

## General Description

The TP8290S6 is a high efficiency 2MHz, adaptive constant OFF time controlled asynchronous step-down DC-DC regulator capable of delivering 300mA output current. The TP8290S6 operates over a wide input voltage range from 5V to 40V.

Low output voltage ripple and small external inductor and capacitor sizes are achieved with 2MHz switching frequency.

## Applications

- 5-40V input voltage range
- 2MHz switching frequency
- Adaptive constant OFF time control
- Internal softstart limits the inrush current
- 2% 0.6V reference
- RoHS Compliant and Halogen Free
- Compact package: SOT23-6

## Features

- Smart meter
- Set Top Box
- Portable TV
- Access Point Router
- DSL Modem
- LCD TV

## TYPICAL APPLICATION

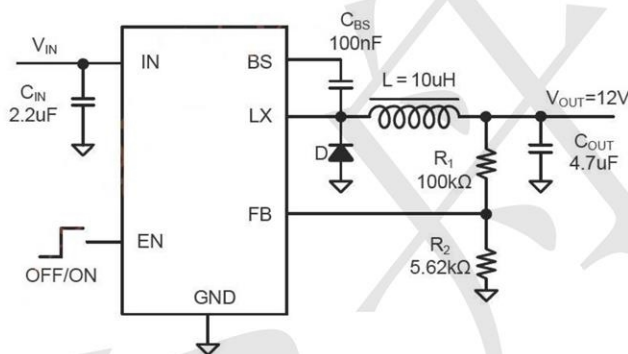


Figure 1 Schematic Diagram

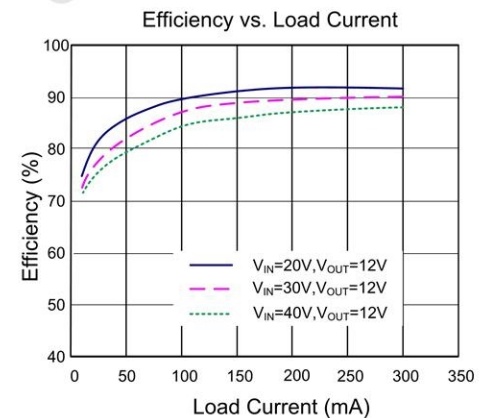
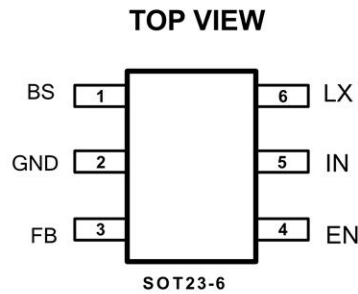


Figure 2 Efficiency Figure

## PIN CONFIGURATION



Pin Name	Pin Number	Pin Description
BS	1	Boot-Strap Pin. Supply high side gate driver. Decouple this pin to LX pin with 0.1uF ceramic cap.
GND	2	Ground pin
FB	3	Output Feedback Pin. Connect this pin to the center point of the output resistor divider (as shown in Figure 1) to program the output voltage: $V_{OUT}=0.6*(1+R1/R2)$
EN	4	Enable control. Pull high to turn on. Do not float.
IN	5	Input pin. Decouple this pin to GND pin with at least 1uF ceramic cap
LX	6	Inductor pin. Connect this pin to the switching node of inductor

### Absolute Maximum Rating ( $T_A=25^\circ\text{C}$ unless otherwise noted)

Supply Input Voltage	42V
Enable Voltage	$V_{IN} + 0.6\text{V}$
FB Voltage	3.6V
BS to LX Voltage	3.6V
Power Dissipation, PD @ $T_A = 25^\circ\text{C}$ , SOT23-6	0.4W
Package Thermal Resistance (Note 2)	
$\theta_{JA}$	250°C/W
$\theta_{JC}$	130°C/W
Junction Temperature Range	150°C
Lead Temperature (Soldering, 10 sec.)	260°C
Storage Temperature Range	-65°C to 150°C

### Recommended Operating Conditions

Supply Input Voltage	5V to 40V
BS to LX Voltage	3.3V
Junction Temperature Range	-40°C to 125°C
Ambient Temperature Range	-40°C to 85°C

