

Technical documentation

Support & ஃ training

AMC1306M05-Q1 ZHCSPG8 – FEBRUARY 2022

AMC1306M05-Q1 汽车类高精度 **±50mV** 输入 增强型隔离式 **Δ-Σ** 调制器

1 特性

- 符合面向汽车应用的 AEC-Q100 标准: – 温度等级 1:–40°C 至 +125°C,T^A
- 提供功能安全 – 有助于进行功能安全系统设计的文档
- 线性输入电压范围:±50mV
- 低直流误差:
	- 失调电压误差:±50μV(最大值)
	- 温漂:1μV/°C(最大值)
	- 增益误差:±0.2%(最大值)
	- 增益漂移:±40ppm/°C(最大值)
- 高 CMTI : 100kV/µs(最小值)
- 低 EMI:符合 CISPR-11 和 CISPR-25 标准
- 安全相关认证:
	- 符合 DIN VDE V 0884-11 标准的 7070V_{PEAK} 增 强型隔离:2017-01
	- 符合 UL1577 标准且长达 1 分钟的 5000V_{RMS} 隔离

2 应用

- 基于分流电阻器的电流感应和隔离式电压测量,包 括:
	- 牵引逆变器
	- 车载充电器
	- 直流/直流转换器
	- 混合动力汽车/电动汽车直流充电器

3 说明

AMC1306M05-Q1 是一款精密 Δ-Σ 调制器,此调制 器的输出与输入电路由抗电磁干扰性能极强的隔离层隔 开。该隔离栅经认证可提供高达 7070V_{PEAK} 的增强型 隔离,符合 DIN VDE V 0884-11 和 UL1577 标准,并 且可支持最高 1.5kV_{RMS} 的工作电压。该隔离层可将系 统中以不同共模电压电平运行的各器件隔开,防止高电 压冲击导致低压侧器件电气损坏或对操作员造成伤害。

AMC1306M05-Q1 的输入端经过了优化,可直接连 接到分流电阻器或其他低电压电平信号源。具有出色 的直流精度和低温漂,可支持精确的电流控制,适用于 车载充电器 (OBC)、直流/直流转换器、牵引逆变器 或其他高压应用。通过使用集成式数字滤波器(如 TMS320F2807x 或 TMS320F2837x 微控制器系列中 的滤波器)来抽取位流,该器件可在 78kSPS 数据速 率下实现 85dB 动态范围的 16 位分辨率。

AMC1306M05-Q1 采用宽体 8 引脚 SOIC 封装,符合 面向汽车应用的 AEC-Q100 标准,并支持 –40°C 至 +125°C 的温度范围。

器件信息(1)

器件型号	赛桂	封装尺寸 (标称值)
AMC1306M05-Q1	SOIC (8)	5.85 mm \times 7.50mm

(1) 如需了解所有可用封装,请参阅数据表末尾的可订购产品附 录。

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4 Revision History

注:以前版本的页码可能与当前版本的页码不同

5 Pin Configuration and Functions

图 **5-1. DWV Package, 8-Pin SOIC (Top View)**

表 **5-1. Pin Functions**

(1) See the *Power Supply Recommendations* section for power-supply decoupling recommendations.

6 Specifications

6.1 Absolute Maximum Ratings

 $see⁽¹⁾$

(1) Operation outside the *Absolute Maximum Ratings* may cause permanent device damage. *Absolute Maximum Ratings* do not imply functional operation of the device at these or any other conditions beyond those listed under *Recommended Operating Conditions* . If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

6.2 ESD Ratings

(1) AEC Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specification.

6.3 Recommended Operating Conditions

over operating ambient temperature range (unless otherwise noted)

6.4 Thermal Information

(1) For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.

6.5 Power Ratings

6.6 Insulation Specifications

over operating ambient temperature range (unless otherwise noted)

(1) Apply creepage and clearance requirements according to the specific equipment isolation standards of an application. Care must be taken to maintain the creepage and clearance distance of a board design to ensure that the mounting pads of the isolator on the printed circuit board (PCB) do not reduce this distance. Creepage and clearance on a PCB become equal in certain cases. Techniques such as inserting grooves, ribs, or both on a PCB are used to help increase these specifications.

(2) This coupler is suitable for *safe electrical insulation* only within the safety ratings. Compliance with the safety ratings shall be ensured by means of suitable protective circuits.

