

LP8864S-Q1

ZHCSLM4A – AUGUST 2020 – REVISED FEBRUARY 2021

具有四个 **150mA** 通道的 **LP8864S-Q1** 汽车显示 **LED** 背光驱动器

1 特性

73 TEXAS

- 符合面向汽车应用的 AEC-Q100 标准:
	- 器件温度等级 1:

INSTRUMENTS

- -40° C $\overline{\oplus}$ +125 $^{\circ}$ C , T_A
- 器件 HBM ESD 分类等级 2
- 器件 CDM ESD 分类等级 C4B
- 输入电压工作范围 : 3V 至 48V
- 四路高精度电流阱
	- 各电流阱直流电流高达 150mA
	- 电流匹配度为 1%(典型值)
	- 使用 152Hz LED 输出 PWM 频率时,调光比为 32000:1
	- 使用 I2C 或 PWM 输入时,最高 16 位 LED 调 光分辨率
	- 可配置 8 个 LED 灯串
- 自动移相 PWM 调光
- 12 位模拟调光
- 最高 48V V_{OUT} 升压或 SEPIC 直流/直流控制器
	- 开关频率为 100kHz 至 2.2MHz
	- 升压扩频功能可降低 EMI
	- 升压同步输入,可通过外部时钟设置升压开关频 率
	- 禁用升压时,输出电压自动放电
- 多种故障诊断功能

2 应用

- 为以下应用提供背光:
	- 汽车信息娱乐系统
	- 汽车仪表组
	- 智能车镜
	- 抬头显示屏 (HUD)

3 说明

LP8864S-Q1 是一款具有升压控制器的汽车类高效 LED 驱动器。四路高精度电流阱支持根据使用的通道 数自动调整相移。可通过 I²C 接口或 PWM 输入对 LED 亮度进行全局控制。

升压控制器具有基于 LED 电流阱余量电压的自适应输 出电压控制。该特性可在所有条件下将升压电压调节到 能够满足需要的最低水平,从而更大限度降低功耗。凭 借宽范围可调频率,LP8864S-Q1 可避免 AM 无线电 频段的干扰。

LP8864S-Q1 支持内置混合 PWM 调光和模拟电流调 光,从而可降低 EMI、延长 LED 使用寿命并提高总光 学效率。

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器件型号(1)	封装	封装尺寸(标称值
LP8864S-Q1	HTSSOP (38)	9.70 mm × 4.40mm
	QFN (32) ⁽²⁾	$5mm \times 5mm$

- (1) 如需了解所有可用封装,请参阅数据表末尾的可订购产品附 录。
- (2) 产品预览。

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注:以前版本的页码可能与当前版本的页码不同

5 Pin Configuration and Functions

图 **5-1. DCP Package 38-Pin HTSSOP Top View**

Product preview

表 **5-1. HTTSOP Pin Functions**

表 **5-2. QFN Pin Functions**

6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)⁽¹⁾ (2)

(1) Stresses beyond those listed under *Absolute Maximum Rating* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Condition*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) All voltages are with respect to the potential at the GND pins.

(3) Internal thermal shutdown circuitry protects the device from permanent damage. Thermal shutdown engages at T $_{\rm J}$ = 165°C (typical) and disengages at T_J = 150°C (typical).

(4) In applications where high power dissipation and/or poor package thermal resistance is present, the maximum ambient temperature may have to be derated. Maximum ambient temperature (T $_{\rm A\text{-}MAX}$) is dependent on the maximum operating junction temperature $(T_{J\text{-MAX}}$ = 150°C), the power dissipation of the device in the application (P), the junction-to-board thermal resistance and the temperature difference between the system board and the ambient (Δt_{BA}), which is given by the following equation: T_{A-MAX} = T_{J-MAX} - $(\Theta_{JB} \times P) - \Delta t_{BA}$.

6.2 ESD Ratings

(1) AEC Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specification.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted) (1)

(1) All voltages are with respect to the potential at the GND pins.

6.4 Thermal Information

(1) For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.

(2) Junction-to-ambient thermal resistance is highly application and board-layout dependent. In applications where high maximum power dissipation exists, special care must be paid to thermal dissipation issues in board design.

6.5 Electrical Characteristics

Limits apply over the full operation temperature range -40°C \leq T_A \leq +125°C, unless otherwise speicified. V_{IN} = 12 V_, VDD = 3.3 V

6.5 Electrical Characteristics (continued)

Limits apply over the full operation temperature range -40°C \leq T_A \leq +125°C, unless otherwise speicified. V_{IN} = 12 V_, VDD $= 3.3 V$

6.5 Electrical Characteristics (continued)

Limits apply over the full operation temperature range $-40^{\circ}C \leq T_A \leq +125^{\circ}C$, unless otherwise speicified. V_{IN} = 12 V_, VDD $= 3.3 V$

(1) This specification is not ensured by ATE.

6.6 Logic Interface Characteristics

Limits apply over the full operation temperature range -40° C \leq T_A \leq +125°C , unless otherwise speicified. V_{IN} = 12 V_, VDD $= 5 V, V_{EN} = 3.3 V$

6.7 Timing Requirements for I2C Interface

Limits apply over the full operation temperature range -40° C \leq T_A \leq +125°C, unless otherwise speicified. V_{IN} = 12 V, VDD $= 5 V, V_{EN} = 3.3 V.$

图 **6-1. I2C Timing Diagram**

6.8 Typical Characteristics

Unless otherwise specified: $C_{IN} = C_{OUT} = 2 \times 10$ - μ F ceramic and 2 × 33- μ F electrolytic, $V_{DD} = 3.3$ V, charge pump enabled, $T_A = 25^{\circ}$ C

7 Detailed Description

7.1 Overview

The LP8864S-Q1 device is a high-voltage LED driver for automotive infotainment, clusters, HUD and other automotive display LED backlight applications. PWM input is used for brightness control by default. Alternatively, the brightness can also be controlled by I2C Interface.

The boost frequency, LED PWM frequency, and LED string current are configured with external resistors through the BST_FSET, PWM_FSET, and ISET pins. The INT pin is used to report faults to the system. Fault interrupt status can be cleared with the I2C interface, or is cleared on the falling edge of the EN pin.

The LP8864S-Q1 supports pure PWM dimming. The six LED current drivers provide up to 150 mA per output and can be tied together to support higher current LEDs. The maximum output current of the LED drivers is set with the ISET resistor and can be optionally scaled by the LEDx_CURRENT[11:0] register bits with I2C interface. The LED output PWM frequency is set with a PWM_FSET resistor. The number of connected LED strings is configured by the LED SET resistor, and the device automatically selects the corresponding phase shift mode. For example, if the device is set to 4-strings mode, each LED output is phase shifted by 90 degrees with each other(= 360 / 4). Unused outputs, which must be connected to GND, will be disabled and excluded from adaptive voltage and won't generate any LED faults.

A resistor divider connected from V_{OUT} to the FB pin sets the maximum voltage of the boost. For best efficiency, the boost voltage is adapted automatically to the minimum necessary level needed to drive the LED strings by monitoring all the LED output voltages continuously. The switching frequency of the boost regulator can be set between 100 kHz and 2.2 MHz by the BST_FSET resistor. The boost has a start-up feature that reduces the peak current from the power-line during start-up. The LP8864S-Q1 can also control a power-line FET to reduce battery leakage when disabled and provide isolation and protection in the event of a fault.

Fault detection features of LP8864S-Q1 include:

- Open-string and shorted LED detection
	- LED fault detection prevents system overheating in case of open or short in some of the LED strings
- LED short-to-ground detection
- ISET/BST_FSET/PWM_FSET/LED_SET/MODE resistor out-of-range detection
- Boost overcurrent
- Boost overvoltage
- Device undervoltage protection (VDD UVLO)

– Threshold sensing from VDD pin

- V_{IN} input overvoltage protection (V_{IN} OVP)
	- Threshold sensing from VSENSE_P pin
- V_{IN} input undervoltage protection $(V_{IN}$ UVLO)
	- Threshold sensing from UVLO pin
- V_{IN} input overcurrent protection (V_{IN} OCP)
	- Threshold sensing across voltage between VSENSE_P pin and VSENSE_N pin
- Thermal shutdown in case of die overtemperature

7.2 Functional Block Diagram

7.3 Feature Description

7.3.1 Control Interface

Device control interface includes:

- EN is the enable input for the LP8864S-Q1 device.
- PWM is the default input to control the brightness of all current sinks by duty cycle.
- INT is an open-drain fault output indicating fault condition detection.
- SDA and SCL are data and clock line for I2C interface to control the brightness of all current sinks and read back the fault conditions for diagnosis.
- BST_SYNC is used to input an external clock for the boost switching frequency and control the internal boost clock mode.
	- The external clock is auto detected at start-up and, if missing, the internal clock is used.

- Optionally, the BST_SYNC can be tied to VDD to enable the boost spread spectrum function or tied to GND to disable it.
- ISET pin to set the maximum LED current level per string.

7.3.2 Function Setting

Device parameter setting includes:

- BST_FSET pin is used to set the boost switching frequency through a resistor to signal ground.
- PWM_FSET pin is used to set the LED output PWM dimming frequency through a resistor to signal ground.
- MODE pin is used to set the dimming mode via an external resistor to signal ground.
- LED SET pin is used to set the LED configuration through a resistor to signal ground.
- ISET pin is used to set the maximum LED current level per OUTx pin.

7.3.3 Device Supply (VDD)

All internal analog and digital blocks of LP8864S-Q1 are biased from external supply from VDD pin. Either a typical 5-V or 3.3-V supply rail is able to supply VDD from previous linear regulator or DC/DC converter with at least 150-mA current capability.

7.3.4 Enable (EN)

The LP8864S-Q1 only turns on when the input voltage of EN pin is above the voltage threshold (VEN_{IH}) and turns off when the voltage of EN pin is below the threshold (VEN $_{\rm II}$). All analog and digital blocks start operating once the LP8864S-Q1 is enabled by asserting EN pin. The SD pin is floating, I2C interface and Fault detection are not active if the EN pin is de-asserted.