**Electrical Characteristics** ( $T_A = 25\text{ C}$  unless otherwise noted)

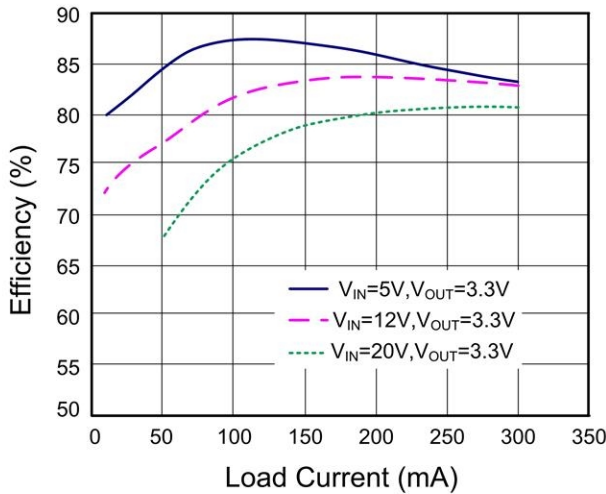
( $V_{IN} = 20\text{V}$ ,  $V_{OUT} = 12\text{V}$ ,  $L = 10\mu\text{H}$ ,  $C_{OUT} = 4.7\mu\text{F}$ ,  $T_A = 25^\circ\text{C}$ ,  $I_{OUT} = 100\text{mA}$  unless otherwise specified)

Parameter	Symbol	Test Conditions	Min	Typ	Max	Unit
Input Voltage Range	$V_{IN}$		5		40	V
Input UVLO Threshold	$V_{UVLO}$	Rising		4.9		V
Input UVLO Hysteresis	$V_{UVLO\ HYS}$			200		mV
Quiescent Current	$I_Q$	$I_{OUT}=0$ , $V_{FB}=V_{REF}\times 105\%$		160		$\mu\text{A}$
Shutdown Current	$I_{SHDN}$	$EN=0$			10	$\mu\text{A}$
Feedback Reference Voltage	$V_{REF}$		0.588	0.6	0.612	V
FB Input Current	$I_{FB}$	$V_{FB}=V_{IN}$	-50	10	50	nA
Power FET RON	$R_{DS(ON)1}$			2		$\Omega$
Power FET Current Limit	$I_{LIM}$		450			mA
EN Rising Threshold	$V_{ENH}$		1.5			V
EN Falling Threshold	$V_{ENL}$				0.4	V
Minimum OFF Time	$T_{OFF}$				100	ns
Minimum ON Time	$T_{OFF}$				100	ns
Soft Start Time	$T_{SS}$			400		$\mu\text{s}$
Switching Frequency	$F_{SW}$		1.6	2	2.4	MHz
Thermal Shutdown Temperature	$T_{SD}$			150		$^\circ\text{C}$
Thermal Recovery Hysteresis	$T_{HYS}$			15		$^\circ\text{C}$