(3) Testing is carried out in air or oil to determine the intrinsic surge immunity of the isolation barrier.

(4) Apparent charge is electrical discharge caused by a partial discharge (pd).

(5) All pins on each side of the barrier are tied together, creating a two-pin device.

6.7 Safety-Related Certifications

Safety Limiting Values

(1) The maximum safety temperature, T_S, has the same value as the maximum junction temperature, T_J, specified for the device. The I_S and P_S parameters represent the safety current and safety power, respectively. Do not exceed the maximum limits of I_S and P_S . These limits vary with the ambient temperature, T_A .

The junction-to-air thermal resistance, R_{θJA}, in the *Thermal Information* table is that of a device installed on a high-K test board for leaded surface-mount packages. Use these equations to calculate the value for each parameter:

 ${\sf T}_{\sf J}$ = ${\sf T}_{\sf A}$ + ${\sf R}_{\sf \theta J A}$ × P, where P is the power dissipated in the device.

 $T_{J(max)}$ = T_S = T_A + R_{θJA} × P_S, where T_{J(max)} is the maximum junction temperature.

 P_S = I_S × AVDD_{max} + I_S × DVDD_{max}, where AVDD_{max} is the maximum high-side voltage and DVDD_{max} is the maximum controller-side supply voltage.

6.8 Electrical Characteristics

minimum and maximum specifications are at T_A = –40°C to 125°C, AVDD = 3.0 V to 5.5 V, DVDD = 2.7 V to 5.5 V, INP = –50 mV to 50 mV, INN = 0 V, and sinc³ filter with OSR = 256 (unless otherwise noted); typical specifications are at T_A = 25°C, CLKIN = 20 MHz, $AVDD = 5$ V, and $DVDD = 3.3$ V

6.8 Electrical Characteristics (continued)

minimum and maximum specifications are at T_A = –40°C to 125°C, AVDD = 3.0 V to 5.5 V, DVDD = 2.7 V to 5.5 V, INP = –50 mV to 50 mV, INN = 0 V, and sinc³ filter with OSR = 256 (unless otherwise noted); typical specifications are at T_A = 25°C, CLKIN = 20 MHz, $AVDD = 5$ V, and $DVDD = 3.3$ V

(1) This parameter is input referred.

(2) Integral nonlinearity is defined as the maximum deviation from a straight line passing through the end-points of the ideal ADC transfer function expressed as number of LSBs or as a percent of the specified linear full-scale range FSR.

(3) Offset error temperature drift is calculated using the box method, as described by the following equation: $TCE_O = (E_{O,MAX} - E_{O,MIN})$ / TempRange where $E_{O,MAX}$ and $E_{O,MIN}$ refer to the maximum and minimum E_O values measured within the temperature range (–40 to 125℃).

(4) Gain error temperature drift is calculated using the box method, as described by the following equation: $TCE_G(ppm) = ((E_{G,MAX} - E_{G,MIN}) / TempRange) \times 10^4$ where $E_{G,MAX}$ and $E_{G,MIN}$ refer to the maximum and minimum E_G values (in %) measured within the temperature range (–40 to 125℃).

(5) THD is the ratio of the rms sum of the amplitudes of first five higher harmonics to the amplitude of the fundamental.

Switching Characteristics

6.9 Timing Diagrams

6.10 Insulation Characteristics Curves

6.11 Typical Characteristics

7 Detailed Description

7.1 Overview

The input stage of the AMC1306M05-Q1 consists of a fully differential amplifier that feeds the switched-capacitor input of a second-order, delta-sigma (ΔΣ) modulator. The modulator converts the analog input signal into a digital bitstream that is transferred across the isolation barrier that separates the high-side from the low-side. The isolated data output DOUT of the converter provides a stream of digital ones and zeros that is synchronous to the externally provided clock source at the CLKIN pin. The time average of this serial bitstream output is proportional to the analog input voltage. The external clock input simplifies the synchronization of multiple current-sensing channels on the system level.

The silicon-dioxide $(SiO₂)$ based capacitive isolation barrier supports a high level of magnetic field immunity as described in the *ISO72x Digital Isolator Magnetic-Field Immunity* application report. The digital modulation used in the AMC1306M05-Q1 to transmit data across the isolation barrier, and the isolation barrier characteristics itself, result in high reliability and common-mode transient immunity.

