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# LM3530 High-Efficiency White-LED Driver with Programmable Ambient Light Sensing Capability and $\mathrm{I}^{2} \mathrm{C}$-Compatible Interface 

## 1 Features

- Drives up to 11 LEDs in series
- 1000:1 Dimming Ratio
- 90\% Efficient
- Programmable Dual Ambient Light Sensor Inputs with Internal ALS Voltage Setting Resistors
- $I^{2} \mathrm{C}$ Programmable Logarithmic or Linear Brightness Control
- External PWM Input for Simple Brightness Adjustment
- True Shutdown Isolation for LEDs and Ambient Light Sensors
- Internal Soft-Start Limits Inrush Current
- Wide 2.7-V to 5.5-V Input Voltage Range
- $40-\mathrm{V}$ and $25-\mathrm{V}$ Overvoltage Protection Options
- $500-\mathrm{kHz}$ Fixed Frequency Operation
- 839-mA Peak Current Limit


## 2 Applications

- Smartphone LCD Backlighting
- Personal Navigation LCD Backlighting
- 2 to 11 Series White-LED Backlit Display Power Source


## 3 Description

The LM3530 current mode boost converter supplies the power and controls the current in up to 11 series white LEDs. The $839-\mathrm{mA}$ current limit and $2.7-\mathrm{V}$ to $5.5-\mathrm{V}$ input voltage range make the device a versatile backlight power source ideal for operation in portable applications.
The LED current is adjustable from 0 mA to 29.5 mA via an $1^{2} \mathrm{C}$-compatible interface. The 127 different current steps and 8 different maximum LED current levels give over 1000 programmable LED current levels. Additionally, PWM brightness control is possible through an external logic level input.
The device also features two Ambient Light Sensor inputs. These are designed to monitor analog output ambient light sensors and provide programmable adjustment of the LED current with changes in ambient light. Each ambient light sensor input has independently programmable internal voltage setting resistors which can be made high impedance to reduce power during shutdown. The $500-\mathrm{kHz}$ switching frequency allows for high converter efficiency over a wide output voltage range accommodating from 2 to 11 series LEDs. Finally, the support of Content Adjusted Backlighting maximizes battery life while maintaining display image quality.
The LM3530 operates over the $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ temperature range.

| Device Information |
| :--- |
| ${ }^{(1)}$ |
| PART NUMBER PACKAGE BODY SIZE (MAX) <br> LM3530 DSBGA (12) $1.64 \mathrm{~mm} \times 1.24 \mathrm{~mm}$ |

(1) For all available packages, see the orderable addendum at the end of the datasheet.


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## 4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.
Changes from Revision K (March 2013) to Revision L Page- Added Device Information and ESD Ratings tables, Detailed Description, Application and Implementation, PowerSupply Recommendations, Layout, Device and Documentation Support and Mechanical, Packaging, and OrderableInformation sections; moved some curves to Application Curves section1
Changes from Revision J (March 2013) to Revision K Page

- Changed layout of National Data Sheet to TI format ..... 34


## $5 \quad I^{2} \mathrm{C}$ Device Options

| ORDERABLE NUMBER | I $^{2}$ C DEVICE OPTION |
| :---: | :---: |
| LM3530TME-40 | $0 \times 38$ |
| LM3530TMX-40 | $0 \times 38$ |
| LM3530UME-25A | $0 \times 36$ |
| LM3530UME-40 | $0 \times 38$ |
| LM3530UME-40B | $0 \times 39$ |
| LM3530UMX-25A | $0 \times 36$ |
| LM3530UMX-40 | $0 \times 38$ |
| LM3530UMX-40B | $0 \times 39$ |

## 6 Pin Configuration and Functions

## DSBGA (YFZ or YFQ) Package

12 Pins
Top View


Pin Functions

| PIN |  | TYPE |  |
| :---: | :---: | :---: | :--- |
| NUMBER | NAME |  |  |
| A1 | SDA | I/O | Serial data connection for I ${ }^{2}$ C-compatible interface. |
| A2 | SCL | I | Serial data connection for I ${ }^{2}$ C-compatible interface. |
| A3 | SW | PWR | Inductor connection, diode anode connection, and drain connection for internal NFET. Connect <br> the inductor and diode as close as possible to SW to reduce parasitic inductance and capacitive <br> coupling to nearby traces. |
| B1 | PWM | I | External PWM brightness control input and simple enable input. |
| B2 | INT | O | Logic interrupt output signaling the ALS zone has changed. |
| B3 | GND |  | Ground |
| C1 | ALS2 | I | Ambient light sensor input 2 with programmable internal pull-down resistor. |
| C2 | HWEN | I | Active high hardware enable (active low reset). pull this pin high to enable the LM3530. |
| C3 | IN | PWR | Input voltage connection. Connect a 2.7-V to 5.5-V supply to IN and bypass to GND with a 2.2- <br> $\mu F$ <br> IN greater ceramic capacitor. |
| D1 | ALS1 | I | Ambient light sensor input 1 with programmable internal pulldown resistor. |
| D2 | OVP | I | Output voltage sense connection for overvoltage sensing. Connect OVP to the positive terminal <br> of the output capacitor. |
| D3 | ILED | PWR | Input terminal to internal current sink. The boost converter regulates ILED to 0.4 V. |

## 7 Specifications

### 7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) ${ }^{(1)(2)(3)}$

|  | MIN MAX | UNIT |
| :---: | :---: | :---: |
| $\mathrm{V}_{\text {IN }}$ to GND | -0.3 6 | V |
| $\mathrm{V}_{\text {SW }}, \mathrm{V}_{\text {OVP }}, \mathrm{V}_{\text {ILED }}$ to GND | 45 |  |
| $\mathrm{V}_{\text {SCL }}, \mathrm{V}_{\text {SDA }}, \mathrm{V}_{\text {ALS } 1}, \mathrm{~V}_{\text {PWM }}, \mathrm{V}_{\text {INT }}, \mathrm{V}_{\text {HWEN }}$ to GND | 6 |  |
| $\mathrm{V}_{\text {ALS2 }}$ to GND | -0.3 V to $\mathrm{V}_{\mathrm{IN}}+0.3 \mathrm{~V}$ |  |
| Continuous power dissipation | Internally limited |  |
| Junction temperature ( $\mathrm{T}_{\text {JMAX }}$ ) | 150 | ${ }^{\circ} \mathrm{C}$ |
| Maximum lead temperature (soldering, 10s) | See ${ }^{(4)}$ |  |
| Storage temperature, $\mathrm{T}_{\text {stg }}$ | -65 150 | ${ }^{\circ} \mathrm{C}$ |

(1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
(2) If Military/Aerospace specified devices are required, please contact the Texas Instruments Sales Office/ Distributors for availability and specifications.
(3) All voltages are with respect to the potential at the GND pin.
(4) For detailed soldering specifications and information, please refer to Application Note 1112: DSBGA Wafer Level Chip Scale Package (SNVA009).

### 7.2 ESD Ratings

|  |  | VALUE | UNIT |
| :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {(ESD) }}$ Electrostatic discharge | Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ${ }^{(1)}$ | $\pm 2000$ | V |

(1) JEDEC document JEP155 states that $500-\mathrm{V}$ HBM allows safe manufacturing with a standard ESD control process.

### 7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

|  | MIN | NOM |
| :--- | ---: | ---: |
| $V_{\text {IN }}$ to $G N D$ | 2.7 | MAX |
| $V_{\text {SW }}, V_{\text {OVP, }} V_{\text {ILED }}$, to GND | UNIT |  |
| Junction temperature $\left(T_{J}\right)^{(1)}$ | 0 | 5.5 |
| Ambient temperature $\left(T_{A}\right)^{(2)}$ | -40 | 40 |

 disengages at $\mathrm{T}_{\mathrm{J}}=125^{\circ} \mathrm{C}$ (typ.).
(2) In applications where high power dissipation and/or poor package thermal resistance is present, the maximum ambient temperature may have to be derated. Maximum ambient temperature ( $\mathrm{T}_{\mathrm{A}-\mathrm{MAX}}$ ) is dependent on the maximum operating junction temperature ( $\mathrm{T}_{\mathrm{J}-\mathrm{MAX}}$-OP $=$ $125^{\circ} \mathrm{C}$ ), the maximum power dissipation of the device in the application ( $\mathrm{P}_{\mathrm{D}-\mathrm{MAX}}$ ), and the junction-to ambient thermal resistance of the part/package in the application $\left(R_{\theta J A}\right)$, as given by the following equation: $T_{A-M A X}=T_{J-M A X-O P}-\left(R_{\theta J A} \times P_{D-M A X}\right)$.

### 7.4 Thermal Information

| THERMAL METRIC ${ }^{(1)}$ |  | DSBGA |  | UNIT |
| :---: | :---: | :---: | :---: | :---: |
|  |  | YFQ | YFZ |  |
|  |  |  |  |  |
| $\mathrm{R}_{\theta \mathrm{JA}}$ | Junction-to-ambient thermal resistance ${ }^{(2)}$ |  |  | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

(1) For more information about traditional and new thermal metrics, see the IC Package Thermal Metrics application report, SPRA953.
(2) Junction-to-ambient thermal resistance $\left(R_{\theta J A}\right)$ is taken from a thermal modeling result, performed under the conditions and guidelines set forth in the JEDEC standard JESD51-7. The test board is a 4-layer FR-4 board measuring $102 \mathrm{~mm} \times 76 \mathrm{~mm} \times 1.6 \mathrm{~mm}$ with a $2 \times 1$ array of thermal vias. The ground plane on the board is $50 \mathrm{~mm} \times 50 \mathrm{~mm}$. Thickness of copper layers are $36 \mu \mathrm{~m} / 18 \mu \mathrm{~m} / 18 \mu \mathrm{~m} / 36 \mu \mathrm{~m}$ ( $1.5 \mathrm{oz} / 1 \mathrm{oz} / 1 \mathrm{oz} / 1.5 \mathrm{oz}$ ). Ambient temperature in simulation is $22^{\circ} \mathrm{C}$ in still air. Power dissipation is 1 W . The value of $\mathrm{R}_{\theta \mathrm{JA}}$ of this product in the DSBGA package could fall in a range as wide as $60^{\circ} \mathrm{C} / \mathrm{W}$ to $110^{\circ} \mathrm{C} / \mathrm{W}$ (if not wider), depending on PCB material, layout, and environmental conditions. In applications where high maximum power dissipation exists special care must be paid to thermal dissipation issues.

### 7.5 Electrical Characteristics

Typical (TYP) limits are for $T_{A}=25^{\circ} \mathrm{C}$; minimum (MIN) and maximum (MAX) apply over the full operating ambient temperature range $\left(-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 85^{\circ} \mathrm{C}\right) ; \mathrm{V}_{\mathbb{I}}=3.6 \mathrm{~V}$, unless otherwise specified. ${ }^{(1)(2)}$

(1) All voltages are with respect to the potential at the GND pin.
(2) Min and Max limits are verified by design, test, or statistical analysis. Typical (typ.) numbers are not verified, but represent the most likely norm.
(3) The ALS voltage specification is the maximum trip threshold for the ALS zone boundary (Code 0xFF). Due to random offsets and the mechanism for which the hysteresis voltage varies, it is recommended that only Codes $0 \times 04$ and above be used for Zone Boundary Thresholds. See Zone Boundary Trip Points and Hysteresis and Minimum Zone Boundary Settings sections.

## Electrical Characteristics (continued)

Typical (TYP) limits are for $T_{A}=25^{\circ} \mathrm{C}$; minimum (MIN) and maximum (MAX) apply over the full operating ambient temperature range $\left(-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 85^{\circ} \mathrm{C}\right) ; \mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$, unless otherwise specified. ${ }^{(1)(2)}$

| PARAMETER |  | TEST CONDITIONS | MIN | TYP | MAX |
| :--- | :--- | :--- | ---: | :---: | :---: |
| UNIT |  |  |  |  |  |
| LOGIC VOLTAGE SPECIFICATIONS (SCL, SDA, PWM, INT) | 0 | 0.54 | V |  |  |
| $\mathrm{~V}_{\mathrm{IL}}$ | Input logic low | $2.7 \mathrm{~V} \leq \mathrm{V}_{\mathbb{I N}} \leq 5.5 \mathrm{~V}$ | 1.26 | $\mathrm{~V}_{\mathrm{IN}}$ | V |
| $\mathrm{V}_{\mathrm{IH}}$ | Input logic high | $2.7 \mathrm{~V} \leq \mathrm{V}_{\text {IN }} \leq 5.5 \mathrm{~V}$ |  | 400 | mV |
| $\mathrm{V}_{\mathrm{OL}}$ | Output logic low (SDA, INT) | $\mathrm{I}_{\text {LOAD }}=3 \mathrm{~mA}$ |  |  |  |

## $7.6 I^{2} \mathrm{C}$-Compatible Timing Requirements (SCL, SDA) ${ }^{(1)}$

|  |  | MIN | NOM |
| :--- | :--- | ---: | :---: |
| $\mathrm{t}_{1}$ | SCL (Clock Period) | 2.5 | MAX |
| $\mathrm{t}_{2}$ | Uata in setup time to SCL high | 100 | $\mathrm{\mu s}$ |
| $\mathrm{t}_{3}$ | Data out stable after SCL low | 0 | ns |
| $\mathrm{t}_{4}$ | SDA low setup time to SCL low (start) | 100 | ns |
| $\mathrm{t}_{5}$ | SDA high hold time after SCL High (stop) | 100 | ns |

(1) SCL and SDA must be glitch-free in order for proper brightness control to be realized.

### 7.7 Simple Interface Timing

|  |  |  | MIN | NOM |
| :--- | :--- | ---: | ---: | ---: |
| $t_{\text {PWM_HIGH }}$ | Enable time, PWM pin must be held high | 1.5 | 2 | MAX |
| tPWM_LOW | Disable time, PWM pin must be held low | 1.48 | 2.6 | ms |



Figure 1. $I^{2} C$-Compatible Timing


Figure 2. Simple Enable/Disable Timing

### 7.8 Typical Characteristics

$\mathrm{V}_{\mathbb{I N}}=3.6 \mathrm{~V}$, LEDs are OVSRWAC1R6 from OPTEK Technology, $\mathrm{C}_{\text {OUT }}=1 \mu \mathrm{~F}, \mathrm{C}_{\mathrm{IN}}=1 \mu \mathrm{~F}, \mathrm{~L}=$ TDK VLF5012ST-100M1R0, $\left(R_{L}=0.24 \Omega\right), L_{L E D}=19 \mathrm{~mA}, T_{A}=25^{\circ} \mathrm{C}$, unless otherwise specified.

