

Technical documentation

TPS2597 ZHCSOF8B – NOVEMBER 2021 – REVISED JANUARY 2022

TPS2597xx 具有精确电流监视器和瞬态过流消隐功能的 **2.7V** 至 **23V**、**7A**、**9.8mΩ** 电子保险丝

1 特性

- 宽工作输入电压范围:2.7V 至 23V – 绝对最大值为 28V
- 具有低导通电阻的集成 FET:R_{ON} = 9.8mΩ(典型 值)
- 快速过压保护
	- 过压钳位 (OVC),可通过引脚选择阈值 (3.89V、5.76V、13.88V),响应时间为 5μs (典型值),或
	- 可调节过压锁定 (OVLO),响应时间为 1.2μs (典型值)
- 过流保护,具有负载电流监控器输出 (ILM)
	- 主动电流限制或断路器选项
	- 可调节阈值 (I_{LIM}) : 0.87A 至 7.7A
		- I_{LIM} > 1.74 A 时精度为 ±10%
	- 可调瞬态消隐计时器 (ITIMER),支持高达 2 × l_{LIM} 的峰值电流
- 输出负载电流监控精度:±8%(最大值)
- 通过快速跳变响应实现短路保护
- 响应时间为 550ns(典型值)
- 可调节 (2 × I_{LIM}) 和固定阈值
- 带有可调节欠压锁定阈值 (UVLO) 的高电平有效使 能输入
- 可调节的输出压摆率控制 (dVdt)
- 过热保护
- 数字输出
	- 故障指示 (FLT) 或
	- 具有可调节阈值 (PGTH) 的电源正常状态指示 (PG)
- UL2367 认证(正在申请中)
- IEC 62368 CB 认证(正在申请中)
- 小尺寸:QFN 2mm × 2mm,0.45mm 间距

2 应用

- 服务器、PC 主板和插件卡
- 企业级存储 RAID/HBA/SAN/eSSD
- 患者监护仪
- 电器和电动工具
- 零售销售点终端
- 智能手机和平板电脑

3 说明

TPS2597xx 系列电子保险丝是采用小型封装的高度集 成电路保护和电源管理解决方案。此类器件只需很少的 外部元件即可提供多种保护模式,能够非常有效地抵御 过载、短路、电压浪涌和过多浪涌电流。

可以使用单个外部电容器来调节输出压摆率和浪涌电 流。通过将输出钳制到安全的固定最大电压(可通过引 脚选择)或在输入超过可调过压阈值时切断输出,可以 保护负载免受输入过压情况的影响。此类器件通过主动 限制电流或断开电路来响应输出过载。用户可以调节输 出电流限制阈值以及瞬态过流消隐计时器。电流限制控 制引脚还用作模拟负载电流监控器。

器件采用 2mm × 2mm 10 引脚 HotRod™ QFN 封装, 旨在改善热性能并减小系统尺寸。

这些器件的额定工作结温范围为 -40°C 至 +125°C。

(1) 如需了解所有可用封装,请参阅数据表末尾的可订购产品附 录。

简化版原理图

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4 Revision History

注:以前版本的页码可能与当前版本的页码不同

5 Device Comparison Table

6 Pin Configuration and Functions

图 **6-1. TPS2597xx RPW Package 10-Pin QFN (Top View)**

表 **6-1. Pin Functions**

7 Specifications

7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) (1)

(1) Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

7.2 ESD Ratings

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

(1) For TPS25972x OVC variants, the input operating voltage must be limited to the selected Output Voltage Clamp Option as listed in the Electrical Characteristics section.

(2) For supply voltages below 5 V, it is okay to pull up the EN pin to IN directly. For supply voltages greater than 5 V, TI recommends to use a resistor divider with a minimum pullup resistor value of 350 kΩ.

7.4 Thermal Information

(1) For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.

(2) Based on simulations conducted with the device mounted on a custom 4-layer PCB (2s2p) with 8 thermal vias under device.

 (3) Based on simulations conducted with the device mounted on a JEDEC 4-layer PCB $(2s2p)$ with no thermal vias under device.

7.5 Electrical Characteristics

(Test conditions unless otherwise noted) –40°C ≤ T」≤ 125°C, V_{IN} = 12 V, OUT = Open, V_{EN/UVLO} = 2 V, V_{OVLO} = 0 V for TPS25970x/4x, OVCSEL = 390 kΩ to GND for TPS25972x, R_{ILM} = 715 Ω , dVdT = Open, ITIMER = Open, FLT = Open for TPS25970x, PGTH = Open for TPS25972x/4x, PG = Open for TPS25972x/4x. All voltages referenced to GND.

7.5 Electrical Characteristics (continued)

(Test conditions unless otherwise noted) –40°C ≤ T」≤ 125°C, V_{IN} = 12 V, OUT = Open, V_{EN/UVLO} = 2 V, V_{OVLO} = 0 V for TPS25970x/4x, OVCSEL = 390 kΩ to GND for TPS25972x, R_{ILM} = 715 Ω , dVdT = Open, ITIMER = Open, FLT = Open for TPS25970x, PGTH = Open for TPS25972x/4x, PG = Open for TPS25972x/4x. All voltages referenced to GND.