7.2 Functional Block Diagram

7.3 Feature Description

7.3.1 Analog Input

The differential amplifier input stage of the AMC1306M05-Q1 feeds a second-order, switched-capacitor, feedforward ΔΣ modulator. The gain of the differential amplifier is set by internal precision resistors with a differential input impedance of R_{IND} . The modulator converts the analog input signal into a bitstream that is transferred across the isolation barrier, as described in the *Isolation Channel Signal Transmission* section.

For reduced offset and offset drift, the differential amplifier is chopper-stabilized with the switching frequency set at $f_{\text{CI KIN}}$ / 32. As shown in $\boxed{8}$ 7-1, the switching frequency generates a spur at 625 kHz.

 $\sf{sinc^3}$ filter, OSR = 2, f_{CLKIN} = 20 MHz, f_{IN} = 1 kHz

图 **7-1. Quantization Noise Shaping**

There are two restrictions on the analog input signals INP and INN. First, if the input voltages V_{IND} or V_{INN} exceed the range specified in the *Absolute Maximum Ratings* table, the input currents must be limited to the absolute maximum value because the electrostatic discharge (ESD) protection turns on. In addition, the linearity and parametric performance of the device are ensured only when the analog input voltage remains within the linear full-scale range (V_{FSR}) and within the common-mode input voltage range (V_{CM}) as specified in the *Recommended Operating Conditions* table.

7.3.2 Modulator

图 7-2 conceptualizes the second-order, switched-capacitor, feed-forward $\Delta \Sigma$ **modulator implemented in the** AMC1306M05-Q1. The analog input voltage V_{IN} and the output V₅ of the 1-bit digital-to-analog converter (DAC) are differentiated, providing an analog voltage V_1 at the input of the first integrator stage. The output of the first integrator feeds the input of the second integrator stage, resulting in output voltage V_3 that is differentiated with the input signal V_{IN} and the output of the first integrator V_2 . Depending on the polarity of the resulting voltage V_4 , the output of the comparator is changed. In this case, the 1-bit DAC responds on the next clock pulse by changing the associated analog output voltage V_5 , causing the integrators to progress in the opposite direction, and forcing the value of the integrator output to track the average value of the input.

The modulator shifts the quantization noise to high frequencies, as illustrated in \boxtimes 7-1. Therefore, use a low-pass digital filter at the output of the device to increase the overall performance. This filter is also used to convert the 1-bit data stream at a high sampling rate into a higher-bit data word at a lower rate (decimation). TI's C2000™ and Sitara™ microcontroller families offer a suitable programmable, hardwired filter structure termed a *sigma-delta filter module* (SDFM) optimized for usage with the AMC1306M05-Q1. Alternatively, a field-programmable gate array (FPGA) or complex programmable logic device (CPLD) can be used to implement the filter.

7.3.3 Isolation Channel Signal Transmission

The AMC1306M05-Q1 uses an on-off keying (OOK) modulation scheme, as shown in \mathbb{R} 7-3, to transmit the modulator output bitstream across the $SiO₂$ -based isolation barrier. The transmit driver (TX) shown in the *Functional Block Diagram* transmits an internally generated, high-frequency carrier across the isolation barrier to represent a digital *one* and does not send a signal to represent a digital *zero*. The nominal frequency of the carrier used inside the AMC1306M05-Q1 is 480 MHz.

The receiver (RX) on the other side of the isolation barrier recovers and demodulates the signal and produces the output. The AMC1306M05-Q1 transmission channel is optimized to achieve the highest level of commonmode transient immunity (CMTI) and lowest level of radiated emissions caused by the high-frequency carrier and RX/TX buffer switching.

图 **7-3. OOK-Based Modulation Scheme**

7.3.4 Digital Output

A differential input signal of 0 V ideally produces a stream of ones and zeros that are high 50% of the time. A differential input of 50 mV produces a stream of ones and zeros that are high 89.06% of the time. With 16 bits of resolution, that percentage ideally corresponds to code 58368. A differential input of –50 mV produces a stream of ones and zeros that are high 10.94% of the time and ideally results in code 7168 with 16-bit resolution. These input voltages are also the specified linear range of the AMC1306M05-Q1. If the input voltage value exceeds this range, the output of the modulator shows nonlinear behavior as the quantization noise increases. The output of the modulator clips with a constant stream of zeros with an input less than or equal to –64 mV or with a constant stream of ones with an input greater than or equal to 64 mV. In this case, however, the AMC1306M05-Q1 generates a single 1 (if the input is at negative full-scale) or 0 (if the input is at positive full-scale) every 128 clock cycles to indicate proper device function (see the *Output Behavior in Case of a Full-Scale Input* section for more details). \mathbb{S} 7-4 shows the input voltage versus the output modulator signal.