$I_{\text {FULL_SCALE }}=19 \mathrm{~mA}$

Figure 3. LED Current vs $\mathrm{V}_{\mathrm{IN}}$


ALS Resistor Select Register $=0 \times 44$

Figure 5. Internal ALS Resistor vs $\mathrm{V}_{\mathrm{IN}}$

$\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C} \quad$ ALS Resistor Select Register $=0 \times 44$

Figure 7. Internal ALS Resistor vs $\mathrm{V}_{\mathrm{IN}}$


Figure 4. Shutdown Current vs $\mathrm{V}_{\mathrm{IN}}$

$\mathrm{T}_{\mathrm{A}}=85^{\circ} \mathrm{C}$
ALS Resistor Select Register $=0 \times 44$

$\mathrm{V}_{\text {OUT }}$ Rising

Figure 8. Overvoltage Protection vs $\mathrm{V}_{\mathrm{IN}}$

## Typical Characteristics (continued)

$\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$, LEDs are OVSRWAC1R6 from OPTEK Technology, $\mathrm{C}_{\mathrm{OUT}}=1 \mu \mathrm{~F}, \mathrm{C}_{\mathrm{IN}}=1 \mu \mathrm{~F}, \mathrm{~L}=$ TDK VLF5012ST-100M1R0, $\left(R_{L}=0.24 \Omega\right), I_{L E D}=19 \mathrm{~mA}, T_{A}=25^{\circ} \mathrm{C}$, unless otherwise specified.


Figure 9. Max Duty Cycle vs $\mathrm{V}_{\mathrm{IN}}$


Figure 11. Switching Frequency vs $\mathrm{V}_{\mathrm{IN}}$


Figure 13. Simple Disable Time vs $\mathrm{V}_{\mathrm{IN}}$


Figure 10. NFET Switch On-Resistance vs $\mathrm{V}_{\mathrm{IN}}$


Figure 12. Simple Enable Time vs $\mathrm{V}_{\mathrm{IN}}$


ILed Full Scale $=19 \mathrm{~mA}$
50\% Duty Cycle

Figure 14. $\mathrm{I}_{\text {LED }}$ vs $\mathrm{F}_{\text {PWM }}$

## Typical Characteristics (continued)

$\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$, LEDs are OVSRWAC1R6 from OPTEK Technology, $\mathrm{C}_{\text {OUT }}=1 \mu \mathrm{~F}, \mathrm{C}_{\mathrm{IN}}=1 \mu \mathrm{~F}, \mathrm{~L}=$ TDK VLF5012ST-100M1R0, $\left(R_{L}=0.24 \Omega\right), I_{L E D}=19 \mathrm{~mA}, T_{A}=25^{\circ} \mathrm{C}$, unless otherwise specified.

|  <br> Channel 2: SDA (5V/div) <br> Time Base ( $40 \mathrm{~ms} / \mathrm{div}$ ) <br> Channel 3: I LED ( $10 \mathrm{~mA} / \mathrm{div}$ ) <br> $1.024 \mathrm{~ms} /$ Step Up And Down <br> Figure 15. Ramp Rate (Exponential) |  <br> Channel 2: SDA (5V/div) <br> Time Base (100ms/div) <br> Channel 3: ILED ( $10 \mathrm{~mA} / \mathrm{div}$ ) <br> 2.048ms/Step Up And Down <br> Figure 16. Ramp Rate (Exponential) |
| :---: | :---: |
| Figure 17. Ramp Rate (Exponential) | Channel 2: SDA (5V/div) <br> Time Base ( $400 \mathrm{~ms} / \mathrm{div}$ ) <br> Channel 3: ILED ( $10 \mathrm{~mA} / \mathrm{div}$ ) <br> $8.192 \mathrm{~ms} /$ Step Up And Down <br> Figure 18. Ramp Rate (Exponential) |
| Figure 19. Ramp Rate (Exponential) |  |

## Typical Characteristics (continued)

$\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$, LEDs are OVSRWAC1R6 from OPTEK Technology, $\mathrm{C}_{\mathrm{OUT}}=1 \mu \mathrm{~F}, \mathrm{C}_{\mathrm{IN}}=1 \mu \mathrm{~F}, \mathrm{~L}=$ TDK VLF5012ST-100M1R0, $\left(R_{L}=0.24 \Omega\right), I_{L E D}=19 \mathrm{~mA}, T_{A}=25^{\circ} \mathrm{C}$, unless otherwise specified.


Channel 2: SDA (5V/div)
Channel 3: ILED ( $10 \mathrm{~mA} / \mathrm{div}$ )
65.538ms/Step Up And Down

Time Base ( $4 \mathrm{~s} / \mathrm{div}$ )

Figure 21. Ramp Rate (Exponential)


Channel 1: $\mathrm{V}_{\mathrm{IN}}(500 \mathrm{mV} / \mathrm{div})$
Channel 2: V
Channel 3: I LED $(500 \mu \mathrm{~A} /$ div)
$\mathrm{V}_{\mathrm{IN}}$ From 3.6 V To 3.2 V

Time Base (400 $\mu \mathrm{s} / \mathrm{div}$ )
$\mathrm{L}=22 \mu \mathrm{H}$
$\mathrm{I}_{\text {LED }}=19 \mathrm{~mA}$

Figure 23. Line Step Response


Figure 22. Start-up Plot


Figure 24. ILED Response To Step Change In PWM Duty Cycle


Closed Loop
$\mathrm{L}=22 \mu \mathrm{H}$
The value for current limit given in the Electrical Characteristics is measured in an open loop test by forcing current into SW until the current limit comparator threshold is reached. The typical curve for current limit is measured in closed loop using the typical application circuit by increasing lout until the peak inductor current stops increasing. Closed loop data appears higher due to the delay between the comparator trip point and the NFET turning off. This delay allows the closed loop inductor current to ramp higher after the trip point by approximately $100 \mathrm{~ns} \times \mathrm{V}_{\mathrm{IN}} / \mathrm{L}$.

Figure 25. Current Limit vs $\mathrm{V}_{\mathrm{IN}}$

## 8 Detailed Description

### 8.1 Overview

The LM3530 utilizes an asynchronous step-up, current mode, PWM controller and regulated current sink to provide an efficient and accurate LED current for white LED bias. The device powers a single series string of LEDs with output voltages of up to 40 V and a peak inductor current of typically 839 mA . The input active voltage range is from 2.7 V to 5.5 V .

### 8.2 Functional Block Diagram



Note 1: $\quad A_{\text {CODE }}$ Is a Scaler between 0 and 1 based on the Brightness Data or Zone Target Data Depending on the ALS Select Bit
Note 2: $\quad D_{\text {PWM }}$ Is a Scaler between 0 and 1 and corresponds to the duty cycle of the PWM input signal
Note 3: For EN_PWM bit = 1
$I_{\text {Led }}=I_{\text {fs }} \times A_{\text {code }} \times D_{\text {pwi }}$
For EN_PWM bit $=0$
$I_{\text {LED }}=I_{\text {FS }} \times A_{\text {CODE }}$

### 8.3 Feature Description

### 8.3.1 Start-Up

An internal soft-start prevents large inrush currents during start-up that can cause excessive current spikes at the input. For the typical application circuit (using a $10-\mu \mathrm{H}$ inductor, a $2.2-\mu \mathrm{F}$ input capacitor, and a $1-\mu \mathrm{F}$ output capacitor) the average input current during start-up ramps from 0 to 300 mA in 3 ms . See Figure 22 in the Typical Characteristics.

### 8.3.2 Light Load Operation

The LM3530 boost converter operates in three modes: continuous conduction, discontinuous conduction, and skip mode. Under heavy loads when the inductor current does not reach zero before the end of the switching period, the device switches at a constant frequency ( 500 kHz typical). As the output current decreases and the inductor current reaches zero before the end of the switching period, the device operates in discontinuous conduction. At very light loads the LM3530 will enter skip mode operation causing the switching period to lengthen and the device to only switch as required to maintain regulation at the output. Light load operation provides for improved efficiency at lighter LED currents compared to continuous and discontinuous conduction. This is due to the pulsed frequency operation resulting in decreased switching losses in the boost converter.

### 8.3.3 Ambient Light Sensor

The LM3530 incorporates a dual input Ambient Light Sensing interface (ALS1 and ALS2) which translates an analog output ambient light sensor to a user-specified brightness level. The ambient light sensing circuit has 4 programmable boundaries (ZB0 - ZB3) which define 5 ambient brightness zones. Each ambient brightness zone corresponds to a programmable brightness threshold (ZOT - Z4T). The ALS interface is programmable to accept the ambient light information from either the highest voltage of ALS1 or ALS2, the average voltage of ALS1 or ALS2, or selectable from either ALS1 or ALS2.

Furthermore, each ambient light sensing input (ALS1 or ALS2) features 15 internal software selectable voltage setting resistors. This allows the LM3530 the capability of interfacing with a wide selection of ambient light sensors. Additionally, the ALS inputs can be configured as high impedance, thus providing for a true shutdown during low power modes. The ALS resistors are selectable through the ALS Resistor Select Register (see Table 9). Figure 26 shows a functional block diagram of the ambient light sensor input. VSNS represents the active input as described in Table 6 bits [6:5].


Figure 26. Ambient Light Sensor Functional Block Diagram

## Feature Description (continued)

### 8.3.4 ALS Operation

The ambient light sensor input has a 0-V to 1-V operational input voltage range. LM3530 Typical Application shows the LM3530 with dual ambient light sensors (AVAGO, APDS-9005) and the internal ALS Resistor Select Register set to $0 \times 44(2.27 \mathrm{k} \Omega)$. This circuit converts 0 to 1000 LUX light into approximately a $0-\mathrm{mV}$ to $850-\mathrm{mV}$ linear output voltage. The voltage at the active ambient light sensor input (ALS1 or ALS2) is compared against the 8 bit values programmed into the Zone Boundary Registers (ZB0-ZB3). When the ambient light sensor output crosses one of the ZBO - ZB3 programmed thresholds the internal ALS circuitry will smoothly transition the LED current to the new 7 bit brightness level as programmed into the appropriate Zone Target Register (ZOT - Z4T) (see Figure 27).
The ALS Configuration Register bits [6:5] programs which input is the active input, bits [4:3] control the on/off state of the ALS circuitry, and bits [2:0] control the ALS input averaging time. Additionally, the ALS Information Register is a read-only register which contains a flag (bit 3) which is set each time the active ALS input changes to a new zone. This flag is reset when the register is read back. Bits [2:0] of this register contain the current active zone information.


Figure 27. Ambient Light Input To Backlight Mapping

### 8.3.5 ALS Averaging Time

The ALS Averaging Time is the time over which the Averager block collects samples from the A/D converter and then averages them to pass to the discriminator block (see Figure 26). Ambient light sensor samples are averaged and then further processed by the discriminator block to provide rejection of noise and transient signals. The averager is configurable with 8 different averaging times to provide varying amounts of noise and transient rejection (see Table 5). The discriminator block algorithm has a maximum latency of two averaging cycles; therefore, the averaging time selection determines the amount of delay that will exist between a steadystate change in the ambient light conditions and the associated change of the backlight illumination. For example, the A/D converter samples the ALS inputs at 16 kHz . If the averaging time is set to 1024 ms then the Averager will send the updated zone information to the discriminator every 1024 ms . This zone information contains the average of 16384 samples ( $1024 \mathrm{~ms} \times 16 \mathrm{kHz}$ ). Due to the latency of 2 averaging cycles, the LED current will not change until there has been a steady-state change in the ambient light for at least 2 averaging periods.

### 8.3.5.1 Averager Operation

The magnitude and direction (either increasing or decreasing) of the Averager output is used to determine whether the LM3530 should change brightness zones. The Averager block functions as follows:

1. First, the Averager always begins with a Zone 0 reading stored at start-up. If the main display LEDs are active before the ALS block is enabled, it is recommended that the ALS Enable 1 bit is set to ' 1 ' at least 3 averaging periods before the ALS Enable 2 bit is set.

## Feature Description (continued)

2. The Averager will always round down to the lower zone in the event of a non-integer zone average. For example, if during an averaging period the ALS input transitions between zones 1 and 2 resulting in an averager output of 1.75 , then the averager output will round down to 1 (see Figure 28).
3. The two most current averaging samples are used to make zone change decisions.
4. To make a zone change, data from three averaging cycles are needed. (Starting Value, First Transition, Second Transition or Rest).
5. To Increase the brightness zone, the Averager output must have increased for at least 2 averaging periods or increased and remained at the new level for at least two averaging periods (' + ' to ' + ' or ' + ' to 'Rest' in Figure 29).
6. To decrease the brightness zone, the Averager output must have decreased for at least 2 averaging periods or decreased and remained at the new level for at least two averaging periods ('-' to '-' or '-' to 'Rest' in Figure 29).

In the case of two consecutive increases or decreases in the Averager output, the LM3530 will transition to zone equal to the last averager output (Figure 29).
Using the diagram for the ALS block (Figure 26), the flow of information is shown in (Figure 30). This starts with the ALS input into the A/D, into the Averager, and then into the Discriminator. Each state filters the previous output to help prevent unwanted zone to zone transitions.
When using the ALS averaging function, it is important to remember that the averaging cycle is free running and is not synchronized with changing ambient lighting conditions. Due to the nature of the averager round down, an increase in brightness can take between 2 and 3 averaging cycles to change zones, while a decrease in brightness can take between 1 and 2 averaging cycles. See Table 6 for a list of possible Averager periods. Figure 31 shows an example of how the perceived brightness change time can vary.


Figure 28. Averager Calculation


Figure 29. Brightness Zone Change Examples


Figure 30. Ambient Light Input To Backlight Transition


Figure 31. Perceived Brightness Change Time

### 8.3.6 Zone Boundary Settings

Registers $0 \times 60,0 \times 61,0 \times 62$, and $0 \times 63$ set the 4 zone boundaries (thresholds) for the ALS inputs. These 4 zone boundaries create 5 brightness zones which map over to 5 separate brightness zone targets (see Figure 27). Each 8 -bit zone boundary register can set a threshold from typically 0 to 1 V with linear step sizes of approximately $1 / 255=3.92 \mathrm{mV}$. Additionally, each zone boundary has built in hysteresis which can be either lower or higher then the programmed Zone Boundary depending on the last direction (either up or down) of the ALS input voltage.

