

SUNTEK

Maximum Input Voltage Rating up to 28V

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Minimum Input Voltage: 3.75V (Typ.)

Programmable Charge Current up to 1A

Input Over Voltage Protection : 6.8V (Typ.) **SK4556 28V 1A Single Li-ion Battery Linear Charger**

GENERAL DESCRIPTION

The SK4556 is a complete constant-current/ constant voltage linear charger for single Lithium-Ion battery with high input voltage rating and large current. The largest input voltage is up to 28V and charge current is up to 1A. The input over voltage protection thread is 6.8V and the lowest input voltage is 3.75V, which can meet the requirement of voltage-adjustment to reduce charging power consumption and improve overall efficiency.

Thermal feedback regulates the charge current to limit the die temperature during high power operation or high ambient temperature. The charge voltage is fixed at 4.2V/4.35V/4.4V/4.45V, and the charge current can be programmed externally with a single resistor.

The SK4556 automatically terminates the charge cycle when the charge current drops to 1/10 the programmed value after the final float voltage is reached.

When the input voltage (supplied by AC adapter or USB power supply) is removed, the SK4556 automatically enters a low current state, decreasing the battery leakage current to less than 1µA.

Other features of SK4556 include over temperature protection, under voltage lockout, automatic recharge and charging state indication (two LED pins to show charge state and charge-ending state).

FEATURES

-
- **•** Minimum Input Voltage: 3.75V (Typ.)
- **•** Programmable Charge Current up to 1A
- Input Over Voltage Protection : 6.8V (Typ.)
- Float Charge Voltage : 4.2V / 4.35V/ 4.4V /4.45V
- Maximum BAT withstand voltage up to 20V
- 1% Charge Voltage Accuracy
- **•** Battery reverse connection protection
- **•** Thermal Regulation to Maximize Charge Rate Without Risk of Overheating
- **1/10C Termination Charge Current**
- Charging status and fault status indication
- **•** Battery Temperature Monitoring
- Chip Enable Input
- Trickle charge threshold: 2.9V (Float Voltage: 4.2V,Typ.)
- Soft-start and surge current limit
- Available ESOP8, DFN2x2-8L, DFN3x3-8L, DFN3x2-10L, DFN3x3-10L Packages

APPLICATIONS

- Standby power supply/ portable power source
- mobile phone, PDA, GPS
- MP3, MP4 player
- Digital camera, electronic dictionary
- Portable devices, Various charg

V_{cc} $1K \leq$ $R1 \le R1$
 $R1 \le R2$
 $R1 \le R1$
 $R1 \le R1$
 $R1 \le R1$
 $R1 \le R1$
Battery C
Battery $_{\rm R1}$ \leq $\overline{+}$ BAT $\begin{array}{|c|c|c|}\n\hline\n\text{10uF} & \text{5} & \text{00uF} \\
\hline\n\text{20uF} & \text{10uF} & \text{10uF} \\
\hline\n\end{array}$ CF TEMP *SK4556* 1 FULL 6 CHG $\qquad \qquad$ $\qquad \qquad$ 7 2 E
El 3 R3 \geq R3 GND

TYPICAL APPLICATION CIRCUIT

PIN ASSIGNMENT

 $\overline{1}$ \bullet 10 CE **TEMP** 11 Thermal pad $\begin{bmatrix} 9 \end{bmatrix}$ CHG PROG $\overline{2}$: $\begin{bmatrix} 8 \end{bmatrix}$ **FULL GND** 3 $\overline{4}$ $\begin{bmatrix} 7 \end{bmatrix}$ **BAT** vcc **NC** $\overline{5}$ $\begin{bmatrix} 6 \end{bmatrix}$ NC DFN3x2-10L / DFN3x3-10L

(Top view)

(Top view) (Top view)

PIN DESCRIPTION

ORDERING INFORMATION

MARKING DESCRIPTION

(DFN2x2-8L / DFN3x2-10L)

XY: Internal control code

W: Code of production week. "A" means 1st week, "Z" means 26th week,

"a" means 27th week, "z" means 52nd week.

V: Voltage code

(DFN3x3-8L / DFN3x3-10L)

XXY: Internal control code

W: Code of production week. "A" means $1st$ week, "Z" means 26th week, "a" means 27th week, "z" means 52nd week.