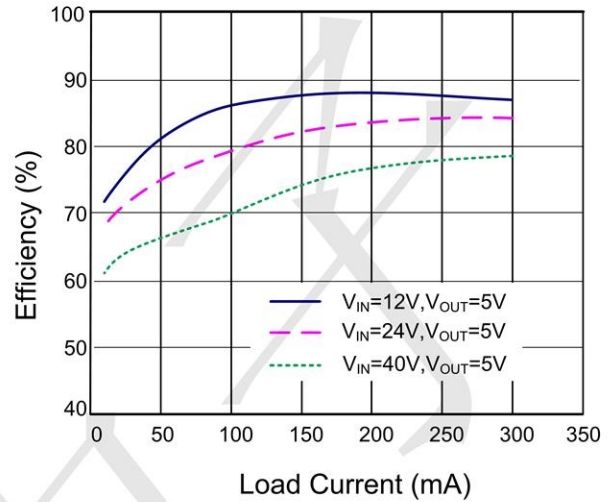


**Typical Performance Characteristics**

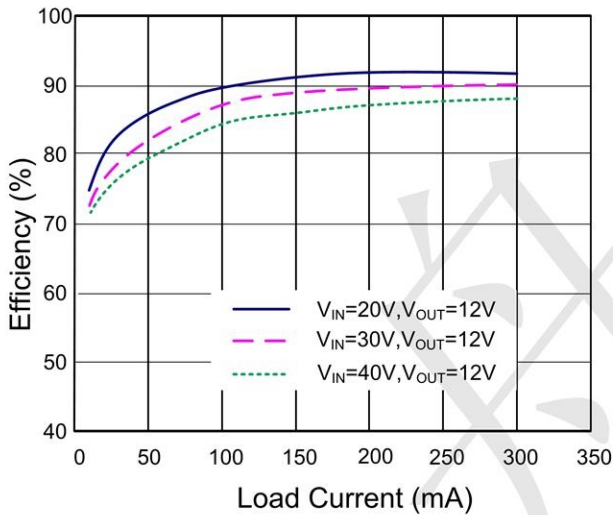
Efficiency vs. Load Current



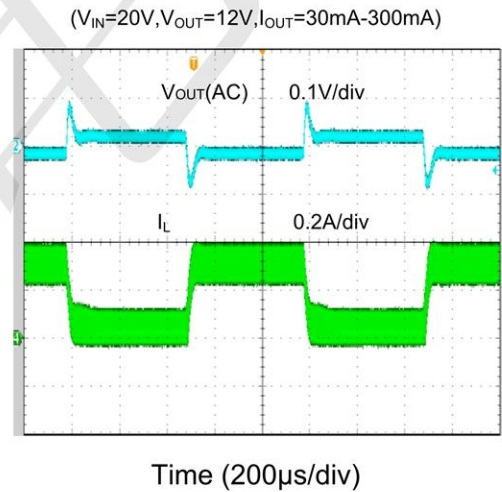
Efficiency vs. Load Current



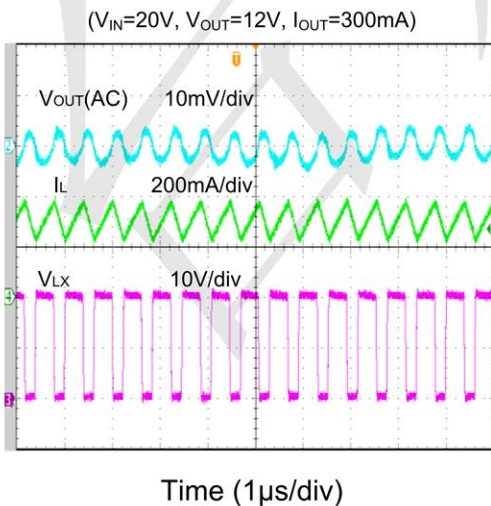
Efficiency vs. Load Current



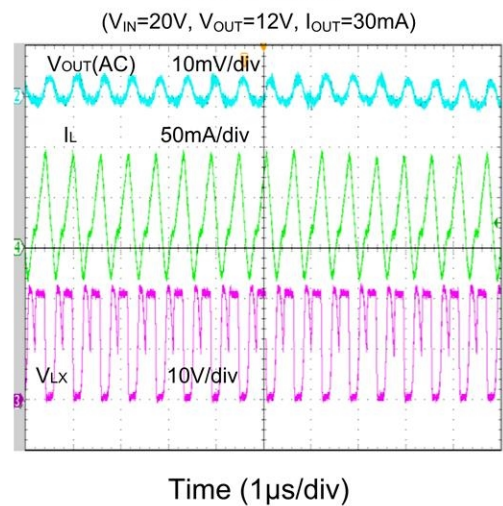
Load Transient



Output Ripple

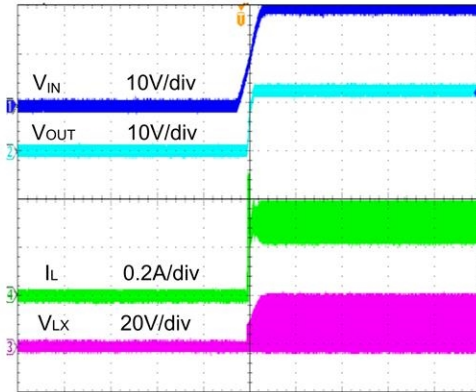


Output Ripple



### Startup From VIN

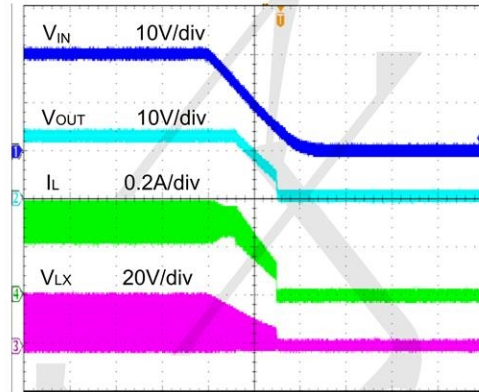
( $V_{IN}=20V$ ,  $V_{OUT}=12V$ ,  $I_{OUT}=300mA$ )