### 8.3.7 Zone Boundary Trip Points and Hysteresis

For each zone boundary setting, the trip point will vary above or below the nominal set point depending on the direction (either up or down) of the ALS input voltage. This is designed to keep the ALS input from oscillating back and forth between zones in the event that the ALS voltage is residing near to the programmed zone boundary threshold. The Zone Boundary Hysteresis will follow these 2 rules:

1. If the last zone transition was from low to high, then the trip point ( $\mathrm{V}_{\text {TRIP }}$ ) will be $\mathrm{V}_{\text {ZONE }}$ boundary $-\mathrm{V}_{\text {HYsT }} / 2$, where $\mathrm{V}_{\text {ZONE }}$ BOUNDARY is the zone boundary set point as programmed into the Zone Boundary registers, and $\mathrm{V}_{\text {HYSt }}$ is typically 7 mV .
2. If the last zone transition was from high to low then the trip point ( $\mathrm{V}_{\text {TRIP }}$ ) will be $\mathrm{V}_{\text {ZONE_BOUNDARY }}+\mathrm{V}_{\mathrm{HYST}} / 2$.

Figure 32 details how the LM3530 ALS Input Zone Boundary Thresholds vary depending on the direction of the ALS input voltage.
Referring to Figure 32, each numbered trip point shown is determined from the direction of the previous ALS zone transition.


Figure 32. Zone Boundaries With Hysteresis

### 8.3.8 Minimum Zone Boundary Settings

The actual minimum zone boundary setting is code $0 \times 03$. Codes of $0 \times 00,0 \times 01$, and $0 \times 02$ are all mapped to code $0 \times 03$. Table 1 shows the Zone Boundary codes $0 \times 00$ through 0x04, the typical thresholds, and the high and low hysteresis values. The remapping of codes $0 \times 00-0 \times 02$ plus the additional 4 mV of offset voltage is necessary to prevent random offsets and noise on the ALS inputs from creating threshold levels that are below GND. This essentially guarantees that any Zone Boundary threshold selected is achievable with positive ALS voltages.

Table 1. Ideal Zone Boundary Settings with Hysteresis (Lower 5 Codes)

| ZONE BOUNDARY CODE | TYPICAL ZONE BOUNDARY <br> THRESHOLD $(\mathbf{m V})$ | TYPICAL THRESHOLD + <br> HYSTERESIS $(\mathbf{m V})$ | TYPICAL THRESHOLD - <br> HYSTERRESIS $(\mathbf{m V})$ |
| :---: | :---: | :---: | :---: |
| $0 \times 00$ | 15.8 | 19.3 | 12.3 |
| $0 \times 01$ | 15.8 | 19.3 | 12.3 |
| $0 \times 02$ | 15.8 | 19.3 | 12.3 |
| $0 \times 03$ | 15.8 | 19.3 | 12.3 |
| $0 \times 04$ | 19.7 | 23.2 | 16.2 |

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### 8.3.9 LED Current Control

The LED current is is a function of the Full Scale Current, the Brightness Code, and the PWM input duty cycle. The Brightness Code can either come from the BRT Register ( $0 x A 0$ ) in $I^{2} \mathrm{C}$-Compatible Current Control, or from the ALS Zone Target Registers (Address 0x70-0x74) in Ambient Light Current Control. Figure 33 shows the current control block diagram.


Note 1: A CODE Is a Scaler between 0 and 1 based on the Brightness Data or Zone Target Data Depending on the ALS Select Bit
Note 2: $\mathrm{D}_{\text {PWM }}$ Is a Scaler between 0 and 1 and corresponds to the duty cycle of the PWM input signal
Note 3: For EN_PWM bit =1
$I_{\text {LED }}=I_{\text {FS }} \times A_{\text {CODE }} \times D_{\text {PWM }}$
For EN_PWM bit $=0$
$I_{\text {LED }}=I_{\text {FS }} \times A_{\text {CODE }}$
Figure 33. Current Control Block Diagram

### 8.3.10 Exponential or Linear Brightness Mapping Modes

With bit [1] of the General Configuration Register set to 0 (default) exponential mapping is selected and the code in the Brightness Control Register corresponds to the Full-Scale LED current percentages in Table 2 and Figure 34. With bit [1] set to 1 linear mapping is selected and the code in the Brightness Control Register corresponds to the Full-Scale LED current percentages in Table 3 and Figure 35.

### 8.3.11 PWM Input Polarity

Bit [6] of the General Configuration Register controls the PWM input polarity. Setting this bit to 0 (default) selects positive polarity and makes the LED current (with PWM mode enabled) a function of the positive duty cycle at PWM. With this bit set to ' 0 ' the LED current (with PWM mode enabled) becomes a function of the negative duty cycle at PWM.
The PWM input is a logic level input with a frequency range of 400 Hz to 50 kHz . Internal filtering of the PWM input signal converts the duty cycle information to an average (analog) control signal which directly controls the LED current.

## Example: PWM $+R^{2} C$-Compatible Current Control:

As an example, assume the the General Configuration Register is loaded with (0x2D). From Table 5, this sets up the LM3530 with:

Simple Enable OFF (bit $7=0$ )
Positive PWM Polarity (bit $6=0$ )
PWM Enabled (bit $5=1$ )
Full-Scale Current set at 15.5 mA (bits $[4: 2]=100$ )
Brightness Mapping set for Exponential (bit $1=0$ )
Device Enabled via $I^{2} C$ (bit $0=1$ )
Next, the Brightness Control Register is loaded with 0x73. This sets the LED current to $51.406 \%$ of full scale (see Equation 1). Finally, the PWM input is driven with a $0-\mathrm{V}$ to $2-\mathrm{V}$ pulse waveform at $70 \%$ duty cycle. The LED current under these conditions will be:
$I_{\text {LED }}=I_{\text {LED_FS }} \times B R T \times D=15.5 \mathrm{~mA} \times 51.4 \% \times 70 \% \approx 5.58 \mathrm{~mA}$.
where

- BRT is the percentage of $\mathrm{I}_{\text {LED_Fs }}$ as set in the Brightness Control Register


### 8.3.12 $I^{2} \mathrm{C}$-Compatible Current Control Only

$1^{2} \mathrm{C}$-Compatible Control is enabled by writing a ' 1 ' to the $\mathrm{I}^{2} \mathrm{C}$ Device Enable bit (bit [ 0 ] of the General Configuration Register), a ' 0 ' to the Simple Enable bit (bit 7), and a ' 0 ' to the PWM Enable bit (bit 5). With bit $5=$ 0 , the duty cycle information at the PWM input is not used in setting the LED current.
In this mode the LED current is a function of the Full-Scale LED current bits (bits [4:2] of the General Configuration Register) and the code in the Brightness Control Register. The LED current mapping for the Brightness Control Register can be linear or exponential depending on bit [1] in the General Configuration Register (see Exponential or Linear Brightness Mapping Modes section). Using $1^{2} \mathrm{C}$-Compatible Control Only, the Full-Scale LED Current bits and the Brightness Control Register code provides nearly 1016 possible current levels selectable over the $\mathrm{I}^{2} \mathrm{C}$-compatible interface.

## Example: $I^{2}$ C-Compatible Current Control Only:

As an example, assume the General Configuration Register is loaded with $0 \times 15$. From Table 5 this sets up the LM3530 with:

Simple Enable OFF (bit $7=0$ )
Positive PWM Polarity (bit $6=0$ )
PWM Disabled (bit $5=0$ )
Full-Scale Current set at 22.5 mA (bits [4:2] = 101)
Brightness Mapping set for Exponential (bit $1=0$ )
Device Enabled via $I^{2} C($ bit $0=1)$
The Brightness Control Register is then loaded with $0 \times 72$ ( $48.438 \%$ of full-scale current from Equation 2). The LED current with this configuration becomes:
$\mathrm{I}_{\text {LED }}=\mathrm{I}_{\text {LED_FS }} \times B R T=22.5 \mathrm{~mA} \times 0.48438 \approx 10.9 \mathrm{~mA}$.
where

- BRT is the \% of $\mathrm{I}_{\text {LED_Fs }}$ as set in the Brightness Control Register.

Next, the brightness mapping is set to linear mapping mode (bit [1] in General Configuration Register set to 1). Using the same Full-Scale current settings and Brightness Control Register settings as before, the LED current becomes:

$$
\begin{equation*}
I_{\text {LED }}=I_{\text {LED_Fs }} \times B R T=22.5 \mathrm{~mA} \times 0.8976 \approx 20.2 \mathrm{~mA} . \tag{3}
\end{equation*}
$$

Which is higher now since the code in the Brightness Control Register (0x72) corresponds to $89.76 \%$ of FullScale LED Current due to the different mapping mode given in Figure 34.


Figure 34. Exponential Brightness Mapping
Table 2. I LED vs. Brightness Register Data (Exponential Mapping)

| BRT DATA (HEX) | \% FULL-SCALE CURRENT | BRT DATA (HEX) | $\begin{aligned} & \text { \% OF FULL- } \\ & \text { SCALE } \\ & \text { CURRENT } \end{aligned}$ | BRT DATA (HEX) | $\begin{aligned} & \text { \% OF FULL- } \\ & \text { SCALE } \\ & \text { CURRENT } \end{aligned}$ | BRT DATA (HEX) | $\begin{gathered} \text { \% OF FULL- } \\ \text { SCALE } \\ \text { CURRENT } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0x00 | 0.00\% | 0x20 | 0.500\% | 0x40 | 2.953\% | 0x60 | 17.813\% |
| $0 \times 01$ | 0.080\% | $0 \times 21$ | 0.523\% | $0 \times 41$ | 3.125\% | $0 \times 61$ | 18.750\% |
| $0 \times 02$ | 0.086\% | $0 \times 22$ | 0.555\% | $0 \times 42$ | 3.336\% | $0 \times 62$ | 19.922\% |
| $0 \times 03$ | 0.094\% | $0 \times 23$ | 0.586\% | $0 \times 43$ | 3.500\% | $0 \times 63$ | 20.859\% |
| $0 \times 04$ | 0.102\% | $0 \times 24$ | 0.617\% | 0x44 | 3.719\% | 0x64 | 22.266\% |
| $0 \times 05$ | 0.109\% | 0x25 | 0.656\% | 0x45 | 3.906\% | 0x65 | 23.438\% |
| $0 \times 06$ | 0.117\% | 0x26 | 0.695\% | 0x46 | 4.141\% | 0x66 | 24.844\% |
| $0 \times 07$ | 0.125\% | $0 \times 27$ | 0.734\% | $0 \times 47$ | 4.375\% | $0 \times 67$ | 26.250\% |
| $0 \times 08$ | 0.133\% | $0 \times 28$ | 0.773\% | $0 \times 48$ | 4.648\% | $0 \times 68$ | 27.656\% |
| $0 \times 09$ | 0.141\% | 0x29 | 0.820\% | 0x49 | 4.922\% | 0x69 | 29.297\% |
| $0 \times 0 \mathrm{~A}$ | 0.148\% | $0 \times 2 \mathrm{~A}$ | 0.867\% | $0 \times 4 \mathrm{~A}$ | 5.195\% | 0x6A | 31.172\% |
| $0 \times 0 \mathrm{~B}$ | 0.156\% | $0 \times 2 \mathrm{~B}$ | 0.914\% | $0 \times 4 \mathrm{~B}$ | 5.469\% | 0x6B | 32.813\% |
| 0x0C | 0.164\% | $0 \times 2 \mathrm{C}$ | 0.969\% | 0x4C | 5.781\% | 0x6C | 34.453\% |
| 0x0D | 0.172\% | 0x2D | 1.031\% | 0x4D | 6.125\% | 0x6D | 35.547\% |
| 0x0E | 0.180\% | $0 \times 2 \mathrm{E}$ | 1.078\% | 0x4E | 6.484\% | $0 \times 6 \mathrm{E}$ | 38.828\% |
| $0 \times 0 \mathrm{~F}$ | 0.188\% | 0x2F | 1.148\% | 0x4F | 6.875\% | 0x6F | 41.016\% |
| $0 \times 10$ | 0.203\% | 0x30 | 1.219\% | 0x50 | 7.266\% | 0x70 | 43.203\% |
| $0 \times 11$ | 0.211\% | $0 \times 31$ | 1.281\% | $0 \times 51$ | 7.656\% | 0x71 | 45.938\% |
| $0 \times 12$ | 0.227\% | $0 \times 32$ | 1.359\% | 0x52 | 8.047\% | 0x72 | 48.438\% |
| $0 \times 13$ | 0.242\% | 0x33 | 1.430\% | 0x53 | 8.594\% | 0x73 | 51.406\% |
| $0 \times 14$ | 0.250\% | $0 \times 34$ | 1.523\% | 0x54 | 9.063\% | 0x74 | 54.141\% |
| $0 \times 15$ | 0.266\% | 0x35 | 1.594\% | 0x55 | 9.609\% | 0x75 | 57.031\% |
| $0 \times 16$ | 0.281\% | $0 \times 36$ | 1.688\% | 0x56 | 10.078\% | $0 \times 76$ | 60.703\% |
| $0 \times 17$ | 0.297\% | $0 \times 37$ | 1.781\% | 0x57 | 10.781\% | 0x77 | 63.984\% |
| $0 \times 18$ | 0.320\% | $0 \times 38$ | 1.898\% | 0x58 | 11.250\% | 0x78 | 67.813\% |
| $0 \times 19$ | 0.336\% | 0x39 | 2.016\% | 0x59 | 11.953\% | $0 \times 79$ | 71.875\% |
| $0 \times 1 \mathrm{~A}$ | 0.352\% | $0 \times 3 \mathrm{~A}$ | 2.109\% | $0 \times 5 \mathrm{~A}$ | 12.656\% | 0x7A | 75.781\% |
| $0 \times 1 \mathrm{~B}$ | 0.375\% | 0x3B | 2.250\% | 0x5B | 13.359\% | 0x7B | 79.688\% |
| 0x1C | 0.398\% | 0×3C | 2.367\% | 0x5C | 14.219\% | 0x7C | 84.375\% |

Table 2. $I_{\text {LED }}$ vs. Brightness Register Data (Exponential Mapping) (continued)

| BRT DATA <br> (HEX) | \% FULL-SCALE <br> CURRENT | BRT DATA (HEX) | \% OF FULL- <br> SCALE <br> CURRENT | BRT DATA <br> (HEX) | \% OF FULL- <br> SCALE <br> CURRENT | BRT <br> DATA <br> (HEX) | \% OF FULL- <br> SCALE <br> CURRENT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0 \times 1 \mathrm{D}$ | $0.422 \%$ | $0 \times 3 \mathrm{D}$ | $2.508 \%$ | $0 \times 5 \mathrm{D}$ | $15.000 \%$ | $0 \times 7 \mathrm{D}$ | $89.844 \%$ |
| $0 \times 1 \mathrm{E}$ | $0.445 \%$ | $0 \times 3 \mathrm{E}$ | $2.648 \%$ | $0 \times 5 \mathrm{E}$ | $15.859 \%$ | $0 \times 7 \mathrm{E}$ | $94.531 \%$ |
| $0 \times 1 \mathrm{~F}$ | $0.469 \%$ | $0 \times 3 F$ | $2.789 \%$ | $0 \times 5 \mathrm{~F}$ | $16.875 \%$ | $0 \times 7 \mathrm{~F}$ | $100.00 \%$ |