7.6 Timing Requirements

7.7 Switching Characteristics

The output rising slew rate is internally controlled and constant across the entire operating voltage range to ensure the turn on timing is not affected by the load conditions. The rising slew rate can be adjusted by adding capacitance from the dVdt pin to ground. As C_{dVdt} is increased it will slow the rising slew rate (SR). See Slew Rate and Inrush Current Control (dVdt) section for more details. The Turn-Off Delay and Fall Time, however, are dependent on the RC time constant of the load capacitance (C_{OUT}) and Load Resistance (R_L). The Switching Characteristics are only valid for the power-up sequence where the supply is available in steady state condition and the load voltage is completely discharged before the device is enabled. Typical values are taken at Tյ = 25°C unless specifically noted otherwise. R_L = 100 Ω, C_{OUT} = 1 µF.

7.8 Typical Characteristics

8 Detailed Description

8.1 Overview

The TPS2597xx is an eFuse with an integrated power path that is used to ensure safe power delivery in a system. The device starts its operation by monitoring the IN bus. When the input supply voltage (V_{N}) exceeds the undervoltage protection threshold (V_{UVP}), the device samples the EN/UVLO pin. A high level (> V_{UVLO}) on this pin enables the internal power path (HFET) to start conducting and allow current to flow from IN to OUT. When EN/UVLO is held low (< V_{UVLO}), the internal power path is turned off.

After a successful start-up sequence, the device now actively monitors its load current and input voltage, and controls the internal HFET to ensure that the user adjustable overcurrent limit threshold (I_{LIM}) is not exceeded and overvoltage spikes are either safely clamped to the selected threshold voltage (V_{OVC}) or cut-off after they cross the user-adjustable overvoltage lockout threshold (V_{OVLO}). The device also provides fast protection against severe overcurrent during short-circuit events. This feature keeps the system safe from harmful levels of voltage and current. At the same time, a user-adjustable overcurrent blanking timer allows the system to pass moderate transient peaks in the load current profile without tripping the eFuse. This action ensures a robust protection solution against real faults which is also immune to transients, thereby ensuring maximum system uptime.

The device also has a built-in thermal sensor based shutdown mechanism to protect itself in case the device temperature $\left(\mathsf{T}_{\mathsf{J}}\right)$ exceeds the recommended operating conditions.

8.2 Functional Block Diagram

图 **8-1. TPS25970x Block Diagram**

Not applicable to Latch-off variants (TPS25972L)

图 **8-2. TPS25972x Block Diagram**

Not applicable to Latch-off variants (TPS25974L)

8.3 Feature Description

The TPS2597xx eFuse is a compact, feature-rich power management device that provides detection, protection, and indication in the event of system faults.

8.3.1 Undervoltage Lockout (UVLO and UVP)

The TPS2597xx implements undervoltage protection on IN in case the applied voltage becomes too low for the system or device to properly operate. The undervoltage protection has a default lockout threshold of V_{UVP} which is fixed internally. Also, the UVLO comparator on the EN/UVLO pin allows the undervoltage protection threshold to be externally adjusted to a user-defined value. 图 8-4 and 方程式 1 show how a resistor divider can be used to set the UVLO set point for a given voltage supply.

图 **8-4. Adjustable Undervoltage Protection**

8.3.2 Overvoltage Lockout (OVLO)

The TPS25970x and TPS25974x variants allow the user to implement overvoltage lockout to protect the load from input overvoltage conditions. The OVLO comparator on the OVLO pin allows the overvoltage protection threshold to be adjusted to a user-defined value. After the voltage at the OVLO pin crosses the OVLO rising threshold, $V_{\text{OV(R)}}$, the device turns off the power to the output. Thereafter, the devices wait for the voltage at the OVLO pin to fall below the OVLO falling threshold, $V_{\text{OV}(F)}$ before the output power is turned ON again. The rising and falling thresholds are slightly different to provide hysteresis. 图 8-5 and 方程式 2 show how a resistor divider can be used to set the OVLO set point for a given voltage supply.

图 **8-5. Adjustable Overvoltage Protection**

$$
VIN(OV) = \frac{VOV \times (R1 + R2)}{R2}
$$
 (2)

While recovering from a OVLO event, the TPS25970x variants start up with inrush control (dVdt).

While recovering from an OVLO event, the TPS25974x variants start up with inrush control (dVdt).

图 **8-7. TPS25974x Overvoltage Lockout and Recovery**

8.3.3 Overvoltage Clamp (OVC)

The TPS25972x variants implement a voltage clamp on the output to protect the system in the event of input overvoltage. When the device detects the input has exceeded the overvoltage clamp threshold (V_{OVC}), it quickly responds within t_{OVC} and stops the output from rising further. the device then regulates the HFET linearly to clamp the output voltage below V_{ClAMP} as long as an overvoltage condition is present on the input.