V: Voltage code

X, BB: Internal control code YM: Date code AA: Series number V: Voltage code

ABSOLUTE MAXIMUM RATINGS (Note1)

Note 1: Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

RECOMMENDED OPERATING CONDITION

ELECTRICAL CHARACTERISTICS

The following specifications apply for V_{CC}=5V T_A=25[°]C, unless specified otherwise.

ELECTRICAL CHARACTERISTICS(Continued)

The following specifications apply for Vcc=5V T_A=25[°]C, unless specified otherwise.

TYPICAL CHARACTERISTICS

TYPICAL COMPLETED CHARGING CURVE

APPLICATION INFORMATIONS

The SK4556 is a single cell Li-Ion battery liner charger using a constant-current /constant-voltage algorithm. Charging current can be programmed with external resistor and maximum continuous charging current is up to 1A. The SK4556 contains two open-drain indicators for the charge status indicate, one is CHG (charging status), and the other is FULL (full-charged status). FULL can be also used to indicate fault status. Inner temperature management circuit can automatically decrease charging current when Junction Temperature is over TLIM. This function can maximize the load capacity of the chip and prevent the damage to chip or external component caused by overtemperature.

The SK4556 begins a charge cycle when the voltage at the VCC pin rises above the UVLO threshold level. Thus, the CHG pin is pulled low, which means charging is in progress. If the BAT pin is less than the VTRIKL, the charger enters trickle charge mode. In this mode, the SK4556 supplies approximately 1/10 the programmed charge current to bring the battery voltage up to a safe level for full current charging. When the BAT pin voltage rises above the VTRIKL, the charger enters constant-current mode, where the programmed charge current is supplied to the battery. When the BAT pin approaches the final float voltage, the SK4556 enters constant-voltage mode and the charge current begins to decrease. The charging cycle terminates when the charging current drops to charging-over threshold. Under this condition, output of CHG is in high-impedance state while output of FULL is in low potential.

Charging-over threshold is 10% of constant charging current. A new charging cycle is started when battery voltage drops below recharging voltage threshold. High-accuracy inner reference voltage source makes sure a float voltage accuracy of 1%, which meets the requirements of Li-ion and Li-polymer battery.

The charger enters sleeping mode with low power consumption when input voltage drops or lower than battery voltage. In this mode, current consumed by battery is lower than 1uA, which helps to increase standby time. The charger stops charging when enable input CE is connected to low level.

Input Overvoltage Protection

The SK4556 has built-in input voltage surge protection as high as 28V. The charger cycle will be automatically closed when the input voltage is higher than 6.8V to avoid high-voltage damage and reworks when input voltage is below 6.8V.

Setting of Charging Current

The charge current is set by a resistor connecting between the PROG pin and GND. The relationship of the charging current and the programming resistance is established by the following equations:

$$
R_{\text{PROG}} = \frac{1000}{I_{BAT}}
$$

In applications, R_{PROG} could be selected according to requirements.

Relationship between R_{PROG} and charge current could be as follow:

Charging Termination

A charge cycle is terminated when the charge current falls to 1/10th the programmed value after the final float voltage is reached. When the time that PROG pin voltage falls below 150mV (typ.) is longer than T_{TERM} and charging cycle is terminated. Then SK4556 enters standby mode, and input current drops to 155uA (typ.).

The chip has designed the function of preventing the false turn off caused by the load transient jump. 1ms TTERM on Terminating Comparator prevents the early termination caused by load transient. Once the average charging current drops to 1/10 of the preset value and ends the charge cycle. No more current is outputted to BAT. Under this state, all load of BAT is powered by battery.

In standby mode, SK4556 keeps monitoring voltage of BAT pin. When BAT pin voltage drops below VRECHRG (recharge threshold Voltage), another charge cycle starts and supplies current to power again. Pic 1 shows a typical charging cycle.

PIC 1: A Typical Charging Cycle

Charge Status Indicator (CHG and FULL)

SK4556 has two different open-drain status outputs of charge status, one is CHR, and the otheris FULL. If those two outputs are connected to LED light, light goes on when the pin to pull low and light goes off when high impedance.