Figure 35. Linear Brightness Mapping

Table 3. I Led vs. Brightness Register Data (Linear Mapping)

| BRT DATA <br> (HEX) | \% FULL- <br> SCALE <br> CURREN <br> T | BRT DATA <br> (HEX) <br> (LINEAR) | \% OF FULL- <br> SCALE <br> CURRENT <br> (LINEAR) | BRT DATA <br> (HEX) | \% OF <br> FULL- <br> SCALE <br> CURRE <br> NT <br> (LINEA | BRT DATA (HEX) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CURRENT (LINEAR) |  |  |  |  |  |  |  |
| R) |  |  |  |  |  |  |  |

Table 3. I Led vs. Brightness Register Data (Linear Mapping) (continued)

| $\begin{aligned} & \text { BRT DATA } \\ & \text { (HEX) } \end{aligned}$ | \% FULLSCALE CURREN T (LINEAR) | $\begin{aligned} & \text { BRT DATA } \\ & \text { (HEX) } \end{aligned}$ | \% OF FULLSCALE CURRENT (LINEAR) | $\begin{aligned} & \text { BRT DATA } \\ & \text { (HEX) } \end{aligned}$ | \% OF FULLSCALE CURRE NT (LINEA R) | BRT DATA (HEX) | \% OF FULL-SCALE CURRENT (LINEAR) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0 \times 13$ | 15.63\% | $0 \times 33$ | 40.63\% | $0 \times 53$ | 65.63\% | $0 \times 73$ | 90.63\% |
| $0 \times 14$ | 16.41\% | $0 \times 34$ | 41.41\% | $0 \times 54$ | 66.41\% | 0x74 | 91.41\% |
| $0 \times 15$ | 17.19\% | 0x35 | 42.19\% | 0x55 | 67.19\% | 0x75 | 92.19\% |
| $0 \times 16$ | 17.97\% | 0x36 | 42.97\% | 0x56 | 67.97\% | 0x76 | 92.97\% |
| $0 \times 17$ | 18.76\% | $0 \times 37$ | 43.75\% | $0 \times 57$ | 68.75\% | $0 \times 77$ | 93.75\% |
| $0 \times 18$ | 19.54\% | $0 \times 38$ | 44.53\% | $0 \times 58$ | 69.53\% | 0x78 | 94.53\% |
| $0 \times 19$ | 20.32\% | $0 \times 39$ | 45.32\% | 0x59 | 70.39\% | 0x79 | 95.31\% |
| $0 \times 1 \mathrm{~A}$ | 21.10\% | $0 \times 3 \mathrm{~A}$ | 46.10\% | $0 \times 5 \mathrm{~A}$ | 71.10\% | 0x7A | 96.09\% |
| $0 \times 1 \mathrm{~B}$ | 21.88\% | $0 \times 3 \mathrm{~B}$ | 46.88\% | $0 \times 5 B$ | 71.88\% | 0x7B | 96.88\% |
| $0 \times 1 \mathrm{C}$ | 22.66\% | 0x3C | 47.66\% | 0x5C | 72.66\% | 0x7C | 97.66\% |
| $0 \times 1 \mathrm{D}$ | 23.44\% | $0 \times 3 \mathrm{D}$ | 48.44\% | $0 \times 5 \mathrm{D}$ | 73.44\% | 0x7D | 98.44\% |
| 0x1E | 24.22\% | 0x3E | 49.22\% | 0x5E | 74.22\% | 0x7E | 99.22\% |
| 0x1F | 25.00\% | 0x3F | 50.00\% | 0x5F | 75.00\% | 0x7F | 100.00\% |

## NOTE

When determining the LED current from (Table 2 and Table 3 ) there is a typical offset of $113 \mu \mathrm{~A}$ with a $\pm 300-\mu \mathrm{A}$ variation that must be added to the calculated value for codes $0 \times 0 \mathrm{~A}$ and below. For example, in linear mode with $\mathrm{I}_{\text {FULL_scale }}=19 \mathrm{~mA}$ and brightness code $0 \times 09$ chosen, the nominal current setting is $0.0782 \times 19 \mathrm{~mA}=1.4858 \mathrm{~mA}$. Adding in the $113-\mu \mathrm{A}$ typical offset gives $1.4858 \mathrm{~mA}+0.113 \mathrm{~mA}=1.5988 \mathrm{~mA}$. With the typical $\pm 300-\mu \mathrm{A}$ range, the high and low currents can be $\mathrm{I}_{\text {LOw }}=1.2988 \mathrm{~mA}, \mathrm{I}_{\text {HIGH }}=1.8988 \mathrm{~mA}$. For exponential mode with codes $0 \times 0 \mathrm{~A}$ and below, this offset and variation error gets divided down by 10 ( $11.3 \mu \mathrm{~A}$ offset with $\pm 30-\mu \mathrm{A}$ typical range).

### 8.3.13 Simple Enable Disable With PWM Current Control

With bits [7 and 5] of the General Configuration Register set to ' 1 ' the PWM input is enabled as a simple enable/disable. The simple enable/disable feature operates as described in Figure 36. In this mode, when the PWM input is held high (PWM Polarity bit $=0$ ) for $>2 \mathrm{~ms}$ the LM3530 will turn on the LED current at the programmed Full-Scale Current $\times \%$ of Full-Scale Current as set by the code in the Brightness Control Register. When the PWM input is held low for $>2 \mathrm{~ms}$ the device will shut down. With the PWM Polarity bit = 1 the PWM input is configured for active low operation. In this configuration holding PWM low for $>2 \mathrm{~ms}$ will turn on the device at the programmed Full-Scale Current $\times \%$ of Full-Scale Current as set by the code in the Brightness Control Register. Likewise, holding PWM high for > 2 ms will put the device in shutdown.
Driving the PWM input with a pulsed waveform at a variable duty cycle is also possible in simple enable/Disable mode, so long as the low pulse width is $<2 \mathrm{~ms}$. When a PWM signal is used in this mode the input duty cycle information is internally filtered, and an analog voltage is used to control the LED current. This type of PWM control (PWM to Analog current control) prevents large voltage excursions across the output capacitor that can result in audible noise. Simple Enable/Disable mode can be useful since the default bit setting for the General Configuration Register is 0xCC (Simple Enable bit =1, PWM Enable $=$ 1, and Full-Scale Current $=19 \mathrm{~mA}$ ). Additionally, the default Brightness Register setting is 0x7F (100\% of Full-Scale current). This gives the LM3530 the ability to turn on after power up (or after reset) without having to do any writes to the $\mathrm{I}^{2} \mathrm{C}$-compatible bus.


Figure 36. Simple Enable/Disable Timing

## Example: Simple Enable Disable with PWM Current Control):

As an example, assume that the HWEN input is toggled low then high. This resets the LM3530 and sets all the registers to their default value. When the PWM input is then pulled high for $>2 \mathrm{~ms}$ the LED current becomes:
$I_{\text {LED }}=I_{\text {LED_FS }} \times B R T \times D=19 \mathrm{~mA} \times 1.00 \times 100 \% \approx 19 \mathrm{~mA}$.
where

- BRT is the \% of $\mathrm{I}_{\text {LED_Fs }}$ as set in the Brightness Control Register.

If then the PWM input is fed with a $5-\mathrm{kHz}$ pulsed waveform at $40 \%$ duty cycle the LED current becomes:

$$
I_{\text {LED }}=I_{\text {LED_Fs }} \times B R T \times D=19 \mathrm{~mA} \times 1.00 \times 0.4 \approx 7.6 \mathrm{~mA} .
$$

Then, if the Brightness Control Register is loaded with $0 \times 55$ ( $9.6 \%$ of Full-Scale Current) the LED current becomes:

$$
\begin{equation*}
I_{\text {LED }}=I_{\text {LED } \_ \text {FS }} \times B R T \times D=19 \mathrm{~mA} \times 9.65 \times 0.4 \approx 0.73 \mathrm{~mA} . \tag{6}
\end{equation*}
$$

### 8.3.14 Ambient Light Current Control

With bits [4:3] of the ALS Configuration Register both set to 1, the LM3530 is configured for Ambient Light Current Control. In this mode the ambient light sensing inputs (ALS1, and/or ALS2) monitor the outputs of analog output ambient light sensing photo diodes and adjust the LED current depending on the ambient light. The ambient light sensing circuit has 4 configurable Ambient Light Boundaries (ZB0 - ZB3) programmed through the four (8-bit) Zone Boundary Registers. These zone boundaries define 5 ambient brightness zones (Figure 27). Each zone corresponds to a programmable brightness setting which is programmable through the 5 Zone Target Registers (ZOT - Z4T). When the ALS1, and/or ALS2 input (depending on the bit settings of the ALS Input Select bits) detects that the ambient light has crossed to a new zone (as defined by one of the Zone Boundary Registers) the LED current becomes a function of the Brightness Code loaded in the Zone Target Register which corresponds to the new ambient light brightness zone.
On start-up the 4 Zone Boundary Registers are pre-loaded with $0 \times 33$ (51d), $0 \times 66$ (102d), $0 \times 99$ (153d), and 0xCC (204d). Each ALS input has a $1-\mathrm{V}$ active input voltage range with a 4 mV offset voltage which makes the default Zone Boundaries set at:
Zone Boundary $0=1 \mathrm{~V} \times 51 / 255+4 \mathrm{mV}=204 \mathrm{mV}$
Zone Boundary $1=1 \mathrm{~V} \times 102 / 255+4 \mathrm{mV}=404 \mathrm{mV}$
Zone Boundary $2=1 \mathrm{~V} \times 153 / 255+4 \mathrm{mV}=604 \mathrm{mV}$
Zone Boundary $3=1 \mathrm{~V} \times 204 / 255+4 \mathrm{mV}=804 \mathrm{mV}$
These Zone Boundary Registers are all 8 -bit (readable and writable) registers. The first zone $(Z 0)$ is defined between 0 and 204 mV , the Z 1 default is defined between 204 mV and 404 mV , the Z2 default is defined between 404 mV and 604 mV , the Z 3 default is defined between 604 mV and 804 mV , and the Z 4 default is defined between 804 mV and 1.004 V . The default settings for the 5 Zone Target Registers are $0 \times 19$, $0 \times 33$, $0 \times 4 \mathrm{C}, 0 \times 66$, and $0 \times 7 \mathrm{~F}$. This corresponds to LED brightness settings of $0.336 \%, 1.43 \%, 5.781 \%, 24.844 \%$, and $100 \%$ of full-scale current respectively (assuming exponential backlight mapping).
Example: Ambient Light Control Current:

As an example, assume that the APDS-9005 is used as the ambient light sensing photo diode with its output connected to the ALS1 input. The ALS Resistor Select Register is loaded with 0x04 which configures the ALS1 input for a $2.27-\mathrm{k} \Omega$ internal pull-down resistor (see Table 9). The APDS-9005 has a typical 400nA/LUX response. With a $2.27-\mathrm{k} \Omega$ resistor the sensor output would see a $0-\mathrm{mV}$ to $908-\mathrm{mV}$ swing with a 0 to 1000 LUX change in ambient light. Next, the ALS Configuration Register is programmed with 0x3C. From Table 6, this configures the LM3530's ambient light sensing interface for:
ALS1 as the active ALS input (bits [6:5] = 01)
Ambient Light Current Control Enabled (bit $4=1$ )
ALS circuitry Enabled (bit $3=1$ )
Sets the ALS Averaging Time to 512 ms (bits [2:0] = 100)
Next, the General Configuration Register is programmed with $0 \times 19$ which sets the Full-Scale Current to 26 mA , selects Exponential Brightness Mapping, and enables the device via the $\mathrm{I}^{2} \mathrm{C}$-compatible interface.

Now assume that the APDS-9005 ambient light sensor detects a 100 LUX ambient light at its input. This forces the ambient light sensors output (and the ALS1 input) to 87.5 mV corresponding to Zone 0 . Since Zone 0 points to the brightness code programmed in Zone Target Register 0 (loaded with code $0 \times 19$ ), the LED current becomes:

$$
\begin{equation*}
I_{\text {LED }}=I_{\text {LED_FS }} \times \text { ZoneTarget0 }=26 \mathrm{~mA} \times 0.336 \% \approx 87 \mu \mathrm{~A} . \tag{7}
\end{equation*}
$$

Where the code in Zone Target Register 0 points to the \% of ILED_FS as given by Table 2 or Table 3, depending on whether Exponential or Linear Mapping are selected.
Next, assume that the ambient light changes to 500 LUX (corresponding to an ALS1 voltage of 454 mV ). This moves the ambient light into Zone 2 which corresponds to Zone Target Register 2 (loaded with code 0x4C) the LED current then becomes:

$$
\begin{equation*}
I_{\text {LED }}=I_{\text {LED_FS }} \times \text { ZoneTarget2 }=26 \mathrm{~mA} \times 5.781 \% \approx 1.5 \mathrm{~mA} \text {. } \tag{8}
\end{equation*}
$$

### 8.3.15 Ambient Light Current Control + PWM

The Ambient Light Current Control can also be a function of the PWM input duty cycle. Assume the LM3530 is configured as described in the above Ambient Light Current Control example, but this time the Enable PWM bit set to '1' (General Configuration Register bit [5]).

## Example: Ambient Light Current Control + PWM

In this example, the APDS-9005 detects that the ambient light has changed to 1 kLUX . The voltage at ALS 1 is now around 908 mV , and the ambient light falls within Zone 5. This causes the LED brightness to be a function of Zone Target Register 5 (loaded with 0x7F). Now assume the PWM input is also driven with a $50 \%$ duty cycle pulsed waveform. The LED current now becomes:
$I_{\text {LED }}=I_{\text {LED_FS }} \times$ ZoneTarget5 $\times \mathrm{D}=26 \mathrm{~mA} \times 100 \% \times 50 \% \approx 13 \mathrm{~mA}$.