Time (4ms/div)

### Shutdown From VIN

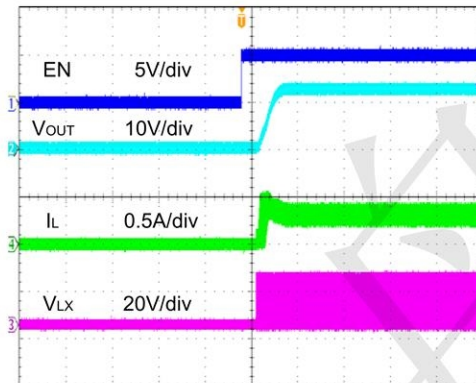
( $V_{IN}=20V$ ,  $V_{OUT}=12V$ ,  $I_{OUT}=300mA$ )



Time (20ms/div)

### Startup From Enable

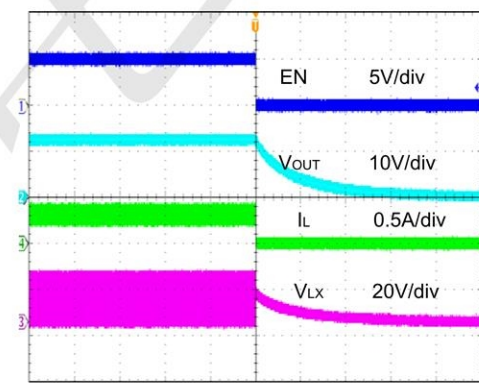
( $V_{IN}=20V$ ,  $V_{OUT}=12V$ ,  $I_{OUT}=300mA$ )



Time (800 $\mu$ s/div)

### Shutdown From Enable

( $V_{IN}=20V$ ,  $V_{OUT}=12V$ ,  $I_{OUT}=300mA$ )



Time (200 $\mu$ s/div)



# FUNCTIONAL DESCRIPTION

## Operation

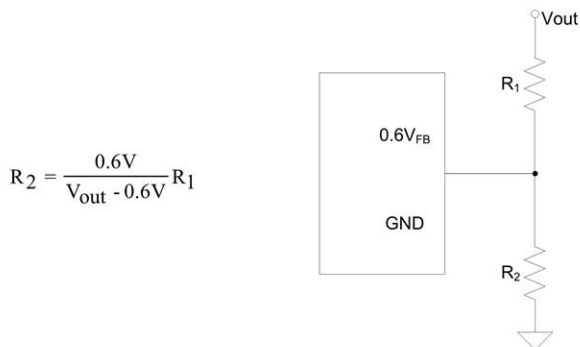
TP8290 is an asynchronous buck regulator IC that integrates the PWM control, main switch on the same die. High switch frequency minimizes the external inductor and capacitor size, thus minimizes the PCB area and cost. It features low output voltage ripple, cycle by cycle current limit output short circuit protection and thermal shutdown protection.

## Applications Information

Because of the high integration in the TP8290 IC, the application circuit based on this regulator IC is rather simple. Only input capacitor  $C_{IN}$ , output capacitor  $C_{OUT}$ , output inductor  $L$  and feedback resistors ( $R_1$  and  $R_2$ ) need to be selected for the targeted applications.

### Feedback resistor dividers $R_1$ and $R_2$

Choose  $R_1$  and  $R_2$  to program the proper output voltage. To minimize the power consumption under light loads, it is desirable to choose large resistance values for both  $R_1$  and  $R_2$ . A value of between  $10k\Omega$  and  $1M\Omega$  is highly recommended for both resistors. If  $V_{out}$  is 5V,  $R_1=100k\Omega$  is chosen, then using following equation,  $R_2$  can be calculated to be  $13.7k\Omega$ :



### Input capacitor $C_{IN}$

The ripple current through input capacitor is calculated as:

$$I_{CIN\_RMS} = I_{OUT} \sqrt{D(1-D)}$$

To minimize the potential noise problem, place a typical X5R or better grade ceramic capacitor really close to the IN pin and the negative end of rectifier. A low ESR ceramic capacitor is recommended with greater than  $1\mu F$  capacitance.

### Output capacitor $C_{OUT}$

The output capacitor is selected to handle the output ripple noise requirements. Both steady state ripple and transient requirements must be taken into consideration when selecting this capacitor. For the best performance, it is recommended to use X5R or better grade ceramic capacitor with greater than  $4.7\mu F$  capacitance.

