisely because the TSM9634's input stage was designed to exhibit a very low input offset voltage, small RSENSE values can be used to reduce power dissipation and minimize local hot spots on the pcb.

### 5) **RSENSE** Kelvin Connections

For optimal  $V_{\text{SENSE}}$  accuracy in the presence of large load currents, parasitic pcb track resistance should be minimized. Kelvin-sense pcb connections





between RSENSE and the TSM9634's RS+ and RSterminals are strongly recommended. The drawing in Figure 1 illustrates the connections between the current-sense amplifier and the current-sense resistor. The pcb layout should be balanced and symmetrical to minimize wiring-induced errors. In addition, the pcb layout for RSENSE should include good thermal management techniques for optimal RSENSE power dissipation.

### **Optional Output Filter Capacitor**

If the TSM9634 is part of a signal acquisition system where its OUT terminal is connected to the input of an ADC with an internal, switched-capacitor track-and-hold circuit, the internal track-and-hold's sampling capacitor can cause voltage droop at  $V_{OUT}$ . A 22nF to 100nF good-quality ceramic capacitor from the OUT terminal to GND should be used to minimize voltage droop (holding  $V_{OUT}$  constant during the sample interval. Using a capacitor on the OUT terminal will also reduce the TSM9634's small-signal bandwidth as well as band-limiting amplifier noise.

# Using the TSM9634 in Bidirectional Load Current Applications

In many battery-powered systems, it is oftentimes necessary to monitor a battery's discharge and charge currents. To perform this function, a bidirectional current-sense amplifier is required. The circuit illustrated in Figure 2 shows how two TSM9634s can be configured as a bidirectional current-sense amplifier. As shown in the figure, the

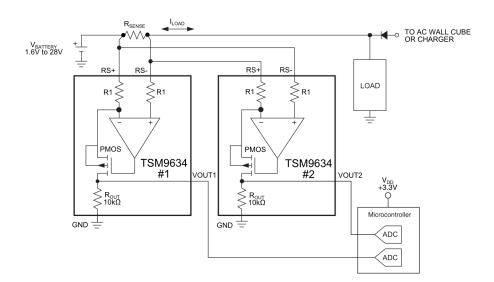


Figure 2: Using Two TSM9634s for Bidirectional Load Current Detection



RS+/RS- input pair of TSM9634 #2 is wired opposite in polarity with respect to the RS+/RS- connections of TSM9634 #1. Current-sense amplifier #1 therefore measures the discharge current and current-sense amplifier #2 measures the charge current. Note that both output voltages are measured with respect to GND. When the discharge current is being measured,  $V_{OUT1}$  is active and  $V_{OUT2}$ is zero; for the case where charge current is being measured,  $V_{OUT1}$  is zero, and  $V_{OUT2}$  is active.

### PC Board Layout and Power-Supply Bypassing

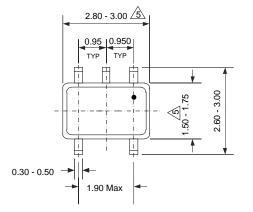
For optimal circuit performance, the TSM9634 should be in very close proximity to the external current-sense resistor and the pcb tracks from RSENSE to the RS+ and the RS- input terminals of the TSM9634 should be short and symmetric. Also recommended are a ground plane and surface mount resistors and capacitors.

# PACKAGE OUTLINE DRAWING

Touchstone

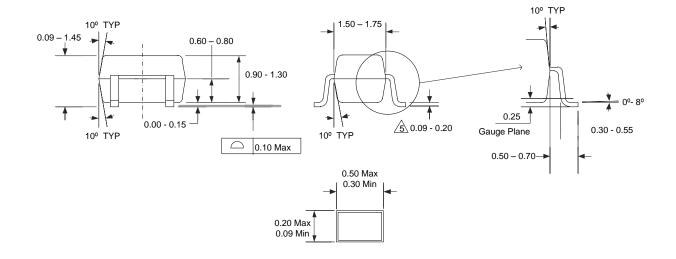
### 5-Pin SOT23 Package Outline Drawing

(N.B., Drawings are not to scale)



#### NOTES:

- 1. Dimensions and tolerances are as per ANSI Y14.5M, 1982.
- 2. Package surface to be matte finish VDI 11~13.
- 3. Die is facing up mold and facing down for trim/form, ie, reverse trim/form.
- 4. The foot length measuring is based on the gauge plane method.
- 5. Dimensions are exclusive of mold flash and gate burr.
- 6. Dimensions are exclusive of solder plating.
- 7. All dimensions are in mm.
- 8. This part is compliant with EIAJ spec. and JEDEC MO-178 AA
- 9. Lead span/stand off height/coplanarity are considered as special characteristic.



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