## Example: ALS Averaging:

As an example, suppose the LM3530 ALS Configuration Register is loaded with 0×3B. This configures the device for:

ALS1 as the active ALS input (bits [6:5] = 01)
Enables Ambient Light Current Control (bit $4=1$ )
Enables the ALS circuitry (bit $3=1$ )
Sets the ALS Averaging Time to 256 ms (bits [2:0] = 011)
Next, the ALS Resistor Select Register is loaded with 0x04. This configures the ALS2 input as high impedance and configures the ALS1 input with a $2.27-\mathrm{k} \Omega$ internal pull-down resistor. The Zone Boundary Registers and Zone Target Registers are left with their default values. The Brightness Ramp Rate Register is loaded with 0x2D. This sets up the LED current ramp rate at $16.384 \mathrm{~ms} / \mathrm{step}$. Finally, the General Configuration Register is loaded with $0 \times 15$. This sets up the device with:
Simple Enable OFF (bit $7=0$ )
PWM Polarity High (bit $6=0$ )
PWM Input Disabled (bit $5=0$ )
Full-Scale Current = 22.5mA (bits [4:2] = 101)
Brightness Mapping Mode as Exponential (bit $1=0$ )
Device Enabled via $I^{2} C$ (bit $0=1$ )
As the device starts up the APDS-9005 ambient light sensor (connected to the ALS1 input) detects 500 LUX. This puts approximately 437.5 mV at ALS1 (see Figure 37). This places the measured ambient light between Zone Boundary Registers 1 and 2, thus corresponding to Zone Target Register 2. The default value for this register is $0 \times 4 \mathrm{C}$. The LED current is programmed to:

$$
\begin{equation*}
I_{\text {LED }}=I_{\text {LED_FS }} \times \text { ZoneTarget2 }=22.5 \mathrm{~mA} \times 5.781 \% \approx 1.3 \mathrm{~mA} . \tag{10}
\end{equation*}
$$

Referring to Figure 37, initially the Averager is loaded with Zone 0 so it takes 2 averaging periods for the LM3530 to change to the new zone. After the ALS1 voltage remains at 437.5 mV for two averaging periods (end of period 2) the LM3530 repeats Zone 2 and signals the LED current to begin ramping to the Zone 2 target beginning at average period 3 . Since the ramp rate is set at $16.384 \mathrm{~ms} /$ step the LED current goes from 0 to 1.3 mA in $76 \times$ $16.384 \mathrm{~ms}=1.245 \mathrm{~s}$ (approximately 5 average periods).
After the LED current has been at its steady state of 1.3 mA for a while, the ambient light suddenly steps to 900 LUX for 500 ms and then steps back to 500 LUX. In this case the 900 LUX will place the ALS1 voltage at approximately 979 mV corresponding to Zone 4 somewhere during average period 10 and fall back to 437.5 mV somewhere during average period 12. The averager output during period \#10 goes to 3, and then during period 11 , goes to 4 . Since there have been 2 increases in the average during period 10 and period 11, the beginning of average period \#12 shows a change in the brightness zone to Zone 4. This results in the LED current ramping to the new value of 22.5 mA (the Zone 4 target). During period \#12 the ambient light steps back to 500 LUX and forces ALS1 to 437.5 mV (corresponding to Zone 2). After average period 12 and period 13 have shown that the averager transitioned lower two times, the brightness zone changes to the new target at the beginning of period 14. This signals the LED current to ramp down to the zone 2 target of 1.3 mA . Looking back at average period 12 and period 13, the LED current was only able to ramp up to 7.38 mA due to the ramp rate of $16.384 \mathrm{~ms} / \mathrm{step}$ (2 average periods of 256 ms each) before it was instructed to ramp back to the Zone 2 target at the start of period 14. This example demonstrates not only the averaging feature, but how additional filtering of transient events on the ALS inputs can be accomplished by using the LED current ramp rates.


Figure 37. ALS Averaging Example

### 8.3.16 Interrupt Output

INT is an open-drain output which pulls low when the Ambient Light Sensing circuit has transitioned to a new ambient brightness zone. When a read-back of the ALS Information Register is done INT is reset to the open drain state.

### 8.3.17 Overvoltage Protection

Overvoltage protection is set at 40 V (minimum) for the LM3530-40 and 23.6 V minimum for the LM3530-25. The 40-V version allows typically up to 11 series white LEDs (assuming 3.5 V per LED +400 mV headroom voltage for the current sink $=38.9 \mathrm{~V}$ ). When the OVP threshold is reached the LM3530 switching converter stops switching, allowing the output voltage to discharge. Switching will resume when the output voltage falls to typically 1 V below the OVP threshold. In the event of an LED open circuit the output will be limited to around 40 V with a small amount of voltage ripple. The $25-\mathrm{V}$ version allows up to 6 series white LEDs (assuming $3.5-\mathrm{V}$ per LED +400 mV headroom voltage for the current sink $=21.4 \mathrm{~V}$ ). The 25-V OVP option allows for the use of lower voltage and smaller sized ( 25 V ) output capacitors. The $40-\mathrm{V}$ device would typically require a $50-\mathrm{V}$ output capacitor.

### 8.3.18 Hardware Enable

The HWEN input is an active high hardware enable which must be pulled high to enable the device. Pulling this pin low disables the $I^{2} \mathrm{C}$-compatible interface, the simple enable/disable input, the PWM input, and resets all registers to their default state (see Table 4).

### 8.3.19 Thermal Shutdown

In the event the die temperature reaches $140^{\circ} \mathrm{C}$, the LM 3530 will stop switching until the die temperature cools by $15^{\circ} \mathrm{C}$. In a thermal shutdown event the device is not placed in reset; therefore, the contents of the registers are left in their current state.

### 8.4 Device Functional Modes

### 8.4.1 Shutdown

With HWEN Low, or bit 0 in register $0 \times 10$ set to 0 , the device is in shutdown. In this mode the boost converter and the current sink are both off and the supply current into IN is reduced to typically $1 \mu \mathrm{~A}$.

### 8.4.2 ${ }^{2}$ ² Mode

$I^{2} \mathrm{C}$-Compatible Control Mode is enabled by writing a ' 1 ' to the $I^{2} \mathrm{C}$ Device Enable bit (bit [0] of the General Configuration Register), a ' 0 ' to the Simple Enable bit (bit 7), and a ' 0 ' to the PWM Enable bit (bit 5). With bit $5=$ 0 , the duty cycle information at the PWM input is not used in setting the LED current. In this mode the LED current is a function of the Full-Scale LED current bits (bits [4:2] of the General Configuration Register) and the code in the Brightness Control Register. The LED current mapping for the Brightness Control Register can be linear or exponential depending on bit [1] in the General Configuration Register (see Exponential or Linear Brightness Mapping Modes section). Using ${ }^{2} \mathrm{C}$-Compatible Control Only, the Full-Scale LED Current bits and the Brightness Control Register code provides nearly 1016 possible current levels selectable over the $\mathrm{I}^{2} \mathrm{C}$-compatible interface.

### 8.4.3 PWM + ${ }^{2} \mathrm{C}$ Mode

PWM $+1^{2} \mathrm{C}$-compatible current control mode is enabled by writing a ' 1 ' to the Enable PWM bit (General Configuration Register bit [5]) and writing a ' 1 ' to the $I^{2} \mathrm{C}$ Device Enable bit (General Configuration Register bit 0 ). This makes the LED current a function of the PWM input duty cycle (D), the Full-Scale LED current (l-LED_FS $)$, and the \% of full-scale LED current. The \% of Full-Scale LED current is set by the code in the Brightness Control Register. The LED current using PWM $+I^{2} \mathrm{C}$-Compatible Control is given by Equation 11:

$$
\begin{equation*}
\mathrm{I}_{\text {LED }}=\mathrm{I}_{\text {LED_FS }} \times \mathrm{BRT} \times \mathrm{D} \tag{11}
\end{equation*}
$$

BRT is the percentage of Full Scale Current as set in the Brightness Control Register. The Brightness Control Register can have either exponential or linear brightness mapping depending on the setting of the BMM bit (bit [1] in General Configuration Register).

### 8.4.4 ALS Mode

With bits [4:3] of the ALS Configuration Register both set to 1, the LM3530 is configured for Ambient Light Current Control. In this mode the ambient light sensing inputs (ALS1, and/or ALS2) monitor the outputs of analog output ambient light sensing photo diodes and adjust the LED current depending on the ambient light.

### 8.4.5 Simple Enable Mode

Simple Enable Mode With bits [7 and 5] of the General Configuration Register set to ' 1 ' the PWM input is enabled as a simple enable/disable. The simple enable/disable feature operates as described in Figure 36. In this mode, when the PWM input is held high (PWM Polarity bit $=0$ ) for $>2 \mathrm{~ms}$ the LM3530 will turn on the LED current at the programmed Full-Scale Current $\times \%$ of Full-Scale Current as set by the code in the Brightness Control Register. When the PWM input is held low for > 2 ms the device will shut down.

### 8.5 Programming

### 8.5.1 $I^{2} \mathrm{C}$-Compatible Interface

### 8.5.1.1 Start and Stop Condition

The LM3530 is controlled via an $I^{2} \mathrm{C}$-compatible interface. START and STOP conditions classify the beginning and the end of the $I^{2} \mathrm{C}$ session. A START condition is defined as SDA transitioning from HIGH to LOW while SCL is HIGH. A STOP condition is defined as SDA transitioning from LOW to HIGH while SCL is HIGH. The I ${ }^{2} \mathrm{C}$ master always generates the START and STOP conditions. The $I^{2} \mathrm{C}$ bus is considered busy after a START condition and free after a STOP condition. During data transmission, the $1^{2} \mathrm{C}$ master can generate repeated START conditions. A START and a repeated START conditions are equivalent function-wise. The data on SDA must be stable during the HIGH period of the clock signal (SCL). In other words, the state of SDA can only be changed when SCL is LOW.


Figure 38. Start and Stop Sequences

### 8.5.1.2 PRC-Compatible Address

The 7 bit chip address for the LM3530 is $(0 \times 38$, or $0 \times 39)$ for the $40-\mathrm{V}$ version and $(0 \times 36)$ for the $25-\mathrm{V}$ version. After the START condition, the IC master sends the 7-bit chip address followed by an eighth bit (LSB) read or write (R/W). R/W = 0 indicates a WRITE and R/W = 1 indicates a READ ${ }^{2}$. The second byte following the chip address selects the register address to which the data will be written. The third byte contains the data for the selected register.


Figure 39. $\mathrm{I}^{2} \mathrm{C}$-Compatible Chip Address ( $0 \times 38$ )


Figure 40. $1^{2} \mathrm{C}$-Compatible Chip Address ( $0 \times 36$ )

### 8.5.1.3 Transferring Data

Every byte on the SDA line must be eight bits long, with the most significant bit (MSB) transferred first. Each byte of data must be followed by an acknowledge bit (ACK). The acknowledge related clock pulse (9th clock pulse) is generated by the master. The master then releases SDA (HIGH) during the 9th clock pulse. The LM3530 pulls down SDA during the 9th clock pulse, signifying an acknowledge. An acknowledge is generated after each byte has been received.

There are fourteen 8-bit registers within the LM3530 as detailed in Table 4.

### 8.6 Register Maps

### 8.6.1 Register Descriptions

Table 4. LM3530 Register Definition

| REGISTER NAME | FUNCTION | ADDRESS | POR VALUE |
| :---: | :---: | :---: | :---: |
| General Configuration | 1. Simple Interface Enable <br> 2. PWM Polarity <br> 3. PWM enable <br> 4. Full-Scale Current Selection <br> 5. Brightness Mapping Mode Select <br> 6. $1^{2} \mathrm{C}$ Device Enable | 0x10 | $0 \times B 0$ |
| ALS Configuration | 1. ALS Current Control Enable <br> 2. ALS Input Enable <br> 3. ALS Input Select <br> 4. ALS Averaging Times | 0x20 | 0x2C |
| Brightness Ramp Rate | Programs the rate of rise and fall of the LED current | $0 \times 30$ | 0x00 |
| ALS Zone Information | 1. Zone Boundary Change Flag <br> 2. Zone Brightness Information | $0 \times 40$ | $0 \times 00$ |
| ALS Resistor Select | Internal ALS1 and ALS2 <br> Resistances | $0 \times 41$ | 0x00 |
| Brightness Control (BRT) | Holds the 7 bit Brightness Data | $0 \times A 0$ | 0x7F |
| Zone Boundary 0 (ZBO) | ALS Zone Boundary \#0 | 0x60 | 0x33 |
| Zone Boundary 1 (ZB1) | ALS Zone Boundary \#1 | $0 \times 61$ | $0 \times 66$ |
| Zone Boundary 2 (ZB2) | ALS Zone Boundary \#2 | $0 \times 62$ | 0x99 |
| Zone Boundary 3 (ZB3) | ALS Zone Boundary \#3 | $0 \times 63$ | 0xCC |
| Zone Target 0 (ZOT) | Zone 0 LED Current Data. The LED Current Source transitions to the brightness code in ZOT when the ALS_input is less than the zone boundary programmed in ZBO. | 0x70 | 0x19 |
| Zone Target 1 (Z1T) | Zone 1 LED Current Data. The LED Current Source transitions to the brightness code in Z1T when the ALS_ input is between the zone boundaries programmed in ZB1 and ZB0. | $0 \times 71$ | $0 \times 33$ |
| Zone Target 2 (Z2T) | Zone 2 LED Current Data. The LED Current Source transitions to the brightness code in Z2T when the ALS_ input is between the zone boundaries programmed in ZB2 and ZB1. | $0 \times 72$ | 0x4C |
| Zone Target 3 (Z3T) | Zone 3 LED Current Data. The LED Current Source transitions to the brightness code in Z3T when the ALS_ input is between the zone boundaries programmed in ZB3 and ZB2. | 0x73 | 0x66 |
| Zone Target 4 (Z4T) | Zone 4 LED Current Data. The LED Current Source transitions to the brightness code in $\mathrm{Z4T}$ when the ALS_ input is between the zone boundaries programmed in ZB4 and ZB3. | 0x74 | 0x7F |

*Note: Unused bits in the LM3530 Registers default to a logic '1'.

### 8.6.1.1 General Configuration Register (GP)

The General Configuration Register (address 0x10) is described in Figure 41 and Table 5.


Figure 41. General Configuration Register
Table 5. General Configuration Register Description (0x10)

| Bit 7 <br> (PWM Simple Enable | Bit 6 (PWM Polarity) | Bit 5 (EN_PWM) see Figure 31 | Bit 4 (Full-Scale Current Select) | Bit 3 (Full-Scale Current Select) | Bit 2 (Full-Scale Current Select) | Bit 1 <br> (Mapping Mode Select) | Bit 0 ( $I^{2} \mathrm{C}$ Device Enable) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 = Simple Interface at PWM Input is Disabled 1 = Simple Interface at PWM Input is Enabled | $0=$ PWM active high 1 = PWM active Iow | 0 = LED current is not a function of PWM duty cycle 1 = LED current is a function of duty cycle | $000=5 \mathrm{~mA}$ full-scale current $001=8.5 \mathrm{~mA}$ full-scale current $010=12 \mathrm{~mA}$ full-scale current $011=15.5 \mathrm{~mA}$ full-scale current $100=19 \mathrm{~mA}$ full-scale current $101=22.5 \mathrm{~mA}$ full-scale current $110=26 \mathrm{~mA}$ full-scale current $111=29.5 \mathrm{~mA}$ full-scale current |  |  | $0=$ exponential mapping 1 = linear mapping | 0 = Device Disabled 1 = Device Enabled |

### 8.6.1.2 ALS Configuration Register

The ALS Configuration Register controls the Ambient Light Sensing input functions and is described in Figure 42 and Table 6.