7.3.5 Charge Pump

An integrated regulated charge pump can be used to supply the gate drive for the external FET of the boost controller. The charge pump is enabled or disabled by automatically detecting whether VDD and CPUMP pin are connected together. If VDD is $<$ 4.5 V then use the charge pump to generate a 5-V gate voltage to drive the external boost switching FET. To use the charge pump, a 2.2-µF capacitor is placed between C1N and C1P. If the charge pump is not required, C1N and C1P could be left unconnected and CPUMP pins tied to VDD. A 4.7 µF CPUMP capacitor is used to store energy for the gate driver. The CPUMP capacitor is required to be used in both charge pump enabled and disabled conditions and must be placed as close as possible to the CPUMP pins. $\boxed{8}$ 7-1and $\boxed{8}$ 7-2 show required connections for both use cases.

图 **7-1. Charge Pump Enabled Circuit**

图 **7-2. Charge Pump Disabled Circuit**

If the charge pump is enabled, the CPCAP_STATUS bit shows whether a fly capacitor was detected and the CP_STATUS bit shows status of any charge pump faults and generates an INT signal. The CP_INT_EN bit can be used to prevent the charge-pump fault from causing an interrupt on the INT pin.

7.3.6 Boost Controller

The LP8864S-Q1 current-mode-controlled boost DC/DC controller generates the anode voltage for the LEDs. The boost is a current-mode-controlled topology with a cycle by cycle current limit. The boost converter senses the switch current and across the external sense resistor connected between ISNS and ISNSGND. A 20-m Ω sense resistor results in a 10-A cycle by cycle current limit. The sense resistor value could vary from 15 m Ω to 50 m Ω depending on the application. Maximum boost voltage is configured with external FB-pin resistor divider connected between V_{OUT} and FB. The FB-divider equation is described in $\#$ 7.3.6.3.

图 **7-3. Boost Controller Block Diagram**

The boost switching frequency is adjustable from 100 kHz to 2.2 MHz via an external resistor at BST_FSET (see $\bar{\textbf{\#}}$ 7-1). Resistor with 1% accuracy is needed to ensure proper operation.

7.3.6.1 Boost Cycle-by-Cycle Current Limit

The voltage between ISNS and ISNSGND is used for both boost DC/DC controller's current sensing and cycleby-cycle current limit settings. When the cycle-by-cycle current limit is reached, the controller will turn off the switching MOSFET immediately and turn on it again in next siwtching cycle. This cycle-by-cycle current limit could be used as a common protection for all related DC/DC components (inductor, schottky diode and switching MOSFET) to avoid current running over their max limit. Cycle-by-Cycle current limit won't trigger any faults of the device.

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$$
I_{\text{CYCLE_LIMIT}} = \frac{V_{\text{ISNS}}}{R_{\text{SENSE}}}
$$

where

• $V_{ISNS} = 200$ mV

7.3.6.2 Controller Min On/Off Time

The device boost DC/DC controller has minimum on/off time as below table. Minimum off time should be specially taken care in system design. The SW node rising time plus falling time should be higher than minimum off time to avoid controller not turning off the MOSFET.

表 **7-2. Controller Minimum On/Off Time**

7.3.6.3 Boost Adaptive Voltage Control

The LP8864S-Q1 boost DC/DC converter generates the anode voltage for the LEDs. During normal operation, boost output voltage is adjusted automatically based on the LED current sink headroom voltages. This is called adaptive boost control. The number of used LED outputs is set by LED SET pin and only the active LED outputs are monitored to control the adaptive boost voltage. Any LED strings with open or short faults are also removed from the adaptive voltage control loop. The LED driver pin voltages are periodically monitored by the control loop and the boost voltage is raised if any of the LED outputs falls below the V_{HEADROOM} threshold. The boost voltage is lowered until any of the LED outputs touch the V_{HEADROOM} threshold. See $\&$ 7-4 for how the boost voltage automatically scales based on the OUTx-pin voltage, $V_{HEADROM}$ and $V_{HEADROOM-HYS}$.

(1)

NSTRUMENTS

图 **7-4. Adaptive Boost Voltage Control Loop Function**

The resistive divider (R_1, R_2) defines both the minimum and maximum adaptive boost voltage levels. The feedback circuit operates the same in boost and SEPIC topologies. Choose maximum boost voltage based on the maximum LED string voltage specification. Before the LED drivers are active, the boost starts up to the initial boost level. The initial boost voltage is approximately in the 88% point of minimum to maximum boost voltage. Once the LED driver channels are active, the boost output voltage is adjusted automatically based on OUTx pin voltages. The FB pin resistor divider also scales the boost OVP, OCP levels and the LED short level in HUD application.

7.3.6.3.1 FB Divider Using Two-Resistor Method

A typical FB-pin circuit uses a two-resistor divider circuit between the boost output voltage and ground.

(2)

Maximum boost voltage can be calculated with Equation 2. The maximum boost voltage can be reached during OPEN string detection or if all LED strings are left disconnected.

$$
V_{\text{BOOST}_\text{MAX}} = I_{\text{SEL}_\text{MAX}} \times R_1 + \left(\frac{R_1}{R_2} + 1\right) \times V_{\text{REF}}
$$

where

- V_{RFF} = 1.21 V
- $I_{\text{SEL MAX}} = 38.7 \mu \text{A}$
- R_1 / R_2 normal recommended range is $7 \sim 15$

The minimum boost voltage must be less than the minimum LED string voltage. Minimum boost voltage is calculated with Equation 3:

$$
V_{\text{BOOST_MIN}} = \left(\frac{R_1}{R_2} + 1\right) \times V_{\text{REF}}
$$
\n(3)

where

• $V_{REF} = 1.21 V$

When the boost OVP LOW level is reached, the boost controller stops switching the boost FET and the BSTOVPL STATUS bit is set. The LED drivers are still active during this condition, and the boost resumes normal switching operation once the boost output level falls. The boost OVP low voltage threshold changes dynamically with current boost voltage. It is calculated in Equation 4:

$$
V_{\text{BOOST_OVPL}} = V_{\text{BOOST}} + \left(\frac{R_1}{R_2} + 1\right) \times (V_{\text{FB_OVPL}} - V_{\text{REF}})
$$
\n
$$
\tag{4}
$$

where

- $V_{FB\ OVPL} = 1.423 V$
- V_{RFF} = 1.21 V

When the boost OVP HIGH level is reached the boost controller enters fault recovery mode, and the BSTOVPH_STATUS bit is set. The boost OVP high-voltage threshold also changes dynamically with current boost voltage and is calculated in Equation 5:

$$
V_{\text{BOOST_OVPH}} = V_{\text{BOOST}} + \left(\frac{R_1}{R_2} + 1\right) \times (V_{\text{FB_OVPH}} - V_{\text{REF}})
$$
\n
$$
\tag{5}
$$

where

- $V_{FB-OVPH}$ = 1.76 V
- $V_{REF} = 1.21 V$

When the boost UVP level is reached the boost controller starts a 110-ms OCP counter. The LP8864S-Q1 device enters the fault recovery mode and sets the BSTOCP STATUS bit if the boost voltage does not rise above the UVP threshold before the timer expires. The boost UVP voltage threshold also changes dynamically with current boost voltage and is calculated in Equation 6:

$$
V_{\text{BOOST_UVP}} = V_{\text{BOOST}} - \left(\frac{R_1}{R_2} + 1\right) \times (V_{\text{REF}} - V_{\text{UVP}})
$$

(6)

where

- $V_{UVP} = 0.886 V$
- $V_{REF} = 1.21 V$

7.3.6.3.2 FB Divider Using Three-Resistor Method

A FB-pin circuit using a three-resistor divider circuit can be used for applications where less than 200-k Ω resistors are required.

图 **7-6. Three-Resistor FB Divider Circuit**

Maximum boost voltage can be calculated with Equation 7. The maximum boost voltage can be reached during OPEN string detection or if all LED strings are left disconnected.

$$
V_{\text{BOOST}_\text{MAX}} = \left(\frac{R_1 \times R_3}{R_2} + R_1 + R_3\right) \times I_{\text{SEL}_\text{MAX}} + \left(\frac{R_1}{R_2} + 1\right) \times V_{\text{REF}} \tag{7}
$$

where

• $V_{REF} = 1.21 V$

- $I_{\text{SEL MAX}} = 38.7 \mu \text{A}$
- R_1/R_2 normal recommended range is 7 to 15

The minimum boost voltage must be less than the minimum LED string voltage. Minimum boost voltage is calculated in Equation 8:

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(8)

$$
V_{\text{BOOST_MIN}} = \left(\frac{R_1}{R_2} + 1\right) \times V_{\text{REF}}
$$

When the boost OVP LOW level is reached the boost controller stops switching the boost FET, and the BSTOVPL STATUS bit is set. The LED drivers are still active during this condition, and the boost resumes normal switching operation once the boost output level falls. The boost OVP low voltage threshold changes dynamically with current boost voltage. It is calculated in Equation 9:

$$
V_{\text{BOOST_OVPL}} = V_{\text{BOOST}} + \left(\frac{R_1}{R_2} + 1\right) \times (V_{\text{FB_OVPL}} - V_{\text{REF}})
$$
\n
$$
\tag{9}
$$

where

- V_{FB_OVPL}= 1.423 V
- V_{BEF} = 1.21 V

When the boost OVP LOW level is reached the boost controller enters fault recovery mode, and the BSTOVPH_STATUS bit is set. The boost OVP high-voltage threshold also changes dynamically with current boost voltage and is calculated in Equation 10:

$$
V_{\text{BOOST_OVPH}} = V_{\text{BOOST}} + \left(\frac{R_1}{R_2} + 1\right) \times (V_{\text{FB_OVPH}} - V_{\text{REF}})
$$
\n
$$
\tag{10}
$$

where

- $V_{FB_{OVPH}} = 1.76 V$
- V_{BEF} = 1.21 V

When the boost UVP level is reached the boost controller starts a 110-ms OCP counter. The LP8864S-Q1 device enters the fault recovery mode and sets the BSTOCP_STATUS bit if the boost voltage does not rise above the UVP threshold before the timer expires. The boost UVP voltage threshold also changes dynamically with current boost voltage and is calculated in Equation 11:

$$
V_{\text{BOOST_UVP}} = V_{\text{BOOST}} - \left(\frac{R_1}{R_2} + 1\right) \times (V_{\text{REF}} - V_{\text{UVP}})
$$
\n
$$
\tag{11}
$$

where

- $V_{UVP} = 0.886 V$
- V_{RFF} = 1.21 V

7.3.6.3.3 FB Divider Using External Compensation

The device has internal compensation network to keep the DC-DC control loop in good stability in most cases. However, an additional external compensation network could also be added on FB-pin to offer more flexibility in loop design or solving some extreme use-cases.