If the part stays in clamping state for an extended period of time, there is higher power dissipation inside the part which can eventually lead to thermal shutdown (TSD). After the part shuts down due to TSD fault, it either

stays latched off (TPS25972L variant) or restart automatically after a fixed delay (TPS25972A variant). See *Overtemperature Protection (OTP)* for more details on device response to overtemperature.

(1) Applicable only for TPS25972A (Auto-retry variant)

图 **8-8. TPS25972x Overvoltage Response (Auto-Retry)**

There are three available overvoltage clamp threshold options, which can be configured using the OVCSEL pin.

表 **8-1. TPS25972x Overvoltage Clamp Threshold Selection**

8.3.4 Inrush Current, Overcurrent, and Short Circuit Protection

TPS2597xx incorporates four levels of protection against overcurrent:

- 1. Adjustable slew rate (dVdt) for inrush current control
- 2. Adjustable threshold (I_{LIM}) for overcurrent protection during start-up or steady-state
- 3. Adjustable threshold (I_{SC}) for fast-trip response to severe overcurrent during start-up or steady-state
- 4. Fixed threshold (I_{FT}) for fast-trip response to quickly protect against hard output short-circuits during steadystate

8.3.4.1 Slew Rate (dVdt) and Inrush Current Control

During hot-plug events or while trying to charge a large output capacitance at start-up, there can be a large inrush current. If the inrush current is not managed properly, it can damage the input connectors or cause the system power supply to droop leading to unexpected restarts elsewhere in the system or both. The inrush current during turn on is directly proportional to the load capacitance and rising slew rate. Use 方程式 3 to find the slew rate (SR) required to limit the inrush current (I_{INRUSH}) for a given load capacitance (C_{OUT}):

$$
SR (V/ms) = \frac{INRUSH (mA)}{COUT (\mu F)}
$$
 (3)

A capacitor can be connected to the dVdt pin to control the rising slew rate and lower the inrush current during turn on. Use 方程式 4 to calulate the required C_{dVdt} capacitance to produce a given slew rate.

$$
C dV dt \left(pF \right) = \frac{3300}{SR (V/ms)} \tag{4}
$$

The fastest output slew rate is achieved by leaving the dVdt pin open.

备注

For C_{dVdt} > 10 nF, TI recommends to add a 100- Ω resistor in series with the capacitor on the dVdt pin.

8.3.4.2 Circuit-Breaker

The circuit-breaker variants (TPS25974x) respond to output overcurrent conditions by turning off the output after a user-adjustable transient fault blanking interval. When the load current exceeds the set overcurrent threshold (I_{LIM}) set by the ILM pin resistor (R_{ILM}), but stays lower than the fast-trip threshold (2 × I_{LIM}), the device starts discharging the ITIMER pin capacitor using an internal 2-μA pulldown current. If the load current drops below I_{LIM} before the ITIMER pin capacitor (C_{ITIMER}) discharges by ΔV_{ITIMER}, the ITIMER is reset by pulling it up to V_{INT} internally and the circuit breaker action is not engaged. This action allows short load transient pulses to pass through the device without tripping the circuit. If the overcurrent condition persists, the C_{ITIMER} continues to discharge and after it discharges by ΔV_{ITIMER} , the circuit breaker action turns off the HFET immediately. At the same time, the C_{ITIMER} is charged up to V_{INT} again so that it is at its default state before the next overcurrent event. This action ensures the full blanking timer interval is provided for every overcurrent event. Use 方程式 5 to calculate the R_{ILM} value for an overcurrent threshold.

$$
RILM (\Omega) = \frac{5747}{ILIM (A)}
$$

(5)

备注

- 1. Leaving the ILM pin Open sets the current limit to nearly zero and results in the part breaking the circuit with the slightest amount of loading at the output.
- 2. Shorting the ILM pin to ground at any point during normal operation is detected as a fault and the part shuts down. There is a minimum current (I_{FLT}) which the part allows in this condition before the pin short condition is detected.

The duration for which transients are allowed can be adjusted using an appropriate capacitor value from ITIMER pin to ground. Use 方程式 6 to calculate the C_{ITIMER} value needed to set the desired transient overcurrent blanking interval.

tITIMER (ms) = $\frac{\Delta VITIMER(V) \times CITIMER(nF)}{IITIMER(\mu A)}$ (6)

备注

- 1. Leave the ITIMER pin open to allow the part to break the circuit with the minimum possible delay.
- 2. Shorting the ITIMER pin to ground results in minimum overcurrent response delay (similar to ITIMER pin open condition), but increases the device current consumption. This action is not a recommended mode of operation.
- 3. Increasing the ITIMER cap value extends the overcurrent blanking interval, but it also extends the time needed for the ITIMER cap to recharge up to V_{INT} . If the next overcurrent event occurs before the ITIMER cap is recharged fully, it takes less time to discharge to the ITIMER expiry threshold, thereby providing a shorter blanking interval than intended.

After the part shuts down due to a circuit-breaker fault, it either stays latched off (TPS25974L variant) or restart automatically after a fixed delay (TPS25974A variant).