Figure 42. ALS Configuration Register

Table 6. ALS Configuration Register Description (0x20)

| Bit 7 | Bit 6 Bit 5 <br> ALS Input ALS Input <br> Select Select | Bit 4 Bit 3 <br> ALS Enable ALS Enable | Bit 2 <br> ALS <br> Averaging Time | Bit 1 <br> ALS <br> Averaging Time | Bit 0 <br> ALS <br> Averaging Time |
| :---: | :---: | :---: | :---: | :---: | :---: |
| N/A | $00=$ The Average of ALS1 and ALS2 is used to control the LED brightness <br> $01=$ ALS1 is used to control the LED brightness <br> $10=$ ALS2 is used to control the LED brightness <br> $11=$ The ALS input with the highest voltage is used to control the LED brightness | 00 or $10=\mathrm{ALS}$ is disabled. The Brightness Register is used to determine the LED current. $01=$ ALS is enabled. The Brightness Register is used to determine the LED Current. $11=$ ALS inputs are enabled. Ambient light determines the LED current. | $\begin{aligned} & 000=32 \mathrm{~ms} \\ & 001=64 \mathrm{~ms} \\ & 010=128 \mathrm{~ms} \\ & 011=256 \mathrm{~ms} \\ & 100=512 \mathrm{~ms} \\ & 101=1024 \mathrm{~ms} \\ & 110=2048 \mathrm{~ms} \\ & 111=4096 \mathrm{~ms} \end{aligned}$ |  |  |

### 8.6.1.3 Brightness Ramp Rate Register

The Brightness Ramp Rate Register controls the rate of rise or fall of the LED current. Both the rising rate and falling rate are independently adjustable Figure 43 and Table 7 describe the bit settings.


Figure 43. Brightness Ramp Rate Register
Table 7. Brightness Ramp Rate Register Description (0x30)

| Bit 7 | Bit 6 | Bit 5 <br> (BRRI2) Bit 4 <br> (BRRI1) Bit 3 <br> (BRRIO) | Bit 2 (BRRD2) | Bit 1 (BRRD1) | Bit 0 (BRRD0) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| N/A | N/A | $000=8 \mu \mathrm{~s} / \mathrm{step}(1.106 \mathrm{~ms}$ from 0 to Full Scale) $001=1.024 \mathrm{~ms} / \mathrm{step}$ ( 130 ms from 0 to Full Scale) $010=2.048 \mathrm{~ms} / \mathrm{step}(260 \mathrm{~ms}$ from 0 to Full Scale) $011=4.096 \mathrm{~ms} / \mathrm{step}(520 \mathrm{~ms}$ from 0 to Full Scale) $100=8.192 \mathrm{~ms} / \mathrm{step}(1.04 \mathrm{~s}$ from 0 to Full Scale) $101=16.384 \mathrm{~ms} /$ step ( 2.08 s from 0 to Full Scale) $110=32.768 \mathrm{~ms} / \mathrm{step}(4.16 \mathrm{~s}$ from 0 to Full Scale) $111=65.538 \mathrm{~ms} / \mathrm{step}(8.32 \mathrm{~s}$ from 0 to Full Scale) | $000=8 \mu \mathrm{~s} / \mathrm{step}(1.106 \mathrm{~ms}$ from Full Scale to 0 ) <br> $001=1.024 \mathrm{~ms} /$ step ( 130 ms from Full Scale to 0 ) <br> $010=2.048 \mathrm{~ms} / \mathrm{step}(260 \mathrm{~ms}$ from Full Scale to 0) <br> $011=4.096 \mathrm{~ms} / \mathrm{step}(520 \mathrm{~ms}$ from Full Scale to 0) <br> $100=8.192 \mathrm{~ms} / \mathrm{step}(1.04 \mathrm{~s}$ from Full Scale to 0) <br> $101=16.384 \mathrm{~ms} /$ step $(2.08 \mathrm{~s}$ from Full Scale to 0$)$ <br> $110=32.768 \mathrm{~ms} / \mathrm{step}(4.16 \mathrm{~s}$ from Full Scale to 0$)$ <br> $111=65.538 \mathrm{~ms} /$ step $(8.32 \mathrm{~s}$ from Full Scale to 0 ) |  |  |

### 8.6.1.4 ALS Zone Information Register

The ALS Zone Information Register is a read-only register that is updated every time the active ALS input(s) detect that the ambient light has changed to a new zone as programmed in the Zone Boundary Registers. See Zone Boundary Register description. A new update to the ALS Zone Information Register is signaled by the INT output going from high to low. A read-back of the ALS Zone Information Register will cause the INT output to go open-drain again. The Zone Change Flag (bit 3) is also updated on a Zone change and cleared on a read back of the ALS Zone Information Register. Figure 44 and Table 8 detail the ALS Zone Information Register.


Figure 44. ALS Zone Information Register
Table 8. ALS Zone Information Register Description (0x40)

| Bit 7 | Bit 6 | Bit 5 | Bit 4 | Bit 3 <br> (Zone Boundary Change Flag) | Bit 2 <br> (Z2) | Bit 1 <br> (Z1) | Bit 0 <br> (ZO) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N/A | N/A | N/A | N/A | 1 = the active ALS input has changed to a new ambient light zone as programmed in the Zone Boundary Registers (ZB0 -ZB3) <br> $0=$ no zone change | $\begin{aligned} & 000=\text { Zone } 0 \\ & 001=\text { Zone } 1 \\ & 010=\text { Zone } 2 \\ & 011=\text { Zone } 3 \\ & 100=\text { Zone } 4 \end{aligned}$ |  |  |

### 8.6.1.5 ALS Resistor Select Register

The ALS Resistor Select Register configures the internal resistance from either the ALS1 or ALS2 input to GND. Bits [3:0] program the input resistance at the ALS1 input and bits [7:4] program the input resistance at the ALS2 input. With bits [3:0] set to all zeroes the ALS1 input is high impedance. With bits [7:4] set to all zeroes the ALS2 input is high impedance.


Figure 45. ALS Resistor Select Register

Table 9. ALS Resistor Select Register Description (0x41)

| Bit 7 <br> (ALSR2A) | $\begin{gathered} \text { Bit } 6 \\ \text { (ALSR2B) } \end{gathered}$ | $\begin{gathered} \text { Bit } 5 \\ \text { (ALSR2C) } \end{gathered}$ | Bit 4 (ALSR2D) | $\begin{gathered} \text { Bit } 3 \\ \text { (ALSR1A) } \end{gathered}$ | Bit 2 <br> (ALSR1B) | Bit 1 (ALSR1C) | Bit 0 (ALSR1D) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0000=$ ALS2 is high impedance |  |  |  | $0000=$ ALS2 is high impedance |  |  |  |
| $0001=13.531 \mathrm{k} \Omega(73.9 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  | $0001=13.531 \mathrm{k} \Omega(73.9 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  |
| $0010=9.011 \mathrm{k} \Omega(111 \mu \mathrm{~A}$ at 1 V$)$$0011=5.4116 \mathrm{k} \Omega(185 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  | $0010=9.011 \mathrm{k} \Omega(111 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  |
|  |  |  |  | $0011=5.4116 \mathrm{k} \Omega(185 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  |
| $0011=5.4116 \mathrm{k} \Omega(185 \mu \mathrm{~A}$ at 1 V$)$$0100=2.271 \mathrm{k} \Omega(440 \mu \mathrm{at} 1 \mathrm{~V})$ |  |  |  | $0100=2.271 \mathrm{k} \Omega(440 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  |
| $0100=2.271 \mathrm{k} \Omega(440 \mu \mathrm{~A}$ at 1 V$)$$0101=1.946 \mathrm{k} \Omega(514 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  | $0101=1.946 \mathrm{k} \Omega(514 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  |
| $0101=1.946 \mathrm{k} \Omega(514 \mu \mathrm{~A}$ at 1 V$)$$0110=1.815 \mathrm{k} \Omega(551 \mu \mathrm{~A} 1 \mathrm{~V})$ |  |  |  | $0110=1.815 \mathrm{k} \Omega$ | at 1 V ) |  |  |
| $0111=1.6 \mathrm{k} \Omega(625 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  | $0111=1.6 \mathrm{k} \Omega(625 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  |
| $1000=1.138 \mathrm{k} \Omega(879 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  | $1000=1.138 \mathrm{k} \Omega(879 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  |
| $1001=1.05 \mathrm{k} \Omega(952 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  | $1001=1.05 \mathrm{k} \Omega(952 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  |
| $1010=1.011 \mathrm{k} \Omega(989 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  | $1010=1.011 \mathrm{k} \Omega(989 \mu \mathrm{~A}$ at 1 V$)$ |  |  |  |
| $1011=941 \Omega(1.063 \mathrm{~mA}$ at 1 V$)$ |  |  |  | $1011=941 \Omega(1.063 \mathrm{~mA}$ at 1 V$)$ |  |  |  |
| $1100=759 \Omega(1.318 \mathrm{~mA}$ at 1 V$)$$1101=719 \Omega(1.391 \mathrm{~mA}$ at 1 V$)$ |  |  |  | $1100=759 \Omega(1.318 \mathrm{~mA}$ at 1 V$)$ |  |  |  |
|  |  |  |  | $1101=719 \Omega(1.391 \mathrm{~mA}$ at 1 V$)$ |  |  |  |
| $\begin{aligned} & 1101=719 \Omega(1.391 \mathrm{~mA} \text { at } 1 \mathrm{~V}) \\ & 1110=700 \Omega(1.429 \mathrm{~mA} \text { at } 1 \mathrm{~V}) \end{aligned}$ |  |  |  | $1110=700 \Omega(1.429 \mathrm{~mA}$ at 1 V$)$ |  |  |  |
| $\begin{aligned} & 1110=700 \Omega(1.429 \mathrm{~mA} \text { at } 1 \mathrm{~V}) \\ & 1111=667 \Omega(1.499 \mathrm{~mA} \text { at } 1 \mathrm{~V}) \end{aligned}$ |  |  |  | $1111=667 \Omega(1.4$ | at 1 V ) |  |  |

### 8.6.1.6 Brightness Control Register

The Brightness Register (BRT) is an 8-bit register that programs the 127 different LED current levels (Bits [6:0]). The code written to BRT is translated into an LED current as a percentage of $\mathrm{I}_{\text {Led_fullscale }}$ as set via the FullScale Current Select bits (General Configuration Register bits [4:2]). The LED current response has a typical 1000:1 dimming ratio at the maximum full-scale current (General Configuration Register bits [4:2] $=(111$ ) and using the exponential weighted dimming curve.
There are two selectable LED current profiles. Setting the General Configuration Register bit 1 to 0 selects the exponentially weighted LED current response (see Figure 34). Setting this bit to '1' selects the linear weighted curve (see Figure 35). Table 2 and Table 3 show the percentage Full-Scale LED Current at a given Brightness Register Code for both the Exponential and Linear current response.


Figure 46. Brightness Control Register

Table 10. Brightness Control Register Description (0xA0)

| Bit 7 <br> N/A | $\begin{gathered} \text { Bit } 6 \\ \text { Data (MSB) } \end{gathered}$ | Bit 5 Data | Bit 4 Data | Bit 3 Data | Bit 2 <br> Data | Bit 1 Data | Bit 0 Data |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LED Brightness Data (Bits [6:0] |  |  |  |  |  |  |
|  | Exponential Mapping (see Table 2) Linear Mapping (see Table 3) <br> $0000000=$ LEDs Off  <br> $0000001=0.08 \%$ of Full Scale $0000000=$ LEDs Off <br> $\vdots$ $0000001=0.79 \%$ of Full Scale <br> $\vdots$ $\vdots$ <br> $1111111=100 \%$ of Full Scale $\vdots$ |  |  |  |  |  |  |

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### 8.6.1.7 Zone Boundary Register

The Zone Boundary Registers are programmed with the ambient light sensing zone boundaries. The default values are set at $20 \%(200 \mathrm{mV}$ ), $40 \%$ ( 400 mV ), $60 \%$ ( 600 mV ), and $80 \% ~(800 \mathrm{mV}$ ) of the full-scale ALS input voltage range (1V). The necessary conditions for proper ALS operation are that the data in ZB0 < data in ZB1 < data in ZB2 < data in ZB3.


Figure 47. Zone Boundary Registers

### 8.6.1.8 Zone Target Registers

The Zone Target Registers contain the LED brightness data that corresponds to the current active ALS zone. The default values for these registers and their corresponding percentage of full-scale current for both linear and exponential brightness is shown in Figure 48 and Table 11.


Figure 48. Zone Target Registers

Table 11. Zone Boundary and Zone Target Default Mapping

| ZONE BOUNDARY <br> (DEFAULT) | ZONE TARGET <br> REGISTER <br> (DEFAULT) | FULL-SCALE <br> CURRENT <br> (DEFAULT) | LINEAR MAPPING <br> (DEFAULT) | EXPONENTIAL <br> MAPPING <br> (DEFAULT) |
| :--- | :---: | :---: | :---: | :---: |
| Boundary 0, <br> Active ALS input is less than 200 mV | $0 \times 19$ | 19 mA | $19.69 \%(3.74 \mu \mathrm{~A})$ | $0.336 \%(68.4 \mu \mathrm{~A})$ |
| Boundary 1, <br> Active ALS input is between 200 mV and <br> 400 mV | $0 \times 33$ | 19 mA | $40.16 \%(7.63 \mu \mathrm{~A})$ | $1.43 \%(272 \mu \mathrm{~A})$ |
| Boundary 2, <br> Active ALS input is between 400 mV and <br> 600 mV | $0 \times 4 \mathrm{C}$ | 19 mA | $59.84 \%(11.37 \mathrm{~mA})$ | $5.78 \%(1.098 \mathrm{~mA})$ |
| Boundary 3, <br> Active ALS input is between 600 mV and <br> 800 mV | $0 \times 66$ | 19 mA | $80.31 \%(15.26 \mathrm{~mA})$ | $24.84 \%(4.72 \mathrm{~mA})$ |
| Boundary 4, <br> Active ALS input is greater than 800 mV | $0 \times 7 \mathrm{~F}$ | 19 mA | $100 \%(19 \mathrm{~mA})$ | $100 \%(19 \mathrm{~mA})$ |

## 9 Application and Implementation

## NOTE

Information in the following applications sections is not part of the Tl component specification, and TI does not warrant its accuracy or completeness. Tl's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 9.1 Application Information

The LM3530 incorporates a 40-V (maximum output) boost, a single current sink, and a dual ambient light sensor interface. The maximum boost output voltage is $40 \mathrm{~V}(\mathrm{~min})$ for the LM3530-40 version. The LM3530 boost will drive the output voltage to whatever voltage necessary to maintain 400 mV at the ILED input. The $40-\mathrm{V}$ max output typically allows the LM3530 to drive from 2 series up to 12 series LEDs ( 3.2 V max voltage per LED). For applications that do not use one or both of the ALS inputs, the ALS input can be connected to GND or left floating.