Battery temperature monitor works when typical connection of TEMP pin is used. No-battery pulse signal is outputted by CHG pin if battery is not connected to charger. CHG and FULL pin will be in high-impedance state if battery temperature is out of normal range.

Battery temperature monitor doesn't work if TEMP is connected to GND. No-battery pulse signal is outputted by CHG pin if battery is not connected to charger.

When the external capacitance of BAT pin connected to battery is 10uF, flash frequency of CHG is 1-4s. The output of status indicator should be connected to GND, when status indicator function is not used. When the external capacitance of BAT pin

ponnected to battery is 10uF, flash frequency of

HG is 1-4s. The output of status indicator should

e connected to GND, when status indicator

unction is not used.

efer to the f

Refer to the following table for the function of status indication:

Thermal Limit

If the chip temperature is above preset T_{LIM} , an inner thermal reflective circuit will decrease charging current. This function can prevent SK4556 from overheating and damage caused by increase load capacity. Charging current can be set according to typical (not the worst) ambient temperature on the premise that the charger will automatically reduce the current under the worst conditions.

Battery Temperature Monitoring

To prevent damage to battery caused by too high or too low temperature, the SK4556 integrates batter temperature monitoring circuit. It monitors temperature by measuring the voltage of TEMP PIN. The voltage is developed by a NTC thermistor and an external voltage divider, which is showed by typical application circuit.

SK4556 Compares this voltage against its internal VLOW and V_{HIGH} to make sure if the battery temperature exceeds normal range. Inner SK4556, V_{LOW} is fixed at 45% \times V_{CC} (K₁) and V_{HIGH} is fixed at 80% \times V_{cc} (K₂). The charging cycle will be suspended when $V_{\text{TEMP}} < V_{\text{LOW}}$ or $V_{\text{TEMP}} > V_{\text{HIGH}}$, which means battery temperature is too high or too low. The charging cycle will continue if V_{TEMP} is in the range of V_{LOW} and V_{HIGH} .

The battery temperature monitoring function will be forbidden if the TEMP pin is connected to ground.

Determining the Value of R¹ and R²

The values of R_1 and R_2 shall be determined according to the temperature monitoring range of the battery and the resistance value of the Therefore, in T_L , the voltage of TEMP is **SUNTEK**
thermistor. Examples are as follows: If the preset
battery temperature is from T_L to T_H , $(T_L \leq T_H)$ and
the negative temperature coefficient (NTC)
thermistor is used, R_{TL} means the resistance of T_L **SUNTEK**
thermistor. Examples are as follows: If the preset
battery temperature is from T_L to T_H, (T_L $\lt T_H$) and
the negative temperature coefficient (NTC)
thermistor is used, R_{TL} means the resistance of T_L
and **SUNTEK**
thermistor. Examples are as follows: If the preset
battery temperature is from T_L to T_H , $(T_L < T_H)$ and
the negative temperature coefficient (NTC)
thermistor is used, R_{TL} means the resistance of T_L
and $R_{$ **SUNTEK**
thermistor. Examples are as follows: If the preset
battery temperature is from T_L to T_H, (T_L < T_H) and
the negative temperature coefficient (NTC)
thermistor is used, R_{TL} means the resistance of T_L
and Example 15 and Section 1 and the preset

2 is from T_L to T_H, (T_L < T_H) and

imperature coefficient (NTC)
 R_{TL} means the resistance of T_L

resistance of T_H. Then R_{TL} > R_{TH} .

voltage of TEMP is
 $\frac{R_2$ ws: If the preset
 T_{H} , ($T_{L} < T_{H}$) and

befficient (NTC)

e resistance of T_{L}
 H . Then $R_{TL} > R_{TH}$.