8.3.4.3 Active Current Limiting

The active current limit variants (TPS25970x and TPS25972x) respond to output overcurrent conditions by actively limiting the current after a user adjustable transient fault blanking interval. When the load current exceeds the set overcurrent threshold (I_{LIM}) set by the ILM pin resistor (R_{ILM}), but stays lower than the short-circuit threshold $(2 \times I_{LM})$, the device starts discharging the ITIMER pin capacitor using an internal 2-µA pulldown current. If the load current drops below the overcurrent threshold before the ITIMER capacitor (C_{ITIMER}) discharges by ΔV_{ITIMER} , the ITIMER is reset by pulling it up to V_{INT} internally and the current limit action is not engaged. This event allows short load transient pulses to pass through the device without getting current limited. If the overcurrent condition persists, the C_{ITIMER} continues to discharge and after it discharges by ΔV_{ITIMER} , the current limit starts regulating the HFET to actively limit the current to the set overcurrent threshold (I_{LIM}) . At the same time, the C_{ITIMER} is charged up to V_{INT} again so that it is at its default state before the next overcurrent event. This event ensures the full blanking timer interval is provided for every overcurrent event. Use 方程式 7 to calculate the R_{ILM} value for a desired overcurrent threshold.

$$
RILM (\Omega) = \frac{5747}{ILIM (A)}
$$

(7)

备注

- 1. Leaving the ILM pin open sets the current limit to nearly zero and results in the part entering current limit with the slightest amount of loading at the output.
- 2. The current limit circuit employs a foldback mechanism. The current limit threshold in the foldback region (0 V < V_{OUT} < V_{FB}) is lower than the steady state current limit threshold (I_{LIM}).
- 3. Shorting the ILM pin to ground at any point during normal operation is detected as a fault and the part shuts down. There's a minimum current (I_{FLT}) which the part allows in this condition before the pin short condition is detected.

The duration for which transients are allowed can be adjusted using an appropriate capacitor value from ITIMER pin to ground. Use 方程式 8 to calculate the C_{ITIMER} value needed to set the desired transient overcurrent blanking interval.

tITIMER (ms) = $\frac{\Delta VITIMER(V) \times CTIMER(nF)}{IITIMER(\mu A)}$ (8)

 1 Applicable only to TPS25972x and TPS25974x variants (2) Applicable only to $T = 25$ and (2) Applicable only to TPS25970x variants

图 **8-10. TPS25970x and TPS25972x Active Current Limit Response**

备注

- 1. Leave the ITIMER pin open to allow the part to limit the current with the minimum possible delay.
- 2. Shorting the ITIMER pin to ground results in minimum overcurrent response delay (similar to ITIMER pin open condition), but increases the device current consumption. This action is not a recommended mode of operation.
- 3. Active current limiting based on R_{ILM} is active during start-up for TPS25970x, TPS25972x (active current limit) as well as TPS25974x (circuit-breaker) variants. In case the start-up current exceeds I_{LIM} , the device regulates the current to the set limit. However, during start-up the current limit is engaged without waiting for the ITIMER delay.
- 4. For the TPS25972x variants, during overvoltage clamp condition, if an overcurrent event occurs, the current limit is engaged without waiting for the ITIMER delay.
- 5. Increasing the C_{ITIMER} value extends the overcurrent blanking interval, but it also extends the time needed for the C_{ITIMER} to recharge up to V_{INT} . If the next overcurrent event occurs before the C_{ITIMER} is recharged fully, it takes lesser time to discharge to the ITIMER expiry threshold, thereby providing a shorter blanking interval than intended.

During active current limit, the output voltage drops, resulting in increased device power dissipation across the HFET. If the device internal temperature (T $_{\rm J}$) exceeds the thermal shutdown threshold (TSD), the HFET is turned off. After the part shuts down due to TSD fault, it either stays latched off (TPS2597xL variants) or restarts automatically after a fixed delay (TPS2597xA variants). See *Overtemperature Protection (OTP)* for more details on device response to overtemperature.

8.3.4.4 Short-Circuit Protection

During an output short-circuit event, the current through the device increases very rapidly. When a severe overcurrent condition is detected, the device triggers a fast-trip response to limit the current to a safe level. The internal fast-trip comparator employs a scalable threshold (I_{SC}) which is equal to 2 × I_{LIM} . This action enables the user to adjust the fast-trip threshold rather than using a fixed threshold which can be too high for some low current systems. The device also employs a fixed fast-trip threshold (I_{FT}) to protect fast protection against hard short-circuits during steady state. The fixed fast-trip threshold is higher than the maximum recommended user adjustable scalable fast-trip threshold. After the current exceeds I_{SC} or I_{FT} , the HFET is turned off completely within t_{FT}. Thereafter, the devices tries to turn the HFET back on after a short de-glitch interval (30 µs) in a current limited manner instead of a dVdt limited manner. This action ensures that the HFET has a faster recovery after a transient overcurrent event and minimizes the output voltage droop. However, if the fault is persistent, the device stays in current limit causing the junction temperature to rise and eventually enter thermal shutdown. For details on the device response to overtemperature, see *Overtemperature Protection (OTP)*.