图 **7-7. External Compensation Network**

This network will create one additional pole and one additional zero in the loop.

$$
f_{\text{POLE_COMP}} = \frac{1}{2\pi \left[(R_1 \parallel R_2) + R_4 \right] C_{\text{COMP}}}
$$
\n
$$
f_{\text{ZERO_COMP}} = \frac{1}{2\pi R_4 C_{\text{COMP}}}
$$
\n(12)

It could be noted that $R₃$ doesn't take part in the compensation. So this external compensation network could be both used in two-divider netwrok and T-divider network with no equation change.

In real application, for example, when DC-DC loop has stability concern, putting the additional pole in 1 kHz and the additional zero in 2 kHz will suppress the loop gain by approximately 6 dB after 2 kHz. This will benefit gain margin and phase margin a lot.

7.3.6.4 Boost Sync and Spread Spectrum

Spread spectrum function could be enabled when BST_SYNC pin is high and disabled when BST_SYNC pin is low.

If an external CLK signal is on the BST_SYNC pin, the boost controller can be clocked by this signal. If the clock disappears later, the boost continues operation at the frequency defined by RBST_FSET resistor, and the spread spectrum function will be enabled or disabled depending on the final pin level of BST_SYNC.

表 **7-3. Boost Synchronization Mode**

表 **7-3. Boost Synchronization Mode (continued)**

If using the external BST_SYNC input, the $R_{BST, SFT}$ resistor should be chosen the closest boost frequency options with the external frequency.

The spread spectrum function helps to reduce EMI noise around the switching frequency and its harmonic frequencies. The internal spread spectrum function modulates the boost frequency ±3.3% to 7.2% from the central frequency with a 200-Hz to 1.2-kHz modulation frequency. The switching frequency variation is programmable by SPREAD_RANGE register, and the modulation frequency is programmable by SPREAD_MOD_FREQ register. The spread-spectrum function cannot be used when an external synchronization clock is used.

表 **7-5. Spread Spectrum Modulation Frequency**

7.3.6.5 Boost Output Discharge

When the EN pin is pulled low, the device stops the boost controller and LED current sinks, turns off the powerline FET, and starts to discharge the boost output. The discharge pin typically sinks 30-mA current. The discharge duration is 400 ms. After 400 ms, the device shuts down. The DISCHARGE pin must be connected with boost output for normal operation.

There is one internal comparator to monitor the voltage of DISCHARGE pin. As soon as the voltage of DISCHARGE pin is higher than $V_{\text{BST OVPH}}$ (typically 50 V), the device enters into fault recovery mode, and BST_OVPH fault is reported. This provides further protection if boost voltage is out of control because of system failure.

Discharge function is only available in HTSSOP package. It's not available in QFN package.

7.3.6.6 Light Load Mode

The DC-DC controller will enter into light load mode in below condition:

- V_{IN} voltage is very close to V_{OUT}
- Loading current is very low
- PWM pulse width is very short

When DC-DC converter enters into light load mode, it stops switching occasionally to make sure output voltage won't rise up too much. It could also be called as PFM mode, since the DC-DC converter switching frequency will change in this mode.

7.3.7 LED Current Sinks

7.3.7.1 LED Output Current Setting

The maximum output LED current is set by an external resistor value. For the application only using external resistor R_{ISET} to set the maximum LED current for each string, the Equation 14 is used to calculate the current setting of all strings:

$$
I_{LED} = \frac{1.21V}{R_{ISET}} \times 2580
$$
 (14)

The LEDx_CURRENT[11:0] registers can also be used to adjust strings current down from this maximum. The default value for LEDx_CURRENT[11:0] registers is the maximum 0xFFF(4095). Equation 15 is used to calculate the current setting of an individual string:

$$
I_{LED} = \left(\frac{1.21V}{R_{ISET}} \times 2580\right) \times \left(\frac{LED_CURRENT[11:0]}{4095}\right)
$$
\n(15)

For high accuracy of LED current, the ILED current is recommended to set in range from 30 mA to 200 mA. So the R_{ISET} value is in the range from 15.6 k Ω to 104 k Ω .

图 **7-8. LED Driver Current Setting Circuit**

7.3.7.2 LED Output String Configuration

The Four LED driver channels of the LP8864S-Q1 device is configured by the LED_SET resistor, which supports applications using one to Four LED strings. Resistor with 1% accuracy is needed to ensure proper operation. The driver channels can also be tied together in groups of one, two or three. This allows the LP8864S-Q1 device to drive two 300-mA LED strings, or one 600-mA LED string. The LED strings are always appropriately phase shifted for their string configuration. This reduces the ripple seen at the boost output, which allows smaller output capacitors and reduces audible ringing in the capacitors. Phase shift increases the load frequency, which can move potential capacitor noise above the audible band while still keeping PWM frequency low to support a higher dimming ratio.

When the LP8864S-Q1 device is firstly powered on, the string configuration is configured by the LED SET resistor and the phases of each channel are automatically configured. The LED string configuration must not be

changed unless the LP8864S-Q1 is powered off in shutdown state. The unused LEDx pins should be tied to ground.

表 **7-6. LED Output String Configuration**

7.3.7.3 LED Output PWM Clock Generation

The LED PWM frequency is asynchronous from the input PWM frequency. The LED PWM frequency is generated from the internal 20-MHz oscillator and can be set to eight discrete frequencies from 152 Hz to 19.531 kHz. The PWM dimming resolution is highest when the lowest PWM frequency is used. The PWM_FSET resistor determines the LED PWM frequency based on $# 7-8$. PWM resolution in Table 7-8 is with PWM dither disabled.

7.3.8 Brightness Control

The LP8864S-Q1 supports global brightness control for all LED strings through either duty cycle input on PWM pin or register by I2C bus. An internal 20-MHz clock is used for generating PWM outputs.

7.3.8.1 Brightness Control Signal Path

The BRT MODE register selects whether the input to the display brightness path is the PWM input pin or DISP_BRT register. PWM input control will be the default setup after power on. The brightness control signal path diagram is shown in $\boxed{8}$ 7-9

The display brightness path has sloper function that can be enabled. By default the sloper function is enabled. The sloper and dither function also can be programmable by I2C control. The sloper function is described in $\ddot{\text{t}}$ 7.3.8.7, and the dither function is described in \ddagger 7.3.8.9.

图 **7-9. LP8864S-Q1 Brightness Path Diagram**

7.3.8.2 Dimming Mode

Dimming mode can be adjusted via an external resistor to MODE pin (see $\bar{\mathcal{R}}$ 7-7). Resistor with 1% accuracy is needed to ensure proper operation.

表 **7-7. Dimming Mode Configuration**

表 **7-7. Dimming Mode Configuration (continued)**

7.3.8.3 LED Dimming Frequency

The LED dimming frequency is asynchronous from the input PWM frequency for phase-shift PWM mode and hybrid dimming mode. The LED dimming frequency is generated from the internal 20-MHz oscillator and can be set to eight discrete frequencies from 152 Hz to 19.531 kHz. The PWM dimming resolution is highest when the lowest PWM frequency is used. The PWM_FSET resistor determines the LED Dimming frequency based on $\frac{1}{\mathcal{R}}$ 7-8. Resistor with 1% accuracy is needed to ensure proper operation. PWM resolution in $\frac{1}{\sqrt{6}}$ 7-8 is with PWM dither disabled.

表 **7-8. LED PWM Frequency Selection**

7.3.8.4 Phase-Shift PWM Mode

In Phase-Shift PWM mode, all current active channels are turned on and off at LED dimming frequency with a constant delay. However, the number of used channels or channel groups determine the phase delay time between two neighboring channels as shown in $\boxed{8}$ 7-10.

图 **7-10. Phase-Shift Dimming Diagram**

7.3.8.5 Hybrid Mode

In addition to phase-shift PWM dimming, LP8864S-Q1 supports a hybrid-dimming mode. Hybrid dimming combines PWM and current modes for brightness control for the display brightness path. By using hybrid dimming, dimming ratio could be increased by another 8 times. In hybrid mode, PWM dimming is used for low brightness range of brightness, and current dimming is used for high brightness levels as shown in \boxtimes 7-11. Current dimming control enables improved optical efficiency due to increased LED efficiency at lower currents. PWM dimming control at low brightness levels ensures linear and accurate control. Hybrid mode can be selected through resistor value at MODE pin as 表 7-7. The PWM and current modes transition threshold can be set at 12.5% or at 0% brightness. The latter selection allows for pure current dimming control mode.

图 **7-11. Hybrid Dimming Diagram**

7.3.8.6 Direct PWM Mode

In direct PWM mode, all active channels are turned on and off and are synchronized with the input PWM signal.

图 **7-12. Direct PWM Dimming Diagram**

7.3.8.7 Sloper

An optional sloper function makes the transition from one brightness value to another optically smooth. By default the advanced sloper is enabled with a 200-ms linear sloper duration. Transition time between two brightness values is programmed with the SLOPE SELECT[2:0] bits (when 000, sloper is disabled). With advanced sloper enabled the brightness changes are further smoothed to be more pleasing to the human eye. Advanced slope is enabled with ADV_SLOPE_ENABLE register bit.