MP is
 \times VIN
 \times VIN

(K2=0.8) thermistor. Examples are as follows: If the preset

battery temperature is from T_L to T_H, (T_L \lt T_H) and

the negative temperature coefficient (NTC)

thermistor is used, R_{TL} means the resistance of T_L

and R R_{TL} means the resistance of T_L

resistance of T_H. Then $R_{TL} > R_{TH}$.

voltage of TEMP is
 $\frac{R_2||R_{TL}}{R_1 + R_2||R_{TL}} \times VIN$

TEMP is:
 $\frac{R_2||R_{TH}}{R_1 + R_2||R_{TH}} \times VIN$

41GH = K2 × V_{CC} (K2=0.8)

LOW = K1 × V_{CC} (K1=0. resistance of T_L

H. Then R_{TL} > R_{TH}.

AP is
 \times *VIN*
 \times *VIN*
 (K2=0.8)
 (K1=0.45)
 $\frac{\text{K}_1}{\text{K}_1}$ battery temperature is from T_L to T_H , $(T_L \sim$
the negative temperature coefficient
thermistor is used, R_{TL} means the resistan
and R_{TH} means the resistance of T_H . Then R
Therefore, in T_L , the voltage of TEMP i

$$
V_{\text{TEMPI}} = \frac{R_2 || R_{TL}}{R_1 + R_2 || R_{TL}} \times \text{VIN}
$$

$$
V_{\text{TEMPH}} = \frac{R_2 || R_{TH}}{R_1 + R_2 || R_{TH}} \times \text{VIN}
$$

$$
V_{\text{TEMPI}}\!=\!V_{\text{HIGH}}\!=\!K2\!\times\!V_{\text{CC}}\left(K2\!=\!0.8\right)
$$

$$
V_\text{TEMPH} \!=\! V_\text{LOW} \!=\! K1 \!\times\! V_\text{CC} \left(K1\text{=}0.45\right)
$$

and RTH means the resistance of ΗH. Then RTL > RTH.
\nTherefore, in T_L, the voltage of TEMP is
\n
$$
V_{TEMPL} = \frac{R_2||R_{TL}}{R_1 + R_2||R_{TL}} \times VIN
$$
\nIn T_H, the voltage of TEMP is:
\n
$$
V_{TEMPH} = \frac{R_2||R_{TH}}{R_1 + R_2||R_{TH}} \times VIN
$$
\nThen, according to
\n
$$
V_{TEMPL} = V_{HIGH} = K2 \times V_{CC} \text{ (K2=0.8)}
$$
\n
$$
V_{TEMPH} = V_{LOW} = K1 \times V_{CC} \text{ (K1=0.45)}
$$
\nWe get equals below:
\n
$$
R_1 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{(R_{TL} - R_{TH})K_1K_2}
$$
\n
$$
R_2 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{R_{TL}(K_1 - K_1K_2) - R_{TH}(K_2 - K_1K_2)}
$$
\nSimilarly, if there is a positive temperature coefficient (PTC) thermistor, according to R_{TL}
\nR_{TH}, we get the equals below:
\n
$$
R_1 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{(R_{TH} - R_{TL})K_1K_2}
$$
\n
$$
R_{LT} = \frac{R_{TL}R_{TH}(K_2 - K_1)}{(R_{TH} - R_{TL})K_1K_2}
$$

 $V_{\text{TEMPH}} = \frac{R_2 || R_{TH}}{R_1 + R_2 || R_{TH}} \times V I N$

Then, according to
 $V_{\text{TEMPH}} = V_{\text{HIGH}} = K2 \times V_{\text{CC}}$ (K2=0.8)
 $V_{\text{TEMPH}} = V_{\text{LOW}} = K1 \times V_{\text{CC}}$ (K1=0.45)

We get equals below:
 $R_1 = \frac{R_{TL} R_{TH} (K_2 - K_1)}{(R_{TL} - R_{TH}) K_1 K_2}$
 $R_2 =$ Then, according to
 $R_1 + R_2\left|1R_7H\right|$

Then, according to
 $V_{\text{TEMPH}} = V_{\text{HIGH}} = K2 \times V_{\text{CC}}$ (K2=0.8)
 $V_{\text{TEMPH}} = V_{\text{LOW}} = K1 \times V_{\text{CC}}$ (K1=0.45)

We get equals below:
 $R_1 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{(R_{TL} - R_{TH})K_1K_2}$
 $R_2 = \$ Then, according to
 $V_{\text{TEMPH}} = V_{\text{HighH}} = K2 \times V_{\text{CC}}$ (K2=0.8)
 $V_{\text{TEMPH}} = V_{\text{LOW}} = K1 \times V_{\text{CC}}$ (K1=0.45)