8.3.5 Analog Load Current Monitor

The device allows the system to accurately monitor the output load current by providing an analog current sense output on the ILM pin, which is proportional to the current through the FET. The user can sense the voltage (V_{ILM}) across the R_{ILM} to get a measure of the output load current.

$$
IOUT (A) = \frac{VILM (\mu V)}{RILM (\Omega) \times GIMON (\mu A/A)}
$$
\n(9)

The waveform below shows the ILM signal response to a load step at the output.

 V_{IN} = 12 V, R_{ILM} = 715 Ω, I_{OUT} varied dynamically between 0 A and 5.5 A

图 **8-12. Analog Load Current Monitor Response**

备注 The ILM pin is sensitive to capacitive loading. Careful design and layout is needed to ensure the parasitic capacitive loading on the ILM pin is < 50 pF for stable operation.

8.3.6 Overtemperature Protection (OTP)

The device monitors the internal die temperature $(\mathsf{T}_{\mathsf{J}})$ at all times and shuts down the part as soon as the temperature exceeds a safe operating level (TSD), thereby protecting the device from damage. The device does not turn back on until the junction cools down sufficiently, that is the die temperature falls below (TSD – TSD_{HYS}).

When the TPS2597xL (latch-off variant) detects thermal overload, it shuts down and remains latched-off until the device is power cycled or re-enabled. When the TPS2597xA (auto-retry variant) detects thermal overload, it remains off until it has cooled down by TSD_{HYS} . Thereafter, the device remains off for an additional delay of t_{RST} after which it automatically retries to turn on if it is still enabled.

表 **8-2. Thermal Shutdown**

8.3.7 Fault Response and Indication (FLT)

表 8-3 summarizes the device response to various fault conditions. Additionally, an active low external fault indication (FLT) pin is available on the TPS25970x variants.

表 **8-3. Fault Summary**

表 **8-3. Fault Summary (continued)**

(1) Applicable to TPS25970x variants only.

(2) Applicable to TPS25972x variants only.

(3) Applicable to TPS25974x variants only.

(4) Applicable to TPS25970x and TPS25972x variants only.

Faults which are latched internally can be cleared either by power cycling the part (pulling V_{IN} to 0 V) or by pulling the EN/UVLO pin voltage below V_{SD} . This action also releases the FLT pin for the TPS25970x variants and resets the t_{RST} timer for the TPS2597xA (auto-retry) variants.

During a latched fault, pulling the EN/UVLO just below the UVLO threshold has no impact on the device. This fact is true for both TPS2597xL (latch-off) and TPS2597xA (auto-retry) variants.

For TPS2597xA (auto-retry) variants, on expiry of the t_{RST} timer after a fault, the device restarts automatically and the FLT pin is de-asserted (TPS25970A variant).

8.3.8 Power-Good Indication (PG)

The TPS25972x and TPS25974x variants provide an active high digital output (PG) which serves as a powergood indication signal and is asserted high depending on the voltage at the PGTH pin along with the device state information. The PG is an open-drain pin and must be pulled up to an external supply.

After power up, PG is pulled low initially. The device initiates a inrush sequence in which the HFET is turned on in a controlled manner. When the HFET gate voltage reaches the full overdrive indicating that the inrush sequence is complete and the voltage at PGTH is above $V_{PGTH(R)}$, the PG is asserted after a de-glitch time (t_{PGA}) .

PG is de-asserted if at any time during normal operation, the voltage at PGTH falls below $V_{PGTH(F)}$, or the device detects a fault (except overcurrent). The PG de-assertion de-glitch time is t_{PGD}.

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When there is no supply to the device, the PG pin is expected to stay low. However, there is no active pulldown in this condition to drive this pin all the way down to 0 V. If the PG pin is pulled up to an independent supply which is present even if the device is unpowered, there can be a small voltage seen on this pin depending on the pin sink current, which is a function of the pullup supply voltage and resistor. Minimize the sink current to keep this pin voltage low enough not to be detected as a logic HIGH by associated external circuits in this condition.

8.4 Device Functional Modes

The TPS25970x and TPS25974x variants have only one functional mode that applies when operated within the recommended operating conditions.

The TPS25972x variants have three different functional modes depending on the OVCSEL pin connection.

OVCSEL PIN CONNECTION OVERVOLTAGE CLAMP THRESHOLD Shorted to GND 3.89 V Open 5.76 V Connected to GND through a 390-kΩ resistor 13.88 V

表 **8-5. TPS25972x Overvoltage Clamp Threshold Selection**

9 Application and Implementation

备注

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

9.1 Application Information

The TPS2597xx is a 2.7-V to 23-V, 7-A eFuse that is typically used for power rail protection applications. The device operates from 2.7 V to 23 V with adjustable overvoltage and undervoltage protection. The device provides ability to control inrush current and protection against overcurrent conditions. The device can be used in a variety of systems such as adapter input protection, server, PC motherboard, add-on cards, enterprise storage – RAID/HBA/SAN/eSSD, retail point-of-sale terminals, smartphones, and tablets. The design procedure explained in the subsequent sections can be used to select the supporting component values based on the application requirement. Additionally, a spreadsheet design tool, *TPS2597xx Design Calculator*, is available in the web product folder.