### Output inductor $L$

There are several considerations in choosing this inductor.

- 1) Choose the inductance to provide the desired ripple current. It is suggested to choose the ripple current to be about 40% of the maximum output current. The

inductance is calculated as:

$$L = \frac{V_{OUT}(1 - V_{OUT}/V_{IN,MAX})}{F_{SW} \times I_{OUT,MAX} \times 40\%}$$

Where  $F_{SW}$  is the switching frequency and  $I_{OUT,MAX}$  is the maximum load current.

The TP8290 regulator IC is quite tolerant of different ripple current amplitude. Consequently, the final choice of inductance can be slightly off the calculation value without significantly impacting the performance.

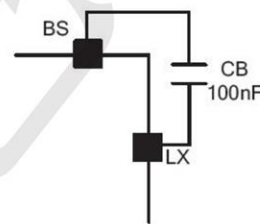
- 2) The saturation current rating of the inductor must be selected to be greater than the peak inductor current under full load conditions.

$$I_{SAT,MIN} > I_{OUT,MAX} + \frac{V_{OUT}(1 - V_{OUT}/V_{IN,MAX})}{2 \times F_{SW} \times L}$$

- 3) The DCR of the inductor and the core loss at the switching frequency must be low enough to achieve the desired efficiency requirement. It is desirable to choose an inductor with  $DCR < 50m\Omega$  to achieve a good overall efficiency.

### External Bootstrap Cap

This capacitor provides the gate driver voltage for internal high side MOSEFET. A  $100nF$  low ESR ceramic capacitor connected between BS pin and LX pin is recommended.

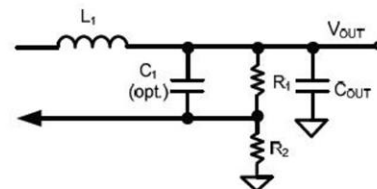


### Rectifier Diode

Because of high switching speed of TP8290 a schottky diode with low forward voltage and fast switching speed is desirable for the application. The voltage rating of the diode must be higher than maximum output voltage. The diode's average and peak current rating should exceed the average output current and peak current.

### Load Transient Considerations

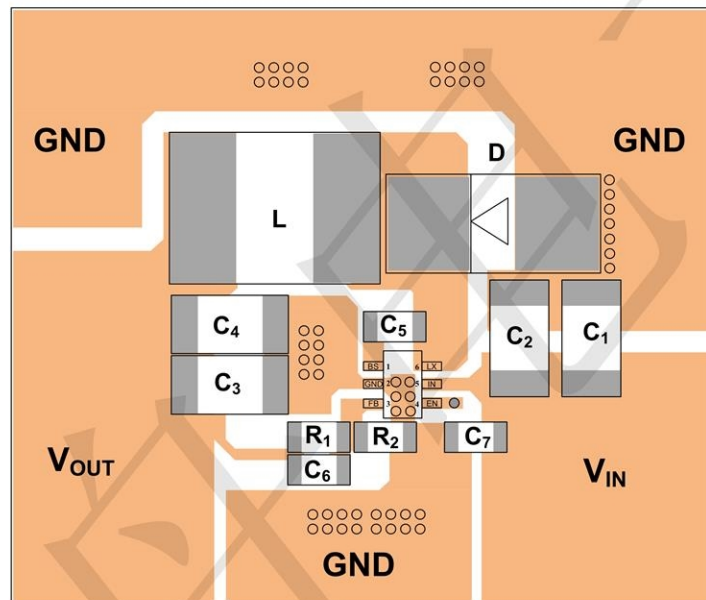
The TP8290 regulator IC integrates the compensation components to achieve good stability and fast transient responses. In some applications, adding a small ceramic cap in parallel with  $R_1$  may further speed up the load transient response and it is recommended for high step load applications.