We get equals below:
 $R_1 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{(R_{TL} - R_{TH})K_1K_2}$
 $R_2 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{R_{TL}(K_1 - K_1K_2) - R_{TH}(K_2 -$

$$
R_1 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{(R_{TL} - R_{TH})K_1K_2}
$$

\n
$$
R_2 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{R_{TL}(K_1 - K_1K_2) - R_{TH}(K_2 - K_1K_2)}
$$

\nllarly, if there is a positive temperature
\nfficient (PTC) thermistor, according to R_{TL}
\nwe get the equals below:
\n
$$
R_1 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{(R_{TH} - R_{TL})K_1K_2}
$$

\n
$$
R_2 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{R_{TH}(K_1 - K_1K_2) - R_{TL}(K_2 - K_1K_2)}
$$

\nan be seen from the above derivation that the
\nperature range to be set is independent of the
\n*ner* voltage *Vce* and only related to R_{12} , R_{23} , R_{T12} .

 $R_{TL} - R_{TH}$ K_1K_2
 $R_{TL}R_{TH}(K_2 - K_1)$
 K_1K_2) $- R_{TH}(K_2 - K_1K_2)$

is a positive temperature

thermistor, according to R_{TL}
 R_{TH} is below:
 $R_{TL}R_{TH}(K_2 - K_1)$
 $R_{TH} - R_{TL}$ K_1K_2
 $R_{TL}R_{TH}(K_2 - K_1)$
 K_1K_2 $R_{TL}R_{TH}(K_2 - K_1)$
 $R_1K_2) - R_{TH}(K_2 - K_1K_2)$

E is a positive temperature

thermistor, according to R_{TL}
 $R_{TL}R_{TH}(K_2 - K_1)$
 $(R_{TH} - R_{TL})K_1K_2$
 $R_{TL}R_{TH}(K_2 - K_1)$
 $- K_1K_2) - R_{TL}(K_2 - K_1K_2)$

in the above derivation t $R_{TL}(K_1 - K_1K_2) - R_{TH}(K_2 - K_1K_2)$

if there is a positive temperature

t (PTC) thermistor, according to $R_{TL} <$

et the equals below:
 $R_1 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{(R_{TH} - R_{TL})K_1K_2}$
 $\frac{R_{TL}R_{TH}(K_2 - K_1)}{R_{TH}(K_1 - K_1K_2) - R_{TL}(K$ $R_2 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{R_{TL}(K_1 - K_1K_2) - R_{TH}(K_2 - K_1K_2)}$

Similarly, if there is a positive temperature

coefficient (PTC) thermistor, according to $R_T < R_{TH}$, we get the equals below:
 $R_1 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{(R_{TH} - R_{TL})K$ $R_2 = \frac{R_{TL}K_{TH}r_H(R_2 - K_1)}{R_{TL}(K_1 - K_1K_2) - R_{TH}(K_2 - K_1K_2)}$

Similarly, if there is a positive temperature

coefficient (PTC) thermistor, according to $R_T < R_{TH}$, we get the equals below:
 $R_1 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{(R_{TH} - R_{TL$ $R_{TL}(R_1 - R_1R_2) - R_{TH}(R_2 - R_1R_2)$

Similarly, if there is a positive temperature

coefficient (PTC) thermistor, according to $R_T < R_{TH}$, we get the equals below:
 $R_1 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{(R_{TH} - R_{TL})K_1K_2}$
 $R_2 = \frac{R_{TL}R_{TH$ Similarly, it there is a positive temperature

coefficient (PTC) thermistor, according to R_{TL}
 R_{TH} , we get the equals below:
 $R_1 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{(R_{TH} - R_{TL})K_1K_2}$
 $R_2 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{R_{TH}(K_1 - K_1K_2) - R_{TL}($ coefficient (PTC) thermistor, according to R_{TH} , R_{TH} , we get the equals below:
 $R_1 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{(R_{TH} - R_{TL})K_1K_2}$
 $R_2 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{R_{TH}(K_1 - K_1K_2) - R_{TL}(K_2 - K_1K_2)}$