9.1.1 Single Device, Self-Controlled

图 **9-1. Single Device, Self-Controlled**

Other variations:

In a Host MCU controlled system, EN/UVLO or OVLO can also be driven from the host GPIO to control the device.

ILM pin can be connected to the MCU ADC input for current monitoring purpose.

备注

TI recommends to keep parasitic capacitance on ILM pin below 50 pF to ensure stable operation.

For the TPS25972x and TPS25974x variants, either V_{IN} or V_{OUT} can be used to drive the PGTH resistor divider depending on which supply must be monitored for Power Good indication.

9.2 Typical Application

TPS2597xx can be used for server add-on card input power protection. During overcurrent or short-circuit event at load side, TPS2597xx can quickly respond to this fault event by turning off the device and thus protect the load from damage as well as prevent input supply from drooping. The ITIMER feature allows short duration peak currents to pass through without tripping the eFuse, thereby meeting the transient load current profile of these cards.

* Optional circuit components needed for transient protection depending on input and output inductance. Please refer to *Transient Protection* section for details.

图 **9-2. Server Add-on Card Input Power Protection**

9.2.1 Design Requirements

表 **9-1. Design Parameters**

9.2.2 Detailed Design Procedure

9.2.2.1 Device Selection

Because the application requires circuit-breaker response to overcurrent with latch-off response after a fault, the TPS25974L variant is selected after referring to the *Device Comparison Table*.

9.2.2.2 Setting Undervoltage and Overvoltage Thresholds

The supply undervoltage and overvoltage thresholds are set using the resistors R1, R2, and R3, whose values can be calculated using 方程式 10 and 方程式 11:

$$
VIN(UV) = \frac{VUVLO(R) \times (R1 + R2 + R3)}{R2 + R3}
$$
\n(10)

$$
VIN(0V) = \frac{VON(N) \times (N + N2 + N3)}{R3}
$$
\nWhere V_{UVLO(R)} is the UVLO rising threshold and V_{OV(R)} is the OVLO rising threshold. Because R1, R2, and R3

leak the current from input supply V_{IN} , these resistors must be selected based on the acceptable leakage current from input power supply V_{IN}. The current drawn by R1, R2, and R3 from the power supply is IR123 = V_{IN} / (R1 + R2 + R3). However, leakage currents due to external active components connected to the resistor string can add error to these calculations. So, the resistor string current, IR123 must be chosen to be 20 times greater than the leakage current expected on the EN/UVLO and OVLO pins.

From the device electrical specifications, both the EN/UVLO and OVLO leakage currents are 0.1 μA (maximum), $V_{\text{OV(R)}}$ = 1.2 V and $V_{\text{UVLO(R)}}$ = 1.2 V. From design requirements, $V_{\text{IN(OV)}}$ = 13.2 V and $V_{\text{IN(UV)}}$ = 10.8 V. To solve the equation, first choose the value of R1 = 470 kΩ and use the above equations to solve for R2 = 10.7 kΩ and $R3 = 48$ kΩ.

Using the closest standard 1% resistor values, we get R1 = 470 kΩ, R2 = 11 kΩ, and R3 = 47 kΩ.

9.2.2.3 Setting Output Voltage Rise Time (tR)

For a successful design, the junction temperature of the device must be kept below the absolute maximum rating during both dynamic (start-up) and steady-state conditions. Dynamic power stresses often are an order of magnitude greater than the static stresses, so it is important to determine the right start-up time and inrush current limit required with system capacitance to avoid thermal shutdown during start-up.

The slew rate (SR) needed to achieve the desired output rise time can be calculated as:

$$
SR (V/ms) = \frac{VIN (V)}{tR (ms)} = \frac{12 V}{20 ms} = 0.6 V / ms
$$
\n(12)

The C_{dVdt} needed to achieve this slew rate can be calculated as:

$$
C dV dt (pF) = \frac{3300}{SR (V/ms)} = \frac{3300}{0.6} = 5500 pF
$$
 (13)

Choose the nearest standard capacitor value as 5600 pF.

For this slew rate, the inrush current can be calculated as:

$$
IINRUSH (mA) = SR (V/ms) \times COUT (\mu F) = 0.6 \times 470 = 282 mA
$$
\n(14)

The average power dissipation inside the part during inrush can be calculated as:

$$
PDINRUSH (W) = \frac{IINRUSH (A) \times VIN (V)}{2} = \frac{0.282 \times 12}{2} = 1.69 W
$$
 (15)

For the given power dissipation, the thermal shutdown time of the device must be greater than the ramp-up time t_R to avoid start-up failure. 图 9-3 shows the thermal shutdown limit. For 1.69 W of power, the shutdown time is more than 10 s, which is very large as compared to t_R = 20 ms. Therefore, it is safe to use 20 ms as the start-up time for this application.