### 9.2 Typical Application



Figure 49. LM3530 Typical Application

### 9.2.1 Design Requirements

Example requirements for typical voltage inverter applications:
Table 12. Design Parameters

| DESIGN PARAMETER | EXAMPLE VALUE |
| :---: | :---: |
| Input voltage range | 2.7 V to 5.5 V |
| Output current | 0 mA to 30 mA |
| Boost switching frequency | 500 kHz |

Table 13. Application Circuit Component List

| COMPONENT | MANUFACTURER | PART NUMBER | VALUE | SIZE | CURRENT/VOLTAGE RATING |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L | TDK | VLF3014ST100MR82 | $10 \mu \mathrm{H}$ | $3 \mathrm{~mm} \times 3 \mathrm{~mm} \times 1.4 \mathrm{~mm}$ | $\mathrm{I}_{\text {SAT }}=820 \mathrm{~mA}$ |
| COUT | Murata | GRM21BR71H105KA12 | $1 \mu \mathrm{~F}$ | 0805 | 50 V |
| CIN | Murata | GRM188B31A225KE33 | $2.2 \mu \mathrm{~F}$ | 0603 | 10 V |
| D1 | Diodes Inc. | B0540WS | Schottky | SOD-323 | $40 \mathrm{~V} / 500 \mathrm{~mA}$ |
| ALS1 | Avago | APDS-9005 | Ambient Light Sensor | $1.6 \mathrm{~mm} \times 1.5 \mathrm{~mm} \times 0.6 \mathrm{~mm}$ | 0 to 1100 Lux |
| ALS2 | Avago | APDS-9005 | Ambient Light Sensor | $1.6 \mathrm{~mm} \times 1.5 \mathrm{~mm} \times 0.6 \mathrm{~mm}$ | 0 to 1100 Lux |

### 9.2.2 Detailed Design Procedure

### 9.2.2.1 LED Current Setting/Maximum LED Current

The maximum LED current is restricted by the following factors: the maximum duty cycle that the boost converter can achieve, the peak current limitations, and the maximum output voltage.

### 9.2.2.2 Maximum Duty Cycle

The LM3530 can achieve up to typically $94 \%$ maximum duty cycle. Two factors can cause the duty cycle to increase: an increase in the difference between $\mathrm{V}_{\text {OUT }}$ and $\mathrm{V}_{\mathbb{I N}}$ and a decrease in efficiency. This is shown by Equation 12:

$$
\begin{equation*}
\mathrm{D}=1-\frac{\mathrm{VIN} \times \eta}{\mathrm{VOUT}} \tag{12}
\end{equation*}
$$

For a 9-LED configuration $V_{\text {OUT }}=(3.6 \mathrm{~V} \times 9$ LED +VHR$)=33 \mathrm{~V}$ operating with $\eta=70 \%$ from a 3-V battery, the duty cycle requirement would be around $93.6 \%$. Lower efficiency or larger $\mathrm{V}_{\text {OUT }}$ to $\mathrm{V}_{\mathbb{I N}}$ differentials can push the duty cycle requirement beyond $94 \%$.

### 9.2.2.3 Peak Current Limit

The LM3530 boost converter has a peak current limit for the internal power switch of 839 mA typical ( 739 mA minimum). When the peak switch current reaches the current limit, the duty cycle is terminated resulting in a limit on the maximum output current and thus the maximum output power the LM3530 can deliver. Calculate the maximum LED current as a function of $\mathrm{V}_{\mathrm{IN}}, \mathrm{V}_{\text {OUT }}, \mathrm{L}$, efficiency $(\eta)$ and $\mathrm{I}_{\text {PEAK }}$ as:

$$
\begin{aligned}
& \mathrm{I}_{\text {OUT_MAX }}=\frac{\left(\mathrm{I}_{\text {PEAK }}-\Delta \mathrm{I}_{\mathrm{L}}\right) \times \eta \times \mathrm{V}_{\text {IN }}}{\mathrm{V}_{\text {OUT }}} \\
& \text { where } \Delta \mathrm{I}_{\mathrm{L}}=\frac{\mathrm{V}_{\mathrm{IN}} \times\left(\mathrm{V}_{\text {OUT }}-\mathrm{V}_{\text {IN }}\right)}{2 \times \mathrm{f}_{\mathrm{SW}} \times \mathrm{L} \times \mathrm{V}_{\text {OUT }}}
\end{aligned}
$$

where

- $f_{\text {sw }}=500 \mathrm{kHz}$
- $\eta$ and $I_{\text {PEAK }}$ can be found in the Efficiency and $I_{\text {PEAK }}$ curves in the Specifications and Application Curves.


### 9.2.2.4 Output Voltage Limitations

The LM3530 has a maximum output voltage of 41 V typical ( 40 V minimum) for the LM3530-40 version and 24 V typical ( 23.6 V minimum) for the LM3530-25 version. When the output voltage rises above this threshold ( $\mathrm{V}_{\text {ovp }}$ ) the overvoltage protection feature is activated and the duty cycle is terminated. Switching will cease until $\mathrm{V}_{\text {OUT }}$ drops below the hysteresis level (typically 1 V below $\mathrm{V}_{\text {ovp }}$ ). For larger numbers of series connected LEDs the output voltage can reach the OVP threshold at larger LED currents and colder ambient temperatures. Typically white LEDs have a $-3 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ temperature coefficient.

### 9.2.2.5 Output Capacitor Selection

The LM3530's output capacitor has two functions: filtering of the boost converters switching ripple, and to ensure feedback loop stability. As a filter, the output capacitor supplies the LED current during the boost converters on time and absorbs inductor energy during the switch off time. This causes a sag in the output voltage during the on time and a rise in the output voltage during the off time. Because of this, the output capacitor must be sized large enough to filter the inductor current ripple that could cause the output voltage ripple to become excessive. As a feedback loop component, the output capacitor must be at least $1 \mu \mathrm{~F}$ and have low ESR otherwise the LM3530 boost converter can become unstable. This requires the use of ceramic output capacitors. Table 14 lists part numbers and voltage ratings for different output capacitors that can be used with the LM3530.

Table 14. Recommended Input/Output Capacitors

| MANUFACTURER | PART NUMBER | VALUE $(\boldsymbol{\mu F})$ | SIZE | RATING $(\mathbf{V})$ | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Murata | GRM21BR71H105KA12 | 1 | 0805 | 50 | COUT |
| Murata | GRM188B31A225KE33 | 2.2 | 0805 | 10 | CIN |
| TDK | C1608X5R0J225 | 2.2 | 0603 | 6.3 | CIN |

### 9.2.2.6 Inductor Selection

The LM3530 is designed to work with a $10-\mu \mathrm{H}$ to $22-\mu \mathrm{H}$ inductor. When selecting the inductor, ensure that the saturation rating for the inductor is high enough to accommodate the peak inductor current. Equation 14 and Equation 15 calculate the peak inductor current based upon LED current, $\mathrm{V}_{\mathbb{I N}_{N}}, \mathrm{~V}_{\mathrm{OUT}}$, and efficiency.

$$
\begin{equation*}
I_{\text {PEAK }}=\frac{I_{\text {LED }}}{\eta} \times \frac{V_{\text {OUT }}}{V_{\text {IN }}}+\Delta I_{\text {L }} \tag{14}
\end{equation*}
$$

where:

$$
\begin{equation*}
\Delta \mathrm{L}_{\mathrm{L}}=\frac{\mathrm{V}_{\text {IN }} \times\left(\mathrm{V}_{\text {OUT }}-\mathrm{V}_{\text {IN }}\right)}{2 \times f_{\text {SW }} \times \mathrm{L} \times \mathrm{V}_{\text {OUT }}} \tag{15}
\end{equation*}
$$

When choosing L , the inductance value must also be large enough so that the peak inductor current is kept below the LM3530 switch current limit. This forces a lower limit on $L$ given by Equation 16.

$$
\begin{equation*}
L>\frac{V_{\text {IN }} \times\left(V_{\text {OUT }}-V_{\text {IN }}\right)}{2 \times f_{\text {SW }} \times V_{\text {OUT }} \times\left(I_{\text {SW_MAX }}-\frac{\mathrm{I}_{\text {LED_MAX }} \times V_{\text {OUT }}}{\eta \times V_{\text {IN }}}\right)} \tag{16}
\end{equation*}
$$

$I_{\text {sw_max }}$ is given in , efficiency $(\eta)$ is shown in the Application Curves, and $f_{\text {sw }}$ is typically 500 kHz .
Table 15. Suggested Inductors

| MANUFACTURER | PART NUMBER | $\begin{aligned} & \text { VALUE } \\ & (\mu \mathrm{H}) \end{aligned}$ | SIZE (mm) | RATING (mA) | DC RESISTANCE ( $\Omega$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| TDK | VLF3014ST-100MR82 | 10 | $2.8 \times 3 \times 1.4$ | 820 | 0.25 |
| TDK | VLF3010ST-220MR34 | 22 | $2.8 \times 3 \times 1$ | 340 | 0.81 |
| TDK | VLF3010ST-100MR53 | 10 | $2.8 \times 3 \times 1$ | 530 | 0.41 |
| TDK | VLF4010ST-100MR80 | 10 | $2.8 \times 3 \times 1$ | 800 | 0.25 |
| TDK | VLS252010T-100M | 10 | $2.5 \times 2 \times 1$ | 650 | 0.71 |
| Coilcraft | LPS3008-103ML | 10 | $2.95 \times 2.95 \times 0.8$ | 520 | 0.65 |
| Coilcraft | LPS3008-223ML | 22 | $2.95 \times 2.95 \times 0.8$ | 340 | 1.5 |
| Coilcraft | LPS3010-103ML | 10 | $2.95 \times 2.95 \times 0.9$ | 550 | 0.54 |
| Coilcraft | LPS3010-223ML | 22 | $2.95 \times 2.95 \times 0.9$ | 360 | 1.2 |
| Coilcraft | XPL2010-103ML | 10 | $1.9 \times 2 \times 1$ | 610 | 0.56 |
| Coilcraft | EPL2010-103ML | 10 | $2 \times 2 \times 1$ | 470 | 0.91 |
| TOKO | DE2810C-1117AS-100M | 10 | $3 \times 3.2 \times 1$ | 600 | 0.46 |

### 9.2.2.7 Diode Selection

The diode connected between SW and OUT must be a Schottky diode and have a reverse breakdown voltage high enough to handle the maximum output voltage in the application. Table 16 lists various diodes that can be used with the LM3530. For 25-V OVP devices a $30-\mathrm{V}$ Schottky is adequate. For $40-\mathrm{V}$ OVP devices, a $40-\mathrm{V}$ Schottky diode should be used.

Table 16. Suggested Diodes

| MANUFACTURER | PART NUMBER | VALUE | SIZE (mm) | RATING |
| :---: | :---: | :---: | :---: | :---: |
| Diodes Inc | B0540WS | Schottky | SOD-323 $(1.7 \times 1.3)$ | $40 \mathrm{~V} / 500 \mathrm{~mA}$ |
| Diodes Inc | SDM20U40 | Schottky | SOD-523 $(1.2 \times 0.8 \times 0.6)$ | $40 \mathrm{~V} / 200 \mathrm{~mA}$ |
| On Semiconductor | NSR0340V2T1G | Schottky | SOD-523 $(1.2 \times 0.8 \times 0.6)$ | $40 \mathrm{~V} / 250 \mathrm{~mA}$ |
| On Semiconductor | NSR0240V2T1G | Schottky | SOD-523 $(1.2 \times 0.8 \times 0.6)$ | $40 \mathrm{~V} / 250 \mathrm{~mA}$ |

### 9.2.3 Application Curves


$I_{\text {FULL_SCALE }}=19 \mathrm{~mA}$

Figure 50. Efficiency vs $\mathrm{V}_{\mathrm{IN}}$

$I_{\text {FULL_SCALE }}=19 \mathrm{~mA}$

Figure 52. Efficiency vs $\mathrm{V}_{\mathrm{IN}}$


Figure 54. Efficiency vs $\mathrm{I}_{\text {LED }}$

$I_{\text {FULL_SCALE }}=19 \mathrm{~mA}$

Figure 51. Efficiency vs $\mathrm{V}_{\mathrm{IN}}$


Figure 53. Efficiency vs $\mathrm{I}_{\text {LED }}$


Figure 55. Efficiency vs $\mathrm{I}_{\text {LED }}$

## 10 Power Supply Recommendations

The LM3530 operates from a $2.7-\mathrm{V}$ to $5.5-\mathrm{V}$ input voltage. The $500-\mathrm{kHz}$ switching frequency for the boost can lead to ripple voltage on the input voltage rail. To minimize this, the input to the inductor should be well bypassed with a $1-\mu \mathrm{F}$ ( min ) ceramic bypass capacitor (see Output Capacitor Selection).

## 11 Layout

### 11.1 Layout Guidelines

The LM3530 contains an inductive boost converter which detects a high switched voltage (up to 40 V ) at the SW pin, and a step current (up to 900 mA ) through the Schottky diode and output capacitor each switching cycle. The high switching voltage can create interference into nearby nodes due to electric field coupling ( $\mathrm{I}=\mathrm{CdV} / \mathrm{dt}$ ). The large step current through the diode and the output capacitor can cause a large voltage spike at the SW pin and the OVP pin due to parasitic inductance in the step current conducting path ( $\mathrm{V}=\mathrm{Ldi} / \mathrm{dt}$ ). Board layout guidelines are geared towards minimizing this electric field coupling and conducted noise. Figure 56 highlights these two noise generating components.