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图 **7-13. Brightness Sloper**

7.3.8.8 PWM Detector Hysteresis

PWM detector has an internal hysteresis function. It means when PWM input is used (except direct PWM mode), PWM output duty cycle will change only when PWM input on-time changes by more than 6.4us. This is to avoid the PWM duty cycle sampling error due to the onboard PWM signal's rising/falling time.

7.3.8.9 Dither

The number of brightness steps when using LED output PWM dimming is equal to the 20-MHz oscillator frequency divided by the LED PWM frequency (set by PWM_FSET resistor). The PWM duty cycle dither is a function the LP8864S-Q1 uses to increase the number of brightness dimming steps beyond this oscillator clock limitation. The dither function modulates the LED driver output duty cycle over time to create more possible average brightness levels. The DITHER_SELECT[3:0] register bits control the level of dither, disabled, 1, 2, 3 or 4 bits using the I2C interface. By default the dither is disabled.

When the 1-bit dither is selected, to support higher brightness resolution, the width of every second PWM pulse could be increased by one LSB (one 20-MHz clock period). When the 3-bit dither is selected, within a sequence of 8 PWM periods the number of pulses with increased length varies depending on the dither value: dither value 000 - all 8 pulses at default length; 001 - one of the 8 pulses is longer; 010 - two of the 8 pulses are longer, and so forth, until at 111 - seven of the 8 pulses have increased length. \boxtimes 7-14 shows one example of PWM output dither.

图 **7-14. PWM Dither Example**

The dither block also helps in low brightness scenario when dimming ratio is limited by LED PWM output frequency and the LED output pulse is less than the minimum pulse width (200 ns). In such scenario, the dither block will skip some of the PWM pulses to reduce the brightness further, enabling high dimming ratio. The end result is that the LED PWM frequency is reduced as more and more minimum pulses are skipped or dithered out. At the same time, dither block will also guarantee that the minimum LED PWM frequency is not less than 152 Hz to ensure no brightness flickering. $\boxed{8}$ 7-15 shows how the dither works in low brightness scenario.

图 **7-15. Minimum Brightness Dither Example**

7.3.9 Protection and Fault Detections

The LP8864S-Q1 device includes fault detections for LED open, short and short-to-GND conditions, boost input undervoltage, overvoltage and overcurrent, boost output overvoltage and overcurrent, VDD undervoltage, die overtemperature and external components. The host can monitor the status of the faults in registers SUPPLY_FAULT_STATUS, BOOST_FAULT_STATUS and LED_STATUS.

7.3.9.1 Supply Faults

7.3.9.1.1 VIN Undervoltage Faults (VINUVLO)

The LP8864S-Q1 device supports V_{IN} undervoltage and overvoltage protection. The undervoltage threshold is programmable through external resistor divider on UVLO pin. If during operation of the LP8864S-Q1 device, the UVLO pin voltage falls below the UVLO falling level (0.787 V typical), the boost, LED outputs, and power-line FET will be turned off, and the device will enter STANDBY mode. The VINUVLO STATUS bit is also set in the SUPPLY_FAULT_STATUS register, and the INT pin is triggered. When the UVLO voltage rises above the rising threshold level the LP8864S-Q1 exits STANDBY and begins the start-up sequence.

图 **7-16. VIN UVLO Setting Circuit**

The following equation is used to calculate the UVLO threshold for VIN rising edge:

$$
VIN_{UVLO_RISING} = (\frac{R_4}{R_5} + 1) \times VIN_{UVLO_TH}
$$
\n(16)

where

• $VIN_{UVLO_TH} = 0.787 V$

The hysteresis of UVLO threshold can be designed and calculated with the following equation.

$$
VIN_{HYST} = R_4 \times I_{UVLO}
$$
 (17)

where

• $I_{UVLO} = 5 \mu A$

So the following equation can be used for UVLO threshold for VIN falling edge:

$$
VIN_{UVLO_FALLING} = VIN_{UVLO_RISING} - VIN_{HYST}
$$
\n
$$
(18)
$$

The bottom resistors, R_5 of voltage divider is able to be disconnected to the GND through an additional external N-type of FET as 图 7-17. This design is to minimize the current leakage from VIN in shutdown mode to extend the battery life.

图 7-17. V_{IN} UVLO Setting Circuit Without Current Leakage Path

7.3.9.1.2 VIN Overvoltage Faults (VINOVP)

The overvoltage threshold for V_{IN} rising edge is internal fixed at typical 43 V. If during LP8864S-Q1 operation, VSENSE_P pin voltage rises above the OVP rising threshold, boost, LED outputs, and power-line FET will be turned off, and the device will enter STANDBY mode. The VINOVP_STATUS bit will also be set in the SUPPLY_FAULT_STATUS register, and the INT pin will be triggered. When the VSENSE_P pin voltage falls below the falling threshold level, the LP8864S-Q1 exits STANDBY and begins the start-up sequence.

7.3.9.1.3 V_{DD} Undervoltage Faults (VDDUVLO)

If during LP8864S-Q1 device operation VDD falls below VDDUVLO falling level, boost, power-line FET, and LED outputs are turned off, and the device enters STANDBY mode. The VDDUVLO_STATUS fault bit will be set in the SUPPLY_FAULT_STATUS register, and the INT pin will be triggered. The LP8864S-Q1 restarts automatically to ACTIVE mode when V_{DD} rises above VDDUVLO rising threshold.

7.3.9.1.4 VIN OCP Faults (VINOCP)

If during LP8864S-Q1 device operation voltage drop on RISENSE resistor rises above 220 mV, boost, powerline FET, and LED outputs are turned off, and the device enters Fault Recovery mode and then attempt to restart 100 ms after fault occurs. The VINOCP_STATUS fault bit are set in the SUPPLY_FAULT_STATUS register, and the INT pin is triggered.

$$
I_{\text{VIN}_\text{OCP}} = \frac{\text{VIN}_{\text{OCP}_\text{TH}}}{R_{\text{ISENSE}}}
$$

where

• VIN_{OCP} $_{TH}$ = 220 mV

7.3.9.1.4.1 VIN OCP Current Limit vs. Boost Cycle-by-Cycle Current Limit

VIN OCP current limit is totally different from boost cycle-by-cycle current limit.

Boost cycle-by-cycle current limit is to protect the DC/DC components (inductor, schottky diode and switching MOSFET) in normal scenario, avoiding current running over their max limit. The normal scenario means when loading has sharp change or input voltage has sharp change. It won't trigger any device fault.

VIN OCP current limit is to protect system from ciritical system hazard (e.g, inductor short, switching MOSFET short). It will trigger the device to shutdown all the LED channels and enter into fault recovery state.

VIN OCP current limit should be always greater than boost cycle-by-cycle current limit. This means R_{ISENSE} should be always no smaller than R_{SFNSF} .

(19)

7.3.9.1.5 Charge Pump Faults (CPCAP, CP)

If during LP8864S-Q1 device operation voltage of CPUMP pin falls below typical 4.2-V, boost, power-line FET, and LED outputs are turned off, and the device enters Fault Recovery mode and then attempt to restart 100 ms after fault occurs. The CP_STATUS fault bit will beset in the SUPPLY_FAULT_STATUS register, and the INT pin are triggered.

If during LP8864S-Q1 device initialization, the charge pump fly capacitor is disconnected or shorted, charge pump are turned off. In result, boost, power-line FET, and LED outputs are turned off, and the device enters Fault Recovery mode and then attempt to restart 100 ms after fault occurs. Both CPCAP STATUS and CP_STATUS fault bits are set in the SUPPLY_FAULT_STATUS register, and the INT pin are triggered.

7.3.9.1.6 CRC Error Faults (CRCERR)

If during LP8864S-Q1 device initialization, the factory default configuration for registers, options and trim bits are not corrected loaded from memory, LP8864S-Q1 keeps operating normally, unless other fault criteria is triggered. The CRCERR_STATUS fault bit are set in the SUPPLY_FAULT_STATUS register and the INT pin are triggered.

7.3.9.2 Boost Faults

7.3.9.2.1 Boost Overvoltage Faults (BSTOVPL, BSTOVPH)

Boost overvoltage is detected if the FB pin voltage exceeds the $V_{FB-OVPL}$ threshold. When boost overvoltage is detected, BSTOVPL STATUS bit will be set in the BOOST FAULT STATUS register. The boost FET stops switching, and the output voltage will be automatically limited. If the BSTOVPL STATUS bit is continually set (that is, reappears after clearing), it may indicate an loop issue in the application. Boost overvoltage low is monitored during device Boost Softstart and Normal mode.

A second boost overvoltage high fault is detected if the FB pin voltage exceeds the $V_{FB-OVPH}$ threshold or the DISCHARGE pin voltage exceeds the V_{BST OVPH}. The LP8864S-Q1 device enters the fault recovery state to protect system damage from a high boost voltage. When boost overvoltage is detected, BSTOVPH_STATUS bit is set in the BOOST FAULT STATUS register. A fault interrupt is also generated. The device enters Fault Recovery mode and then attempt to restart after 100 ms. Boost overvoltage high is monitored during Boost Softstart and Normal mode.

7.3.9.2.2 Boost Overcurrent Faults (BSTOCP)

Boost overcurrent is detected if the FB pin voltage drops below the V_{UVP} threshold for 110 ms. If the boost overcurrent timer expires before the output voltage recovers, the BSTOCP_STATUS bit is set in the BOOST_FAULT_STATUS register. The fault recovery state is entered, and a fault interrupt is generated. The device will enter Fault Recovery mode and then attempt to restart after 100 ms. If the BSTOCP_STATUS bit is permanently set, it may indicate an issue in the application. Boost overcurrent is monitored from the boost start, and fault may trigger during boost start-up.