图 **9-3. Thermal Shut-Down Plot During Inrush**

备注

In some systems, there can be active load circuits (for example, DC-DC converters) with low turnon threshold voltages which can start drawing power before the eFuse has completed the inrush sequence. This action can cause additional power dissipation inside the eFuse during start-up and can lead to thermal shutdown. TI recommends to use the Power Good (PG) pin of the eFuse to enable and disable the load circuit. This action ensures that the load is turned on only when the eFuse has completed its start-up and is ready to deliver full power without the risk of hitting thermal shutdown.

9.2.2.4 Setting Power-Good Assertion Threshold

The Power Good assertion threshold can be set using the resistors R4 and R5 connected to the PGTH pin, whose values can be calculated as:

$$
VPG = \frac{VPGTH(R) \times (R4 + R5)}{R5}
$$
 (16)

Because R4 and R5 leak the current from the output rail V_{OUT} , these resistors must be selected to minimize the leakage current. The current drawn by R4 and R5 from the power supply is IR45 = V_{OUT} / (R4 + R5). However, leakage currents due to external active components connected to the resistor string can add error to these calculations. So, the resistor string current, IR123 must be chosen to be 20 times greater than the PGTH leakage current expected.

From the device electrical specifications, PGTH leakage current is 1 μ A (maximum), V_{PGTH(R)} = 1.2 V and from design requirements, V_{PG} = 11.4 V. To solve the equation, first choose the value of R4 = 47 kΩ and calculate R5 $= 5.52$ kΩ. Choose the nearest 1% standard resistor value as R5 = 5.6 kΩ.

9.2.2.5 Setting Overcurrent Threshold (ILIM)

The overcurrent protection (Circuit Breaker) threshold can be set using the R_{ILM} resistor whose value can be calculated as:

$$
RILM (\Omega) = \frac{5747}{ILIM (\text{A})} = \frac{5747}{7.7 \text{ A}} = 746.4 \ \Omega
$$
\n(17)

Choose nearest 1% standard resistor value as 715 Ω.

9.2.2.6 Setting Overcurrent Blanking Interval (tITIMER)

The overcurrent blanking timer interval can be set using the C_{ITIMER} capacitor whose value can be calculated as:

CITIMER (nF) =
$$
\frac{\text{tITIMER (ms)} \times \text{IITIMER (\mu A)}}{\Delta \text{VITIMER (V)}} = \frac{1 \times 2}{1.52} = 1.32 \text{ nF}
$$
 (18)

Choose nearest standard capacitor value as 1.3 nF.

9.2.3 Application Curves

9.3 Parallel Operation

Applications that need higher steady current can use two TPS25974x devices connected in parallel as shown in 图 9-7. In this configuration, the first device turns on initially to provide the inrush current control. The second device is held in an OFF state by driving its EN/UVLO pin low using the PG signal of the first device. After the inrush sequence is complete, the first device asserts its PG pin high and turns on the second device. The second device asserts its PG signal to indicate when it has turned on fully, thereby indicating to the system that the parallel combination is ready to deliver the full steady state current.

After in steady state, both devices share current nearly equally. There can be a slight skew in the currents depending on the part-to-part variation in the R_{ON} as well as the PCB trace resistance mismatch.

The waveforms below illustrate the behavior of the parallel configuration during start-up as well as during steady state.

图 **9-8. Parallel Devices Sequencing During Start-Up**

图 **9-9. Parallel Devices Load Current During Steady State and Overload**

10 Power Supply Recommendations

The TPS2597xx devices are designed for a supply voltage range of 2.7 V \leq V_{IN} \leq 23 V. TI recommends an input ceramic bypass capacitor higher than 0.1 μF if the input supply is located more than a few inches from the device. The power supply must be rated higher than the set current limit to avoid voltage droops during overcurrent and short-circuit conditions.

10.1 Transient Protection

In the case of a short-circuit and overload current limit when the device interrupts current flow, the input inductance generates a positive voltage spike on the input, and the output inductance generates a negative voltage spike on the output. The peak amplitude of voltage spikes (transients) is dependent on the value of inductance in series to the input or output of the device. Such transients can exceed the absolute maximum ratings of the device if steps are not taken to address the issue. Typical methods for addressing transients include:

- Minimize lead length and inductance into and out of the device.
- Use a large PCB GND plane.
- Connect a Schottky diode from the OUT pin ground to absorb negative spikes.
- Connect a low ESR capacitor larger than 1μ F at the OUT pin very close to the device.
- Use a low-value ceramic capacitor $C_{\text{IN}} = 1 \mu F$ to absorb the energy and dampen the transients. The capacitor voltage rating must be at least twice the input supply voltage to be able to withstand the positive voltage excursion during inductive ringing.