图 **7-4. AMC1306M05-Q1 Modulator Output vs Analog Input**

The density of ones in the output bitstream can be calculated using 方程式 1 for any input voltage (V_{IN}= V_{INP} – V_{INN}) value with the exception of a full-scale input signal, as described in 方程式 1:

$$
\rho = \frac{V_{IN} + V_{Clipping}}{2 \times V_{Clipping}}\tag{1}
$$

7.3.4.1 Output Behavior in Case of a Full-Scale Input

If a full-scale input signal is applied to the AMC1306M05-Q1 (that is, $|V_{IN}| \ge |V_{Clipping}|$), the device generates a single one or zero every 128 bits at DOUT, as shown in $\overline{8}$ 7-5, depending on the actual polarity of the signal being sensed. In this way, differentiating between a missing AVDD and a full-scale input signal is possible on the system level.

图 **7-5. Output of the AMC1306M05-Q1 in Case of an Input Overrange**

7.3.4.2 Output Behavior in Case of Input Common-Mode Overrange

If INN or INP is disconnected from the shunt resistor, the input bias current of the AMC1306M05-Q1 drives the disconnected terminal towards the positive supply rail, and the common-mode input voltage increases. A similar effect happens when there is no DC current path between INN, INP, and HGND. If the input common-mode voltage exceeds the common-mode overvoltage detection threshold V_{CMov} , the device provides a constant bitstream of logic 1's at the output, as shown in 图 $7-6$; that is, DOUT is permanently high. A zero is not generated every 128 clock pulses, which differentiates this condition from a valid positive full-scale input. This feature is useful to identify interconnect problems on the board.

图 **7-6. Output of the AMC1306M05-Q1 in Case of a Common-Mode Overvoltage**

There is no common-mode overvoltage detection in the negative direction; thus, if the common-mode input voltage is below the minimum V_{CM} value specified in the *Recommended Operating Conditions* table, the bitstream at the DOUT output is not determined.

7.3.4.3 Output Behavior in Case of a Missing High-Side Supply

If the high-side supply is missing, the device provides a constant bitstream of logic 0's at the output, as shown in 图 7-7; that is, DOUT is permanently low. A one is not generated every 128 clock pulses, which differentiates this condition from a valid negative full-scale input. This feature is useful to identify high-side power-supply problems on the board.

图 **7-7. Output of the AMC1306M05-Q1 in Case of a Missing High-Side Supply**

7.4 Device Functional Modes

The AMC1306M05-Q1 is operational when the power supplies AVDD and DVDD are applied as specified in the *Recommended Operating Conditions* table.

8 Application and Implementation

备注

以下应用部分中的信息不属于 TI 器件规格的范围,TI 不担保其准确性和完整性。TI 的客 户应负责确定 器件是否适用于其应用。客户应验证并测试其设计,以确保系统功能。

8.1 Application Information

The low analog input voltage range, excellent accuracy, and low temperature drift make the AMC1306M05-Q1 a high-performance solution for automotive applications where shunt-based current sensing in the presence of high common-mode voltage levels is required.

8.2 Typical Application

The AMC1306M05-Q1 is ideally suited for shunt-based, current-sensing applications where accurate current monitoring is required in the presence of high common-mode voltages.

图 8-1 shows the AMC1306M05-Q1 in a typical application. The load current flowing through an external shunt resistor RSHUNT produces a voltage drop that is sensed by the AMC1306M05-Q1. The AMC1306M05-Q1 digitizes the analog input signal on the high-side, transfers the data across the isolation barrier to the low-side, and outputs the digital bitstream on the DOUT pin. The 5-V high-side power supply (AVDD) is generated from the floating gate driver supply using a resistor (R4) and a Zener diode (D1).

The differential input, digital output, and the high common-mode transient immunity (CMTI) of the AMC1306M05- Q1 ensure reliable and accurate operation even in high-noise environments.

图 **8-1. Using the AMC1306M05-Q1 for Current Sensing in a Typical Application**

8.2.1 Design Requirements

 $\frac{1}{36}$ 8-1 lists the parameters for this typical application.