It can be seen from the abo $R_1 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{(R_{TH} - R_{TL})K_1K_2}$
 $R_2 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{R_{TH}(K_1 - K_1K_2) - R_{TL}(K_2 - K_1K_2)}$

It can be seen from the above derivation that the

temperature range to be set is independent of the

power voltage V $R_1 = \frac{R_{TL}K_{TH}(R_2 - R_1)}{(R_{TH} - R_{TL})K_1K_2}$
 $R_2 = \frac{R_{TL}R_{TH}(K_2 - K_1)}{R_{TH}(K_1 - K_1K_2) - R_{TL}(K_2 - K_1K_2)}$

It can be seen from the above derivation that the

temperature range to be set is independent of the

power voltage V $(R_{TH} - R_{TL}R_{1}R_{2})$
 $R_{2} = \frac{R_{TL}R_{TH}(K_{2} - K_{1})}{R_{TH}(K_{1} - K_{1}K_{2}) - R_{TL}(K_{2} - K_{1}K_{2})}$

It can be seen from the above derivation that the

temperature range to be set is independent of the

power voltage V_{CC}. and only re $R_2 = \frac{R_{TL}R_{TH}(R_2 - R_1)}{R_{TH}(K_1 - K_1K_2) - R_{TL}(K_2 - K_1K_2)}$
It can be seen from the above derivation that the
temperature range to be set is independent of the
power voltage V_{CC}. and only related to R₁, R₂, R_{TH},
R_T $R_{TH}(R_1 - R_1R_2) - R_{TL}(R_2 - R_1R_1R_2)$
It can be seen from the above derivation
temperature range to be set is independ
power voltage V_{CC}. and only related to R
 R_{TL} . R_{TH} , R_{TL} can be obtained from relev
manual or **Examples of TEMP Resistance Calculation:**

TEMPLE-7°C, THEMPLE-7°C, And Only related to R₁, R₂, R_{TH},

R_{TL}. R_{TH}, R_{TL} can be obtained from relevant battery

manual or through experimental tests. In

application temperature range to be set is independent of the
power voltage V_{CC}. and only related to R₁, R₂, R_{TH},
R_{TL}. R_{TH}, R_{TL} can be obtained from relevant battery
manual or through experimental tests. In
application, bower voltage v_{CC}. and only related to κ_1 , κ_2 , κ_{TH} , κ_{TL} . R_{TH} , R_{TL} can be obtained from relevant battery
manual or through experimental tests. In
pplication, R_2 can be ignored if we only focu Fit. NTHS NTL Call be obtained Hoffreevalt battery
manual or through experimental tests. In
pplication, R₂ can be ignored if we only focus on
emperature characteristics at one end, like
wer-heating protection. Then we w application, R_2 can be ignored in we only locus
temperature characteristics at one end, li
over-heating protection. Then we will only foc
on R_1 and the derivation of R_1 will be easier, whi
won't be given details. temperature characteristics at one end, the
over-heating protection. Then we will only focus
on R₁ and the derivation of R₁ will be easier, which
won't be given details.
Examples of TEMP Resistance Calculation:
TEMP

Under-voltage Lockout

Build-in under voltage lockout circuit monitors the input voltage and keeps the charger in shutdown mode until VCC rises above the under-voltage lockout threshold. If the UVLO comparator is tripped, the charger will not come out of shutdown mode until VCC rises 100mV above the battery voltage.

Automatic Recharge

Once the charging cycle is terminated, the SK4556 uses a filtering time Comparator (tRECHARGE) to monitor the voltage on the BAT pin. Once battery voltage drops below ΔV_{RECHRG} (Almost 80% to 90% of Battery capacity), charging cycle reworks, which makes sure the battery is kept in full-charged (or almost full-charged) state and avoids starting a periodic charging cycle. In recharging cycle, the output of CHG pin enters a strong pull-down state.