Use 方程式 19 to estimate the approximate value of input capacitance:

$$
VSPIKE(Absolute) = VIN + ILOAD \times \sqrt{\frac{LIN}{CIN}} \tag{19}
$$

where

- V_{IN} is the nominal supply voltage.
- I_{LOAD} is the load current.
- $-$ L_{IN} equals the effective inductance seen looking into the source.
- $-$ C_{IN} is the capacitance present at the input.
- Some applications can require the addition of a Transient Voltage Suppressor (TVS) to prevent transients from exceeding the absolute maximum ratings of the device. In some cases, even if the maximum amplitude of the transients is below the absolute maximum rating of the device, a TVS can help to absorb the excessive energy dump and prevent it from creating very fast transient voltages on the input supply pin of the IC, which can couple to the internal control circuits and cause unexpected behavior.

图 10-1 shows the circuit implementation with optional protection components.

10.2 Output Short-Circuit Measurements

It is difficult to obtain repeatable and similar short-circuit testing results. The following contribute to variation in results:

- Source bypassing
- Input leads
- Circuit layout
- Component selection
- Output shorting method
- Relative location of the short
- Instrumentation

The actual short exhibits a certain degree of randomness because it microscopically bounces and arcs. Ensure that configuration and methods are used to obtain realistic results. Do not expect to see waveforms exactly like those in this data sheet because every setup is different.

11 Layout

11.1 Layout Guidelines

- For all applications, TI recommends a ceramic decoupling capacitor of 0.1 μF or greater between the IN terminal and GND terminal.
- The optimal placement of the decoupling capacitor is closest to the IN and GND terminals of the device. Care must be taken to minimize the loop area formed by the bypass-capacitor connection, the IN terminal, and the GND terminal of the IC.
- High current-carrying power-path connections must be as short as possible and must be sized to carry at least twice the full-load current.
- The GND terminal must be tied to the PCB ground plane at the terminal of the IC with the shortest possible trace. The PCB ground must be a copper plane or island on the board. TI recommends to have a separate ground plane island for the eFuse. This plane does not carry any high currents and serves as a quiet ground reference for all the critical analog signals of the eFuse. The device ground plane must be connected to the system power ground plane using a star connection.
- The IN and OUT pins are used for heat dissipation. Connect to as much copper area on top and bottom PCB layers using as possible with thermal vias. The vias under the device also help to minimize the voltage gradient across the IN and OUT pads and distribute current uniformly through the device, which is essential to achieve the best on-resistance and current sense accuracy.
- Locate the following support components close to their connection pins:
	- R_{ILM}
	- C_{dVdT}
	- C_{ITIMFR}
	- Resistors for the EN/UVLO, OVLO/OVCSEL, and PGTH pins
- Connect the other end of the component to the GND pin of the device with shortest trace length. The trace routing for the RILM, CITIMER and CdVdt components to the device must be as short as possible to reduce parasitic effects on the current limit, overcurrent blanking interval and soft start timing. It's recommended to keep parasitic capacitance on ILM pin below 50 pF to ensure stable operation. These traces must not have any coupling to switching signals on the board.
- Because the bias current on ILM pin directly controls the overcurrent protection behavior of the device, the PCB routing of this node must be kept away from any noisy (switching) signals.
- Protection devices such as TVS, snubbers, capacitors, or diodes must be placed physically close to the device they are intended to protect. These protection devices must be routed with short traces to reduce inductance. For example, TI recommends a protection Schottky diode to address negative transients due to switching of inductive loads. TI also recommends to add a ceramic decoupling capacitor of 1 μF or greater between OUT and GND. These components must be physically close to the OUT pins. Care must be taken to minimize the loop area formed by the Schottky diode/bypass-capacitor connection, the OUT pin, and the GND terminal of the IC.

11.2 Layout Example

图 **11-1. Layout Example - Single TPS25974x With PGTH Referred to OUT**

12 Device and Documentation Support

TI offers an extensive line of development tools. Tools and software to evaluate the performance of the device, generate code, and develop solutions are listed below.

12.1 Device Support

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12.2 Documentation Support

12.2.1 Related Documentation

For related documentation see the following:

- Texas Instruments, *TPS2597EVM eFuse Evaluation Board* user's guide
- Texas Instruments, *TPS2597xx Design Calculator*

12.3 接收文档更新通知

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12.7 术语表

TI 术语表 本术语表列出并解释了术语、首字母缩略词和定义。

13 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

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(1) The marketing status values are defined as follows:

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(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

⁽⁵⁾ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

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PACKAGE MATERIALS INFORMATION

TEXAS NSTRUMENTS

TAPE AND REEL INFORMATION

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

PACKAGE MATERIALS INFORMATION

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*All dimensions are nominal

RPW0010A

PACKAGE OUTLINE

VQFN-HR - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

-
- per ASME Y14.5M.
This drawing is subject to change without notice.
-

EXAMPLE BOARD LAYOUT

RPW0010A VQFN-HR - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

NOTES: (continued)

-
-

EXAMPLE STENCIL DESIGN

RPW0010A VQFN-HR - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

NOTES: (continued)

design recommendations.

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