表 **8-1. Design Requirements**

PARAMETER	VALUE
High-side supply voltage	3.3 V or 5 V
Low-side supply voltage	3.3 V or 5 V
Voltage drop across RSHUNT for a linear response	±50 mV (maximum)

8.2.2 Detailed Design Procedure

In 图 8-1, the high-side power supply (AVDD) for the AMC1306M05-Q1 is derived from the floating power supply of the upper gate driver, using a resistor (R4) and a Zener diode (D1).

The floating ground reference (AGND) is derived from the end of the shunt resistor that is connected to the negative input of the AMC1306M05-Q1 (INN). If a four-pin shunt is used, the inputs of the AMC1306M05-Q1 are connected to the inner leads and AGND is connected to the outer lead on the INN-side of the shunt. To minimize offset and improve accuracy, route the ground connection as a separate trace that connects directly to the shunt resistor rather than shorting AGND to INN directly at the input to the device. See the *Layout* section for more details.

8.2.2.1 Shunt Resistor Sizing

Use Ohm's Law to calculate the voltage drop across the shunt resistor (V_{SHUNT}) for the desired measured current: $V_{\text{SHUNT}} = I \times \text{RSHUNT}$.

Consider the following two restrictions when selecting the value of the shunt resistor, RSHUNT:

- The voltage drop caused by the nominal current range must not exceed the recommended differential input voltage range for a linear response: $|V_{SHUNT}| \leq |V_{FSR}|$
- The voltage drop caused by the maximum allowed overcurrent must not exceed the input voltage that causes a clipping output: $|V_{SHUNT}| \leq |V_{Clippind}|$

8.2.2.2 Input Filter Design

Place an RC filter in front of the isolated amplifier to improve signal-to-noise performance of the signal path. Design the input filter such that:

- The cutoff frequency of the filter is at least one order of magnitude lower than the sampling frequency ($f_{Cl|KIN}$) of the ΔΣ modulator
- The input bias current does not generate significant voltage drop across the DC impedance of the input filter
- The impedances measured from the analog inputs are equal

For most applications, the structure shown in $\frac{8}{8}$ 8-2 achieves excellent performance.

图 **8-2. Differential Input Filter**

8.2.2.3 Bitstream Filtering

The modulator generates a bitstream that is processed by a digital filter to obtain a digital word similar to a conversion result of a conventional analog-to-digital converter (ADC). As described by 方程式 2, a very simple filter built with minimal effort and hardware, is a sinc³-type filter:

$$
H(z) = \left(\frac{1 - z^{-OSR}}{1 - z^{-1}}\right)^3\tag{2}
$$

This filter provides the best output performance at the lowest hardware size (count of digital gates) for a secondorder modulator. All characterization in this document is also done with a sinc³ filter with an oversampling ratio (OSR) of 256 and an output word width of 16 bits, unless specified otherwise. The measured effective number of bits (ENOB) as a function of the OSR is illustrated in 图 8-3 of the *Typical Application* section.

A *Delta Sigma Modulator Filter Calculator* is available for download at www.ti.com that aids in the filter design and selecting the right OSR and filter order to achieve the desired output resolution and filter response time.

An example code for implementing a sinc³ filter in an FPGA is discussed in the *Combining the ADS1202 with an FPGA Digital Filter for Current Measurement in Motor Control Applications* application note, available for download at www.ti.com.

For modulator output bitstream filtering, a device from TI's C2000™ or Sitara™ microcontroller families is recommended. These families support up to eight channels of dedicated hardwired filter structures that significantly simplify system level design by offering two filtering paths per channel: one providing high-accuracy results for the control loop and one fast-response path for overcurrent detection.

A *delta sigma modulator filter calculator* is available for download at www.ti.com that aids in the filter design and selecting the right OSR and filter order to achieve the desired output resolution and filter response time.

8.2.3 Application Curve

The effective number of bits (ENOB) is often used to compare the performance of ADCs and $\Delta\Sigma$ modulators. \mathbb{B} 8-3 shows the ENOB of the AMC1306M05-Q1 with different oversampling ratios. By using 方程式 3, this number can also be calculated from the SINAD:

图 **8-3. Measured Effective Number of Bits vs Oversampling Ratio**

8.3 What to Do and What Not to Do

Do not leave the inputs of the AMC1306M05-Q1 unconnected (floating) when the device is powered up. If the device inputs are left floating, the input bias current may drive the inputs to a positive value that exceeds the operating common-mode input voltage and DOUT is permanently high as described in the *Output Behavior in Case of Input Common-Mode Overrange* section.