Figure 56. LM3530 Boost Converter Showing Pulsed Voltage At SW (High Dv/Dt) and Current Through Schottky and Cout (High Di/Dt)

## Layout Guidelines (continued)

The following lists the main (layout sensitive) areas of the LM3530 in order of decreasing importance:

- Output Capacitor
- Schottky Cathode to Cout+
- Cout to GND
- Schottky Diode
- SW Pin to Schottky Anode
- Schottky Cathode to Cout+
- Inductor
- SW Node PCB capacitance to other traces
- Input Capacitor
- $\mathrm{C}_{\mathrm{IN}^{+}}$to IN pin
- $\mathrm{C}_{\mathrm{IN}^{-}}$to GND


### 11.1.1 Output Capacitor Placement

The output capacitor is in the path of the inductor current discharge path. As a result $\mathrm{C}_{\text {OUt }}$ detects a high current step from 0 to $\mathrm{I}_{\text {PEAK }}$ each time the switch turns off and the Schottky diode turns on. Any inductance along this series path from the cathode of the diode through $\mathrm{C}_{\text {out }}$ and back into the LM3530 GND pin will contribute to voltage spikes $\left(V_{\text {SPIKE }}=L_{p} \times d / / d t\right)$ at SW and OUT which can potentially overvoltage the SW pin, or feed through to GND. To avoid this, Cout+ must be connected as close as possible to the Cathode of the Schottky diode and $\mathrm{C}_{\text {OUT }}$ must be connected as close as possible to the device GND bump. The best placement for $\mathrm{C}_{\text {OUt }}$ is on the same layer as the LM3530 so as to avoid any vias that can add excessive series inductance (see Figure 58, Figure 59, and Figure 60).

### 11.1.2 Schottky Diode Placement

The Schottky diode is in the path of the inductor current discharge. As a result the Schottky diode detects a high current step from 0 to $I_{\text {PEAK }}$ each time the switch turns off and the diode turns on. Any inductance in series with the diode will cause a voltage spike ( $\mathrm{V}_{\text {SPIKE }}=\mathrm{L}_{\mathrm{P}_{-}} \times \mathrm{dl} / \mathrm{dt}$ ) at SW and OUT which can potentially overvoltage the SW pin, or feed through to $\mathrm{V}_{\text {OUT }}$ and through the output capacitor and into GND. Connecting the anode of the diode as close as possible to the SW pin and the cathode of the diode as close as possible to $\mathrm{C}_{\text {out }}$ will reduce the inductance ( $L_{P_{-}}$) and minimize these voltage spikes (see Figure 58, Figure 59, and Figure 60 ).

### 11.1.3 Inductor Placement

The node where the inductor connects to the LM3530 SW bump has 2 issues. First, a large switched voltage ( 0 to $\mathrm{V}_{\text {OUT }}+\mathrm{V}_{\text {F_SchотtкY }}$ ) appears on this node every switching cycle. This switched voltage can be capacitively coupled into nearby nodes. Second, there is a relatively large current (input current) on the traces connecting the input supply to the inductor and connecting the inductor to the SW bump. Any resistance in this path can cause large voltage drops that will negatively affect efficiency.
To reduce the capacitively coupled signal from SW into nearby traces, the SW bump to inductor connection must be minimized in area. This limits the PCB capacitance from SW to other traces. Additionally, the other traces need to be routed away from SW and not directly beneath. This is especially true for high impedance nodes that are more susceptible to capacitive coupling such as (SCL, SDA, HWEN, PWM, and possibly ASL1 and ALS2). A GND plane placed directly below SW will dramatically reduce the capacitive coupling from SW into nearby traces
To limit the trace resistance of the VBATT to inductor connection and from the inductor to SW connection, use short, wide traces (see Figure 58, Figure 59, and Figure 60).

### 11.1.4 Input Capacitor Selection and Placement

The input bypass capacitor filters the inductor current ripple, and the internal MOSFET driver currents during turn on of the power switch.

## Layout Guidelines (continued)

The driver current requirement can range from 50 mA at 2.7 V to over 200 mA at 5.5 V with fast durations of approximately 10 ns to 20 ns . This will appear as high di/dt current pulses coming from the input capacitor each time the switch turns on. Close placement of the input capacitor to the IN pin and to the GND pin is critical since any series inductance between $\mathbb{I N}$ and $\mathrm{C}_{\mathbb{N}^{+}}$or $\mathrm{C}_{\mathbb{N}^{-}}$and GND can create voltage spikes that could appear on the $\mathrm{V}_{\mathrm{IN}}$ supply line and in the GND plane.

Close placement of the input bypass capacitor at the input side of the inductor is also critical. The source impedance (inductance and resistance) from the input supply, along with the input capacitor of the LM3530, form a series RLC circuit. If the output resistance from the source $\left(R_{S}\right)$ is low enough the circuit will be underdamped and will have a resonant frequency (typically the case). Depending on the size of $L_{s}$ the resonant frequency could occur below, close to, or above switching frequency of the device. This can cause the supply current ripple to be:

1. Approximately equal to the inductor current ripple when the resonant frequency occurs well above the LM3530 switching frequency;
2. Greater then the inductor current ripple when the resonant frequency occurs near the switching frequency; and
3. Less then the inductor current ripple when the resonant frequency occurs well below the switching frequency.

Figure 57 shows the series RLC circuit formed from the output impedance of the supply and the input capacitor. The circuit is re-drawn for the AC case where the $\mathrm{V}_{\text {IN }}$ supply is replaced with a short to GND and the LM3530 + Inductor is replaced with a current source ( $\Delta \mathrm{I}_{\mathrm{L}}$ ). In Figure 57 below,

1. = the criteria for an underdamped response.
2. = the resonant frequency, and
3. = the approximated supply current ripple as a function of $\mathrm{L}_{\mathrm{s}}, \mathrm{R}_{\mathrm{S}}$, and $\mathrm{C}_{\mathbb{N}}$.

As an example, consider a $3.6-\mathrm{V}$ supply with $0.1-\Omega$ of series resistance connected to $\mathrm{C}_{\mathbb{N}}$ through 50 nH of connecting traces. This results in an underdamped input filter circuit with a resonant frequency of 712 kHz . Since the switching frequency lies near to the resonant frequency of the input RLC network, the supply current is probably larger then the inductor current ripple. In this case using Equation 2 from Figure 57 the supply current ripple can be approximated as 1.68 multiplied by the inductor current ripple. Increasing the series inductance ( $L_{\mathrm{S}}$ ) to 500 nH causes the resonant frequency to move to around 225 kHz and the supple current ripple to be approximately 0.25 multiplied by the inductor current ripple.

## Layout Guidelines (continued)



1. $\frac{1}{\mathrm{~L}_{\mathrm{S}} \times \mathrm{C}_{\mathrm{IN}}}>\frac{\mathrm{R}_{\mathrm{S}}{ }^{2}}{4 \times \mathrm{L}_{\mathrm{S}}^{2}}$
2. $\quad f_{\text {RESONANT }}=\frac{1}{2 \pi \sqrt{L_{S} \times C_{I N}}}$
3. $I_{\text {SUPPLYRIPPLE }} \approx \Delta I_{L} \times \frac{\frac{1}{2 \pi \times 500 \mathrm{kHz} \mathrm{\times C}_{\text {IN }}}}{\sqrt{R_{S}{ }^{2}+\left(2 \pi \times 500 \mathrm{kHz} \times \mathrm{L}_{\mathrm{S}}-\frac{1}{\left.2 \pi \times 500 \mathrm{kHz} \mathrm{\times C}_{\text {IN }}\right)^{2}}\right.}}$

Figure 57. Input RLC Network

### 11.2 Layout Example

Figure 58, Figure 59, and Figure 60 show example layouts which apply the required proper layout guidelines. These figures should be used as guides for laying out the LM3530 circuit.


Figure 58. Layout Example 1

## Layout Example (continued)



Figure 59. Layout Example 2


Figure 60. Layout Example 3

## 12 Device and Documentation Support

### 12.1 Device Support

### 12.1.1 Third-Party Products Disclaimer

TI'S PUBLICATION OF INFORMATION REGARDING THIRD-PARTY PRODUCTS OR SERVICES DOES NOT CONSTITUTE AN ENDORSEMENT REGARDING THE SUITABILITY OF SUCH PRODUCTS OR SERVICES OR A WARRANTY, REPRESENTATION OR ENDORSEMENT OF SUCH PRODUCTS OR SERVICES, EITHER ALONE OR IN COMBINATION WITH ANY TI PRODUCT OR SERVICE.

### 12.2 Documentation Support

### 12.2.1 Related Documentation

For related documentation, see the following:
Texas Instruments Application Note 1112: DSBGA Wafer Level Chip Scale Package (SNVA009).

### 12.3 Trademarks

All trademarks are the property of their respective owners.

### 12.4 Electrostatic Discharge Caution

This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

### 12.5 Glossary

SLYZ022 - TI Glossary.
This glossary lists and explains terms, acronyms, and definitions.

## 13 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

## PACKAGING INFORMATION

| Orderable Device | Status <br> (1) | Package Type | Package Drawing | Pins | Package Qty | Eco Plan <br> (2) | Lead finish/ Ball material (6) | MSL Peak Temp <br> (3) | Op Temp ( ${ }^{\circ} \mathrm{C}$ ) | Device Marking <br> (4/5) | Samples |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LM3530TME-40/NOPB | ACTIVE | DSBGA | YFQ | 12 | 250 | RoHS \& Green | SNAGCU | Level-1-260C-UNLIM |  | DX | Samples |
| LM3530TMX-40/NOPB | ACTIVE | DSBGA | YFQ | 12 | 3000 | RoHS \& Green | SNAGCU | Level-1-260C-UNLIM |  | DX | Samples |
| LM3530UME-25A/NOPB | ACTIVE | DSBGA | YFZ | 12 | 250 | RoHS \& Green | SNAGCU | Level-1-260C-UNLIM | -30 to 85 | DS | Samples |
| LM3530UME-40/NOPB | ACTIVE | DSBGA | YFZ | 12 | 250 | RoHS \& Green | SNAGCU | Level-1-260C-UNLIM | -30 to 85 | 40 | Samples |
| LM3530UME-40B/NOPB | ACTIVE | DSBGA | YFZ | 12 | 250 | RoHS \& Green | SNAGCU | Level-1-260C-UNLIM |  | DT | Samples |
| LM3530UMX-25A/NOPB | ACTIVE | DSBGA | YFZ | 12 | 3000 | RoHS \& Green | SNAGCU | Level-1-260C-UNLIM | -30 to 85 | DS | Samples |
| LM3530UMX-40/NOPB | ACTIVE | DSBGA | YFZ | 12 | 3000 | RoHS \& Green | SNAGCU | Level-1-260C-UNLIM | -30 to 85 | 40 | Samples |
| LM3530UMX-40B/NOPB | ACTIVE | DSBGA | YFZ | 12 | 3000 | RoHS \& Green | SNAGCU | Level-1-260C-UNLIM |  | DT | Samples |

${ }^{(1)}$ The marketing status values are defined as follows:
ACTIVE: Product device recommended for new designs.
LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.
NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.
PREVIEW: Device has been announced but is not in production. Samples may or may not be available.
OBSOLETE: TI has discontinued the production of the device.
${ }^{(2)}$ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed $0.1 \%$ by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".
RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.
Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.
${ }^{(3)}$ MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
${ }^{(4)}$ There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device
${ }^{(5)}$ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
${ }^{(6)}$ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annul basis.

## TAPE AND REEL INFORMATION



TAPE DIMENSIONS


| A0 | Dimension designed to accommodate the component width |
| :---: | :--- |
| B0 | Dimension designed to accommodate the component length |
| K0 | Dimension designed to accommodate the component thickness |
| W | Overall width of the carrier tape |
| P1 | Pitch between successive cavity centers |

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

*All dimensions are nominal

| Device | Package <br> Type | Package <br> Drawing | Pins | SPQ | Reel <br> Diameter <br> $(\mathbf{m m})$ | Reel <br> Width <br> W1 $(\mathbf{m m})$ | A0 <br> $(\mathbf{m m})$ | B0 <br> $(\mathbf{m m})$ | K0 <br> $(\mathbf{m m})$ | P1 <br> $(\mathbf{m m})$ | W <br> $(\mathbf{m m})$ | Pin1 <br> Quadrant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LM3530TME-40/NOPB | DSBGA | YFQ | 12 | 250 | 178.0 | 8.4 | 1.35 | 1.75 | 0.76 | 4.0 | 8.0 | Q1 |
| LM3530TMX-40/NOPB | DSBGA | YFQ | 12 | 3000 | 178.0 | 8.4 | 1.35 | 1.75 | 0.76 | 4.0 | 8.0 | Q1 |
| LM3530UME-25A/NOPB | DSBGA | YFZ | 12 | 250 | 178.0 | 8.4 | 1.37 | 1.77 | 0.56 | 4.0 | 8.0 | Q1 |
| LM3530UME-40/NOPB | DSBGA | YFZ | 12 | 250 | 178.0 | 8.4 | 1.37 | 1.77 | 0.56 | 4.0 | 8.0 | Q1 |
| LM3530UME-40B/NOPB | DSBGA | YFZ | 12 | 250 | 178.0 | 8.4 | 1.37 | 1.77 | 0.56 | 4.0 | 8.0 | Q1 |
| LM3530UMX-25A/NOPB | DSBGA | YFZ | 12 | 3000 | 178.0 | 8.4 | 1.37 | 1.77 | 0.56 | 4.0 | 8.0 | Q1 |
| LM3530UMX-40/NOPB | DSBGA | YFZ | 12 | 3000 | 178.0 | 8.4 | 1.37 | 1.77 | 0.56 | 4.0 | 8.0 | Q1 |
| LM3530UMX-40B/NOPB | DSBGA | YFZ | 12 | 3000 | 178.0 | 8.4 | 1.37 | 1.77 | 0.56 | 4.0 | 8.0 | Q1 |


*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Length (mm) | Width (mm) | Height (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LM3530TME-40/NOPB | DSBGA | YFQ | 12 | 250 | 208.0 | 191.0 | 35.0 |
| LM3530TMX-40/NOPB | DSBGA | YFQ | 12 | 3000 | 208.0 | 191.0 | 35.0 |
| LM3530UME-25A/NOPB | DSBGA | YFZ | 12 | 250 | 208.0 | 191.0 | 35.0 |
| LM3530UME-40/NOPB | DSBGA | YFZ | 12 | 250 | 208.0 | 191.0 | 35.0 |
| LM3530UME-40B/NOPB | DSBGA | YFZ | 12 | 250 | 208.0 | 191.0 | 35.0 |
| LM3530UMX-25A/NOPB | DSBGA | YFZ | 12 | 3000 | 208.0 | 191.0 | 35.0 |
| LM3530UMX-40/NOPB | DSBGA | YFZ | 12 | 3000 | 208.0 | 191.0 | 35.0 |
| LM3530UMX-40B/NOPB | DSBGA | YFZ | 12 | 3000 | 208.0 | 191.0 | 35.0 |



NOTES: A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
B. This drawing is subject to change without notice.


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B. This drawing is subject to change without notice.

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