7.3.9.2.3 LEDSET Resistor Missing Faults (LEDSET)

The LEDSET resistor missing or invalid is detected if the resistor is not assembled or not valid value as requested during the initialization. The LP8864S-Q1 device defaults to 4-channel/150-mA configuration if the LEDSET resistor is missing or invalid. The LEDSET STATUS fault bit is set in the BOOST FAULT STATUS register. The LEDSET resistor missing or invalid fault will not be monitored after initialization, so that the LP8864S-Q1 is operating in the configuration determined during initialization even though the LEDSET resistor is missing or invalid after initialization.

7.3.9.2.4 MODE Resistor Missing Faults (MODESEL)

The MODE resistor missing or invalid is detected if the resistor is not assembled or not valid value as requested during the initialization. LP8864S-Q1 defaults to phase-shift PWM mode with I2C address 0x3A if the MODE resistor is missing or invalid. The MODESEL_STATUS fault bit will be set in the BOOST_FAULT_STATUS register. The MODE resistor missing or invalid fault is not monitored after initialization, so that the LP8864S-Q1 operates in the mode determined during initialization even though the MODE resistor is missing or invalid after initialization.

7.3.9.2.5 FSET Resistor Missing Faults (FSET)

The FSET resistor missing or invalid for both BOOST_FSET and PWM_FSET is detected if any one of them is not assembled or not a valid value as requested during the initialization. LP8864S-Q1 defaults the switching frequency of boost to 400 kHz if BOOST_FSET resistor is missing or invalid, or PWM dimming frequency to 305 Hz if PWM_FSET resistor is missing or invalid. The FSET_STATUS fault bit is set in the BOOST_FAULT_STATUS register. The FSET resistor missing or invalid fault is not monitored after initialization, so that the LP8864S-Q1 device operates at the boost switching frequency and the PWM dimming frequency determined during initialization even though the FSET resistor is missing or invalid after initialization.

7.3.9.2.6 ISET Resistor Out of Range Faults (ISET)

If the ISET pin resistor is shorted to GND during normal operation, the maximum current for each LED channel can be calculated in Equation 20:

$$
I_{LED_ISET_FAULT} = I_{LED_LIMIT} \times \left(\frac{LED_CURRENT[11:0]}{4095} \right)
$$
 (20)

where

 \cdot I_{LED LIMIT} = 280 mA

LED_CURRENT[11:0] register will be automatically modified to 1/4 of latest programmed data. if it is not programmed after device enabling, the default value of LED_CURRENT[11:0] register is 0xFFF and automatically modified to 0x3FF after the fault occurs. If ISET pin voltage returns back to above 1.1 V, the LED_CURRENT[11:0] register data automatically returns to latest programmed data. The ISET_STATUS fault bit will be set in the BOOST_FAULT_STATUS register and the INT pin is triggered.

7.3.9.2.7 Thermal Shutdown Faults (TSD)

If the die temperature of LP8864S-Q1 reaches the thermal shutdown threshold T_{SD} , the boost, power-line FET, and LED outputs on LP8864S-Q1 shuts down to protect the device from damage. Fault status bit TSD_STATUS bit will be set, and the INT pin will be triggered. The device restarts the power-line FET, the boost, and LED outputs when temperature drops by TSD_HYS amount.

7.3.9.3 LED Faults

7.3.9.3.1 Open LED Faults (OPEN_LED)

During normal boost operation, boost voltage is raised if any of the used LED outputs falls below the LED DRV HEADROOM threshold level. Open LED fault is detected if boost output voltage has reached the maximum and at least one LED output is still below the threshold. The open string is then disconnected from the boost adaptive control loop and its output is disabled. Any LED fault sets the status bit LED_STATUS and an interrupt is generated unless LED interrupt is disabled. The detail of open LED faults can be read from bits OPEN LED and LEDx FAULT $(x = 1...4)$. These bits maintain their value until device power-down. But the LED STATUS bit could be cleared by the interrupt clearing procedure. If a new LED fault is detected, LED STATUS is set and an interrupt generated again.

图 **7-18. LED Open and Short Detection Logic**

7.3.9.3.2 Short LED Faults (SHORT_LED)

Short LED fault is detected if one or more LED outputs are above the $V_{LEDSHORT}$ typical 5.4 V and at least one LED output is inside the normal operation window (see $\&$ 7-18). Shorted string is disconnected from the boost adaptive control loop and the LED PWM output is disabled. LED_STATUS status bit is set and an interrupt generated similarly as in open LED case. Detailed shorted LED fault can be read from bits SHORT_LED and LEDx_FAULT $(x = 1...4)$, indicating the faulty LED) in LED_FAULT_STATUS register.

In HUD application, when output channels are connected as groups and only one or two groups are active, one more special condition will trigger the short LED fault. This is when boost adaptive voltage comes to minimum and one of the LED channels voltage is still higher than $V_{HEADROM} + V_{HEADROM HYS}$.

7.3.9.3.3 LED Short to GND Faults (GND_LED)

During boost soft start and normal boost operation, if LED output is lower than VSHORTGND for 20 ms, device turns off the corresponding LED output channel and output a typical 6-mA current for 300-µs period again. After this operation, if output voltage is still lower than $V_{HEABROM}$, LED short to GND fault will be reported.

If LED short to GND is reported, boost, LED outputs and power-line FET is turned off, the device will enter Fault Recovery mode. LED STATUS bit is set and an interrupt generated similarly as in open LED case. LED short to GND fault reason can be read from bits LED GND and LEDx FAULT $(x = 1...4)$ in LED FAULT STATUS register. These bits maintain their value until device powers are down while the LED_STATUS bit is cleared by the interrupt clearing procedure.

7.3.9.3.4 Invalid LED String Faults (INVSTRING)

During device initialization, any of un-used LED outputs pins are checked whether connected to GND or not. If they are not connected to GND as expected, the LP8864S-Q1 reports invalid string fault and tries to function normally if possible. The INVSTRING_STATUS fault bit is set in the LED_FAULT_STATUS register, and the INT pin is triggered. The LEDSET resistor missing or invalid fault is not detected after initialization, so that the LP8864S-Q1 operates in the configuration determined during initialization even though the LEDSET resistor is missing or invalid after initialization.

7.3.9.3.5 I2C Timeout Faults

If chip receives I2C command without STOP signal for 500 ms, I2C communication block auto resets and waits for the next command. I2C_ERROR_STATUS fault bit is set in the LED_FAULT_STATUS register, and the INT pin is triggered.

7.3.9.4 Overview of the Fault and Protection Schemes

表 **7-9. Fault and Protection Schemes**

 $\begin{array}{c|c}\n\text{Yes} & \text{No} \\
\end{array}$ No Device functions normally, if possible.

 Yes No $\begin{array}{c} \begin{array}{c} \end{array}$ No $\begin{array}{c} \end{array}$ Device functions normally and waits for the next I2C command.

voltage of one or more used LED output is below V_{SHORTGND}.and keeps still when the corresponding channel is off and small test current is injected.

Invalid LED string detected INVSTRING_STATUS Configured unused LED output is

I2C timeout I2C_ERROR_STATUS Device receives I2C command without STOP signal for 500 ms.

表 **7-9. Fault and Protection Schemes (continued)**

7.4 Device Functional Modes

7.4.1 State Diagram

图 **7-19. State Machine Diagram**

7.4.2 Shutdown

When EN is pulled low, boost, power-line FET, and LED outputs are turned off, and the device tries to discharge the boost output for 400 ms. After this, the device is totally turned off.

7.4.3 Device Initialization

After POR is released device initialization begins. During this state the LDO is started up, EEPROM default and trim configurations are loaded, LEDSET, MODE, BOOST_FSET and PWM_FSET resistors are detected.

7.4.4 Standby Mode

Starting from Standby mode, the device can be accessed with I2C to change any configuration registers.

Standby Mode is immediately switched to Power-line FET Soft Start mode if there's no fault.

7.4.5 Power-line FET Soft Start

Power-line FET is gradually enabled during this 25-ms long state. Boost input and output capacitors are charged to V_{IN} level. V_{IN} faults for OCP, OVP, and UVP and fault for LED short to GND are enabled.

7.4.6 Boost Start-Up

Boost voltage is ramped to initial boost voltage level with reduced current limit for 50 ms. All boost faults are now enabled.

7.4.7 Normal Mode

LED drivers are enabled when brightness is greater than zero. All LED faults are active.

7.4.8 Fault Recovery

Some critical faults can trigger fault recover state. LED drivers, boost converter, and power-line FET are disabled for 100 ms, and the device attempts to restart from standby mode if EN is still high and brightness is greater than zero.

7.4.9 Latch Fault

If all LED strings are disabled due to faults then the LP8864S-Q1 enters the latch fault mode. This state can be exited only by pulling the EN pin low.

7.4.10 Start-Up Sequence

图 **7-20. Start-Up Sequence Diagram**

7.5 Programming

7.5.1 I2C-Compatible Interface

The LP8864S-Q1 device supports I2C interface to access and change the configuration. The 7-bit base slave address is 0x3A or 0x3B. The address could be configured through the resistor settings of MODE pin.

Write I2C transactions are made up of 4 bytes. The first byte includes the 7-bit slave address and Write bit. The 7-bit slave address selects the LP8864S-Q1 slave device. The second byte is eight bits register address. The last two bytes are the 16-bit register value.

Read I2C transactions are made up of 5 bytes. The first byte includes the 7-bit slave address and Write bit. The 7-bit slave address selects the LP8864S-Q1 slave device. The second byte is eight bits register address. The third byte includes the 7-bit slave address and Read bit. The last two bytes are the 16-bit register value returned from the slave.

where

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• W bit = 1

图 **7-21. I2C Write**

- where
- R bit = 0
- W bit = 1

图 **7-22. I2C Read**

7.5.2 Programming Examples

7.5.2.1 General Configuration Registers

The LP8864S-Q1 does not require any serial interface configuration. It can be simply controlled with the EN pin and PWM pin. Most of the device configuration is accomplished using external resistor values. If I2C interface is available then extended configuration is possible. The configuration registers can be written from standby state to normal state as shown in $\overline{\mathcal{R}}$ 7-10.