Consideration of Stability

Under constant current mode, it is the PROG pin not the battery that in the feedback loop. The stability of constant-current mode is affected by impedance of PROG pin. When there is no additional capacitance on the PROG pin, the maximum allowable resistance value of the preset resistance will be reduced. The maximum resistance value can be calculated by the equals below: Example the PROG pin, the also

resistance value of the preset rise

reduced. The maximum

be calculated by the equals **Soft**

A so
 $\frac{1}{2\pi \times 10^5 \times C_{PROG}}$ curr

more interested in charging chai

more interested in char For user, they are more interested in charging

for user, the stability of constant-current mode is affected by

sources n the

additional capacitance on the PROG pin, the

maximum allowable resistance value of the preset Example the URL Constant-current mode is a
recited by
impedance of PROG pin. When there is no
additional capacitance on the PROG pin, the
maximum allowable resistance value of the preset
resistance will be reduced. The ma Impedance or PROG pin. When there is no

additional capacitance on the PROG pin, the

maximum allowable resistance value of the preset

resistance value can be calculated by the equals

Soft star

below:
 $R_{PROG} \leq \frac{1}{2\$

$$
R_{\text{PROG}} \le \frac{1}{2\pi \times 10^5 \times C_{PROG}}
$$

additional capacitance on the PROG pin, the

maximum allowable resistance value of the preset

resistance value can be calculated by the equals

Soft start for

below:

A soft-start circle connected to battery,

For user, maximum allowable resistance value of the preset

resistance will be reduced. The maximum

resistance value can be calculated by the equals

Soft start for

below:

A soft-start circle

below:

A soft-start for
 $R_{PROG} \leq$

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important than the transient current. In this

condition, a simple RC filter on prog PIN can be

used to measure the average current. (Showed by

PIC 2). An additional 10k resistance is added **SUNTEK**

important than the transient current. In this

condition, a simple RC filter on prog PIN can be

used to measure the average current. (Showed by

PIC 2). An additional 10k resistance is added

between PROG pin an **SUNTEK**

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PIC 2). An additional 10k resistance is added

between PROG pin an stability.

Thermal Design

Due to the small package dimension of ESOP8, an elaborate thermal design of PCB layout, which is used for increasing usable charging current to maximum extent, is very important. The heat radiation circuit, used to dissipate the heat generated by IC, runs from chip to lead frame, and arrives PCB copper foil (which is an auxiliary radiator) through radiator below. The measure of copper foil, connected to radiator, should be as large as possible and stretch out to external larger copper foil to spread the heat to surrounding environment. The holes placed on the middle layer or back copper foil layer are also useful in improving the overall thermal performance of the charger. When designing PCB layout, other heat sources n the circuit board not related to the charger must also be considered. Because they will also have an impact on the overall temperature rise and the maximum charging current.

Soft start for charging current

A soft-start circuit is designed to decrease inrush current to maximum extent at the beginning of charging cycle. When a charging cycled starts, the charging current will rise from 0 to the max in around 20μs, which can decrease the load of transient current to the maximum.

Protection of Reverse Connection of Battery

In SK4556, a reversed-connection protection circuit is designed to avoid the damage to chips caused by reverse connection of battery during production and assembly.

Reverse Polarity Input Voltage Protection

In some applications, reverse polarity voltage protection of VCC is necessary. A series isolating diode can be used if power voltage is high enough. Under other conditions that need to keep low voltage, a P channel MOSFET can be chose.

PIC 3: VCC Reverse Protection

USB and AC adapter Power Supply

SK4556 allows charging from an AC adapter or an

USB port. Pic 4 shows a real example of how to

combine AC adapter with USB. A P channel

MOSFET (MP1) is use

SUNTEK
USB port when AC adapter is connected. A
Schottky diode is used to prevent USB power
consumption when it passes 1K pull-down resistor. **SUNTEK**
USB port when AC adapter is connected. A
Schottky diode is used to prevent USB power
consumption when it passes 1K pull-down resistor.
Generally, current supplied by AC adapter is larger **SUNTEK**
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Generally, current supplied by AC adapter is larger
than that supplied by USB, USB port when AC adapter is connected. A
Schottky diode is used to prevent USB power
consumption when it passes 1K pull-down resistor.
Generally, current supplied by AC adapter is larger
than that supplied by USB, which li USB port when AC adapter is
Schottky diode is used to preve
consumption when it passes 1K pul
Generally, current supplied by AC a
than that supplied by USB, which
500mA. Therefore, when AC adapt
a N channel MOSFET (MN1) an

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