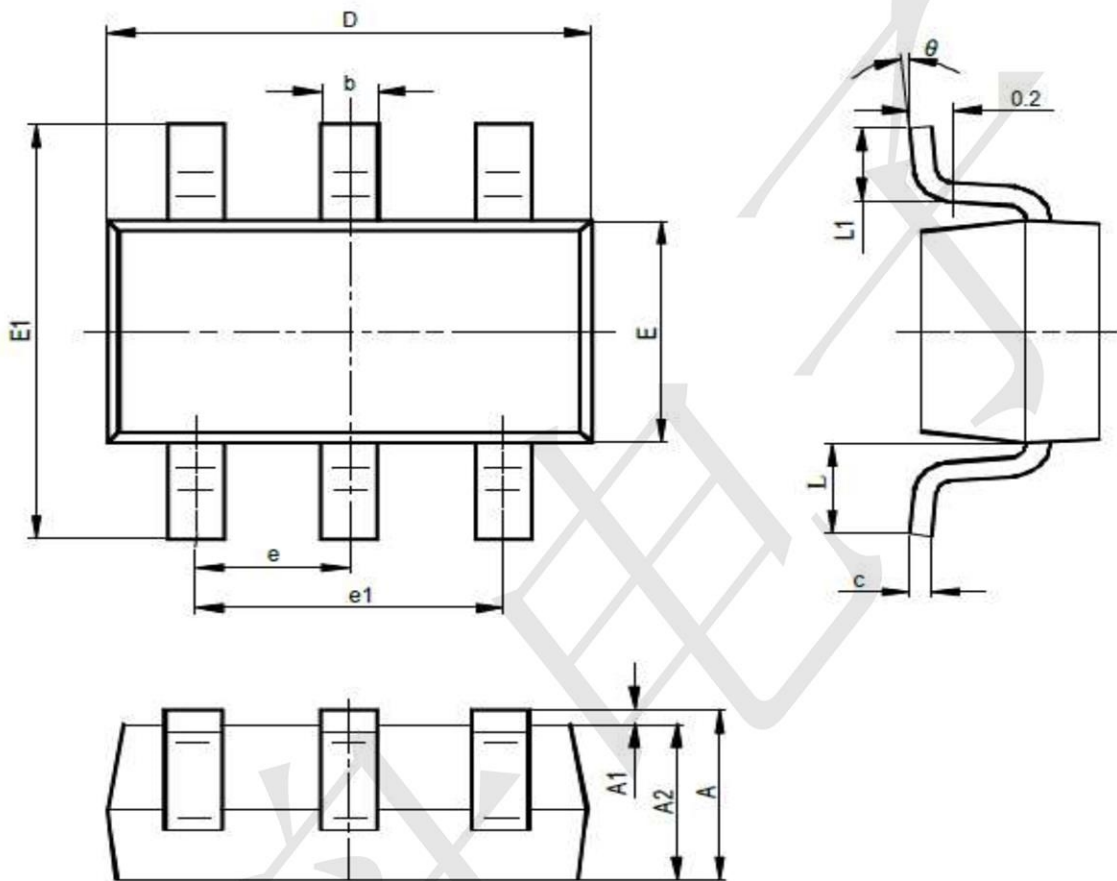
### Layout Design

The layout design of TP8290 regulator is relatively simple. For the best efficiency and minimum noise problem, we should place the following components close to the IC:  $C_{IN}$ , L,  $R_1$  and  $R_2$ .

- 1) It is desirable to maximize the PCB copper area connecting to GND pin to achieve the best thermal and noise performance. If the board space allowed, a ground plane is highly desirable.
- 2) The loop area formed by IN, LX,  $C_{IN}$  and the rectifier diode must be minimized.
- 3) The PCB copper area associated with LX pin must be minimized to avoid the potential noise problem.
- 4) The components  $R_1$  and  $R_2$ , and the trace connecting to the FB pin must NOT be adjacent to the LX net on the PCB layout to avoid the noise problem.
- 5) If the system chip interfacing with the EN pin has a high impedance state at shutdown mode and the IN pin is connected directly to a power source, it is desirable to add a pull down  $1M\Omega$  resistor between the EN and GND pins to prevent the noise from falsely turning on the regulator at shutdown mode.



SOT23-6



SYMBOL	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	1.050	1.250	0.041	0.049
A1	0.000	0.100	0.000	0.004
A2	1.050	1.150	0.041	0.045
b	0.300	0.400	0.012	0.016
c	0.100	0.200	0.004	0.008
D	2.820	3.020	0.111	0.119
E	1.500	1.700	0.059	0.067
E1	2.650	2.950	0.104	0.116
e	0.950TYP		0.037TYP	
e1	1.800	2.000	0.071	0.079
L	0.700REF		0.028REF	
L1	0.300	0.600	0.012	0.024
θ	0°	8°	0°	8°



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