表 **7-10. Configuration Registers**

7.5.2.2 Clearing Fault Interrupts

The LP8864S-Q1 has an INT pin to alert the host when a fault occurs. If I2C interface is available, the Interrupt Fault Status registers can be read back to learn which fault(s) have been detected. These status bits are located in the SUPPLY_STATUS, BOOST_STATUS and LED_STATUS registers. Each interrupt status has a STATUS bit and a CLEAR bit. To clear a fault interrupt status a 1 must be written to both the STATUS bit and CLEAR bit at the same time.

7.5.2.3 Disabling Fault Interrupts

By default, most of the LP8864S-Q1 faults trigger the INT pin. Each fault has two INT_EN bits. These bits are located in the SUPPLY_INT_EN, BOOST_INT_EN, and LED_INT_EN registers. If the INT_EN bit is read and returns 2b'10, the INT pin is triggered when that fault occurs. The fault interrupt can be disabled by writing 2b'01 to its INT_EN bits, or it can be enabled by writing 2b'11 to its INT_EN bits. There is also a GLOBAL fault interrupt that can be disabled to prevent any faults from triggering the INT pin.

7.5.2.4 Diagnostic Registers

The LP8864S-Q1 contains several diagnostic registers than can be read with the serial interface for debugging or additional device information. $# 7-11$ is a summary of the available registers.

表 **7-11. Diagnostic Registers**

7.6 Register Maps

7.6.1 FullMap Registers

表 7-12 lists the memory-mapped registers for the FullMap registers. All register offset addresses not listed in 表 7-12 should be considered as reserved locations and the register contents should not be modified.

Complex bit access types are encoded to fit into small table cells. $\frac{1}{100}$ 7-13 shows the codes that are used for access types in this section.

表 **7-13. FullMap Access Type Codes**

7.6.1.1 BRT_CONTROL Register (Offset = 00h) [reset = 0h]

BRT_CONTROL is shown in $\overline{\mathbb{R}}$ 7-23 and described in $\overline{\mathbb{R}}$ 7-14.

Return to Summary Table.

表 **7-14. BRT_CONTROL Register Field Descriptions**

7.6.1.2 LED_CURR_CONFIG Register (Offset = 02h) [reset = 0FFFh]

LED_CURR_CONFIG is shown in \boxtimes 7-24 and described in $\ddot{\otimes}$ 7-15.

Return to Summary Table.

图 **7-24. LED_CURR_CONFIG Register**

表 **7-15. LED_CURR_CONFIG Register Field Descriptions**

7.6.1.3 USER_CONFIG1 Register (Offset = 04h) [reset = 8A3h]

USER_CONFIG1 is shown in $\boxed{8}$ 7-25 and described in $\frac{1}{\sqrt{6}}$ 7-16.

Return to Summary Table.

图 **7-25. GROUPING1 Register**

表 **7-16. USER_CONFIG1 Register Field Descriptions**

表 **7-16. USER_CONFIG1 Register Field Descriptions (continued)**

7.6.1.4 USER_CONFIG2 Register (Offset = 06h) [reset = 100h]

USER_CONFIG2 is shown in $\boxed{8}$ 7-26 and described in $\frac{1}{\sqrt{6}}$ 7-17.

Return to Summary Table.

图 **7-26. USER_CONFIG2 Register**

表 **7-17. USER_CONFIG2 Register Field Descriptions**

表 **7-17. USER_CONFIG2 Register Field Descriptions (continued)**

7.6.1.5 SUPPLY_INT_EN Register (Offset = 08h) [reset = 2AAAh]

SUPPLY_INT_EN is shown in 图 7-27 and described in 表 7-18.

Return to Summary Table.

图 **7-27. SUPPLY_INT_EN Register**

表 **7-18. SUPPLY_INT_EN Register Field Descriptions**

表 **7-18. SUPPLY_INT_EN Register Field Descriptions (continued)**

7.6.1.6 BOOST_INT_EN Register (Offset = 0Ah) [reset = A028h]

BOOST_INT_EN is shown in 图 7-28 and described in 表 7-19.

Return to Summary Table.

图 **7-28. BOOST_INT_EN Register**

表 **7-19. BOOST_INT_EN Register Field Descriptions**

表 **7-19. BOOST_INT_EN Register Field Descriptions (continued)**

7.6.1.7 LED_INT_EN Register (Offset = 0Ch) [reset = AAh]

LED_INT_EN is shown in $\boxed{8}$ 7-29 and described in $\frac{1}{\sqrt{6}}$ 7-20.

Return to Summary Table.

表 **7-20. LED_INT_EN Register Field Descriptions**

表 **7-20. LED_INT_EN Register Field Descriptions (continued)**

7.6.1.8 SUPPLY_STATUS Register (Offset = 0Eh) [reset = 0h]

SUPPLY_STATUS is shown in 图 7-30 and described in 表 7-21.

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表 **7-21. SUPPLY_STATUS Register Field Descriptions**

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表 **7-21. SUPPLY_STATUS Register Field Descriptions (continued)**

7.6.1.9 BOOST_STATUS Register (Offset = 10h) [reset = 0h]

BOOST_STATUS is shown in $\boxed{8}$ 7-31 and described in $\frac{1}{\sqrt{6}}$ 7-22.

Return to Summary Table.

图 **7-31. BOOST_STATUS Register**

表 **7-22. BOOST_STATUS Register Field Descriptions**

表 **7-22. BOOST_STATUS Register Field Descriptions (continued)**

7.6.1.10 LED_STATUS Register (Offset = 12h) [reset = 0h]

LED_STATUS is shown in $\overline{\mathbb{R}}$ 7-32 and described in $\overline{\mathbb{R}}$ 7-23.

Return to Summary Table.

图 **7-32. LED_STATUS Register**

表 **7-23. LED_STATUS Register Field Descriptions**

表 **7-23. LED_STATUS Register Field Descriptions (continued)**

7.6.1.11 FSM_DIAGNOSTICS Register (Offset = 14h) [reset = 0h]

FSM_DIAGNOSTICS is shown in \boxtimes 7-33 and described in $\ddot{\otimes}$ 7-24.

Return to Summary Table.

表 **7-24. FSM_DIAGNOSTICS Register Field Descriptions**

7.6.1.12 PWM_INPUT_DIAGNOSTICS Register (Offset = 16h) [reset = 0h]

PWM_INPUT_DIAGNOSTICS is shown in $\boxed{8}$ 7-34 and described in $\frac{1}{\sqrt{6}}$ 7-25.

Return to Summary Table.

图 **7-34. PWM_INPUT_DIAGNOSTICS Register**

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图 **7-34. PWM_INPUT_DIAGNOSTICS Register (continued)**

R-0h

表 **7-25. PWM_INPUT_DIAGNOSTICS Register Field Descriptions**

7.6.1.13 PWM_OUTPUT_DIAGNOSTICS Register (Offset = 18h) [reset = 0h]

PWM_OUTPUT_DIAGNOSTICS is shown in $\boxed{8}$ 7-35 and described in $\frac{1}{\mathcal{R}}$ 7-26.

Return to Summary Table.

图 **7-35. PWM_OUTPUT_DIAGNOSTICS Register**

表 **7-26. PWM_OUTPUT_DIAGNOSTICS Register Field Descriptions**

7.6.1.14 LED_CURR_DIAGNOSTICS Register (Offset = 1Ah) [reset = 0h]

LED_CURR_DIAGNOSTICS is shown in $\boxed{8}$ 7-36 and described in $\frac{1}{\sqrt{6}}$ 7-27.

Return to Summary Table.

图 **7-36. LED_CURR_DIAGNOSTICS Register**

表 **7-27. LED_CURR_DIAGNOSTICS Register Field Descriptions**

7.6.1.15 ADAPT_BOOST_DIAGNOSTICS Register (Offset = 1Ch) [reset = 0h]

ADAPT_BOOST_DIAGNOSTICS is shown in $\boxed{8}$ 7-37 and described in $\frac{1}{\sqrt{6}}$ 7-28.

Return to Summary Table.

图 **7-37. ADAPT_BOOST_DIAGNOSTICS Register**

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图 **7-37. ADAPT_BOOST_DIAGNOSTICS Register (continued)**

VBOOST_STATUS

R-0h

表 **7-28. ADAPT_BOOST_DIAGNOSTICS Register Field Descriptions**

7.6.1.16 AUTO_DETECT_DIAGNOSTICS Register (Offset = 1Eh) [reset = 0h]

AUTO_DETECT_DIAGNOSTICS is shown in $\boxed{8}$ 7-38 and described in $\frac{1}{\sqrt{6}}$ 7-29.

Return to Summary Table.

图 **7-38. AUTO_DETECT_DIAGNOSTICS Register**

表 **7-29. AUTO_DETECT_DIAGNOSTICS Register Field Descriptions**

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表 **7-29. AUTO_DETECT_DIAGNOSTICS Register Field Descriptions (continued)**

8 Application and Implementation

Note

以下应用部分中的信息不属于 TI 器件规格的范围,TI 不担保其准确性和完整性。TI 的客 户应负责确定 器件是否适用于其应用。客户应验证并测试其设计,以确保系统功能。

8.1 Application Information

The LP8864S-Q1 device is designed for automotive applications, and an input voltage V_{IN} is intended to be connected to the vehicle battery. Depending on the input voltage, the device may be used in either boost mode or SEPIC mode. The device is internally powered from the VDD pin, and voltage must be in 2.7-V to 5.5-V range. The device has flexible configurability through external components or by an I2C interface. If the VDD voltage is not high enough to drive an external nMOSFET gate, an internal charge pump must be used to power the gate driver (GD pin).

8.2 Typical Applications

8.2.1 Full Feature Application for Display Backlight

 \boxtimes 8-1 shows a full application for the LP8864S-Q1 device in a boost topology. It supports 6 LED strings in display mode, each at 150 mA, with an automatic 60° phase shift. Brightness control register is used for LED dimming method through I2C communication. The charge pump is enabled for a 400-kHz boost switching frequency with spread spectrum.