Connect the high-side ground (AGND) to INN, either by a hard short or through a resistive path. A DC current path between INN and AGND is required to define the input common-mode voltage. Take care not to exceed the input common-mode range as specified in the *Recommended Operating Conditions* table. For best accuracy, route the ground connection as a separate trace that connects directly to the shunt resistor rather than shorting AGND to INN directly at the input to the device. See the *Layout* section for more details.

9 Power Supply Recommendations

The AMC1306M05-Q1 does not require any specific power-up sequencing. The high-side power supply (AVDD) is decoupled with a low-ESR, 100-nF capacitor (C1) parallel to a low-ESR, 1-µF capacitor (C2). The low-side power supply (DVDD) is equally decoupled with a low-ESR, 100-nF capacitor (C3) parallel to a low-ESR, 1-µF capacitor (C4). Place all four capacitors (C1, C2, C3, and C4) as close to the device as possible.

The ground reference for the high-side (AGND) is derived from the end of the shunt resistor that is connected to the negative input (INN) of the device. For best DC accuracy, use a separate trace to make this connection instead of shorting AGND to INN directly at the device input. If a four-terminal shunt is used, the device inputs are connected to the inner leads and AGND is connected to the outer lead on the INN-side of the shunt. $\boxed{8}$ 9-1 shows a decoupling diagram of the AMC1306M05-Q1.

图 **9-1. Decoupling of the AMC1306M05-Q1**

Capacitors must provide adequate effective capacitance under the applicable DC bias conditions they experience in the application. Multilayer ceramic capacitors (MLCC) typically exhibit only a fraction of their nominal capacitance under real-world conditions and this factor must be taken into consideration when selecting these capacitors. This problem is especially acute in low-profile capacitors, in which the dielectric field strength is higher than in taller components. Reputable capacitor manufacturers provide capacitance versus DC bias curves that greatly simplify component selection.

10 Layout

10.1 Layout Guidelines

图 10-1 shows a layout recommendation with the critical placement of the decoupling capacitors (as close as possible to the AMC1306M05-Q1 supply pins) and placement of the other components required by the device. For best performance, place the shunt resistor close to the INP and INN inputs of the AMC1306M05-Q1 and keep the layout of both connections symmetrical.

10.2 Layout Example

11 Device and Documentation Support

11.1 Documentation Support

11.1.1 Related Documentation

For related documentation see the following:

- Texas Instruments, *Isolation Glossary* application report
- Texas Instruments, *Semiconductor and IC Package Thermal Metrics* application report
- Texas Instruments, *ISO72x Digital Isolator Magnetic-Field Immunity* application report
- Texas Instruments, *Delta Sigma Modulator Filter Calculator* design tool

11.2 接收文档更新通知

要接收文档更新通知,请导航至 ti.com 上的器件产品文件夹。点击*订阅更新* 进行注册,即可每周接收产品信息更 改摘要。有关更改的详细信息,请查看任何已修订文档中包含的修订历史记录。

11.3 支持资源

TI E2E™ 支持论坛是工程师的重要参考资料,可直接从专家获得快速、经过验证的解答和设计帮助。搜索现有解 答或提出自己的问题可获得所需的快速设计帮助。

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11.4 Trademarks

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11.5 Electrostatic Discharge Caution

This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

11.6 术语表

TI 术语表 本术语表列出并解释了术语、首字母缩略词和定义。

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures. "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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OTHER QUALIFIED VERSIONS OF AMC1306M05-Q1 :

• Catalog : AMC1306M05

NOTE: Qualified Version Definitions:

• Catalog - TI's standard catalog product

DWV0008A SOIC - 2.8 mm max height

SOIC

NOTES:

- 1. All linear dimensions are in millimeters. Dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm, per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm, per side.

EXAMPLE BOARD LAYOUT

DWV0008A SOIC - 2.8 mm max height

SOIC

NOTES: (continued)

5. Publication IPC-7351 may have alternate designs.

6. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

EXAMPLE STENCIL DESIGN

DWV0008A SOIC - 2.8 mm max height

SOIC

NOTES: (continued)

8. Board assembly site may have different recommendations for stencil design.

^{7.} Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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