图 **8-1. Full Feature Application for Display Backlight**

8.2.1.1 Design Requirements

This typical LED-driver application is designed to meet the parameters listed in $\frac{1}{\mathcal{R}}$ 8-1:

表 **8-1. LP8864S-Q1 Full-Feature Design Parameters**

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表 **8-1. LP8864S-Q1 Full-Feature Design Parameters (continued)**

8.2.1.2 Detailed Design Procedure

8.2.1.2.1 Inductor Selection

There are a few things to consider when choosing an inductor: inductance, current rating, and DC resistance (DCR). 表 8-2 shows recommended inductor values for each operating frequency. The LP8864S-Q1 device automatically sets internal boost compensation controls depending on the selected switching frequency.

表 **8-2. Inductance Values for Boost Switching Frequencies**

The current rating of inductor must be at least 25% higher than maximum boost switching current $I_{SW(max)}$, which can be calculated with Equation 21. TI recommends to use an inductor with low DCR to achieve good efficiency. Efficiency varies with load condition, switching frequency, and components. 80% can be used as a typical estimation. 65% efficiency needs to take into account in extreme condition.

$$
I_{SW(max)} = \frac{\Delta I_L}{2} + \frac{I_{OUT(max)}}{1 - D}
$$

where

- $\Delta I_L = V_{IN(min)} \times D / f_{SW} \times L$
- $D = 1 V_{IN(min)} \times n / V_{OUT}$
- I_{SW(max)}: Maximum switching current
- ΔI_1 : Inductor ripple current
- \cdot I_{OUT(max}): Maximum output current
- D: Boost duty cycle
- $V_{IN(min)}$: Minimum input voltage

(21)

- f_{SW} : Minimum switching frequency of the converter
- L: Inductance
- V_{OUT} : Output voltage
- η: Efficiency of boost converter

8.2.1.2.2 Output Capacitor Selection

Recommended voltage rating for output capacitors is 50% higher than maximum output voltage level. Capacitance value determines voltage ripple and boost stability. The DC-bias effect can reduce the effective capacitance significantly, by up to 80%, a consideration for capacitance value selection. The conservative target effective capacitance is 50 µF to achieve good phase and gain margin levels. A design table in product webpage could be refered for the target effective capacitance in a certain application. TI recommends using 33-µF Alpolymer electrolytic capacitor together with 10-µF ceramic capacitors in parallel to reduce ripple, increase stability, and reduce ESR effect.

8.2.1.2.3 Input Capacitor Selection

Recommended input capacitance is the same as output capacitance although input capacitors are not as critical to boost operation. Input capacitance can be reduced but must ensure enough filtering for input power.

8.2.1.2.4 Charge Pump Output Capacitor

TI recommends a ceramic capacitor with at least 10-V voltage rating for the output capacitor of the charge pump. A 10-μF capacitor can be used for most applications.

8.2.1.2.5 Charge Pump Flying Capacitor

TI recommends a ceramic capacitor with at least 10-V voltage rating for the flying capacitor of the charge pump. One 2.2- μ F capacitor connecting C1P and C1N pins can be used for most applications.

8.2.1.2.6 Output Diode

A Schottky diode must be used for the boost output diode. Current rating must be at least 25% higher than the maximum output current. Schottky diodes with a low forward drop and fast switching speeds are ideal for increasing efficiency. At maximum current, the forward voltage must be as low as possible; less than 0.5 V is recommended. Reverse breakdown voltage of the Schottky diode must be significantly larger than the output voltage, 25% higher voltage rating is recommended. Do not use ordinary rectifier diodes, because slow switching speeds and long recovery times cause efficiency and load regulation to suffer.

8.2.1.2.7 Switching FET

Gate-drive voltage for the FET is 5V. Switching FET is a critical component for determining power efficiency of the boost converter. Several aspects need to be considered when selecting switching FET such as voltage and current rating, R_{DSON}, power dissipation, thermal resistance and rise/fall times. An N type MOSFET with at least 25% higher voltage rating than maximum output voltage must be used. Current rating of switching FET should be same or higher than inductor rating. R_{DSON} must be as low as possible, less than 20 mΩ is recommended. Thermal resistance $(R_{\theta,IA})$ must also be low to dissipate heat from power loss on switching FET. In most cases, a resistance is recommended between GD pin and Switching FET's gate terminal. It could be used to control the rising/falling time of the switching FET. This gate resistance could offer the flexibility of balancing between EMC performance and efficiency.

8.2.1.2.8 Boost Sense Resistor

The R_{SENSE} resistor determines the boost overcurrent limit and is sensed every boost switching cycle. A highpower 20-mΩ resistor can be used for sensing the boost SW current and setting maximum current limit at 10 A (typical). R_{SENSE} can be increased to lower this limit and can be calculated with Equation 22. In typical condition, to avoid too much efficiency loss on RSENSE resistor, boost overcurrent limit is recommended to be set above 4A, therefore R_{SENSE} doesn't exceed 50 mΩ. Power rating can be calculated from the inductor current and sense resistor resistance value.

 mV SENSE = $\frac{1}{1000}$ $R_{\text{SENSE}} = \frac{200}{I_{\text{ROOST}}}$ $=$

where

- R_{SENSE} : boost sense resistor (m Ω)
- $I_{\text{BOOST-OCP}}$: boost overcurrent limit

8.2.1.2.9 Power-Line FET

A power line FET can be used to disconnect input power from boost input to protect the LP8864S-Q1 device and boost components in case an overcurrent event occurs. A P type MOSFET is used for the power-line FET. Voltage rating must be at least 25% higher than maximum input voltage level. Low R_{DSON} is important to reduce power loss on the FET — less than 20 mΩ is recommended. Current rating for the FET must be at least 25% higher than input peak current. Minimum Gate-to-Source voltage (V_{GS}) to turn on transistor fully must be less than minimum input voltage; use a 20-k Ω resistor between the pFET gate and source.

8.2.1.2.10 Input Current Sense Resistor

A high-power resistor can be used for sensing the boost input current. Overcurrent condition is detected when the voltage across R_{ISENSE} reaches 220 mV. Typical 20-m Ω sense resistor is used to set 11-A input current limit. Sense resistor value can be increased to lower overcurrent limit for application as needed. Power rating can be calculated from the input current and resistance value.

8.2.1.2.11 Feedback Resistor Divider

Feedback resistors R_{FB1} and R_{FB2} determine the maximum boost output level. Output voltage can be calculated as in Equation 23:

$$
V_{OUT_MAX} = \left(\frac{V_{BG}}{R_{FB2}} + I_{SEL_MAX}\right) \times R_{FB1} + V_{BG}
$$
\n(23)

where

- $V_{BG} = 1.21 V$
- $I_{\text{SEI} \text{ MAX}}$ = 38.7 µA
- R_{FB1} / R_{FB2} normal recommended range is $7 \sim 15$

8.2.1.2.12 Critical Components for Design

 \boxtimes 8-2 shows the critical part of circuitry: boost components, the LP8864S-Q1 internal charge pump for gatedriver powering, and powering/grounding of LP8864S-Q1. Schematic example is shown in \boxtimes 8-2.

(22)

图 **8-2. Critical Components for Full Feature Design**

表 **8-3. Recommended Component Values for Full Feature Design Example**

8.2.1.3 Application Curves

8.2.2 Application with Basic/Minimal Operation

The LP8864S-Q1 needs only a few external components for basic functionality if material cost and PCB area for a solution need to be minimized. In this example LP8864S-Q1 is configured with external components and no I2C communication. The power-line FET is removed, as is input current sensing. Internal charge pump is not used, and all external synchronization functions and special features are disabled. The 33-µF Al-polymer electrolytic capacitor is removed for PCB area and height limitation. And boost external compensation is used to compensate the removal of the 33-µF Al-polymer electrolytic capacitor.

图 **8-5. Minimal Solution/Minimum Components Application**

8.2.2.1 Design Requirements

This typical LED-driver application is designed to meet the parameters listed in $\frac{1}{\mathcal{R}}$ 8-4:

表 **8-4. LP8864S-Q1 Minimal Solution Design Parameters**

8.2.2.2 Detailed Design Procedure

See *Detailed Design Procedure*.

8.2.2.3 Application Curves

See *Application Curves*.

8.2.3 SEPIC Mode Application

When LED string voltage can be above and below the input voltage level, use the SEPIC configuration. In SEPIC mode, the SW pin detects a maximum voltage equal to the sum of the input and output voltages, a consideration when selecting components.

图 **8-6. SEPIC Mode with Three LEDs in Series**

8.2.3.1 Design Requirements

This typical LED-driver application is designed to meet the parameters listed in $\frac{1}{10}$ 8-5:

表 **8-5. LP8864S-Q1 SEPIC Mode Design Parameters**

8.2.3.2 Detailed Design Procedure

8.2.3.2.1 Inductor Selection

Inductance for both inductors can be selected from $\frac{1}{6}$ 8-6, depending on operating frequency for the application. Current rating is recommended to be at least 25% higher than maximum inductor peak current. Peak-to-peak ripple current can be estimated to be approximately 40% of the maximum input current and and inductor peak current can be calculated with Equation 24, Equation 25, and Equation 26:

表 **8-6. Inductance Values for SEPIC Switching Frequencies**

$$
I_{L1 (peak)} = I_{OUT} \times \frac{V_{OUT} + V_D}{V_{IN(min)}} \times \left(1 + \frac{40\%}{2}\right)
$$

where

- \cdot I_{L1(peak)}: Peak current for inductor 1
- I_{OUT}: Maximum output current
- V_{OUT}: Output voltage
- V_D : Diode forward voltage drop
- $V_{IN(min)}$: Minimum input voltage

$$
I_{L2(\text{peak})} = I_{\text{OUT}} \times \left(1 + \frac{40\%}{2}\right)
$$

where

- $I_{L2(peak)}$: Peak current for inductor 2
- $I_{OUT}:$ Maximum output current

$$
\Delta I_L = I_{IN} \times 40\% = I_{OUT} \times \frac{V_{OUT}}{V_{IN(min)}} \times 40\%
$$

where

- ΔI_L : Inductor ripple current
- I_{IN}: Input current
- V_{OUT}: Output voltage
- $V_{IN(min)}$: Minimum input voltage

8.2.3.2.2 Coupling Capacitor Selection

The coupling capacitors Cs isolate the input from the output and provide protection against a shorted load. The selection of SEPIC capacitors, Cs, depends mostly on the RMS current, which can be calculated with Equation 27. The capacitors must be rated for a large RMS current relative to the output power; TI recommends at least 25% higher rating for I_{RMS} . When using uncoupled inductors, use one 10- μ F ceramic capacitor in parallel with one 33-µF electrolytic capacitor and series 2-Ω resistor. If coupled inductors are used, then use only one 10-µF ceramic capacitor.

$$
I_{\text{Cs(rms)}} = I_{\text{OUT}} \times \sqrt{\frac{V_{\text{OUT}} + V_{\text{D}}}{V_{\text{IN(min)}}}}
$$

where

- $I_{Cs(rms)}$: RMS current of Cs capacitor
- I_{OUT}: Output current
- V_{OUT}: Output voltage
- V_D : Diode forward voltage drop
- $V_{IN(min)}$: Minimum input voltage

8.2.3.2.3 Output Capacitor Selection

See *Detailed Design Procedure*.

8.2.3.2.4 Input Capacitor Selection

See *Detailed Design Procedure*.

(27)

(24)

(25)

(26)

8.2.3.2.5 Charge Pump Output Capacitor

See *Detailed Design Procedure*.

8.2.3.2.6 Charge Pump Flying Capacitor

See *Detailed Design Procedure*.

8.2.3.2.7 Switching FET

Gate-drive voltage for the FET is 5V. Use an N-type MOSFET for the switching FET. The switching FET for SEPIC mode sees a maximum voltage of V_{IN(max)} + V_{OUT}, 25% higher rating is recommended. Current rating is also recommended to be 25% higher than peak current, which can be calculated with Equation 28. R_{DSON} must be as low as possible — less than 20 mΩ is recommended. Thermal resistance (R $_{\theta$ JA) must also be low to dissipate heat from power loss on switching FET. Typical rise/fall time values recommended are less than 10 ns.

 $I_{Q1(peak)} = I_{L1(peak)} + I_{L2(peak)}$

(28)

(29)

where

- $I_{Q1(peak)}$: Peak current for switching FET
- $I_{L1(peak)}$: Peak current for inductor 1
- I_{IL2(peak):} : Peak current for inductor 2 BOOST_OCP

8.2.3.2.8 Output Diode

A Schottky diode must be used for the SEPIC output diode. Current rating must be at least 25% higher than the maximum current, which is the same as switch peak current. Schottky diodes with a low forward drop and fast switching speeds are ideal for increasing efficiency. At maximum current, the forward voltage must be as low as possible; TI recommends less than 0.5 V. Reverse breakdown voltage of the Schottky diode must be able to withstand $V_{IN(max)}$ + $V_{OUT(max)}$; at least 25% higher voltage rating is recommended. Do not use ordinary rectifier diodes, because slow switching speeds and long recovery times cause efficiency and load regulation to suffer.

8.2.3.2.9 Switching Sense Resistor

See *Detailed Design Procedure*.

8.2.3.2.10 Power-Line FET

See *Detailed Design Procedure*.

8.2.3.2.11 Input Current Sense Resistor

See *Detailed Design Procedure*.

8.2.3.2.12 Feedback Resistor Divider

Feedback resistors R_{FB1} and R_{FB2} determine the maximum boost output level. Output voltage can be calculated as follows:

$$
V_{OUT_MAX} = \left(\frac{V_{BG}}{R_{FB2}} + I_{SEL_MAX}\right) \times R_{FB1} + V_{BG}
$$

where

- $V_{BG} = 1.21 V$
- $I_{\text{SEL MAX}} = 38.7 \mu \text{A}$
- R_{FB1} / R_{FB2} normal recommended range is 5~15 (recommended for SEPIC Mode)

8.2.3.2.13 Critical Components for Design

shows the critical part of circuitry: SEPIC components, the LP8864S-Q1 internal charge pump for gate-driver powering, and powering/grounding of LP8864S-Q1. Schematic example is shown below.

图 **8-7. SEPIC Mode with Three LEDs in Series**

表 **8-7. Recommended Components for SEPIC Design Example**

8.2.3.3 Application Curves

See *Application Curves.*

9 Power Supply Recommendations

The LP8864S-Q1 is designed to operate from a car battery. The V_{IN} input must be protected from reverse voltage and voltage dump condition over 48 V. The impedance of the input supply rail must be low enough that the input current transient does not cause drop below VIN UVLO level. If the input supply is connected with long wires, additional bulk capacitance may be required in addition to normal input capacitor.

The voltage range for V_{DD} is 3 V to 5.5 V. A ceramic capacitor must be placed as close as possible to the VDD pin. The boost gate driver is powered from the CPUMP pins. A ceramic capacitor must be placed as close to the CPUMP pins as possible.

10 Layout

10.1 Layout Guidelines

 $\overline{8}$ 10-1 shows a layout recommendation for the LP8864S-Q1 used to illustrate the principles of good layout. This layout can be adapted to the actual application layout if and where possible. It is important that all boost components are close to each other and to the chip; the high-current traces must be wide enough. VDD must be as noise-free as possible. Place a V_{DD} bypass capacitor near the VDD and GND pins. A charge-pump capacitor, boost input capacitors, and boost output capacitors must have closest VIAs to GND. Place the charge-pump capacitors close to the device. The main points to guide the PCB layout design:

- Current loops need to be minimized:
	- For low frequency the minimal current loop can be achieved by placing the boost components as close as possible to each other. Input and output capacitor grounds need to be close to each other to minimize current loop size.
	- Minimal current loops for high frequencies can be achieved by making sure that the ground plane is intact under the current traces. High frequency return currents follow the route with minimum impedance, which is the route with minimum loop area, not necessarily the shortest path. Minimum loop area is formed when return current flows just under the *positive* current route in the ground plane, if the ground plane is intact under the route.
	- For high frequency the copper area capacitance must be taken into account. For example, the copper area for the drain of boost N-MOSFET is a tradeoff between capacitance and the cooling capacity of the components.
- GND plane must be intact under the high-current-boost traces to provide shortest possible return path and smallest possible current loops for high frequencies.
- Route boost output voltage (V_{OUT}) to LEDs, FB pin & Discharge pin after output capacitors not straight from the diode cathode.
- FB network should be placed as close as possible to the FB pin, not near boost output
- A small bypass capacitor (TI recommends a 39-pF capacitor) could be placed close to the FB pin and GND to suppress high frequency noise
- VDD line must be separated from the high current supply path to the boost converter to prevent high frequency ripple affecting the chip behavior.
- Capacitor connected to charge pump output CPUMP is recommended to have 10-µF capacitance. This capacitor must be as close as possible to CPUMP pin. This capacitor provides a greater peak current for gate driver and must be used even if the charge pump is disabled. If the charge pump is disabled, the VDD and CPUMP pins must be tied together.
- Input and output capacitors need low-impedance grounding (wide traces with many vias to GND plane).
- Input/output ceramic capacitors have DC-bias effect. If the output capacitance is too low, it can cause boost to become unstable under certain load conditions. DC bias characteristics should be obtained from the component manufacturer; DC bias is not taken into account on component tolerance.

10.2 Layout Example

图 **10-1. LP8864S-Q1 Layout Guidelines**

11 Device and Documentation Support

11.1 Device Support

11.1.1 第三方产品免责声明

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ESD 的损坏小至导致微小的性能降级,大至整个器件故障。精密的集成电路可能更容易受到损坏,这是因为非常细微的参 数更改都可能会导致器件与其发布的规格不相符。

11.6 术语表

TI 术语表 本术语表列出并解释了术语、首字母缩略词和定义。

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures. "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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PACKAGE OPTION ADDENDUM

TEXAS

TAPE AND REEL INFORMATION

ISTRUMENTS

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

Pack Materials-Page 1

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PACKAGE MATERIALS INFORMATION

*All dimensions are nominal

GENERIC PACKAGE VIEW

RHB 32 VQFN - 1 mm max height

5 x 5, 0.5 mm pitch PLASTIC QUAD FLATPACK - NO LEAD

Images above are just a representation of the package family, actual package may vary. Refer to the product data sheet for package details.

4224745/A

PACKAGE OUTLINE

RHB0032T VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.

EXAMPLE BOARD LAYOUT

RHB0032T VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

NOTES: (continued)

4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).

5. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.

EXAMPLE STENCIL DESIGN

RHB0032T VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

GENERIC PACKAGE VIEW

DCP 38 PowerPAD TSSOP - 1.2 mm max height

4.4 x 9.7, 0.5 mm pitch SMALL OUTLINE PACKAGE

This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.

PACKAGE OUTLINE

DCP0038A PowerPAD[™] TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE

NOTES:

PowerPAD is a trademark of Texas Instruments.

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
- 4. Reference JEDEC registration MO-153.
- 5. Features may differ or may not be present.

EXAMPLE BOARD LAYOUT

DCP0038A PowerPAD™ TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 8. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature numbers SLMA002 (www.ti.com/lit/slma002) and SLMA004 (www.ti.com/lit/slma004).
- 9. Size of metal pad may vary due to creepage requirement.
- 10. Vias are optional depending on application, refer to device data sheet. It is recommended that vias under paste be filled, plugged or tented.

EXAMPLE STENCIL DESIGN

DCP0038A PowerPAD™ TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE

NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

12. Board assembly site may have different recommendations for stencil design.

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